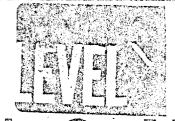
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U.S.NAW

MARINE CLIMATICE

OF THE WORF

VOLUME III

INDIAN OCEA!

(REVISED 1976)

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S. NAVY CLIMATIC ATLAS THE WORLD

OLUME III
DIAN OCEAN

REVISED 1976)





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U. S. N A V Y MARINE CLIMATIC OF THE WORLI VOLUME III INDIAN OCEAN

THIS REPLACES NAVAER 50-1C-530 DATED 1957

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S. NAVY CLIMATIC ATLAS THE WORLD VOLUME III.

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REPLACES NAVAER 50-1C-530 DATED 1957

WEATHER SERVICE DETACHMENT, ASHEVILLE, N.C. MMANDER, NAVAL WEATHER SERVICE COMMAND

DOCUMENTS, U.S. GOVERNMENT PRINTING OFFICE, WASHINGTON D.C. 20402

FOREWORD

A joint feasibility study for producing a combined climatological/oceanographic atlas of the water areas of the world was undertaken by the Naval Weather Service Command and the Naval Oceanographic Office in 1969. The results of this feasibility study revealed a twofold increase in surface marine observations over the Indian Ocean basin since Volume III of the U.S. NAVY MARINE CLIMATIC ATLAS OF THE WORLD was published. The additional data plus recommendations for revised content and format, provided by various Naval Weather Service fleet units and field activities, warranted the updating of the entire series of marine climatic charts of the world.

The Naval Weather Service Detachment, Asheville, was tasked to produce a technical model of the atlas providing a sample of each type of page presentation proposed with supporting documentation. The atlas mock-up was approved by Headquarters, Naval Weather Service Command in 1971 as the model for Volume I (1974) as well as for this atlas and future volumes of this series. Volume III has followed production of Volume I because of intense scientific interest in the Indian Ocean Basin. Volume II, The North Pacific, will follow this volume in the publication sequence.

ACKNOWLEDGMENT

The revision of the U.S. NAVY MARINE CLIMATIC ATLAS OF THE WORLD series is managed by the Naval Weather Service Detachment, Asheville by direction of the Commander, Naval Weather Service Command. This volume was prepared at the National Climatic Center.

Specific acknowledgement is made to the following members of the National Climatic Center; Project Leaders Messrs. J. M. Meserve, R. G. Quayle and D. C. Fulbright; Messrs. J. D. Elms, A.W.Y. Chen and H. F. Diaz for their assistance in the editorial evaluation and analyses of the data; Messrs. R. H. Courtney, R. G. Baldwin, D. Swann, E. Gilreath, Mrs. D. T. Hawkins and Miss E. Cook for drafting.

The oceanographic part was based upon data provided by the U.S. Naval Oceanographic Office, whose contribution is acknowledged with thanks.

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PART I - METEOROLOGY

INTRODUCTION

The eight volume series of the U.S. Navy Marine Climatic Atlas of the World has had wide acceptance as an authoritative reference for large scale operational planning and applied research. This volume, based on nearly 120 years of data (1854-early 1973), is an update of Volume III (U.S. Navy Marine Climatic Atlas of the World, 1957) and is designed to fulfill the same requirements. This volume is not, however, a one for one revision. Some of the data presentations have been changed and wave statistics have been added. There are no upper air charts presented since in recent years several comprehensive volumes of upper air data have been published separately: (Upper Wind Statistics Charts of the Northern Hemisphere, Volumes I and II, NAVAER 50-1C-535, 1959; Components of the 1000 MB Winds of the Northern Hemisphere, NAVAIR 50-1C-51, 1966; Selected Level Heights, Temperatures and Dew Points for the Northern Hemisphere, including Monthly Mean Wind Speed and Direction, NAVAIR 50-1C-52, 1970; Selected Meridional Cross Sections of Heights, Temperatures and Dew Points of the Northern Hemisphere, NAVAIR 50-1C-59, 1971; Climate of the Upper Air: Southern Hemisphere, Volume I, Temperatures, Dew Points, and Heights at Selected Pressure Levels, NAVAIR 50-1C-55, 1969; Volume II, Zonal Geostrophic Winds, NAVAIR 50-1C-56, 1971; Volume III, Vector Mean Geostrophic Winds, NAVAIR 50-1C-57, 1971; Volume IV, Selected Meridional Cross Sections of Temperature, Dew Points, and Height, NAVAIR 50-1C-58, 1971).

The descriptive explanations which follow give details concerning the quality control and processing of the observations, the development of the charts and graphs and a few possible applications of the various charts. Also discussed are limitations imposed by the quality of the data and the methods adapted to help overcome them.

This Atlas is the result of a concerted and extensive effort by many people (aided by automatic data processing equipment) to present a detailed and useful ocean climatology.

THE GENERAL PLAN OF THE CHARTS

The "point statistics" of land climatology are made possible by the maintenance of weather records at fixed locations for long periods. Such statistics are not generally available for Ocean Basins. Where the number of observations is sufficient, it is possible to select areas small enough to permit an approximation to the "point statistics" of land stations. For this Atlas 45 such representative areas are used. The locations are outlined on the base chart and numbered. The graphs and tables computed for these areas have been placed on the facing page for ready reference to the base chart.

THE OBSERVATIONS AND THEIR PROCESSING

Variations in definitions, codes and units of measurements used by maritime nations for recording and punching marine observations have resulted in 18 different forms (or "decks") of punched cards available for use at the National Climatic Center. These data have been converted to a common format and placed on magnetic tape. For a more detailed explanation of the conversion procedures, the reader is referred to the Tape Data Family-11 (TDF-11) Reference Manual (National Climatic Center, 1968). This tape deck was the primary data source for this volume. Funding for the development of TDF-11 was provided primarily by the Naval Weather Service Command with supplemental support from the National Oceanic and Atmospheric Administration (NOAA), formerly ESSA, and the Department of Defense.

The data were subjected to complex quality control procedures before processing. First, duplicate observations (which entered the data base from different sources) were eliminated. The remaining observations were then checked for internal consistency. Elements which failed to meet the internal consistency checks were either adjusted or eliminated. The data were subjected to an extreme value check in which the highest and lowest values of appropriate elements were listed and checked. These quality controlled data have been retained in a separate tape file designated as the U.S. Navy Marine Atlas Work Tapes.

Regardless of the amount of quality control to which marine observations are subjected there are many inherent problems which can be corrected in only a general way. Among these are: the difficulty in taking observations of meteorological elements from an unstable platform, different levels of observer experience, recording errors, variations in observing and coding practices, punching errors, the scarcity of observations over vast areas, and the effect of weather

elements themselves on measurements. Ships may avoid bad weather when possible (Quayle, 1974), thus decreasing the amount of bad-weather data; or they may slow down in foul weather, thus taking more observations and increasing the data sample.

Complete observations (including all elements) from transient ships are steadily becoming more common. Ships' weather logs of past decades, incomplete by today's standards, show wind direction and speed to be the elements almost invariably recorded. From a survey of the data available for this atlas, the percentage of observations containing other basic weather elements is as follows:

Element	Percent
Air Temperature	98
Sea Temperature	92
Total Cloud Amount	78
Visibility	72
Sea Level Pressure	56
Present Weather	57
Low Cloud Amount	36
Wet Bulb Temperature	36
Waves	26

Because of incompatible observing or coding procedures, many observations of total cloud amount, visibility, present weather, low cloud amount, and wave data have been eliminated from the computations. This significantly reduced the percentages of these elements in the above table.

Some peculiarities of selected elements are listed below:

PRECIPITATION — Of all of the elements recorded in historical marine observations, precipitation is one of those most subject to error in interpretation. This derives from a number of causes such as coding practices, observers' preference for certain present weather codes and other biases.

SEA SURFACE TEMPERATURE — This element is recorded with a fairly high frequency in marine observations. The various methods of recording, however, tend to decrease the reliability of the individual values. Gradients and relative values are considered to be reliable.

SEA LEVEL PRESSURE — This element is one of the least accurate because of instrument, coding and conversion errors. To be capable of registering accurate pressure readings, berometers used on shipboard generally require more frequent calibration than they receive. Despite the inaccuracies of the individual readings, however, the large scale patterns and gradients are relatively accurate.

AIR TEMPERATURE — This element is considered to be generally reliable. However, in the tropics, as the result of poor instrument exposure, observed temperatures on transient ships under sunny conditions appear consistently high. This data subset influences primarily the distribution of maximum temperatures (99th percentile) while the minimum

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(1st percentile) and mean temperatures are relatively unaffected.

VISIBILITY — It is difficult to measure visibility at sea because of the lack of reference points. Also, some observers report reduced visibilities at night because of darkness. The coarseness of the coding intervals, however, tends to minimize serious biases in the summarized data.

WAVE DATA — Suitable quantitative wave records are available only since the late 1940's. This, coupled with an apparent reluctance on the part of many observers to take wave observations, particularly in the early years, leaves waves as the least often recorded element in marine observations. The estimate of wave heights is very subjective and depends upon the experience of the observer and the size of the ship from which the observation is taken. Wave heights reported by most transient ships tend to be low by about 10% when compared to reference measurements. Adjustment for this apparent bias has not been made in this Atlas.

Despite the lower confidence level in the individual values of these elements, through subjective analyses and reference to previous studies, the means, extremes and gradients presented by the isopleths are considered to be quite reliable.

THE ISOPLETH ANALYSES

The climatic data in this atlas are presented by isopleths (lines connecting points of equal magnitude) supplemented by graphs and tables. The isopleth analyses were completed cooperatively by a team of meteorologists. The basic charts were automatically plotted from one or two degree area summaries for the entire ocean basin. As there were no Ocean Weather Station (OWS) data for the Indian Ocean, a valuable tool which was available to analysts in the North Atlantic was lost. Analysts made considerable use of the observation count which was plotted with all summarized data to aid in data interpretation. For the ocean areas southward of 45°S, data were very sparse, thus not affording detailed analyses. Isopleths in these areas should be considered only as presenting a 'best estimate' of the actual climatology.

THE GRAPHS AND TABLES

To supplement the isopleth analyses, graphs and tables are presented for each representative area. The graphs and tables, in most instances, represent the objective compilation of available raw data for specified areas without regard to suspected biases or inconsistencies.

Since the final isopleth analyses reflects both objective and subjective considerations, differences may be found when comparing the graphical data for a representative area with the analyses.

THE INDIVIDUAL SURFACE CHARTS

The legend in each chart is designed to explain data content — tables, graphs and isopleths. Each legend contains detailed instructions on how to read the tables or graphs. The following paragraphs contain additional remarks likely to be of interest to those called upon to interpret the data and provide answers to specific operational questions.

Most of the graphs and tables allow approximation of the empirical probability of occurrence of selected criteria. This is a major factor in assessing the risk involved in operational planning. For certain elements, standard deviations are given on the graphs to provide a measure of relative variability. The standard deviation of these graphs is denoted by 's' and was computed using the expression:

$$s = \left[\frac{N\Sigma x_1^2 - (\Sigma x_1)^2}{N(N-1)}\right]^{1/2}$$

where N denotes the number of observations in the sample and x_i denotes the value of the random variable X. The use of (N-1) in the denominator gives the best estimate of the population standard deviation.

SURFACE WINDS

Surface wind is the element most commonly observed and recorded. It was the element considered basic in the selection of representative areas for construction of complete frequency distributions. Wind distribution is presented by a combination of two graphic forms — the bar graph and the contingency table. The bar graph corresponds to the percent scale at the top of the square and gives ready reference to the wind direction frequency. The contingency table gives the percent frequency of each wind speed class within each direction. By adding the totals lines at the bottom of the graph it is possible to approximate the percent frequency of wind speed occurrence for selected criteria. For the example graph in the legend, 71% of all winds were < 17 knots.

Persistence statistics would be of interest in planning operations, but these are not possible without serially complete observations from fixed points.

AIR TEMPERATURE

The threshold value of $\geq 20^{\circ}C$ for the isopleths of air temperature was selected in response to requests by a number of users who considered that relative degree of warmth to be operationally significant for outside marine activity. The mean temperature for each wind direction and calm is shown by dots in the graph opposite each direction and corresponding to the temperature scale at the bottom. Note the temperature range and scale may vary from area to area and month to month.

T-H INDEX AND TEMPERATURE EXTREMES

The American Society of Heating and Ventilating, as early as 1923, introduced a term called "effective temperature" which is a measure of comfort based on temperature and humidity. This is the term we call THI (Temperature — Humidity Index). It has been empirically determined that a majority of people will be uncomfortable when the index reaches 24°C. THI is computed by the following equation, adapted from one described by E. C. Thom, 1957:

$$THI = 0.4 (T_d + T_{wb}) + 4.7778$$

where: T_d = Dry Bulb Temperature (°C) T_{wb} = Wet Bulb Temperature (°C) THI is in degrees Celsius

Isopleths of the 1% and 99% levels of air temperature have been selected to present extreme temperature conditions. The graphs show air temperature versus wind speed. Use may be made of these charts to determine the extent of discomfort likely because of extreme heat or cold. They may also be used to estimate the likelihood of superstructure icing.

Ice accretion is a complicated process that depends upon sea conditions, temperature, wind and the size and behavior of the ship. Superstructure icing can affect all ships but is more dangerous for smaller vessles. Icing potential exists when the air temperature falls below the freezing temperature of sea water (usually about -2°C) with wind speed equal to or greater than 11 knots. The lower the temperature and higher the wind speed, the greater the icing potential. Ice accretion may become quite severe with temperatures ≤-9°C and wind ≥ 34 knots.

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SEA SURFACE TEMPERATURE

Sea surface temperature is recorded with fairly high frequency in marine observations. The 1% and 99% isopleths give estimates of the extremes that may be encountered at any location. The graphs are simple cumulative percent frequency presentations. The temperature range and scale on the graphs may vary from area to area and month to month.

Sea surface temperature can be used to estimate the approximate time a person in ordinary clothes and life preserver may be expected to survive in the water:

Water	Exhaustion or	Expected Time
Temperature	Unconsciousness	of Survival
< 0°C	< 15 min	< 15-45 min
0-5°C	15-30 min	30-90 min
5-10°C	30-60 min	1-3 hrs
10-15°C	1-2 hrs	1-6 hrs
15-20°C	2-7 hrs	2-40 hrs
20-25°C	3-12 hrs	3 to indefinite hrs
> 25°C	Indefinite	Indefinite

HUMIDITY

Moisture content of the atmosphere is an element which has been recorded relatively infrequently in marine observations. The 1% and 99% dew-point temperature isopleths give estimates of extremes of this element that may be encountered at any location.

The graph depicts wet bulb and relative humidity information. The cumulative percent frequency of wet-bulb temperatures may be read from the solid line with reference to values on the scale at the top of the graph. Relative humidity may be read from the dashed line with reference to the scale at the bottom of the graph.

PRECIPITATION

Precipitation charts and graphs are intended to depict the frequency of precipitation at the time of the observation. Based on work done in connection with Volume I (Revised) North Atlantic Ocean, present weather codes 20-27 (precipitation within the past hour) were counted in precipitation frequencies to correct an apparent observational bias. The graphs show precipitation by wind direction. The percent frequency of all observations which reported precipitation is printed in the upper right corner of each graph. The

distribution of precipitation by wind direction (and calm) is given by the bar graph. This graph is based on precipitation frequency and not on wind direction frequency. The reader should refer to the surface wind chart if he is interested in the wind direction and speed distribution.

No isopleths were drawn for the percent frequency of precipitation observations reporting snow because of inadequate data. However, graphs for some of the representative areas do reflect the presence of snow.

VISIBILITY

The cumulative percent frequency of horizontal visibility is presented by nautical mile class intervals rather than by kilometers. The percentage of horizontal visibility equal to or greater than 25 nautical miles can be obtained by subtracting from 100% the cumulative percent frequency at the point < 25 on each graph. Caution is advised, however, ir interpreting these areas since, because of curvature of the earth, it is virtually impossible to see 25 miles horizontally from the bridge of most ships. The supplemental table at the bottom of the graph gives percentage of visibilities < 2 nautical miles which occurred with each wind direction and calm.

CLOUD COVER

Even with the increased data base, the quality and quantity of low cloud data is quite poor. The total cloud amount element does not suffer from this deficiency to so great an extent. The number of observations available which contain only total cloud amount continues to be higher than those containing both total and low. The use of satellite data also bolsters confidence in the total cloud statistics. Cloud patterns derived from the marine observations and those depicted by satellites show fairly close agreement (U.S. Department of Commerce and United States Air Force, 1971).

The observation count on the graphs is that of observations containing total cloud amount. The low cloud curve on the graph is based on less data than the total cloud curve. This may lead to inconsistencies where low cloud amount appears higher than the total cloud amount. In all cases these were resolved in favor of the total cloud by making the frequency curves coincide.

The cumulative percent frequency of a cloud amount equal to or less than the amount intersected by the curve may be read for total cloud along the solid line or low cloud along the dashed line. The percent frequency of obscurations may be determined by subtracting the cumulative percent frequency corresponding to 8/8 coverage from 100%. The bar

graph portion of the figure shows the percent frequency of low cloud amount equal to or greater than 5/8 and equal to or greater than 7/8 for each wind direction and calm. Total sky obscurations are considered as 8/8 coverage for these purposes.

CEILING AND VISIBILITY

Simultaneous ceiling-visibility contingencies are presented in isopleth and tabular form. They are designed as an aid to situations where both vertical and horizontal visibility are the major items of concern. Since an "aircraft" type ceiling value is not available, the ceiling height is estimated from the height of low cloud (h) when the amount of low cloud (N_h) is greater than 4/8. Total sky obscurations are considered to be ceilings. If they are ground-based, they are considered to have a height equal to zero.

WIND - VISIBILITY - CLOUDINESS

This series of charts is designed to give the planner an estimate of the probability of occurrence of certain significant operational conditions. The conditions for optimum and poor carrier operations are those recommended by the users of the earlier atlas series. Of the elements used in these statistics, height of low cloud ceiling has the least reliability in the case of transient ship observations.

It should be noted that in both the contingency tables and the isopleths, the poor carrier operation conditions are and/or situations. This means if any one of the poor conditions of ceiling, visibility or wind speed exists, the event is counted as poor. However, in the case of optimum conditions it is an and situation. That is, the ceiling must be ≥ 5000 feet and visibility ≥ 5 nautical miles and wind 11-21 knots.

SEA LEVEL PRESSURE AND MEAN WIND

Two sets of wind statistics are presented. The vector mean wind is shown by arrows (direction of flow toward the station dot with the resultant magnitude of the vector plotted at the end of the arrow). The scalar mean speed without regard to direction is shown by isopleth analysis. In areas of high persistence of direction, the magnitude of the mean vector should approximate the scalar mean speed. Pressure graphs and charts are also shown.

WAVES (<1.5 AND <2.5 METERS)

In these analyses, the higher of the sea or swell is selected

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Two sets of wind statistics are presented. The vector mean wind is shown by arrows (direction of flow toward the station dot with the resultant magnitude of the vector plotted at the end of the arrow). The scalar mean speed without regard to direction is shown by isopleth analysis. In areas of high persistence of direction, the magnitude of the mean vector should approximate the scalar mean speed. Pressure graphs and charts are also shown.

WAVES (<1.5 AND <2.5 METERS)

In these analyses, the higher of the sea or swell is selected

for summarization. If the heights are equal, the wave with the longer period is selected. In order to present as broad a spectrum of heights and periods as practicable, two sets of wave charts are furnished. The graphs accompanying the low wave charts (< 1.5 and < 2.5 meters) show wave height versus wave direction. The bar graph and the percent scale at the top of the chart give the percent frequency of waves from each direction. Indeterminate directions are combined with calms. The percent frequency of wave heights (bottom scale) may be read for each height interval and wave direction from the contingency table. The isopleth analyses of the percent frequency of heights < 1.5 and < 2.5 meters are for generally non-hazardous sea conditions.

WAVES (≥3.5 AND ≥6 METERS)

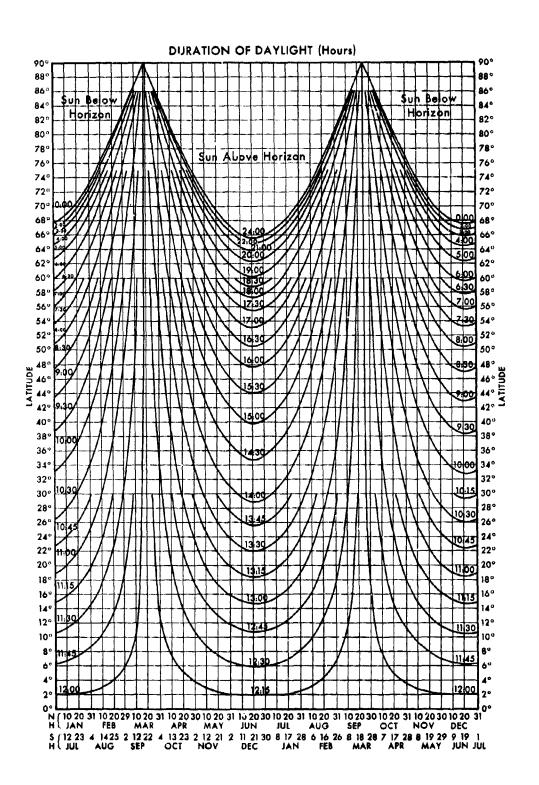
Wave heights in the \geq 3.5 and \geq 6 meter range represent increasingly hazardous conditions. Accompanying these charts are contingency tables of wave period versus wave height.

TROPICAL CYCLONES

The tropical cyclone movement roses in this atlas are reprinted from the Mariners Worldwide Climatic Guide to Tropical Storms at Sea, NAVAIR 50-1C-61, 1974. The data presented here include all tropical cyclones estimated to have wind speeds greater than about 33 knots. All data are combined for each 5° quadrangle. The period of record is 1854-1969 for the Southern Hemisphere; 1877-1970 for the Northern Hemisphere. The reader is referred to the above mentioned "Guide" for more detailed information.

DURATION OF DAYLIGHT

The Duration of Daylight Chart for the Northern and Southern Hemispheres defines daylight as the period from sunrise to sunset. The upper scale at the bottom of the chart is for the Northern Hemisphere; the lower scale is for the Southern Hemisphere. As an example, the daylight on July 20 of any year at 48°N is about 15 hours and 30 minutes for any longitude, approximately the same amount of daylight occurs at 48°S on January 17 for any longitude. The data source was the U.S. Naval Observatory (1945) and is accurate for the entire 20th Century. Further details may be obtained from The Daylighter by the U.S. Navy Weather Research Facility (1960). Additional light (during twilight) may be usable for many purposes. Duration of daylight in high latitudes (poleward of about 60°) becomes increasingly dependent upon atmospheric conditions and refraction and there may be some departure from the values depicted on the charts.



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DAYLIGHT (Hours) 90° 880 860 840 Horizon 82° 80° 78° e Hørizan 76° 740 720 70° 480 664 640 62° 600 580 569 524 50° 480 46° 5 440 420 40° 380 340 32° 30° 280 260 240 20° 180 160 140 100 60 30 10 20 31 10 20 31 10 20 30 10 20 31 10 20 30 10 20 31 AUG NOV 30 8 17 28 6 16 26 8 18 28 7 17 28 8 19 29 9 19 MAR APR MAY JUN JUL

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TIDES

The information presented on the charts (types of tides, typical tide curves and tide ranges) were derived primarily from tide tables and tables of tidal harmonic constants. Tidal information is generally adequate for the Indian Ocean except for the region north of the Gulf of Mannar and the western part of the head of the Bay of Bengal, the Crozet Islands in the southwestern part of the Indian Ocean, and in the Gulfs of Carpentaria and Thailand.

CURRENTS

The ocean current charts are compiled principally from ship drift reports that were forwarded by the various merchant marines to the Naval Oceanographic Office. From these drift observations the sets and average speeds of the prevailing currents are calculated for each 1° quadrangle. The density of observations is greatest along the major shipping lanes and therefore the reliability of the current charts is best in these areas. For the Indian Ocean as a whole, the data is adequate except in the southern part where the data are extremely sparse, and in the central part of the Bay of Bengal. Other areas without adequate data density are: the North and northwest coast of Australia, in the Banda, Ceram and Molucca Seas and off the northwest coasts of Borneo and Palawan, as well as in the Gulfs of Thailand and Tonkin.

The surface currents are shown for four months which are believed to be most representative of the oceans response to the monsoons. The currents for the months of January and July represent ocean current conditions in response to the Northeast and Southwest monsoon seasons respectively. The April and October charts represent ocean surface conditions during the monsoonal transition months.

Where the effect of the monsoons is strongest, e.g., Arabian Sea, Bay of Bengal, and South China Sea, the figures were derived from monthly surface current data. Other regions of the Indian Ocean are less responsive to the monsoon influences and the currents were therefore constructed from seasonal averages adjusted by what monthly data were available to portray the specific months indicated.

Variations from the directions and speeds of the indicated prevailing currents can be expected, especially in areas where the currents are weak.

Tidal currents are shown where they predominate. These are subject to modifications of speed and direction by winds and other nonperiodic variables.

PART II - OCEANOGRAPHY

ICE

Sea Ice

The occurrence of sea ice is limited to a small region in the southwestern part of the Indian Ocean.

Glacier Ice

The mean maximum limit of drifting glacier ice is based on extremely sparse data derived from published sources.

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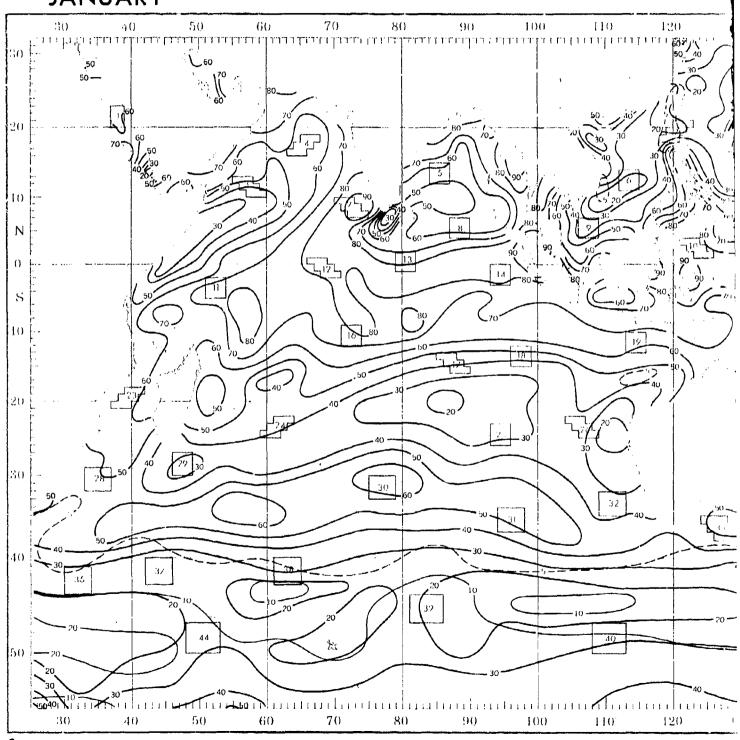
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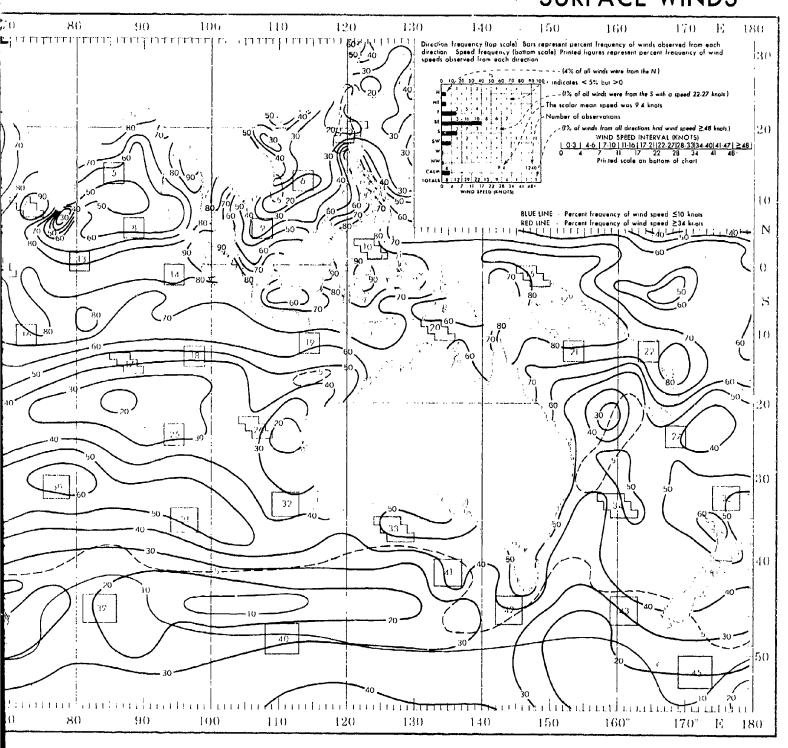
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PART I METEOROLOGY

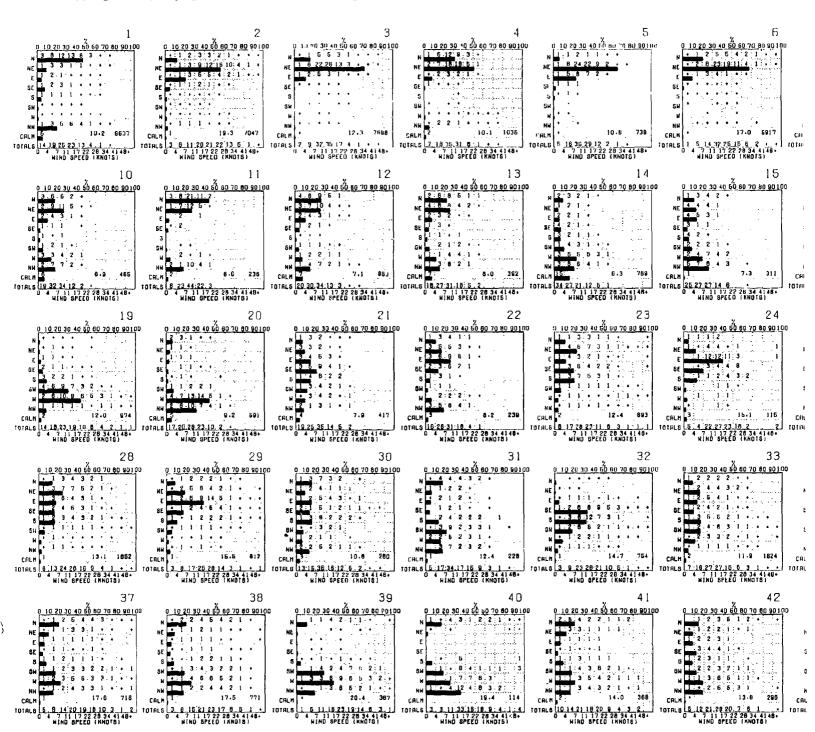
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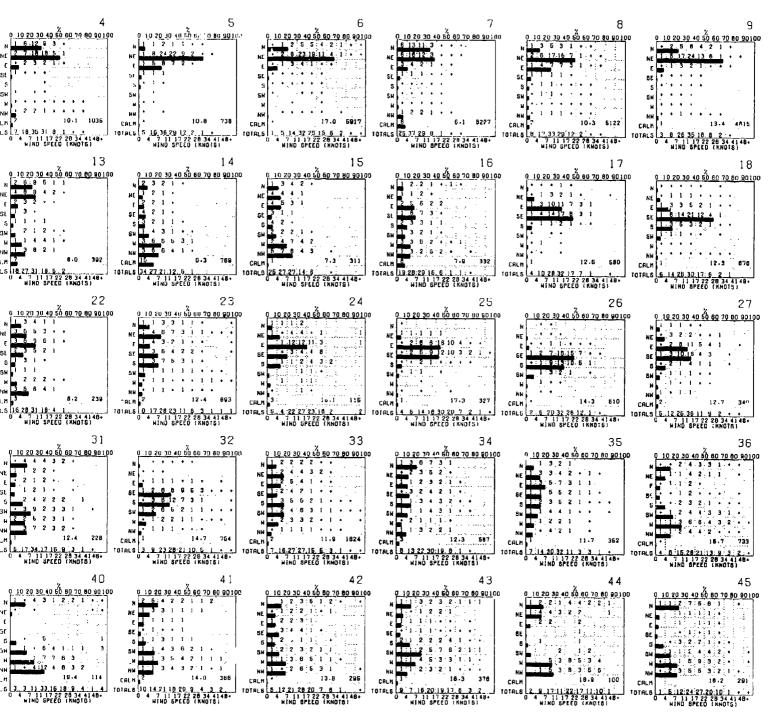


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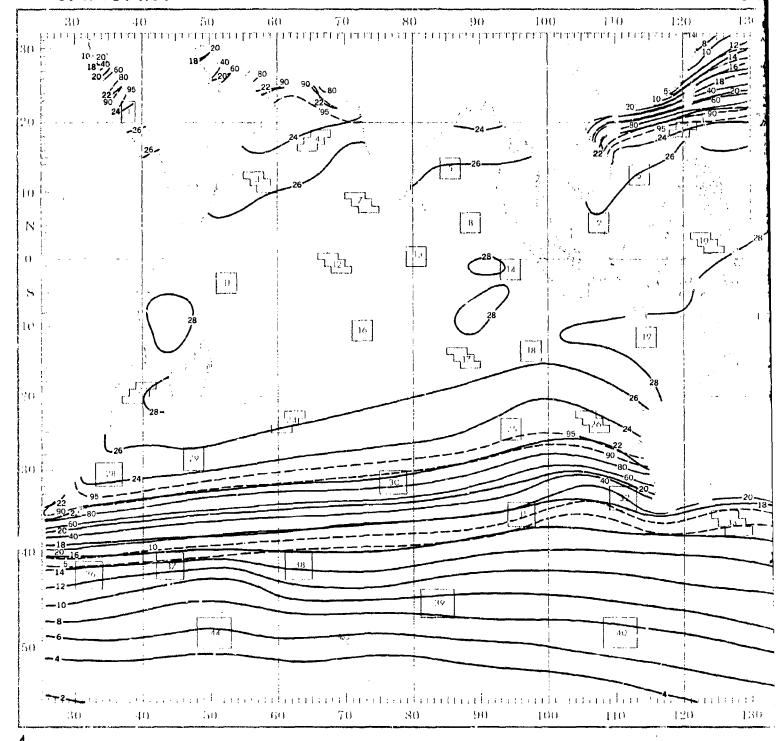


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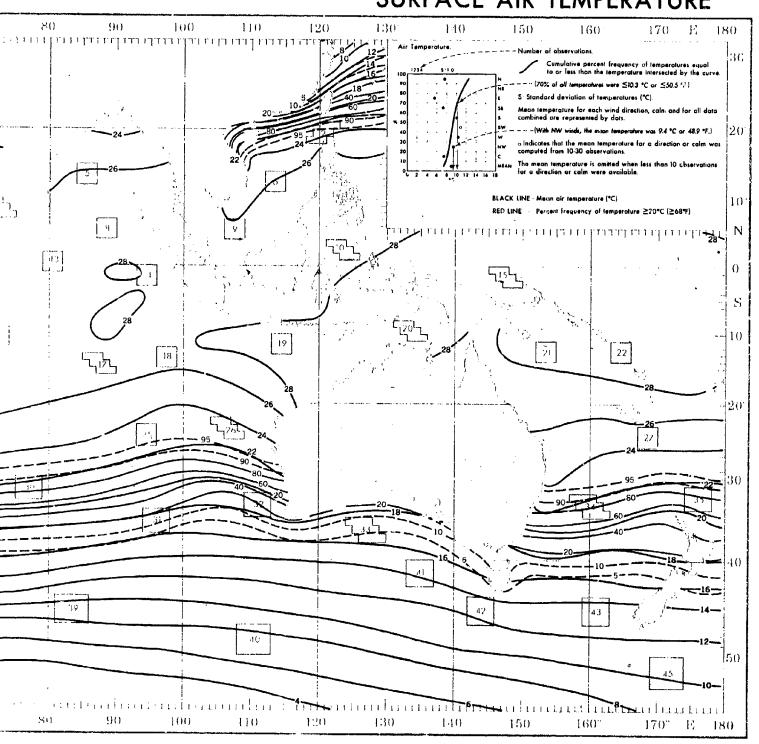
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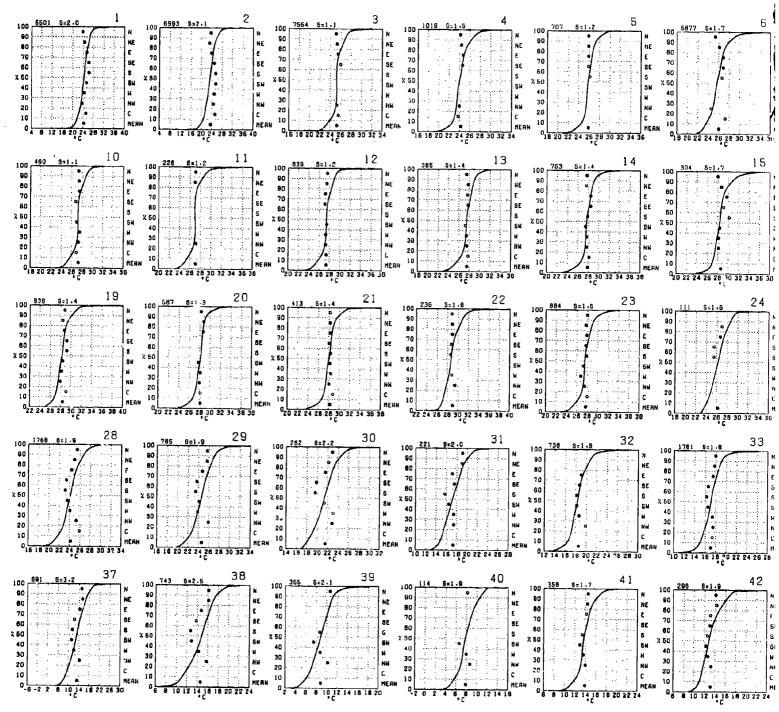
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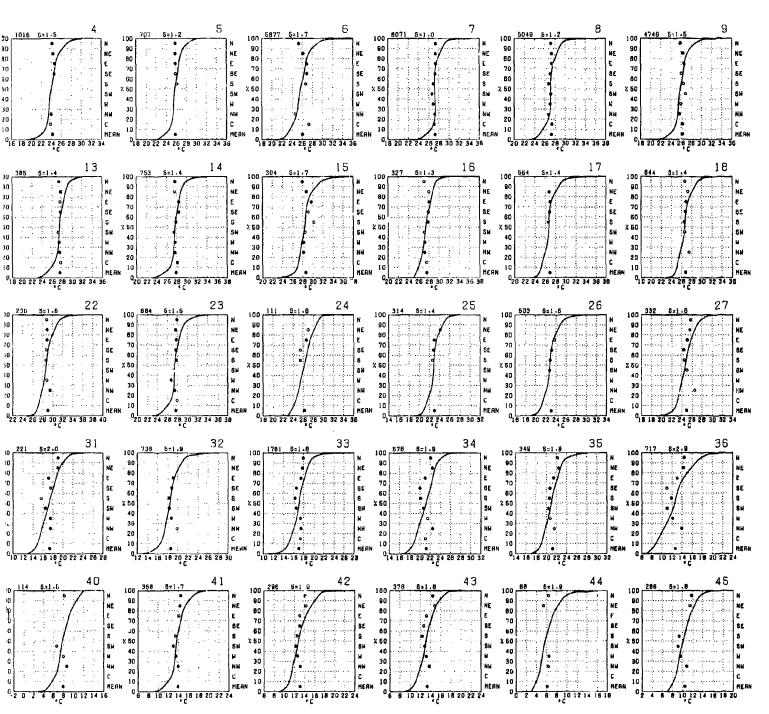


SURFACE AIR TEMPERATURE



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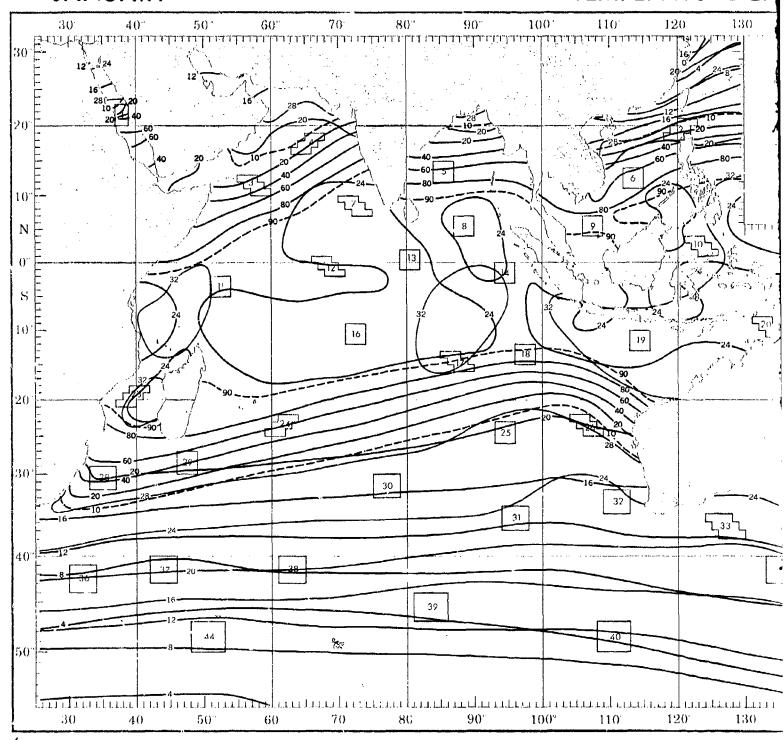
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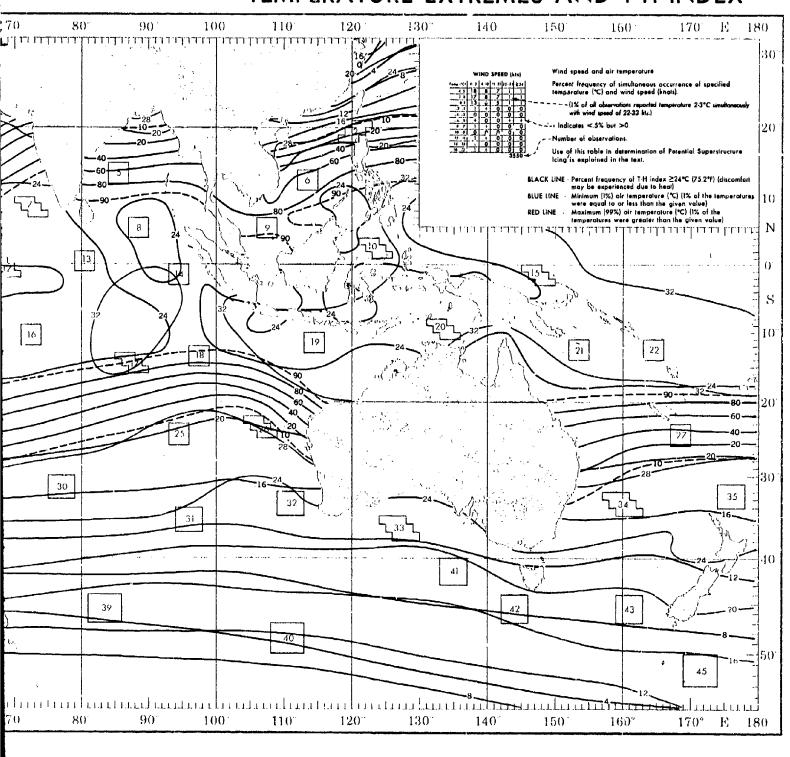
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TEMPERATURE EX



TEMPERATURE EXTREMES AND T-H INDEX



WIND SPEED AND AIR TEMPERATURE

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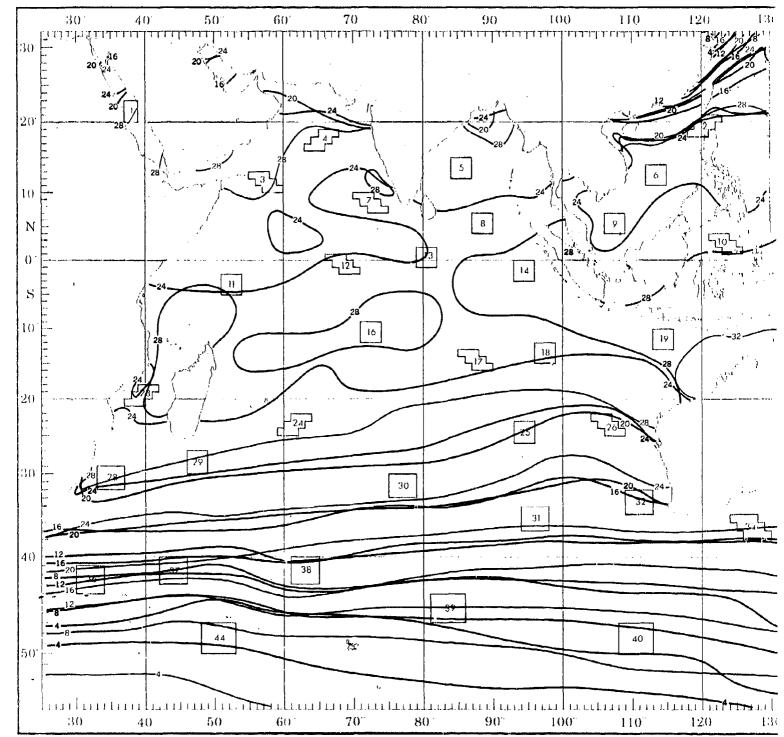
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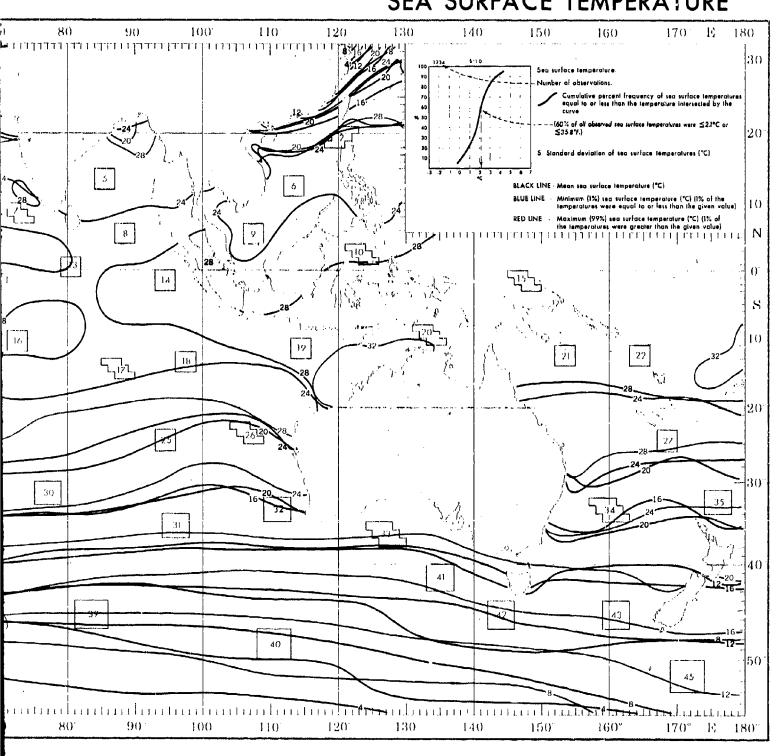
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24,28 + 3 3 0 0 22,29 0 0 1 0 0	24.25 1 2 2 + 0 22.23 0 + 0 0 0	28.27 4 10 7 + 0 24.28 0 1 1 0 0	24.20 1 3 1 + 0 28.83 0 0 0 0 0	24,28 + 4 4 1 + 22,29 0 + 0 0 0	20.23 0 + + 0 0
10.21 0 0 0 0 0	20.21 0 0 0 0 0	22.23 0 0 0 0 0 20.21 0 0 0 0 0	\$0.21 0 0 0 0 0 18.19 0 0 0 0 0	10.10 0 0 0 0 0	10.10 0 0 0 0 0 0 10.17 0 0 0 0 0
16,17 0 0 0 0 0 0 14,18 0 0 0 0 0 0	18.17 0 0 0 0 0 0 14.18 0 0 0 0 0	18.19 0 0 0 0 0 16.17 0 0 0 0 0	18.17 0 0 0 0 0 0 14.18 0 0 0 0 0	18,17 0 0 0 0 0 14,18 0 0 0 0 0	14.18 0 0 0 0 0
38B	12.19 0 0 0 0 0 753	14.16 0 0 0 0 0 0 304	12.13 0 0 0 0 0 333	12.13 0 0 0 0 0 0 568	18-11 0 0 0 D D 0 845
NIND SPEED (KTS) 22	WIND SPEED (KTS) 23	NIND SPEED (KTB) 24	HIND SPEED (KTS) 25	WIND SPEED (KIS) 26	HIND SPEED (KTB) 27
TEMP (*C) 0-3 4-10 11-2122-33 2 34		TEMP (*C) 0-9 4-10 11-21 22-93 2 24	TEMP (*C) G-2 4-10 11-21 22-33 2 24	1EMP (*G) 0-9 4-10 11-2122-33 a 94	TEMP (*C) 0-9 4-10 11-21 22-33 5 34
32.33 1 3 1 0 0 30.31 5 14 6 4 0	32.33 + 1 1 0 0 30.31 1 4 2 0 0	20.20 2 5 10 3 G	26.27 1 2 1 1 0 84.88 1 8 11 5 1	26,27 + 2 3 + + 24,28 + 6 16 1 0	28.28 + 5 2 + 0 28.27 2 10 16 2 0
10.50 8 31 10 1 0 20.27 2 11 3 0 0	20,20 5 23 14 3 0 28,27 2 16 15 6 1	24.25 0 5 14 11 1 E2.25 0 1 1 0 0	\$2.51 1 8 28 15 3 \$0.51 4 3 4 6 0	22,23 1 15 32 5 0 20,21 0 2 5 3 0	24.26 2 16 23 5 1 26.29 1 4 6 2 0
24.88 0 0 + 0 0 20.23 0 0 0 0 0	24.25 4 1 1 + 2 22.23 0 0 + 0 0	20.21 O O O O O	19.19 0 0 0 0 0 19.17 0 0 0 0 0	18.18 O 1 + + O	20.21 + 1 + 1 0
20.21 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	20.21 0 0 0 0 0 10.10 0 0 0 0 0	10.17 0 0 0 0 0 10.16 0 0 0 0 0	14.18 0 0 0 0 0	14.15 0 0 0 0 0	16.17 0 0 0 0 0
14.15 0 0 0 0 0	18.17 O O O O O O O O O	12.13 O O O O O O	10.11 0 0 0 0 0	10,11 O O O O O	12.13 O O O O O
237	699	111	314	503	334
ніно вреео (KT6) ³¹	HIND SPEED (KTS) 3?	HIND SPEED (KTS) 33	HIND SPEED (KIB) 34	HIND SPEED (KTS) 35	HIND SPEED (KTS) 36
TEMP (*C) 0-9 4-10 11-21 22-30 a 34	18MP (*C) 0-9 4-10 11-21 22-33 - 34	784-86 0 + + 0 0	18MP (*C) 0-3 4-10 11-21 22-33 = 34 20-27 1 + 1 0 0	TEMP (*C) 0-8 4-10 11-21 22-98 2-94	TEMP (*C) 0-3 4-10 11-21 22-32 2 34
#0.01 2 6 4 1 0 18.18 2 18 8 1 0	24,26 + 1 + 0 0	20.21 1 3 2 + 0	24.40 1 3 6 2 0 22.43 3 14 19 2 0	26.27 1 1 1 0 0 24.25 1 4 3 0 0	19.19 + 1 3 1 +
18.17 1 19 15 6 0 14.18 0 8 4 3 1	20.21 1 8 10 3 + 10.18 1 18 22 8 +	18.18 3 14 15 2 0 18.17 3 19 18 3 +	20.21 1 10 15 2 0	28,29 1 16 15 2 · 20,21 3 17 19 3 1	14.15 1 6 9 4 1 14.19 1 5 15 6 •
12.13 0 0 0 + 0	18.17 1 6 13 5 1 16.16 • 1 1 1 +	14-18 1 6 5 1 + 12-13 + + + + +	18.17 0 1 + 1 0 14.16 0 0 0 0 0	10.10 2 6 6 2 0 10.17 0 + 0 0 0	10.11 1 4 11 4 1
0.0 0 0 0 0 0 0.7 0 0 0 0 0	12,13 0 0 + + 0	10.11 0 0 0 0 0 0.0 0 0 0 0	12.13 0 0 0 0 0 0	14.18 0 0 0 0 0	4.5 U O O O
4.8 0 0 0 0 0 2.3 0 0 0 0 0	8.8 0 0 0 0 0 6.7 0 0 0 0 0	9.7 0 0 0 0 0 4.6 0 0 0 0 0	6.0 0 0 0 0 0 6.7 0 0 0 0 0	10.11 0 0 0 0 0 0 0.0 0 0 0 0 0	2.3 0 0 0 0 0 0.1 0 0 0 0 0
226	739	1788	682	350	717
	HIND SPEED (KTS) 4 1	HIND SPEED (KTS) 42			HIND SPEED (KTS) 45
12.13 0 0 1 0 0	10.10 0 1 1 0 0	20.21 + 0 0 0 0	10.21 + 0 0 0 0	14,18 0 0 0 1 0	14.16 0 1 2 1 0
10,11 0 3 12 8 3 6.6 0 4 13 11 2	14-18 4 14 15 6 3	18.17 2 5 4 2 0	10.10 + 1 0 + 0 10.17 1 2 5 4 +	18.19 0 0 0 0 0 10.11 0 0 3 0 0	18:19 + 4 15 6 + 10:11 + 5 19 3 1
6.7 3 8 17 6 3 4.6 0 0 6 2 2	19.73 + 9 1 1 1	14.18 1 9 12 3 0 12.13 1 16 23 5 1	15 3 9 10 6 1 2.13 2 9 20 10 3	6.7 0 10 18 6 1	0.0 + 6 12 10 1 0.7 0 1 1 3 0
0.1 0 0 0 0 0	0.7 0 0 0 0 0	10.11 1 4 8 2 0 0.0 0 0 + 0 0	10.11 1 2 4 3 2 0.3 + 1 0 1 0	4,8 2 15 9 13 9 2,8 0 0 0 2 0	4.\$ 0 0 0 U 0 2.3 0 0 0 0 D
-2,-1 0 0 0 0 0 0 -4,-3 0 0 0 0 0	2.3 0 0 0 0 0	4.8 0 0 0 0 0 0 4.8 0 0 0 0 0 0	4.6 0 0 0 0 0 0 4.6 0 0 0 0 0 0	-g1 0 0 0 0 0 0 0 0	-81 0 0 0 0 0 0 -81 0 0 0 0 0 0
-06 0 0 0 0 0 0 -07 0 0 0 0 0 0	-2i 0 0 0 0 0	2.3 0 0 0 0 0 0.1 0 0 0 0 0	2.3 0 0 0 0 0 0 0.1 0 0 0 0 0 0	-49 0 0 0 0 0 -06 0 0 0 0 0	-48 0 0 0 0 0 0 -88 0 0 0 0 0
114	359	296	378	60	286

ective compilation of available data for specified areas without regard to suspected biases.

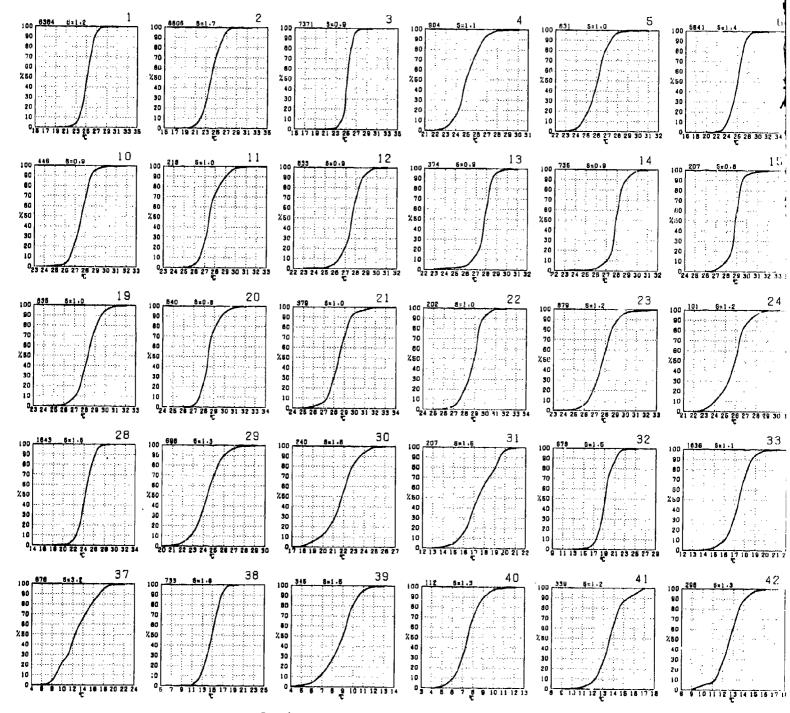
sposite page) are based on all available data subjectively adjusted where bias was evident.



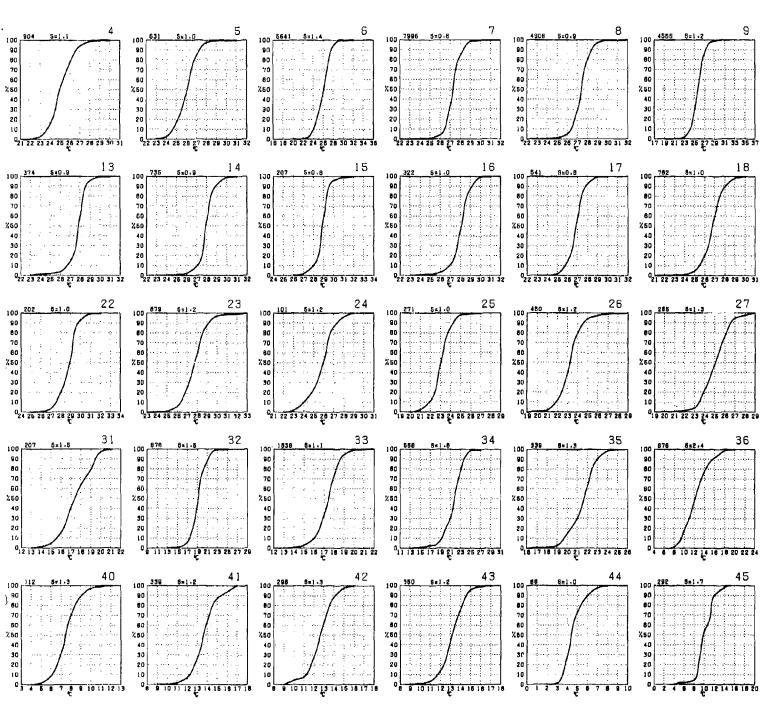
SEA SURFACE TEMPERATURE



SEA SURFACE TEMPERATURE

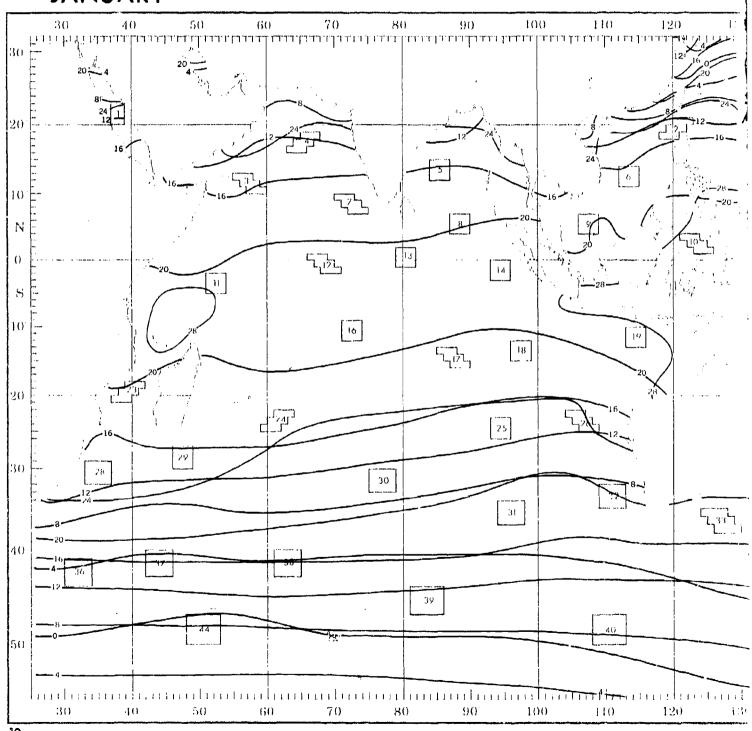


Graphs represent the objective compilation of available data for specified areas without respectively adjusted in a specified areas without respectively.

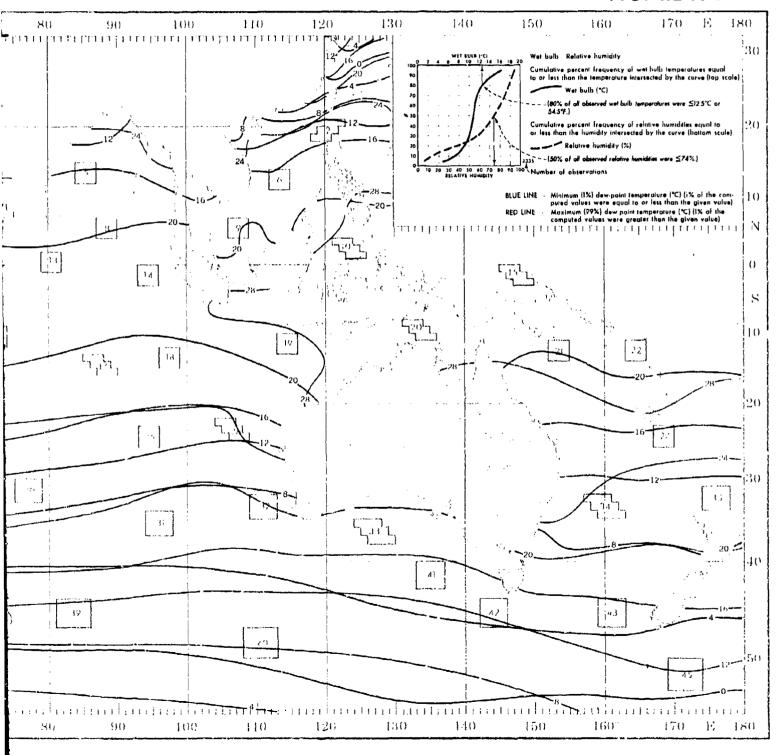


ective compilation of available data for specified areas without regard to suspected biases.

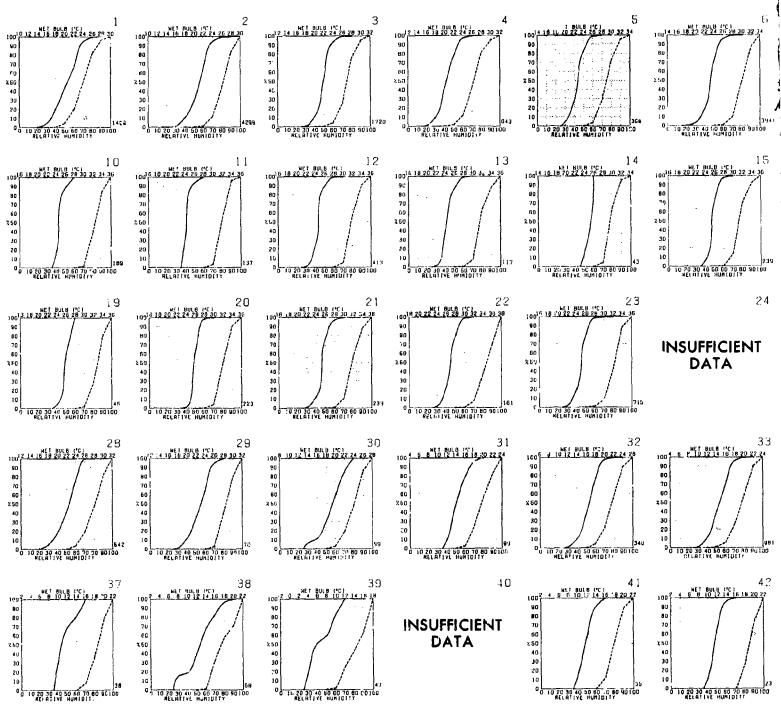
-posite page) are based on all available data subjectively adjusted where bias was evident.



HUMIDITY



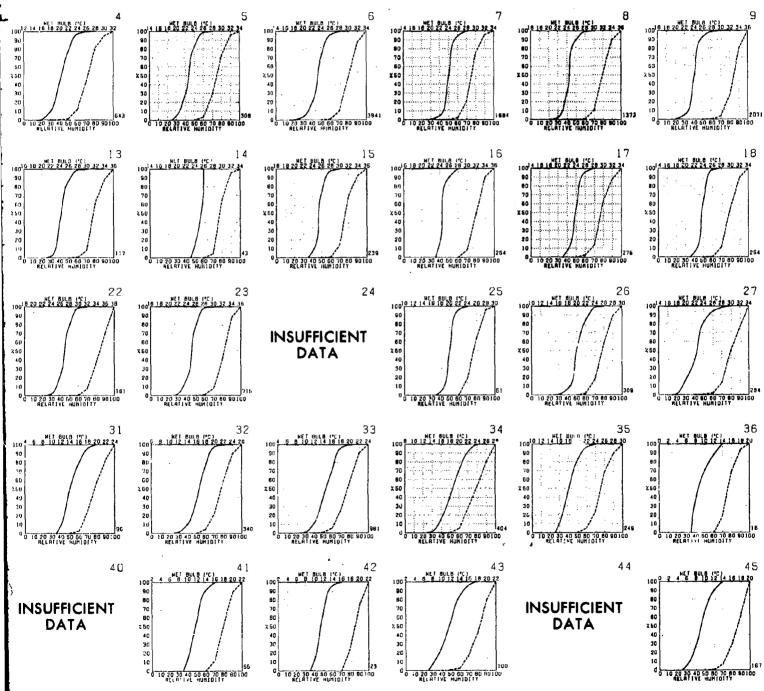
WET BULB AND RELATIVE HUMIDITY



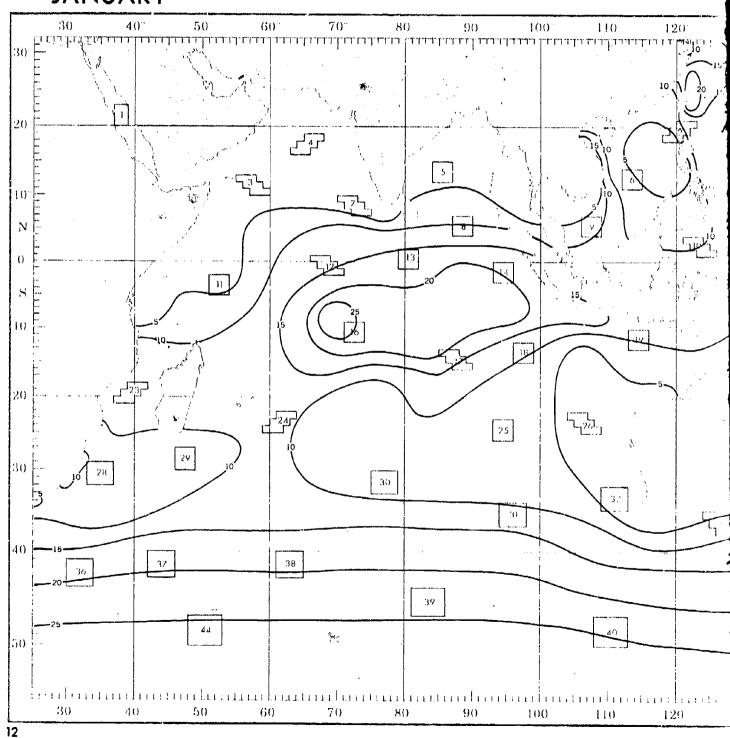
Graphs represent the objective compilation of available data for specified areas without reg The isopleth analyses (apposite page) are based on all available data subjectively adjusted

UMIDITY

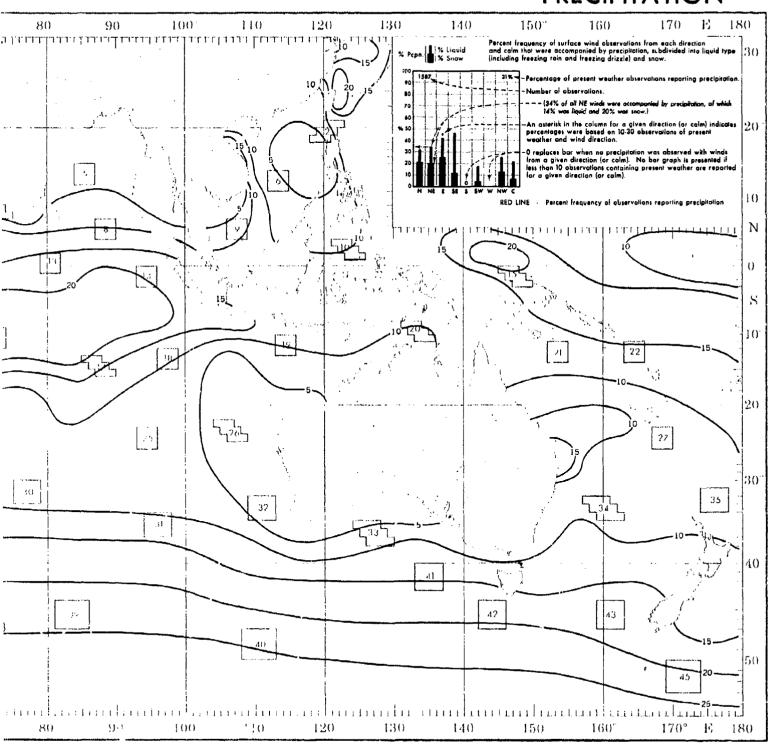
JANUARY



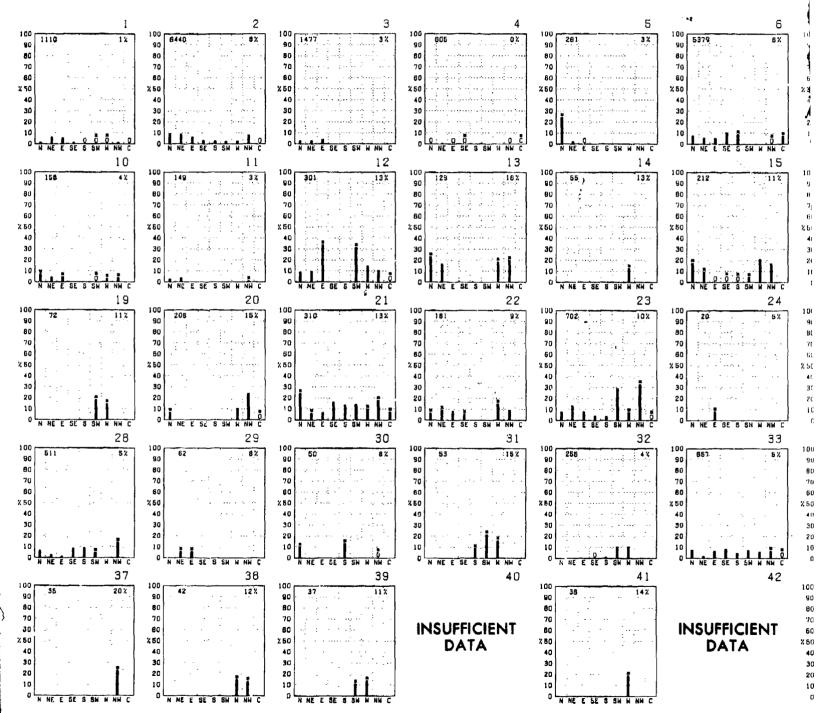
jective compilation of available data for specified areas without regard to suspected biases, pposite page) are based on all available data subjectively adjusted where bias was evident



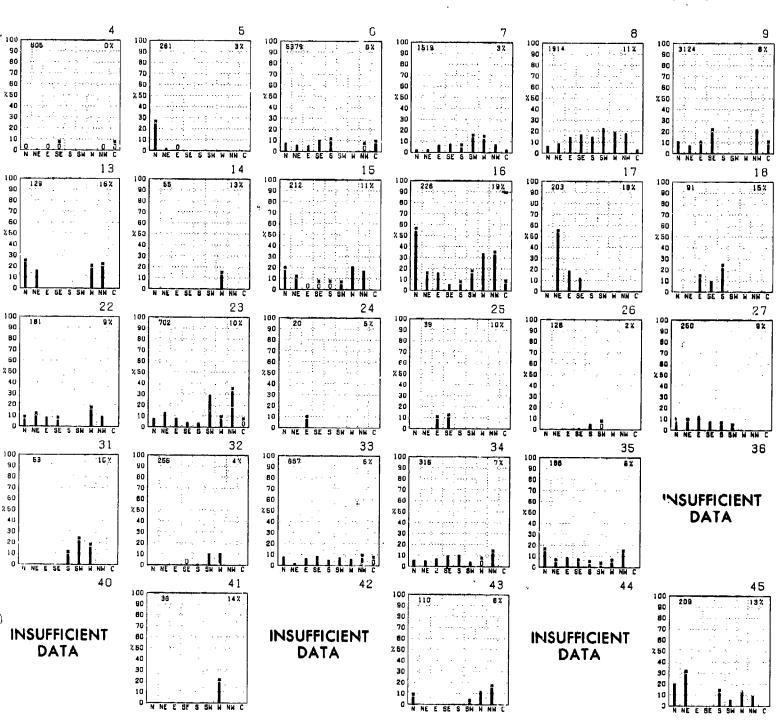
PRECIPITATION



PRECIPITATION

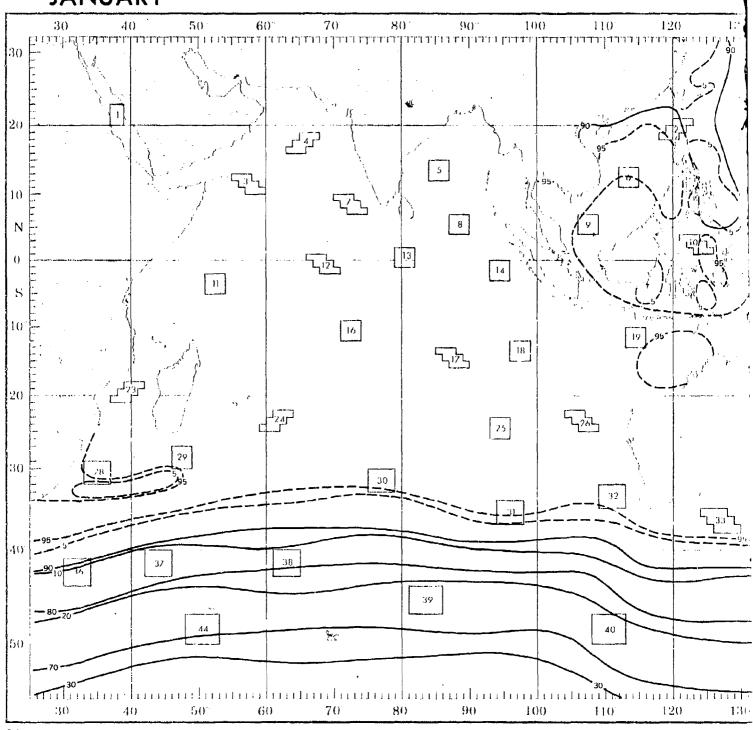


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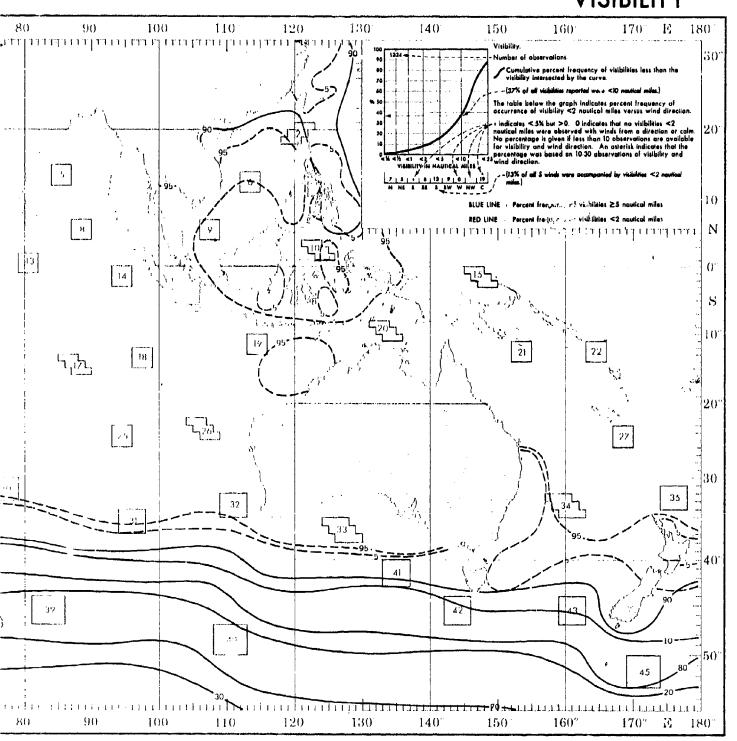


ective compilation of available data for specified areas without regard to suspected biases. posite page) are based on all available data subjectively adjusted where bias was evident.

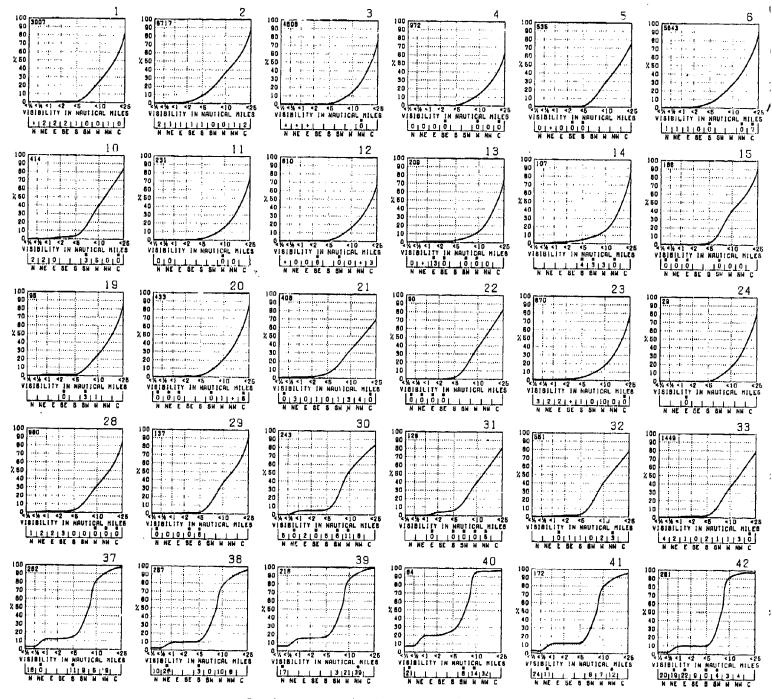
13



VISIBILITY

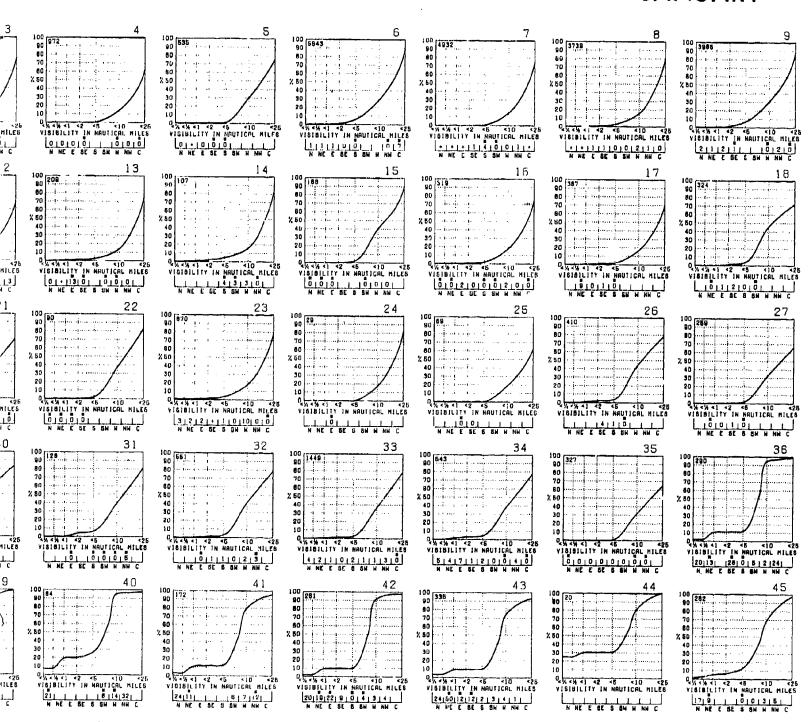


VISIBILITY

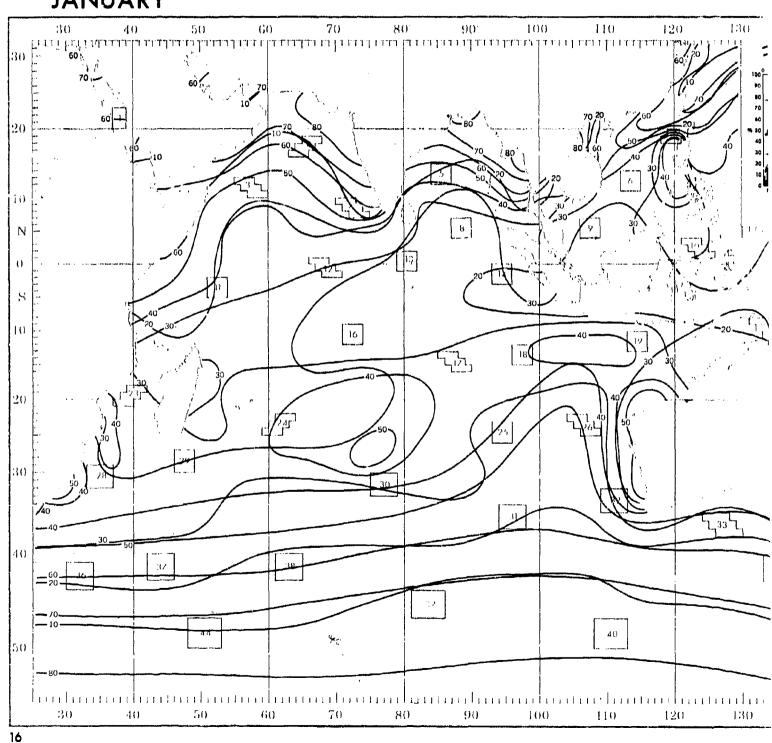


<u>Graphs</u> represent the objective compilation of available data for specified areas without reg.

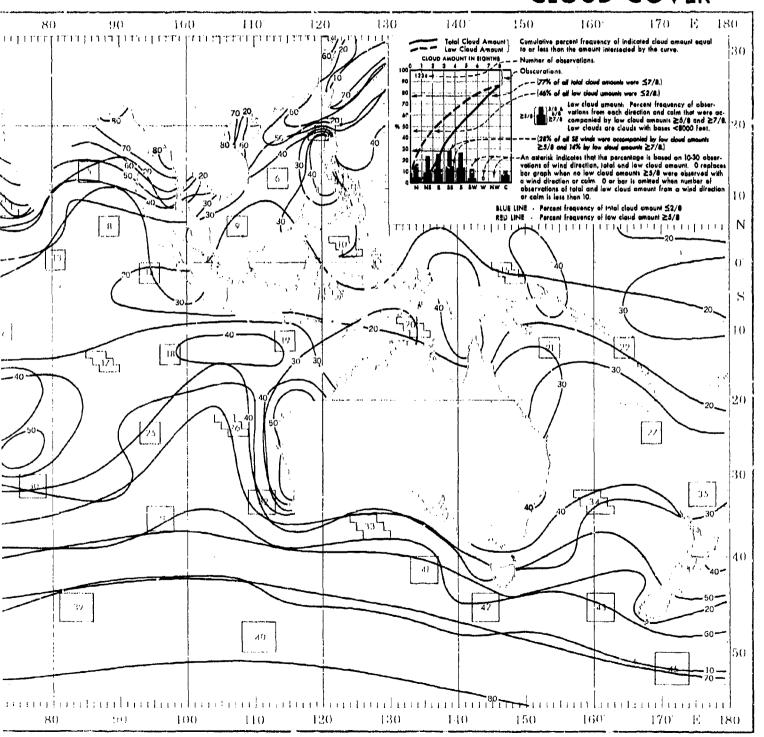
The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjusted



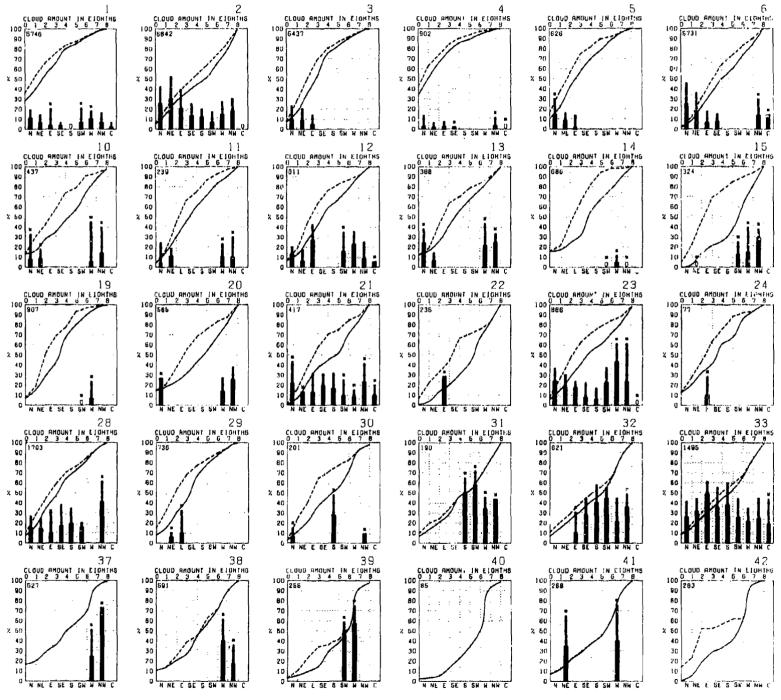
objective compilation of available data for specified areas without regard to suspected biases. s (opposite page) are based on all available data subjectively adjusted where bias was evident.



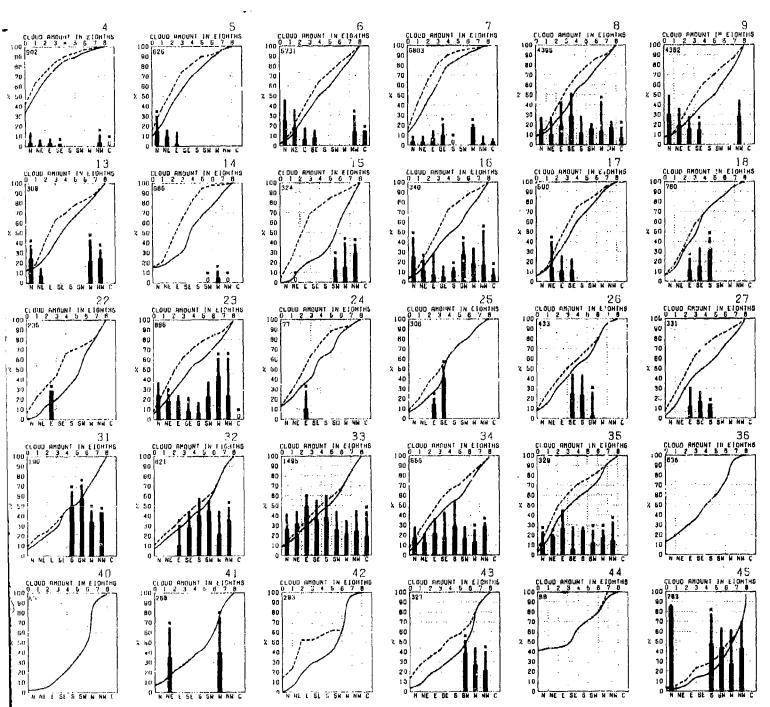
CLOUD COVER



CLOUD COVER

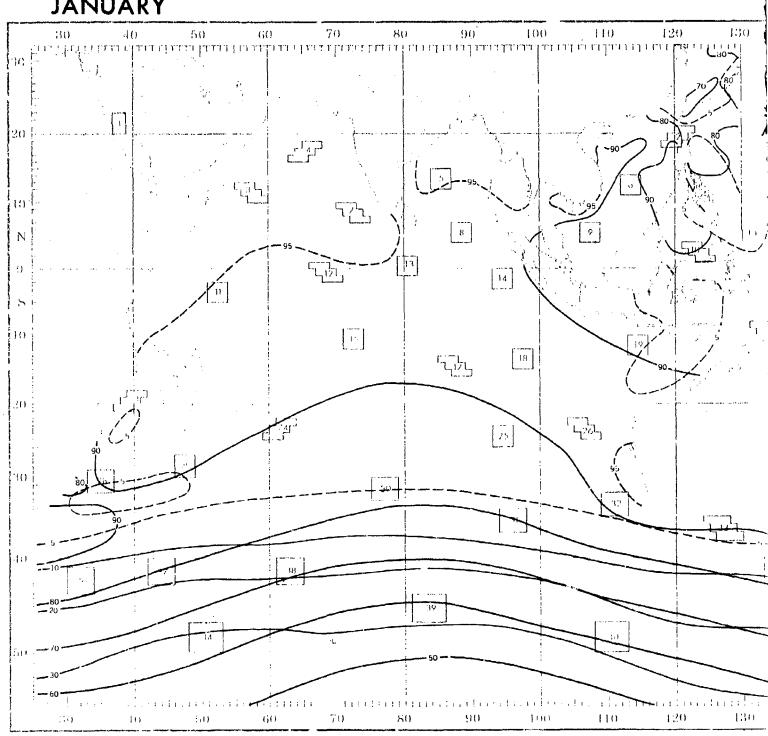


<u>Graphs</u> represent the objective compilation of available data for specified areas without re The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjuste



ctive compilation of available data for specified areas without regard to suspected biases.

osite page) are based on all available data subjectively adjusted where bias was evident.



CEILING AND VISIBILITY 140" Percent frequency of simultaneous occurrence of specified low cloud ceilings (hundreds of feet) and visibilities (nautical miles). Percent frequency of low cloud ceiling ≥1000 leet (or no low cloud ceiling) and visibility ≥5 nautical miles
Percent frequency of low cloud ceiling <600 feet and/or visibility <2 nautical miles \mathbf{S} 160°

CEILING AND VISIBILITY

VISIBILITY 41/2 24/3 14/2 24/3 14/3 11/3	VISIBILITY VISIBILITY VISI	VISIBILITY ***/** **/** ***/*** ***/** ***/** ***/** ***/** ***/** ***/** ***/** ***/** ***/***	VISIBILITY A: VISIBILITY A: 0 0 0 0 . 5 6 6 10 10 0 5 6 6 0 0 0 0 0 0 0 5 7 7 8 0 0 0 0 0 0 0 5 7 8 0 0 0 0 0 0 0 1 5 7 8 0 0 0 0 0 0 0 1 5 7 8 0 0 0 0 0 0 0 1 5 8 0 0 0 0 0 0 0 1 5 8 0 0 0 0 0 0 0 0 5 8 1 0 0 0 0 0 0 0 5 1 1 5 1 0 0 0 0 0 0 0 5 1 5 1 5 0 0 0 0 0 0 0 5 1 7 5 1 5 1 7 5 5 5 10 0 5 1 7 5 1 7 5 10 0 0 0 0 0 0 0 5 1 7 5 1 7 5 10 0 0 0 0 0 0 0 0 5 1 7 5 1 7 5 10 0 0 0 0 0 0 0 0 0 5 1 7 5 1 7 5 10 0 0 0 0 0 0 0 0 0 5 1 7 5 10 0 0 0 0 0 0 0 0 0 0 0 0 5 1 7 5 1 7 5 10 0 0 0 0 0 0 0 0 0 0 0 5 1 7 5 1 7 5 10 0 0 0 0 0 0 0 0 0 0 0 0 5 1 7 5 1 7 5 10 0 0 0 0 0 0 0 0 0 0 0 0 5 1 7 5 1 7 5 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 5 1 7 5 1 7 5 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISTBIL ITY 1/2 2/3 1/3 1/3 2/3 1/3 1/3 AC - 0 0 0 5 7/3 40 - 0 0 0 0 1 2 50 60 60 0 0 0 2 50 50 60 60 0 0 2 50 50 60 60 60 60 50 50 60 60 60 60 50 50 60 60 60 60 50 50 60 60 60 60 50 50 60 60 60 50 60 60 60 60 60 60 60	VISIBILITY 10 12 12 12 13 14
VISIBILITY VISIBILITY 1-79 741 1-62 2-65 5-10 1-10 1-62 0 0 0 0 0 0 1-62 0 0 0 0 0 0 1-62 0 0 0 0 0 0 1-62 0 0 0 0 0 0 1-62 0 0 0 0 0 0 1-62 0 0 0 0 0 0 1-64 0 0 0 0 0 0 1-64 0 0 0 0 0 0 1-64 0 0 0 0 0 0 1-64 0 0 0 0 0 0 1-64 0 0 0 0 0 0 1-64 0 0 0 0 0 0 1-64 0 0 0 0 0 0 1-64 0 0 0 0 0 0 1-64 0 0 0 0 0 0 1-64 0 0 0 0 0 0 0 1-64 0 0 0 0 0 0 0 1-64 0 0 0 0 0 0 0 1-64 0 0 0 0 0 0 0 1-64 0 0 0 0 0 0 0 1-64 0 0 0 0 0 0 0 1-64 0 0 0 0 0 0 0 1-64 0 0 0 0 0 0 0 1-64 0 0 0 0 0 0 0 1-64 0 0 0 0 0 0 0 1-64 0 0 0 0 0 0 0 1-64 0 0 0 0 0 0 0 1-64 0 0 0 0 0 0 0 1-64 0 0 0 0 0 0 0 1-64 0 0 0 0 0 0 0 1-64 0 0 0 0 0 0 1-64 0 0 0 0 0 0 1-64 0 0 0 0 0 1-64 0 0 0 0 0 1-64 0 0 0 0 0 1-64 0 0 0 1-64 0 0 0 1-64 0 0 0 1-64 0 0 0 1-64 0 0 0 1-64 0 0 0 1-64 0 0 0 1-64 0 0 0 1-64 0 0 0 1-64 0 0 0 1-64 0 0 0 1-64 0 0 0 1-64 0 0 0	VISIBILITY 1 1 1	VISIBILITY 2	VISIBILITY 1 3	VISIBILITY 1 4	VISIBILITY ** a /a* 1 ** ** ** ** ** **
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VISIBILITY 37	**************************************	VISIBILITY	INSUFFICIENT DATA	VISIBILITY 4 1	

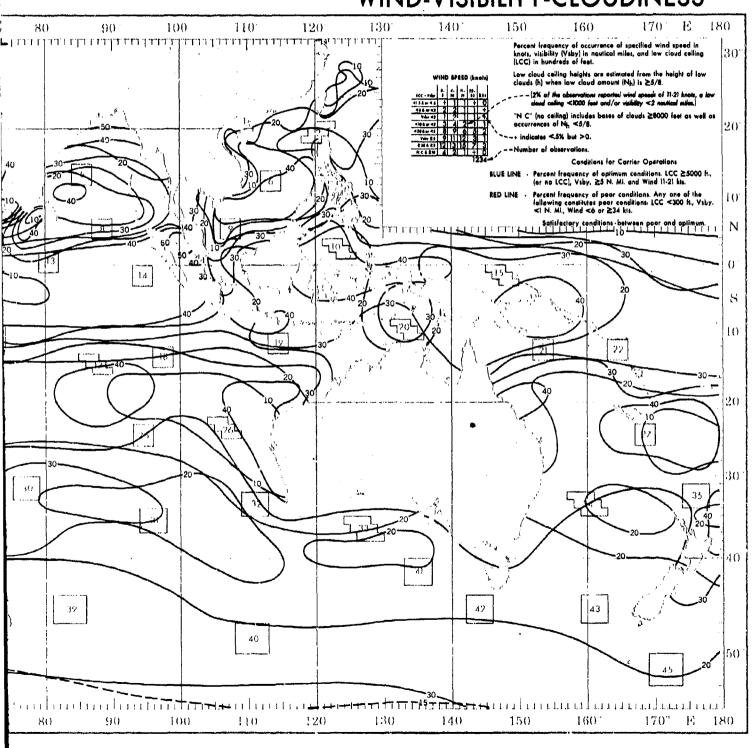
Graphs represent the objective compilation of available data for specified areas without r The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjust-

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No. No.	Visit ITY	State Stat		State Stat	**** **** **** **** **** **** **** **** **** **** **** **** **** **** **** **** **** **** ******
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VIETBILLITY V V V V V V V V V	VISIBILITY 23 **** Aut.) 1-2 2-2 8-10 10 **** Aut. Aut. Aut. Aut. Aut. Aut. **** Aut. Aut. Aut. Aut. Aut. Aut. *** Aut. Aut. Aut. Aut. Aut. Aut. *** Aut. Aut. Aut. Aut. Aut. *** Aut. Aut. Aut. Aut. Aut. *** Aut. *** Aut. Aut. *** Aut. Aut. *** Aut. Aut. *** *** Aut. *** *** Aut. *** Aut. *** *** Aut. *** *** Aut. *** *** Aut. ***	VISIBILITY 24	VISIBIL [17 25]	VISIBILITY 26 (*/*)	VISIGNATIVE 27 VISIGNATIVE PROPERTY OF THE PR
VIBIDIL_ITY 3 }	VISIBILITY 32 NC 0 0 0 0 0 1 10 0 000 0 0 0 1 1 31-40 0 0 0 0 0 1 1 31-40 0 0 0 0 1 2 7 31-40 0 0 0 0 1 3 22 31-50 0 0 0 0 0 0 1 31-50 0 0 0 0 0 0 1 31-50 0 0 0 0 0 0 1 31-50 0 0 0 0 0 0 1 31-50 0 0 0 0 0 0 0 1 31-50 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY ***VISIBILITY ***C C 0 0 0 * 3 49 ***C C 0 0 0 0 * 3 49 ***C C 0 0 0 0 * 3 49 ***C C 0 0 0 0 * 1 13 ***C C 0 0 0 0 * 1 13 ***C C 0 0 0 0 * 2 5 ***C C 0 0 0 0 * 2 5 ***C C 0 0 0 0 * 2 5 ***C C 0 0 0 0 * 2 5 ***C C 0 0 0 0 * 2 5 ***C 0 0 0 0 0 * 2 5 ***C 0 0 0 0 0 * 0 0 0 ***C 0 0 0 0 0 0 0 0 0 0 ***C 0 0 0 0 0 0 0 0 0 0 ***C 0 0 0 0 0 0 0 0 0 0 ***C 0 0 0 0 0 0 0 0 0 0 ***C 0 0 0 0 0 0 0 0 0 0 0 ***C 0 0 0 0 0 0 0 0 0 0 0 ***C 0 0 0 0 0 0 0 0 0 0 0 ***C 0 0 0 0 0 0 0 0 0 0 0 0 ***C 0 0 0 0 0 0 0 0 0 0 0 0 ***C 0 0 0 0 0 0 0 0 0 0 0 0 ***C 0 0 0 0 0 0 0 0 0 0 0 0 0 ***C 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 ***C 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 ***C 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	**************************************	VISIBILITY 35	10 10 10 10 10 10 10 10
INSUFFICIENT DATA	VISIBILIT VISI	VISIBILITY 42 **In	VISIBILITY 4 3 VISIBILITY 4 3 NC 0 0 0 1 1 11 41 B040 0 0 0 0 0 0 2 3 3440 0 0 0 1 0 0 0 2 7 7048 0 0 0 0 1 1 0 0 2 7 7048 0 0 0 0 0 1 1 0 0 1040 0 0 0 0 0 1 1 0 1040 0 0 0 0 0 1 1 0 1040 0 0 0 0 0 1 1 0 1040 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1440 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	INSUFFICIENT DATA	VISIBILITY 45 VISIBILITY 45 NC - 0 0 1 12 16 B0-80 0 0 0 0 0 0 2 10-38 0 0 0 0 0 0 0 2 10-38 0 0 0 0 0 0 0 2 10-40 1 0 0 0 0 0 0 0 1-40 0 0 0 0 0 0 0 0 1-40 0 0 0 0 0 0 0 0 1-40 0 0 0 0 0 0 0 0 1-40 0 0 0 0 0 0 0 0 1-40 0 0 0 0 0 0 0 0 200

ective compilation of available data for specified areas without regard to suspected biases. posite page) are based on allovallable data subjectively adjusted where bias was evident.

JANUARY WIN Ν 4() 8: 4() 90"

WIND-VISIBILITY-CLOUDINESS



LOW CLOUD CEILING-VISIBILITY-WIND

					1
HIND SPEED (KNOTS)	2 WIND SPEED (KNOTS)	3 WIND SPEED (KNOTS)	MIND SPEED (KNOTS)	HIND SPEED (KNOTS)	WIND SPEED IKN
LCC - VBSY 3 10 21 23 234	LCC - VERY 3 10 21 33 434	LCC - VEBY 3 10 21 33 234	LCC - VSBY 3 10 21 33 634	CC - V8BT	LCC - V48Y 3 10 21 3
48 4 00 4Z 0 + + 0 0	46 4 0R 48 0 + 1 2 1	46 4 OR 42	«94 DR «2 0 • 0 0 0	48 £ 0R 42	<6 4 UR <2 + + 1
<10 4 OR <2 + 1 1 + 0	410 4 DR 42 + 3 6 6 1	*10 4 DR *2 0 1 2 + 0	410 4 08 42 0 1 + O D	(10 4 DR (2 D + 2 + D	410 4 0R 42 + 1 5
480 4 68 48 1 3 4 0 0 V887 65 10 42 44 3 0	420 4 98 48	<20 4 DR <6 0 3 6 1 0 VBBY Ab 1 36 50 4 4	480 4 OR 48 0 2 3 0 0 VABY 36 7 50 42 1 0	*20 4 GR 45 1 2 5 2 D	420 4 0R 48 + 2 15 1 9887 88 1 17 57 1
aso 4 ns 9 37 37 2 0 MC 4 a 19 8 34 35 2 0	#60 4 ah 2 12 24 14 2	HC 4 a 10 1 29 46 2 +	*80 4 *B 7 46 37 1 0 MC 4 * 10 7 44 38 1 0	80 4 28 5 54 26 2 0 MC 4 8 10 5 48 23 1 6	80 488 1 14 39 HC 4 8 10 1 13 33
1044	5503	1385	600	286	
10	HIND ALEED (KNOIZ)	HIND SPEED (KNOTS)	WIND BPEED (KNOTS)	14 HIND SPEED (KNOTS)	HIND SPEED IKNI
LCC - YSSY 3 -0 21 38 894	LCC - VERY 3 10 21 33 234	LCC - YSSY 3 10 21 33 334	1.6 4 0R < 8 0 0 2 0 0	LCC - VBBY 3 10 21 33 234	LCC - VORY \$ 10 21 3
46 4 OR 42 0 0 0 0 0	48 4 68 42 0 1 0 0 0	-64 OR -2 + 1 1 0 0	-84 GR -8 1 2 2 0 0	-44 OR 42 D D O O O	«8 4 OR «E 0 2 D
40 4 48 42 0 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VBBY 42 0 0 0 0 0 0 0 410 4 00 4 2 1 3 1 0 0	VBBT 42 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VBSY 48 0 1 1 0 0	V887 42 0 0 0 0 0 0 0 0 410 4 0R 42 0 2 2 0 0	460 4 0R -2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
420 4 pm 46 2 13 0 0 0 VMBY as 13 70 17 0 0	480 4 08 48 2 10 5 0 0	480 4 gR <8 2 9 4 0 0 Y68Y ab 18 68 17 0 0	48G ± 0R 40	420 4 OR 46 2 8 4 0 0 988Y a5 23 58 17 2 0	<20 4 0R 48 0 7 5 VBBY AB 17 49 29
80 4 a5 11 55 15 0 0	850 4 hB 6 54 17 0 0	850 4 85 13 54 10 0 0 MC 4 a 10 12 52 10 0 0	a 50 4 45 7 49 15 0 0	AGU 4 AG 21 49 13 2 0 MC 4 B 10 15 45 13 2 0	>60 4×6 17 44 17 NC 4 > 10 14 37 12
83	142	338	123	53	12/2/12/
19 Hind Breed (Knots)	20 HIND SPEED (KNOTS)	21 HIND SPEED (KNOTS)	22 HIND SPEED (KNOTB)	41ND BPEED (KNOTS)	HIND SPEED CKNC
LCC - VSST 3 10 E1 33 a34	LCC - VBBY 9 10 21 33 a34	LCC - V68Y	LCC - YBEY 3 1U 81 33 834	LCC - YSBY 3 1C 21 33 334	CC - VSST 3 10 21 3:
40 4 00 42 0 0 0 0	48 4 GR 48 0 1 1 0 0	48 4 DR 42 D 1 1 0 0	46 4 DR 42 0 0 0 3 C	-8 4 OR -2 0 + 1 1 2	48 4 SM 42 0 0 0
*10 4 00 *2	4887 48 D O O O O O C C C C C C C C C C C C C C	V847 <2 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 9 P R64 01 P	Y88Y 4Z	V88Y 4E 0 0 0 0
480 4 SM 48 0 B 8 0 0	v667 a6 10 42 43 3 0	*20 4 SH *8 3 13 8 2 0 ************************************	*20 4 6A *5 0 12 8 8 0 ************************************	420 4 gR 45	42D 4 OR 45 C O 5 1
864 a6 10 63 6 2 0	860 4 a6 B 31 31 1 D 8C 4 a 10 B 31 26 D D	#64 + 10 42 19 D O O	#80 4 #6 12 33 24 3 0 MC 4 # 10 6 33 24 3 0	250 424 8 37 25 3 0 HC 4 2 10 8 36 23 1 0	#60 4 = 5 9 23 41 1 HC 4 a 10 9 29 41 1
52 28	172	1H6 30	33	32	
HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	WIND SPEED (KNOTS)	MIND SPEED (KNOTS)	NING SPEED (KNOTS)	HIND BREED CKNC
LCC - Vesy 3 10 21 39 a94	LCC - Y887 3 10 21 35 a34	LCC - VBBY 3 10 21 38 394	tcc - vuer 3 10 81 38 a84	LCC - V48Y 9 10 21 35 294	LCC - V867 3 10 21 32 <1.8 4 SM c.8 Q + Q (
48 4 98 48	*6 4 DR *2 0 0 0 0	48 4 OR 42 4 1 3 D D	43 & SR 42 D D 1 D 1	*8 4 08 <2 0 0 1 1 0	40 A DR 42 D 1 4
<10 4 0R <2 1 5 4 1 +	*10 4 64 42 D D B D D	410 4 0R 42 4 3 4 0 0	410 4 UM 42 D 7 8 1 1	410 4 0R 42 0 1 2 1 0	410 4 0H 42 + 3 4
420 4 0R 46 1 8 8 2 1 YSBY 35 6 41 44 6 1	*80 4 6M *8 0 3 13 2 U	420 4 0R 48 4 7 8 0 0 YEST BE 14 64 16 1 0	*20 4 CR *8 0 18 11 5 1 ************************************	*20 4 0R *6 + 9 17 B + YEST 25 2 33 48 14 1	420 4 0R 46 1 11 12 3 VBBY 25 7 40 43
a 80 4 a 9 6 30 32 6 +	aBC 4 aB 6 24 37 11 0 MC 4 a 10 6 21 34 11 0	860 4 aB 13 52 12 1 0 MC 4 a 10 12 51 12 1 0	80 4 25 5 30 7 4 3 MC 4 2 10 5 28 5 4 1	2 19 20 8 1 HC4210 2 17 18 7 1	#64 & 10 5 19 21 4
508 37	62 38	99 39	78 4 O	303 4 1	
NIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)		HIND SPEED (KNOTS)	MIND SPEED INNO
LCC - Y88Y 3 10 21 38 834	LCC - VBOY 5 10 21 35 634	LCC - V88Y 3 10 21 39 894		LCC - VBBY 9 10 21 33 294	LCC - V687 3 10 21 31
49 4 9R 42 0 3 3 0 0	48 & 0R 42 0 7 2 2 0	49 4 0 4 2	INSUFFICIENT	<84 08 42 0 0 0 0 0 0 0 VBB1 42 0 0 0 0 0 0 0	-0 & OR -2 0 0 0 C
-10 4 SM -2 0 6 8 8 0	410 4 OR -E 0 7 2 9 0	-10 t or -e 0 0 5 0 0	DATA	-10 & DR -2 0 13 8 0 0	410 4 DR 42 () 5 5 (
480 4 98 48 0 8 33 11 0 V60 7 36 0 19 42 17 3	988 4 0R 48 0 9 20 13 0 9 888 48 2 20 35 22 7	*20 t on *6 0 11 11 11 3 veer as 3 24 27 30 3		420 A OR 48 3 23 21 3 3 V667 25 Ø 41 46 3 3	*20 4 DR *6 0 10 5 (YBBT 25 5 35 45 10
80 4 25 0 11 17 5 0 MC 4 2 10 0 11 14 6 0	860 4 2 5 2 15 15 13 2 862 4 2 10 2 13 13 7 0	#C 4 a 10 3 6 16 6 U		250 4 26 5 10 15 0 0 MC 4 2 10 5 10 15 0 0	#C4 n 10 5 5 45 1C

Graphs represent the objective compilation of available data for specified areas withou The isopleth analyses (opposite page) are based on all available data subjectively adju

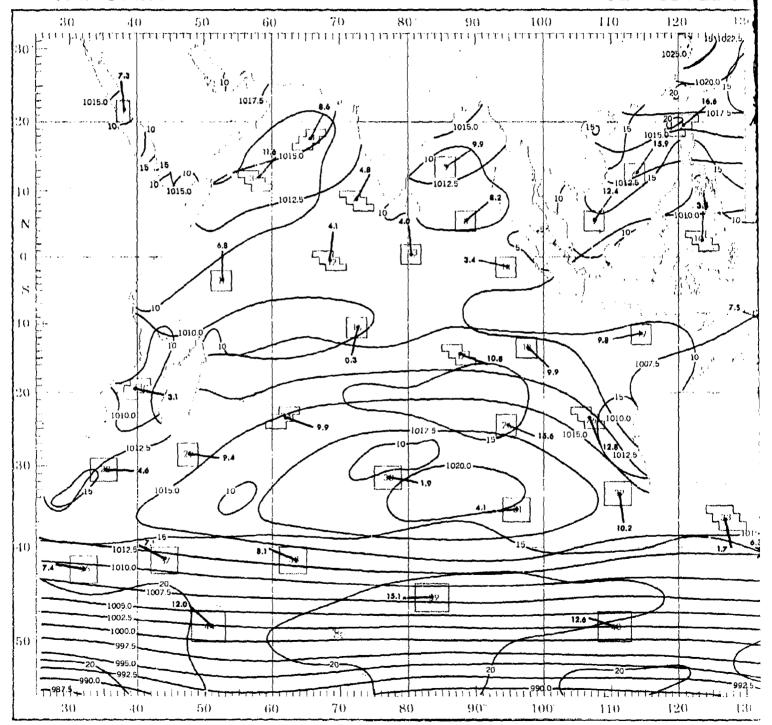
JITY-WIND

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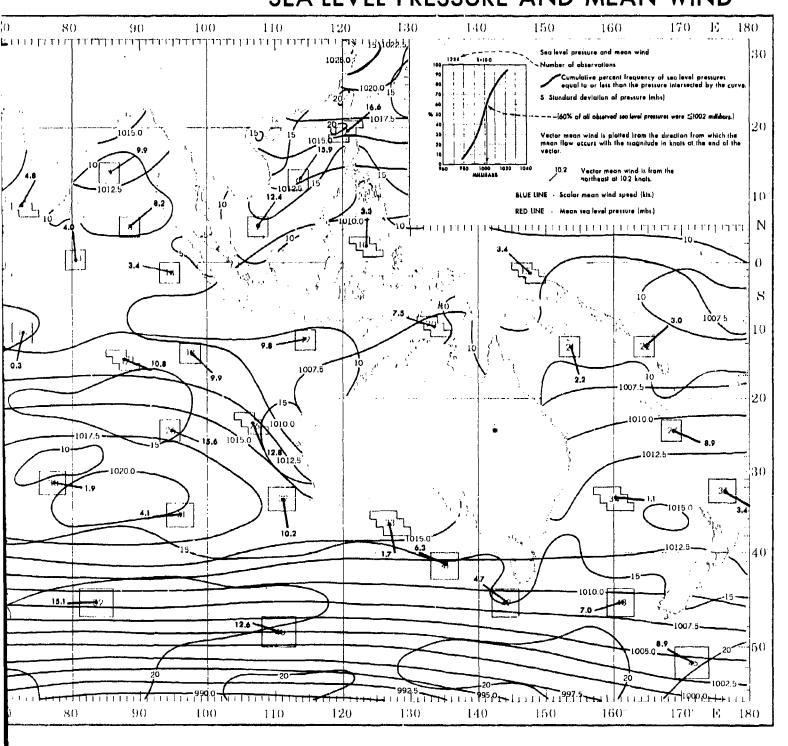
HIND SPEED (XNOTS) 1(f - VSST 3 0 1 13 23 23 1.6 + 0.0 + 0 0 0 0 0 16 + 0.0 + 0 0 0 0 0 10 + 0.0 + 0 0 0 0 0 10 + 0.0 + 0 0 0 0 0 10 + 0.0 + 0 0 0 0 0 10 + 0.0 + 0 0 0 0 0 10 + 0.0 + 0 0 0 0 10 + 0.0 + 0 0 0 0 10 + 0.0 + 0 0 0 0 10 + 0.0 + 0 0 0 0 10 + 0.0 + 0 0 0 0 10 + 0.0 + 0 0 0 0 10 + 0.0 + 0 0 0 10 + 0.0 + 0 0 0 10 + 0.0 + 0 0 0 10 + 0.0 + 0 0 0 10 + 0.0 + 0 0 0 10 + 0.0 + 0 0 0 10 + 0.0 + 0 0 10 + 0.0 + 0 0 10 + 0.0 + 0 0 10 + 0.0 + 0 0 10 + 0.0 + 0 0 10 + 0.0 + 0 0 10 + 0.0 + 0 0 10 + 0.0 + 0 0 10 + 0.0 + 0 0 10 + 0.0 + 0 0 10 + 0.0 + 0	HIND SPEED (KNOIS) LCC - VSAY	HIND SPEED (KNOTS) LCC - V88Y	77 HIND SPEED (KNOTS) LCC - VBBV 9 16 21 33 454 *1.8 4 08 *1 0 + 0 0 0 *18 4 08 *2 + + 0 0 0 *10 4 08 *2 + + 0 0 0 *10 4 08 *2 + + 0 0 0 *10 4 08 *2 + 1 + 0 0 *20 4 08 *5 1 4 1 0 0 *20 4 08 *5 1 8 54 9 0 0 MC + 10 16 83 9 0 0	HIND SPEED (KNOTS)	HIND BPEED (KNOTS) LCC - YEAY
13 NINO SPEED (KNDTS) LCC - YBBY	1 4 HIND SPEED INNOTES 1 4 HIND SPEED INNOTES 1 1 - 1 2 1 4 1 3 2 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4	HIND SPEED (KNDTS) LCC - VASY	HIND SPEED (KNDS) LCC - VABY	17 HIND SPEED (HNDTS) I.CC - VABY 0 1 11 12 13 13 134 11.8 4 0R 4.8 0 0 0 0 0 -8.4 0R 4.9 0 4 2 0 4 104 0R 4.8 0 3 5 0 4 104 0R 4.8 0 5 12 4 VABY 4.5 3 45 48 2 0 240 4 4.5 2 39 34 1 0 MC 4 3 10 2 37 32 1 0	HIND SPEED (KNOE) LCC - VSSY
#IND SPEED (KNOTS) 100 4- 11 12 12 12 12 12 12 1	23 MIND SPEED (KND15) 1.CC - VSSV 3, 10, 21, 32, 324 1.66 4 08 *2 0 + 1 1 2, 32, 324 1.66 4 08 *2 0 + 1 1 2 1.67 4 08 *2 0 + 0 1 2 1.67 4 08 *2 0 + 0 1 2 1.67 4 08 *2 0 + 0 1 2 1.67 4 08 *2 0 + 0 1 2 1.67 4 08 *2 0 + 0 1 2 1.67 4 08 *3 0 + 0 0 1 1 2 1.67 4 08 *4 0 + 0 0 1 1 2 1.67 4 08 *4 0 + 0 0 1 1 2 1.67 4 08 *4 0 + 0 0 1 1 2 1.67 4 08 *4 0 + 0 0 1 1 1 2 1.67 4 08 *4 0 + 0 0 1 1 1 2 1.67 4 08 *4 0 + 0 0 1 1 1 1 1 1 1 1	24 MIND SPEED (KNOTS) LCC - V68Y	25 MIND SPEED (KNDTS) 1.0 1- 22- 22- 22- 22- 22- 22- 22- 22- 22-	### APR 16 APR 16 APR 17 APR 18 APR 1	## 100 SPEED (KNOTS) CCC - VSSY
3 MIND SPEED (KNOTS) LCC - Y88Y 9 10 21 83 1944 -1-8-4-89 -1-8 0 0 0 0 0 0 -68-4-98 -2 0 0 1 0 0 0 -10-4-98 -2 0 0 1 0 0 0 -10-4-98 -2 0 0 1 0 1 0 1 -20-4-98 -5 0 0 18 11 5 1 -20-4-98 -5 0 0 18 11 5 1 -20-4-98 -5 0 0 0 0 0 0 -10-4-98 -5 0 0 0 0 0 0 -10-4-98 -5 0 0 0 0 0 0 0 -10-4-98 -5 0 0 0 0 0 0 0 -10-4-98 -5 0 0 0 0 0 0 0 -10-4-98 -5 0 0 0 0 0 0 0 0 -10-4-98 -5 0 0 0 0 0 0 0 0 -10-4-98 -5 0 0 0 0 0 0 0 0 0 -10-4-98 -5 0 0 0 0 0 0 0 0 0 -10-4-98 -5 0 0 0 0 0 0 0 0 0 0 -10-4-98 -5 0 0 0 0 0 0 0 0 0 0 0 -10-4-98 -5 0 0 0 0 0 0 0 0 0 0 0 0 -10-4-98 -5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	32 HIND SPEED INNOTS: LCC - Year 3 1-11-122- 1-16-684-68 0 0 0 0 0 0 0 -18-684-78 0 0 0 1 1 1 0 -18-684-78 0 0 0 0 1 1 0 -18-684-78 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -18-684-78 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	MIND SPEED (KNOTS)	3 4 HIND SPEED (KNOTS) LCC - Year 9 0 10 21 39 394 -1.84 OR -2 0 0 1 0 0 -48 4 DR -2 0 0 1 0 0 -104 07 -2 -1 1 6 1 0 -104 07 -2 -1	MIND SPEED IXNOTS	36 MIND SPEED (KNOTS) LCC - YSSY
INSUFFICIENT DATA	4 1 MIND SPEED (KNOTS) LCC - V60* 3- 1- 12- 27- 34- 41.840* - 8 0 0 0 0 0 -44.04 - 8 0 0 0 0 0 -48.04 - 8 0 0 0 0 0 -48.04 - 8 0 0 0 0 0 -48.04 - 8 0 0 0 0 0 -48.04 - 8 0 0 0 0 0 -48.04 - 8 0 0 0 0 0 -48.04 - 8 0 0 0 0 0 -48.04 - 8 0 0 0 0 0 0 -48.04 - 8 0 0 0 0 0 0 -48.04 - 8 0 0 0 0 0 0 -48.04 - 8 0 0 0 0 0 0 -48.04 - 8 0 0 0 0 0 0 0 -48.04 - 8 0 0 0 0 0 0 0 -48.04 - 8 0 0 0 0 0 0 0 0 0	42 HIND SPEED (KNOTS) LCC - V&BT 9 10 21 33 334 41.64 08 - 5 0 0 0 0 0 48.48 - 42 0 0 0 0 0 48.48 - 42 0 0 0 0 0 410.408 - 2 0 6 6 0 0 420.408 - 5 0 10 6 0 0 480.435 5 5 5 5 10 0 480.435 5 6 5 10 0 480.435 5 6 5 10 0 480.435 5 6 5 10 0 20 20 20 20 20 20 20	4 3 HIND SPEED (KNOTS) LCC - VEEV 3 10 21 35 354 -1.54 OR -2. 0 0 5 1 0 -1.54 OR -2. 0 0 9 3 0 -1.54 OR -2. 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 0 0 0 -1.54 OR -2. 0 0 0 0 0 0 0 0 0	INSUFFICIENT DATA	45 HIND SPEED (KNDTS) LCC - v687 0

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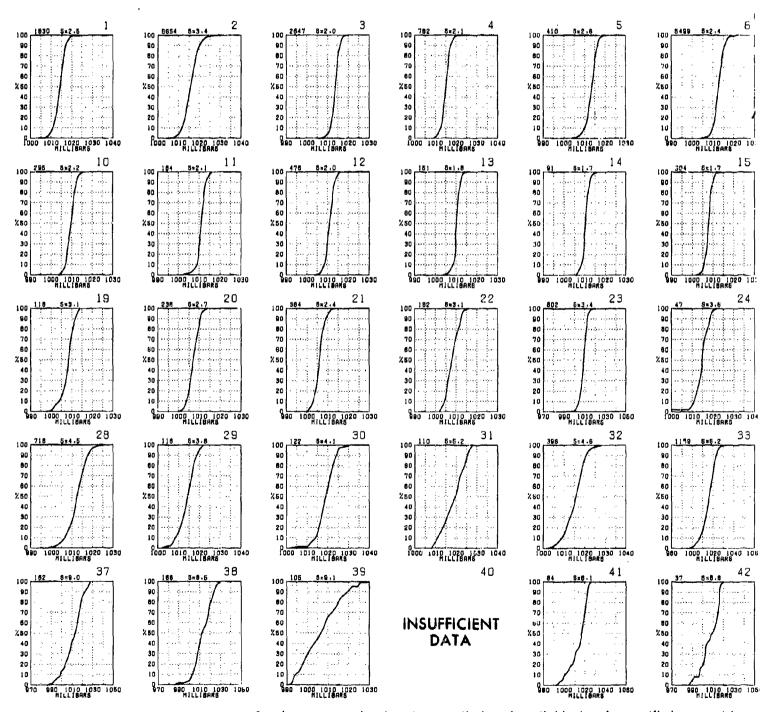
SEA LEVEL PR



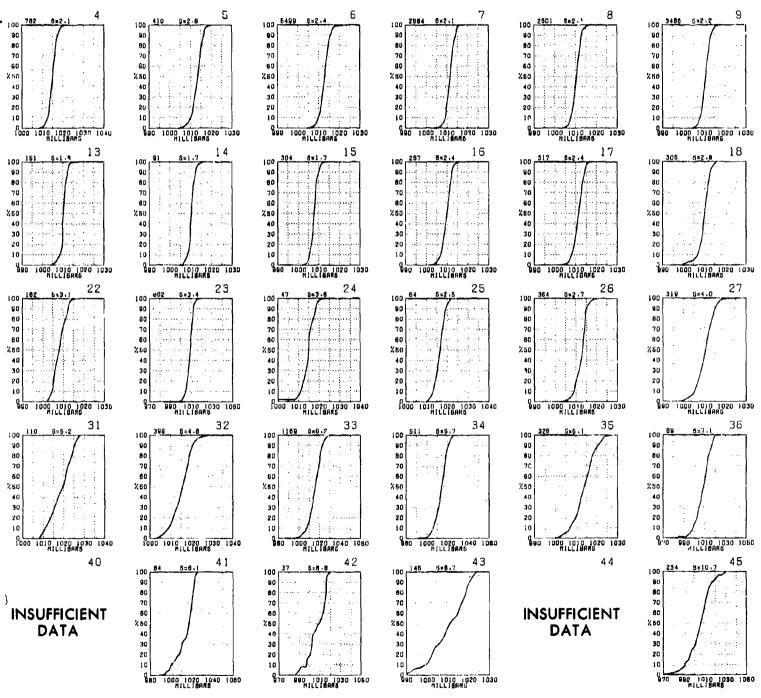
SEA LEVEL PRESSURE AND MEAN WIND



SEA LEVEL PRESSURE

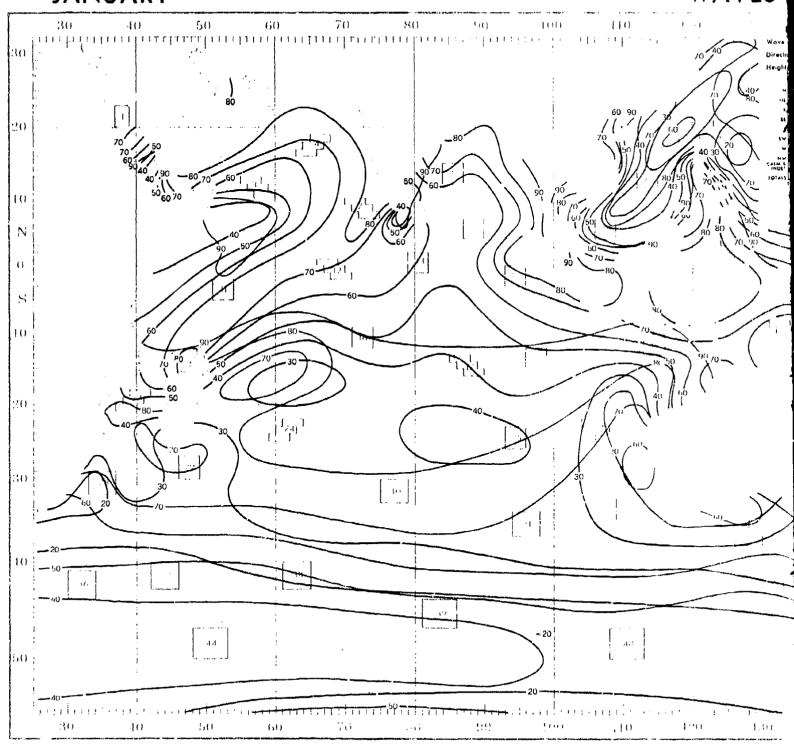


<u>Graphs</u> represent the objective compilation of available data for specified areas without The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjust

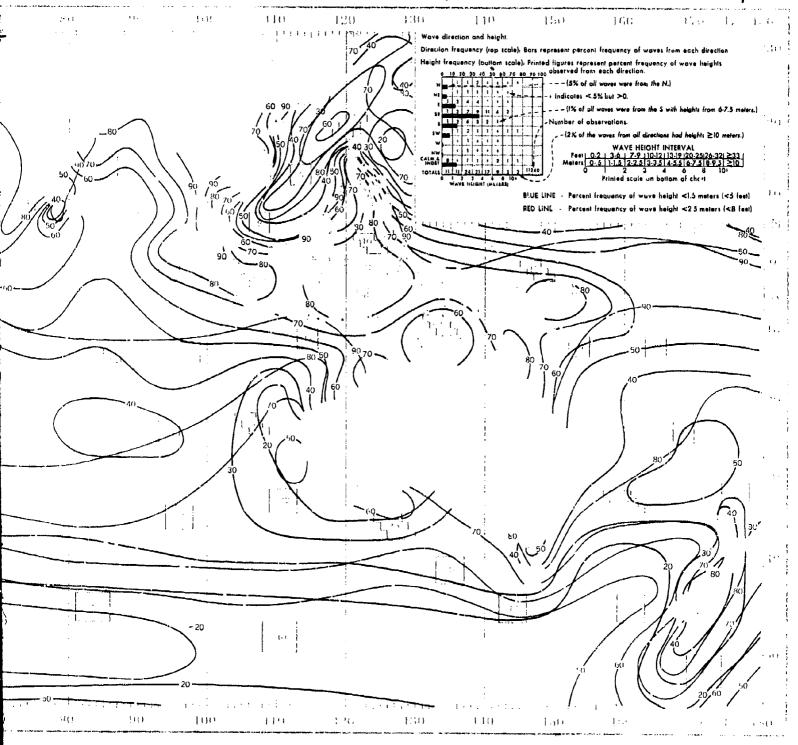


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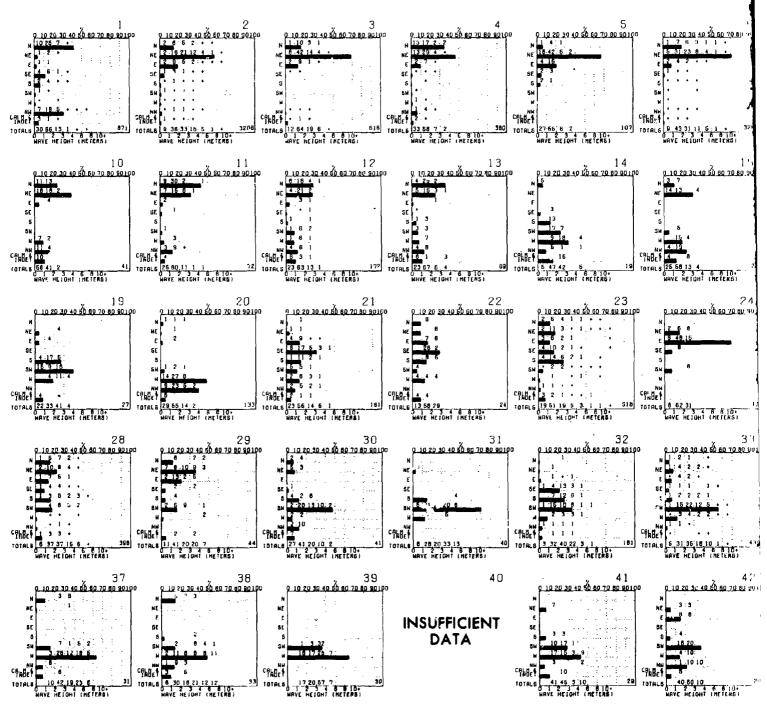
posite page) are based on all available data subjectively adjusted where bias was evident.



WAVES (<1.5 AND <2.5 METERS)



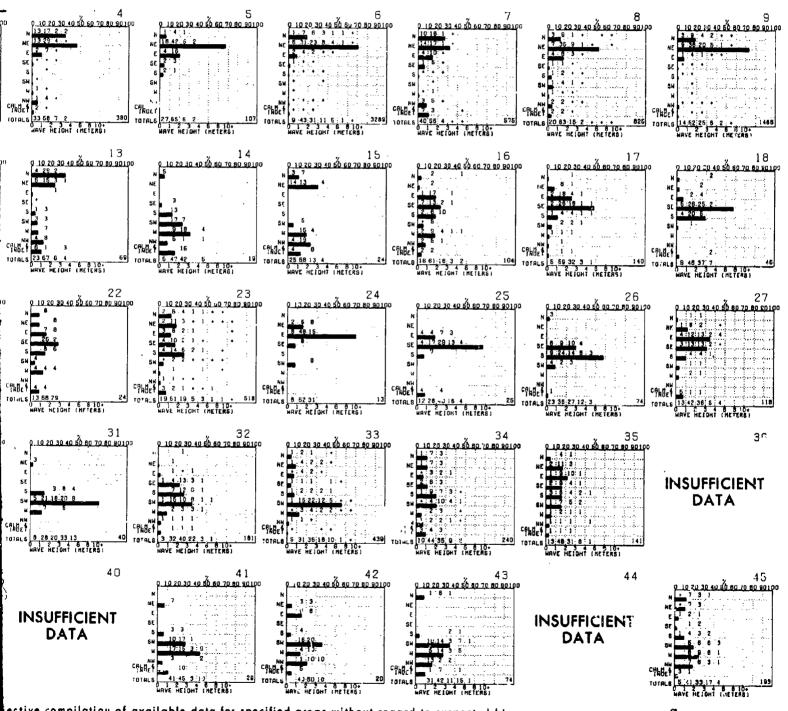
WAVE DIRECTION AND HEIGHT



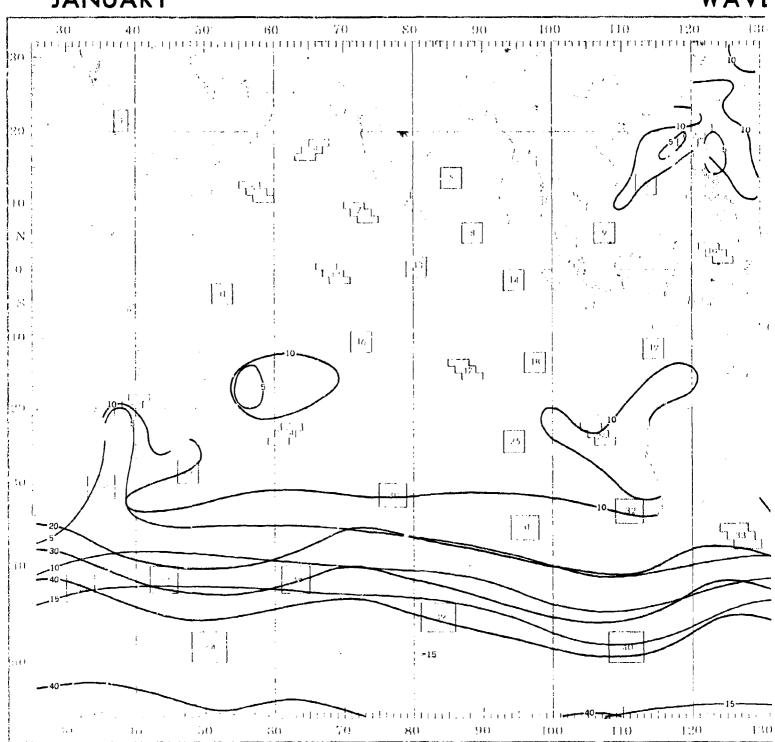
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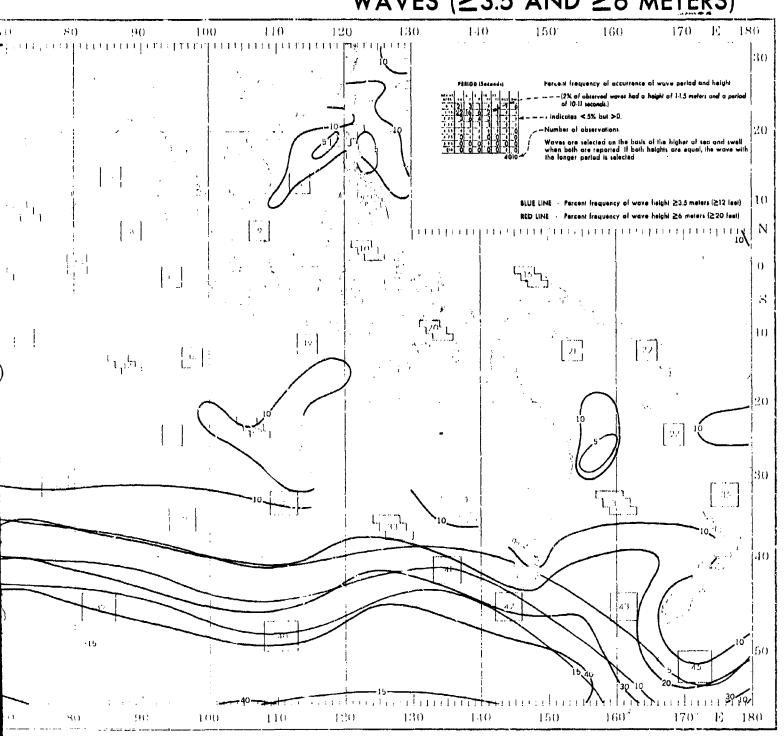
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iective compilation of available data for specified areas without regard to suspected biases. oposite page) are based on all available data subjectively adjusted where bias was evident.



WAVES (≥3.5 AND ≥6 METERS)



WAVE PERIOD AND HEIGHT

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PERIOD (SCONDS) NE (OH)	PERTUD (SECONDS) 18 18 18 18 18 18 18 1	3 NE (0+1) 1 2 2 2 3 3 1 3 2 3 4 4 4 7 7 6 1 1 1 2 3 3 4 3	4 **Clost!	S	PERIOD (SECOND): 10 10 11 12 13 14 15 15 15 15 15 15 15
Company Comp	1	12 2 2 2 2 2 2 2 2 2	3	14 PERIOD (SECONDS) 14 PERIOD (SECONDS) 16 16 17 17 17 17 17	PERIOD (SECOND)
9 PERIOD (SECONDS) 1 1 1 1 1 1 1 1 1	PERIOD (SECONDS) **Closty 6 7 8 10 17 12 180 6 28 0 0 0 0 0 0 1 1 3 1 4 4 3 0 0 2 1 4 4 6 1 0 0 0 2 1 8 0 0 0 0 0 0 2 1 8 0 1 0 0 0 0 4 8 0 0 0 0 0 0 4 9 8 0 0 0 0 0 0 4 9 9 9 0 0 0 0 4 1 1 0 0 0 0 0 4 1 0 0 0 0 0 0 4 1 0 0 0 0 0 0 4 1 0 0 0 0 0 0 4 1 0 0 0 0 0 0 4 1 1 1 1 1 4 1 1 1 1 5 1 1 1 6 7 8 7 8 6 7 8 1 1 6 7 8 7 6 8 7 8 6 7 8 1 1 6 7 8 1 6 7 8 1 6 7 8 1 6 7 8 1 7 8 1 7 8 1 8 7 8 8 7 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8	PERIOD (SECONDS) PERIOD (SEC	22 FERIOD (SECONDS) 10 15 15 160 17 181 181 180 18 18 18 18	23 PERIOD (SECONDS) HE(1041) 46 7 8 11 12 13 140 G-8 18 1 4 0 0 0 0 5 1-1.8 19 18 6 1 1 1 5 1-1.8 19 18 6 1 1 1 0 0	INSUFFICIEN DATA
#ERIOD (SECONDS) #ERIOD (SECONDS) #1488 40 7 0 11 12 12 11 11 11 11 11 11 11 11 11 11	29 F(R) DD (SECONDE)	3 () **Clouff 4	31 PERIOD (SECONDS) INTERIOR (SE	32 PERIOD (SECONDS MC (MT) MC	PERIOD (SECOND)
######################################	38 PERIOD SECONDS	39 PERJOU (BECONDS) **C18817 6 10 12 13 13 13 0 - 4 0 0 0 0 0 0 0 1-1-4 0 17 0 0 0 0 0 2-1-4 0 0 13 10 17 7 10 2-1-4 0 0 0 0 0 0 0 1-1-4 0 0 0 0 0 0 0 1-1-4 0 0 0 0 0 0 0 1-1-4 0 0 0 0 0 0 0 1-1-4 0 0 0 0 0 0 0 1-1-4 0 0 0 0 0 0 0 1-1-4 0 0 0 0 0 0 0 1-1-4 0 0 0 0 0 0 0 1-1-4 0 0 0 0 0 0 0 1-1-4 0 0 0 0 0 0 0 1-1-4 0 0 0 0 0 0 0 1-1-4 0 0 0 0 0 0 0 1-1-4 0 0 0 0 0 0 0 1-1-4 0 0 0 0 0 0 0 1-1-4 0 0 0 0 0 0 0 1-1-4 0 0 0 0 0 0 0 0 0 1-1-4 0 0 0 0 0 0 0 0 0	INSUFFICIENT DATA	## PERIOD (SECONDS) ## 10015	PERIOD (SECONDS METONT (ATRIA) 16 - 1

<u>Graphs</u> represent the objective compilation of available data for specified areas withou The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adju

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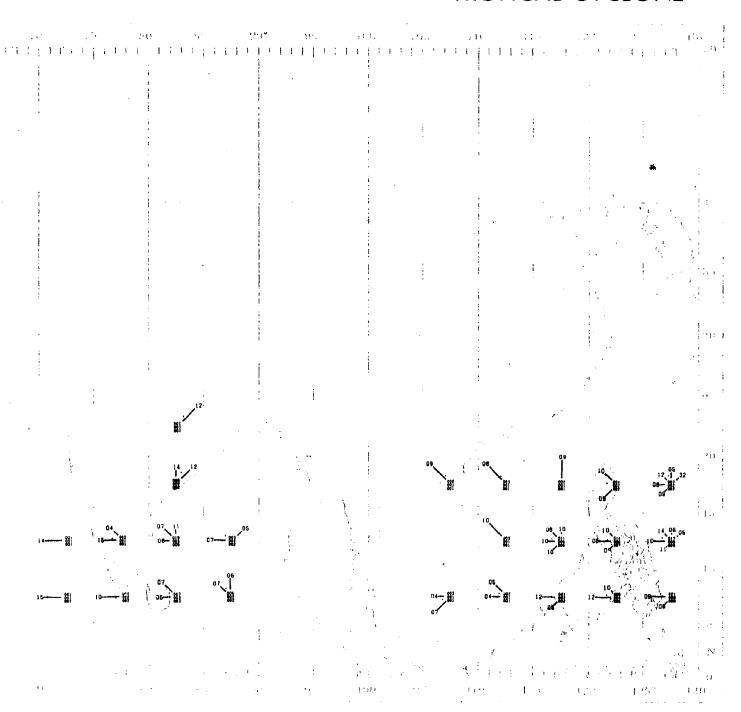
	######################################	PERIOD (SECONDS) ***C10-11	PERIOD (SECONDS) ***********************************	#ER FOO	PERIOD (SECONDS) **HETO** 10 - 10 - 11 - 12 13 140 0 - 0 19 1 + 1 0 0 3 1-1.18 26 21 5 2 1 + 3 1-2.6 0 + 1 + 0 + + 1 1-2.6 0 + 1 + 0 + + + 1 1-2.6 0 + 1 + 0 + + + + + 1-2.6 0 0 0 0 0 0 0 0 0	PERIOD ISECONDS: 10 1 1 1 1 1 1 1 1 1
			7-4-10		2-3-3	8-1-8 4 21 4 2 2 0 2 9-3-6 0 2 0 2 0 0 0 2 1-3-6 0 0 0 0 0 0 0 0 1-7-1 0 0 0 0 0 0 0 0 0
	PERIOD (SECONDA) **[8**] ** 8 * 7 * 8 * 11 * 12 * 13 * 180 *** 8 * 8 * 9 * 9 * 11 * 12 * 13 * 180 *** 9 * 8 * 8 * 9 * 9 * 11 * 12 * 13 * 180 *** 10 * 8 * 8 * 9 * 9 * 9 * 9 * 9 * 9 * 9 * 9	TERIOD SECONDS	INSUFFICIENT DATA	PERIOD (SECONDS) PERIOD (SECONDS) PERIOD (SECO	26 FERIOD (SECONDS) ***********************************	## 100 (SECONDS) ## 100 (SECO
	#11041	HE (001) SECONDS HE (001	NETO- PERIOD (SECONDS NETO- NETO-	34 PEN OD (SECONDS PEN OD (SECONDS PEN OD (SECONDS PEN OD OD OD OD OD OD OD O	ST ST ST ST ST ST ST ST	INSUFFICIENT DATA
)	INSUFFICIENT DATA	4 PERIOD (SECONDS) ***C10MT	# 2 PER 100 ISECONDS	PERIOD (SECONDS) ***PERIOD (SECONDS) **PERIOD (SECONDS) ***PERIOD (SE	INSUFFICIENT DATA	### ### ### ### ### ### ### ### ### ##

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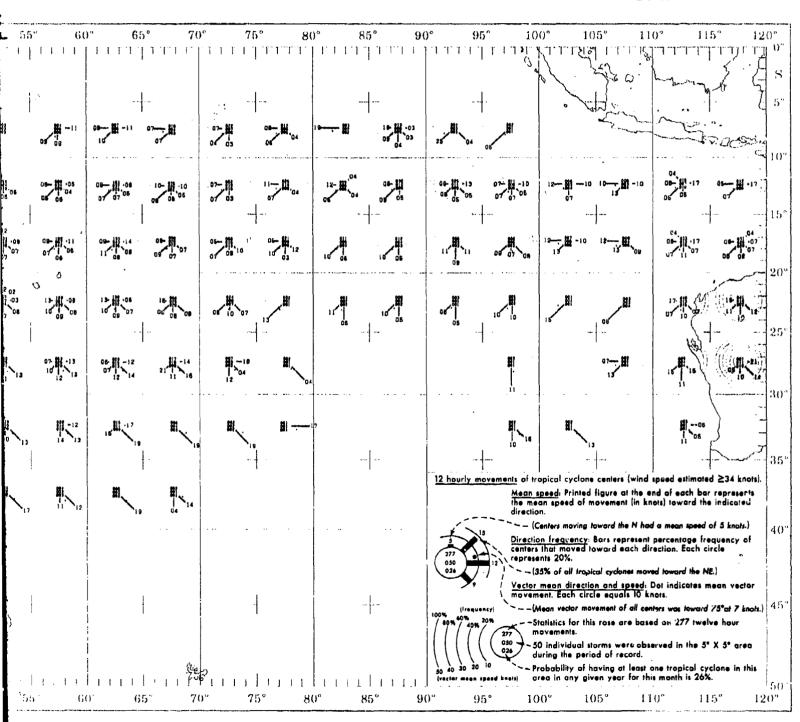
TROPICAL CYCLONE

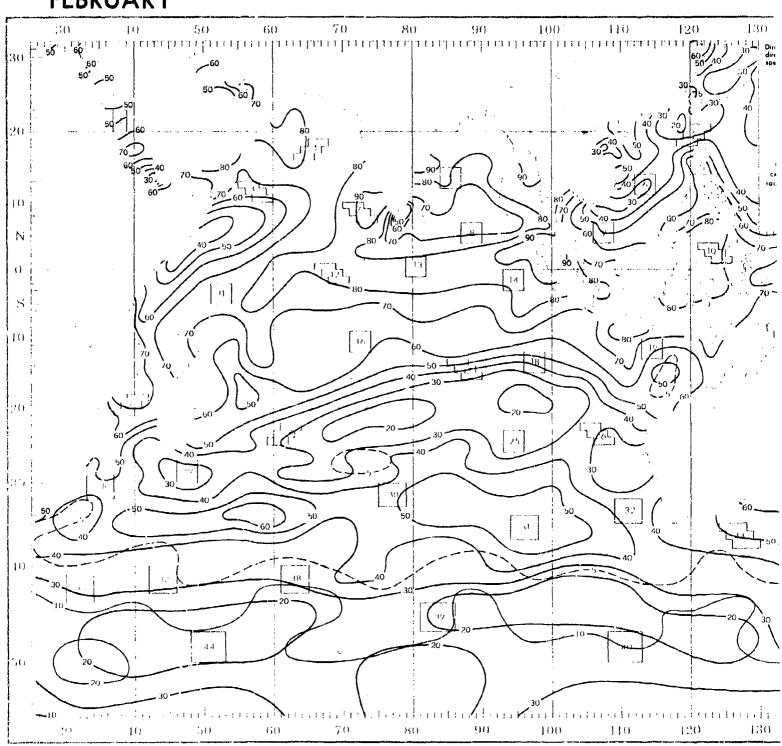


TROPICAL CYCLONE

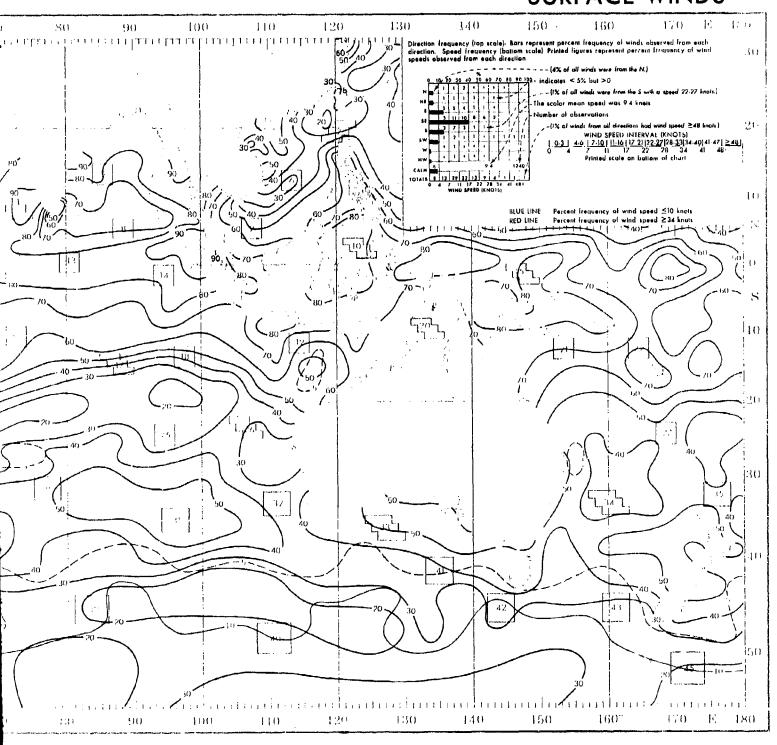
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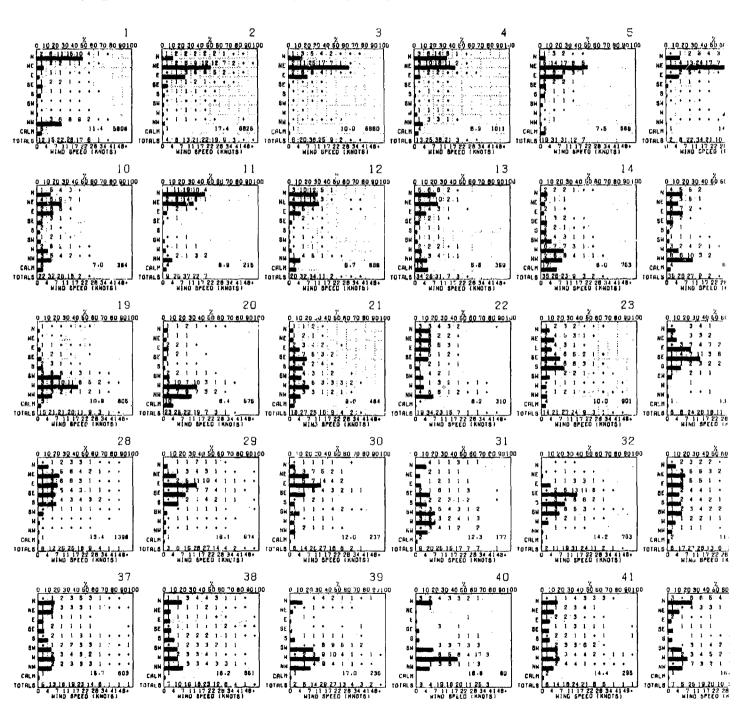




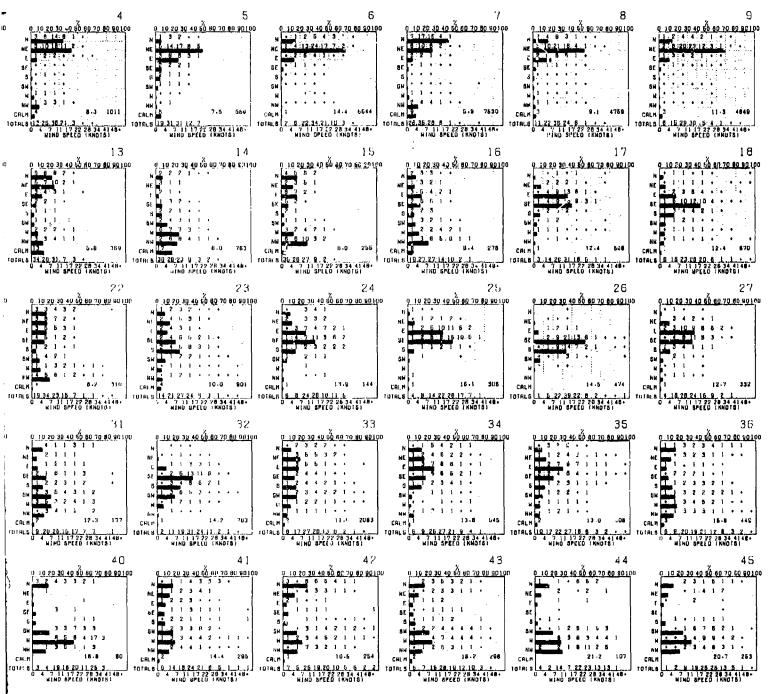
SURFACE WINDS



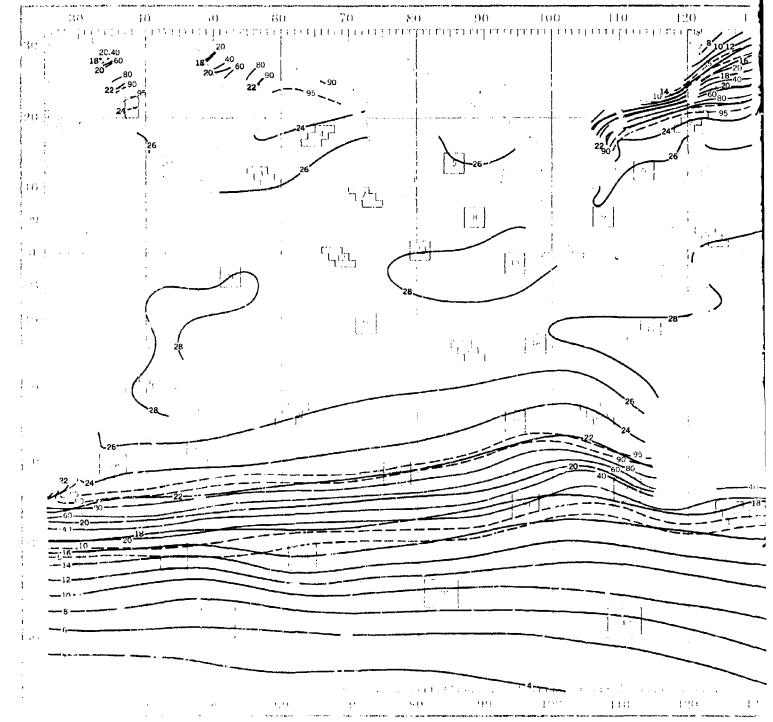
WIND DIRECTION AND SPEED



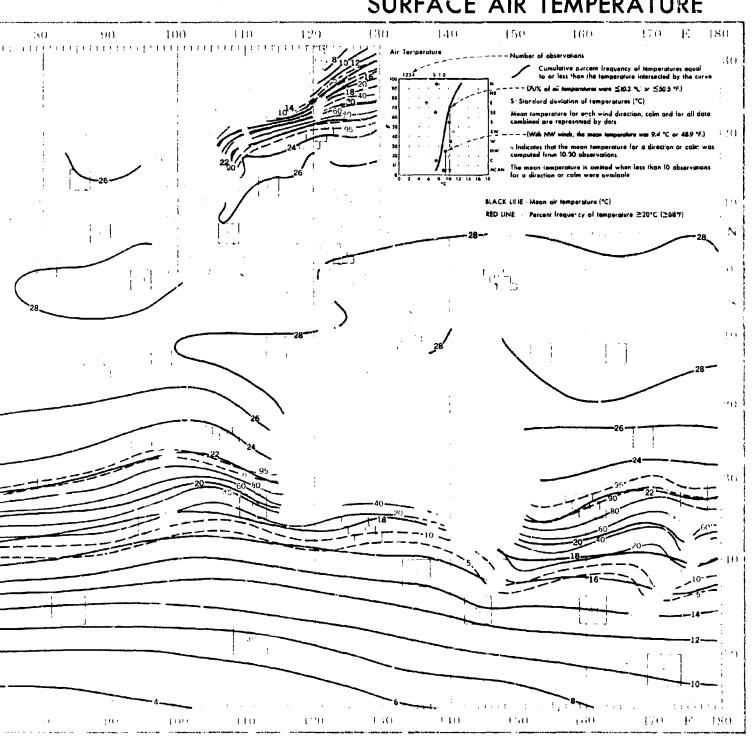
Graphs represent the objective compilation of available data for specified areas wit The isopleth analyses (opposite page) are based on all available data subjectively of



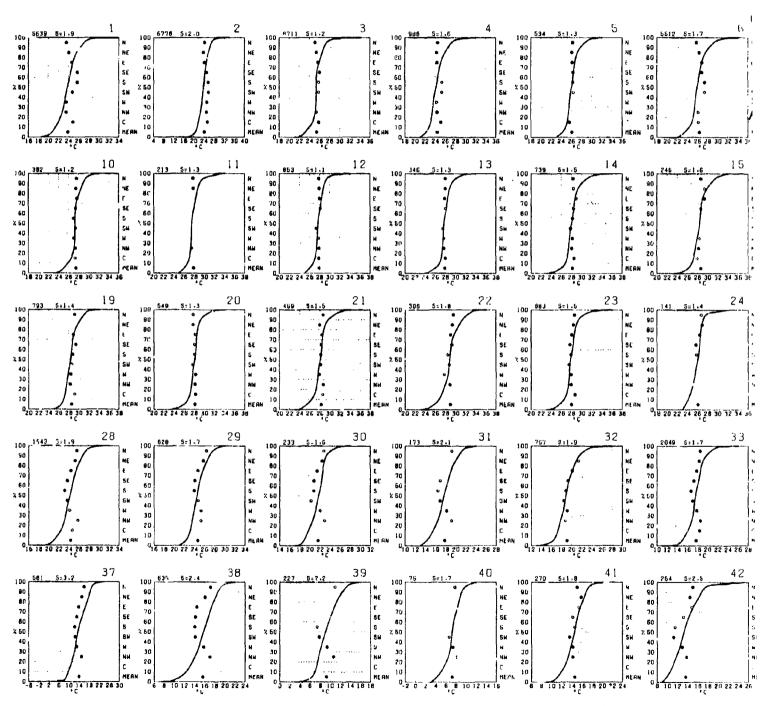
ective compilation of available data for specified areas without regard to suspected biases. posite page) are based on all available data subjectively adjusted where bias was evident.



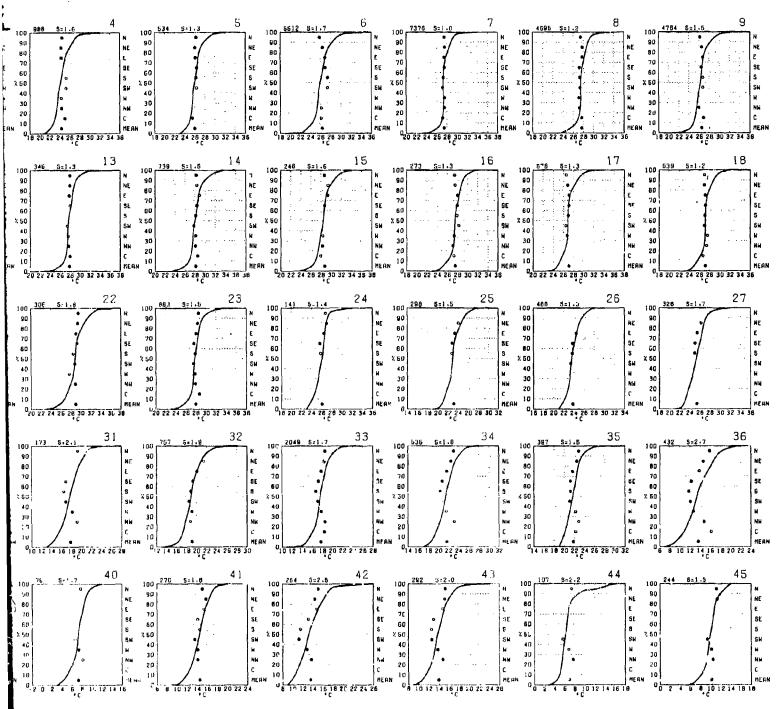
SURFACE AIR TEMPERATURE



SURFACE AIR TEMPERATURE

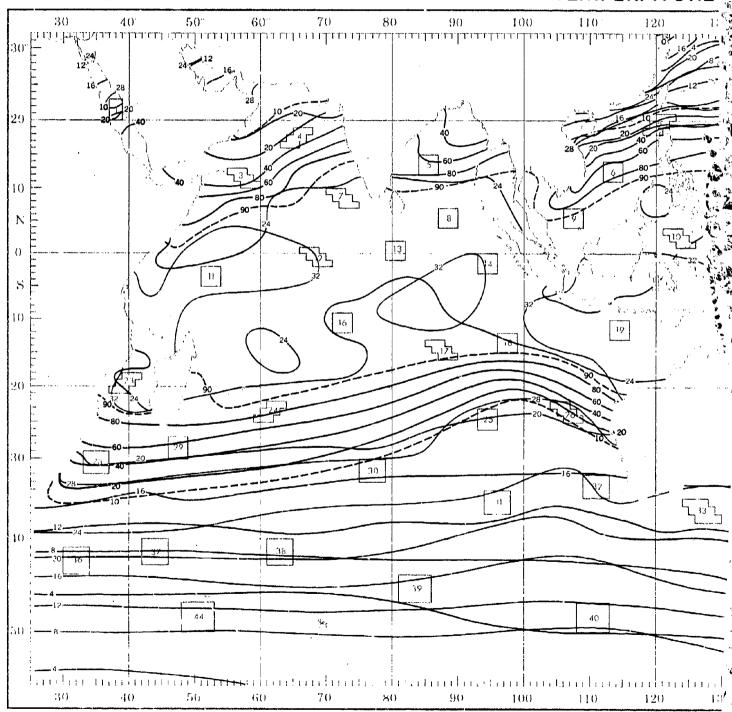


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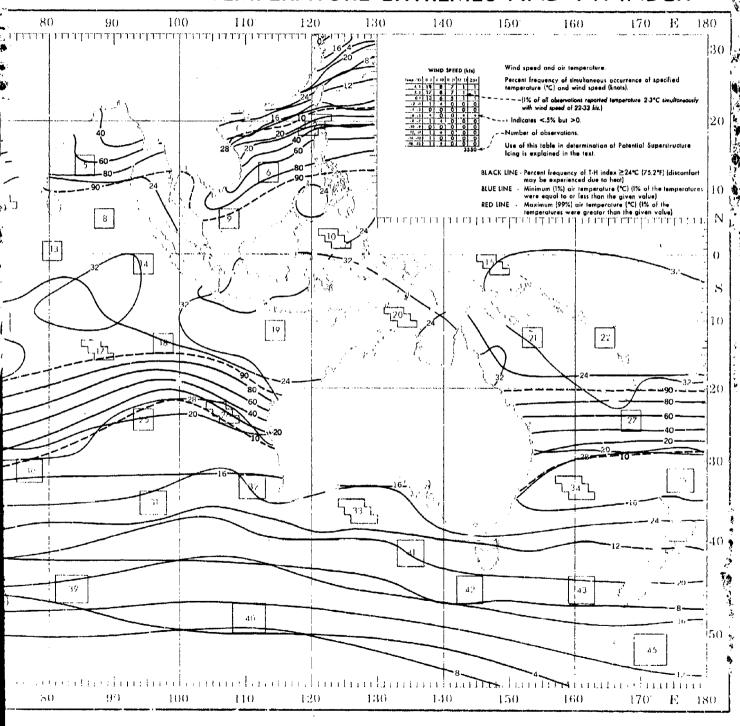


jective compi. Non of available data for specified creas without regard to suspected biases, pposite page) are based on all available data subjectively odjusted where bias was evident.

TEMPERATURE



TEMPERATURE EXTREMES AND T-H INDEX



WIND SPEED AND AIR TEMPERATURE

	_			_	1
HIND SPEED (KTS) 1		HIND SPEED (KTS) 3	HIND SPEED (KT8)		MINC SPEED (KTS)
7EMP (*C) 0-3 4-10 11-81 22-33 > 34 32-33 + + + D D	7EMP (*C1 0-3 4-10 11-2122-33 2 34 32:33 0 + + 0 D	TEMP (*C) 0-3 4-10 11-2122-99 2 94	TEMP (*C) 0-3 4-10 11-21 22-39 8 34	18mp (*C) 0-3 4-10 11-21 22-33 +34 30-31 + + + 0 0	TEMP (*C) - 4-10 11-21 22-33
30.31 + + + 0	30.31 + + + + + + + 20.50 + 20.50 + 2 2 + 0	30.31 + + + 0 0 29.29 1 3 1 + 0	50.31 + + + 0 0 28.28 1 2 1 0 0	20.20 2 11 1 0 0 26.27 9 36 10 0 0	30.31 + 1 2 • 1
26.27 4 8 5 • 0	28.27 2 7 8 2 +	28.27 2 24 12 1 0	26.27 3 12 5 • 0	24.25 8 16 5 0 0	28.27 1 15 28 6
24-25 6 16 16 2 + 22-23 2 9 17 4 +	24.25 2 9 18 10 1 22.23 + 3 11 12 1	24,25 3 30 20 i 0 22,23 + 1 1 + +	22.23 4 17 7 0 0	22.23 0 1 + 0 0 20.21 0 0 0 0 0	24.26 1 6 14 4 22.23 + 1 1
20.21 + 2 4 1 +	20.21 + + 3 4 1 18.19 0 + + + +	20,21 0 + + + + 16,19 0 0 0 0 0	20.21 0 + 1 0 0 10.19 0 0 0 0 0	18.19 0 0 0 0 0 0 18.17 0 0 0 0 0	20.21 0 0 + +
18-17 0 0 0 0 0 D	16.17 0 + + + 0 14.15 0 0 0 0 0 0	16.17 0 0 0 0 0 14.15 0 0 0 0 0	18.17 G O O O O O O O	14.18 0 0 0 0 0 0 12.13 0 0 0 0 0	18.17 0 0 0 0 0 14.15 0 0 0 0
12.13 0 0 0 0 0 0 5648	12.13 0 0 0 0 0	12.13 0 0 0 0 0 0 8716	12.13 0 0 0 0 0 992	10:11 0 0 0 0 0 0 536	12.13 0 0 0 0 5
HIND SPEED (KTS) 10	HIND SPEED (KTS) 11	MIND SPEED (KTS) 12	WIND SPEED (KTS) 13	HIND SPEED (KTS) 14	HIND SPEED (HTS) 1
TORP (*C) 0-3 4-10 11-2122-33 3 34	TEMP (%) 0-3 4-10 11-21 22-99 3 34	TEHP (40) 0-9 4-10 11-21 22-99 # 34	TEMP (*C) 0-3 4-10 11-2122-33 3 34	TEMP (*C) 0-8 4-10 11-21 22-33 + 34	
32.33 + 0 + 0 0 30.31 1 3 2 0 0	32.93 + 3 + 0 0	32.33 + + 0 0 0 30.31 2 4 + 0 0	32.33 0 · 0 0 0 30.31 6 3 1 0 0	34.35 + + 0 0 0 0	34.36 0 + 0 0
28.29 10 21 B 0 0 28.27 11 32 9 0 0	28.20 5 31 15 0 0 28.27 3 24 12 0 0	28.28 11 40 8 0 + 28.27 7 21 4 + 0	28,29 19 33 5 + 0 28,27 9 19 3 0 0	30.31 7 5 1 0 0	30.31 9 10 1 0 20.28 16 30 6 +
84.28 1 3 0 0 0 88.23 0 0 0 0 + 0	24.25 0 0 + 0 0 22.23 0 0 0 0 0	24.26 + 2 + 0 0 22.23 D 0 0 0 0	24.25 1 1 1 0 0 22.23 0 0 0 0 0	26.27 5 13 5 1 0 24.25 1 2 1 + 0	26.27 6 10 4 0
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15.15 0 0 D 0 0 15.17 0 0 D 0 0	18.19 0 0 0 0 0 18.17 0 0 0 0 0	18-19 0 0 0 0 0 18-17 0 0 0 0 0	10.17 0 0 0 0 0	20,21 0 0 0 0 0 10,18 0 0 0 0 0	20.21 0 0 0 0 10.10 0 0 0 0
14.15 U 0 0 0 0 18.13 G 0 D 0 0	14.18 0 0 0 0 0 12.13 0 0 0 0 0	14.15 0 0 0 0 0 12.13 0 0 0 0 0	14.18 0 0 0 0 0 0 12.13 0 0 0 0 0	16.17 0 0 0 0 0 14.15 0 0 0 0 0	16.17 0 C C C C C 14.18 0 0 0 0 0
384 1 O	213	859	346	73 9	2
MIND SPEED (KTS) 19	HIND SPEED (KIS) 20	HEND SPEED (KTS) 21	HIND SPEED (KTS) 22	MIND SPEED (KTS) 23	HIND SPEED (KTS) 2
80.33 2 1 1 0 0	32:33 + 1 + 0 O	34.35 + 0 0 0 0	34.38 0 1 0 0 0	34.38 + + 0 0 G	30.91 1 0 0 6
30,31 S B S 1 + 10.20 6 24 18 6 +	30,31 3 7 2 + 0 28,28 17 26 16 3 0	32.53 1 1 + 0 0 30.31 3 7 3 0 0	32.33 2 7 + 0 0 30.31 6 13 5 0 0	32.33 1 1 + 0 0 30.33 3 5 2 0 0	28.29 1 5 10 2 28.27 3 19 21 8
28.27 2 7 7 4 + 24.28 0 + 1 + +	26.27 3 11 6 1 + 24.28 + 2 + + 0	28.29 12 32 13 4 + 26.27 3 10 5 1 0	29.29 10 26 11 1 + 26.27 1 9 4 1 0	28.28 8 25 17 2 + 25.27 4 16 12 2 +	24.26 1 7 15 7 22.25 0 1 0 0
20.21 0 0 0 0 0	20.21 0 0 0 0 0	24.25 + 1 1 + 0 22.23 0 0 0 0 0	24.25 0 1 2 0 0 22.23 0 0 0 0 0	24.25 + 1 1 + 0 22.23 D O O + O	20.21 0 0 0 0 10.10 0 0 0 0
18-19 0 0 0 0 0 0 16-17 0 0 0 0 0	10.10 0 0 0 0 0 10.17 0 0 0 0 0	20.21 0 0 0 0 0 19.19 0 0 0 0 0	20.21 0 0 0 0 0 10.10 0 0 0 0 0	20.21 0 0 0 0 0 16.19 0 0 0 0 0	10,17 D O O O O
14-16 0 0 0 0 0 0 12-13 0 0 0 0 0	14-15 0 0 0 0 0 12-15 0 0 0 0 0	18·17 0 0 0 0 0 14·15 0 0 0 0 0	18.17 0 0 0 0 0 14.18 0 0 0 0 0	10:17 0 0 0 0 0 0 14:16 0 0 0 0 0 0	12,13 0 0 0 0
794	550	472	306	909	
HIND SPEED (KTS) 28	HIND SPEED (KTS) 29	HIND SPEED INTS 30	HIND SPEED (KTS) 31	HIND SPEED (KTS) 32	HIND SPEED (KTS) 3
7EMP (*C1 0-3 4-30 11-81 22-33 = 34	7ERP (*C) 0-9 4-10 51-E122-33 2-34	1EMP (*C1 0-3 4-10 11-21 22-39 2 34 24 25 2 5 3 + 0	754P (*G) 0-3 4-10 11-21 22-33 2 34 25-25 2 1 2 0 0	TEMP (*C) 0-3 4-10 11-21 22-38 2 34 26-27 0 0 + 0 0	7EMP (*C) 0-3 4-10 31-81 28-39 2
20:20 • 2 1 • 0 26:27 1 10 10 3 •	20.20 + 2 4 0 0 20.27 1 6 13 3 +	27.29 5 16 21 3 + 20.21 1 15 14 2 +	20.t) 2 B 4 3 0 18.19 3 16 13 1 0	24.28 + 1 1 0 0 22.23 + 2 4 1 0	22.23 + 1 1 + 70.21 6 4 1
24.28 2 15 16 5 +	24.28 1 9 28 8 2	16.18 0 3 5 1 +	18.17 3 15 8 6 1	10.21 + 9 18 3 +	10,10 3 19 16 3
FO.21 • 2 2 1 •	20.21 0 . 1 . 0	14-18 0 0 0 0 0	18.19 0 1 1 0 0	16.17 1 4 8 2 +	14.16 + 3 3 1
10-19 0 0 + 0 0 10-17 0 0 0 0 0	10.10 0 0 0 0 0 10.17 0 0 0 0 0	19.13 0 0 0 0 0 10.11 0 0 0 0 0	10.11 0 0 0 0 0 0 •.• 0 0 0 0 0 0	14.15 + + 0 0 12.13 0 4 + 0 D	12.13 0 + + + + 10.11 0 0 0 0
14-18 0 0 0 0 0 18-19 0 0 0 0 0	14-16 0 0 0 0 0 0 12-13 0 0 0 0 0 0 10-11 0 0 0 0 0	6.7 Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q	4.8 0 0 0 0 0	10.11 0 0 0 0 0 0 9.9 0 0 0 0 0 0 8.7 0 0 0 0 0	6.8 0 0 0 0 6.7 0 C 0 0 6.8 0 0 0 0
10.(1 g 0 0 0 0 0 155)	10-11 0 0 0 0 0 0 829	4.6 0 0 0 0 0 0 233	2.3 0 0 0 0 0	6.7 0 0 0 0 0 758	4.6 0 0 0 0
HIND SPEED (HTS) 37	HIND SPEED (KTS) 38	WIND SPEED INTS 39	HIND SPEED (KTS) 40	WIND SPEED (KIS) 41	NINO SPEED (KTS) 42
TEMP (*C) 0-3 4-10 11-81 82-32 3 94	TEMP (*C) 0-8 4-10 11-21 22-33 x 34	TEHP (PC) 0-3 4-10 11-\$1 22-33 8 34	TEHP (*C1 0-8 4-10 11-21 22-59 a 54	TEMP (*C) 0-3 4-10 11-21 22-33 2 34	TEMP (*C) 0-8 4-16 11-21 82-33 2 3
22.23 0 1 + 0 0 20.21 0 1 2 1 +	20.21 4 1 2 1 + 10.10 1 6 8 5 1	14.16 0 + 4 · 0 12.13 0 3 6 3 0	10.11 0 0 4 3 0 0.0 1 11 9 19 0	70.21 0 0 - 0 0 18.18 + 2 3 1 0	#4.28 0 + 0 0 #2,85 + 0 0
18.17 1 3 6 4 1	16.17 3 9 11 6 2 14.15 2 8 11 5 2	10-11 1 6 15 4 1 0-9 + 5 22 4 0	4.8 0 3 5 8 0	16.17 1 9 15 1 0 14.18 1 11 17 8 2	10,10 . 2 1 0
14.18 2 7 6 4 + 18.19 1 8 11 3 1	12,13 1 2 5 2 1 10,11 + + 2 2 +	6.7 + 5 10 7 3 4.5 0 0 0 1 +	2.3 0 0 0 0 0 0.1 0 0 0 0 0	12.13 2 10 B 2 0 10.11 1 1 9 1 0	16,17 2 5 B 2 14,18 1 7 B 4
10.11 1 4 7 3 +	0.0 0 0 1 0 6.7 0 0 0 0 0	f.3 0 0 0 0 0 0.1 0 0 0 0 0	-21 0 0 0 0 0 -43 0 0 0 0 0	0.9 0 0 0 0 0 0.7 0 0 0 0 0	12.13 2 11 13 6 10.11 1 4 5 3
6.7 0 0 0 1 0 4.6 0 0 0 + 0	4.5 0 0 0 0 0 0	-2,-1 0 0 0 0 0 -1,-3 0 0 0 0 0	-85 G O O O O O	2.5 0 0 0 0 0 0	0.0 0 0 2 · 0.7 0 0 0 0
2.3 0 0 0 0	0 0 0 0	-8,-6 0 0 0 0	-106 0 0 0 0	0.1 0 0 0 0 0	4.0 0 0 0 0

<u>Graphs</u> represent the objective compilation of available data for specified areas without in The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjust

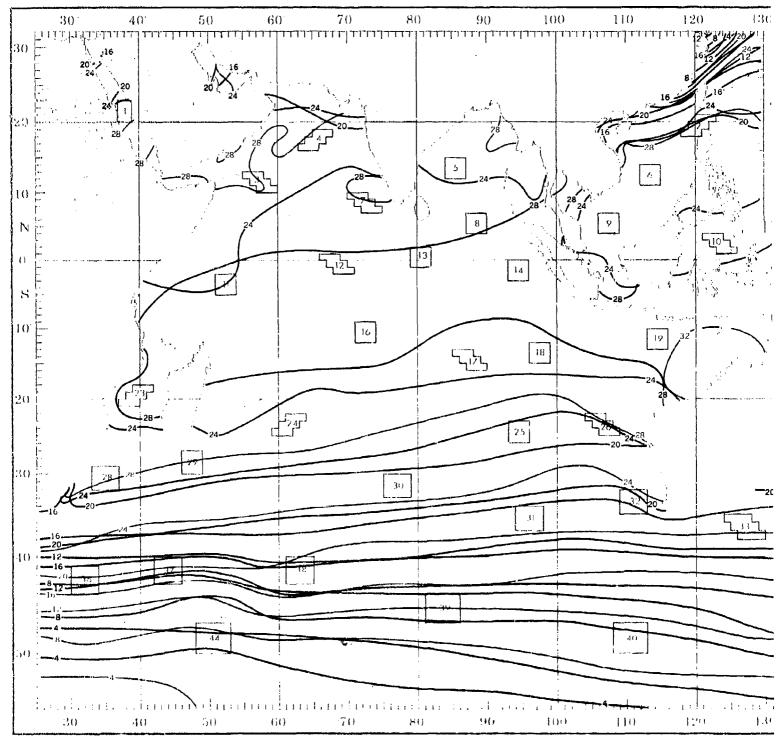
PERATURE

FEBRUARY

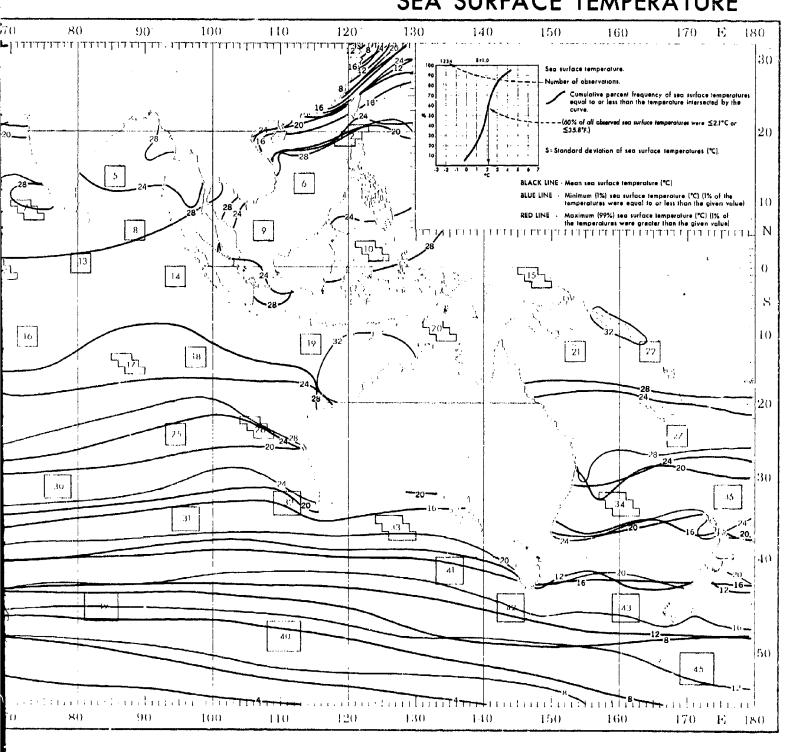
	Δ	5	6	7	8	9
.	HIND SPEED (KTS)	HIND SPEED (KTS) 5				HIND SPEED (KTS)
7	32.33 0 + 0 0 0	30.51 + + + 0 0	97.33 0 + + 0 0	32.33 + + + 0 0	38.33 + + + 0 0	34.95 + + + 0 0
3	28./9 1 2 1 0 0	20.29 2 11 1 0 0 26.27 9 36 10 0 0	30.31 + 1 2 + 0 26.29 + 6 9 2 0	30.31 1 2 + + D 28.28 10 29 5 + +	30.31 1 3 2 + 0 28.29 5 28 17 + 0	32.33 + + + 0 D 30.31 + 1 2 + D
Ħ	25.7 3 12 5 • 0 24.25 5 31 11 • 0	24.25 B 16 6 0 0 22.23 0 1 + 0 0	28.27 1 15 28 6 + 24.25 1 6 14 4 +	26.27 16 31 4 0 0 24.25 • 1 • 0 0	26.27 5 24 11 + +	26.29 2 8 8 1 +
	22.23 4 17 7 0 0 20.21 0 + 1 0 0	20.21 0 0 0 0 0	20.21 0 0 + + 0	22.23 0 + 0 0 0 20.21 0 0 0 0 0	22.23 + + + + 0	22.23 + + + + 0
	18.19 0 0 0 0 0	16.17 0 0 0 0	10.10 0 0 0 0	10.19 0 0 0 0 D	18.19 0 0 0 0	20.21 0 0
	18.17 0 0 0 0 0 14.18 0 0 0 0 0	14.15 0 0 0 0 0 12.13 0 0 0 0 0	18-17 0 0 0 0 0 14-16 0 0 0 0 0	14.15 0 0 0 0	14-15 0 0 0 0 0	18.17 0 0 0 0
Ŋ	12.13 0 0 G U O	10.11 0 0 0 0 0 0 536	12.13 0 0 0 0 0 5612	12.18 0 0 0 0 0 0 7394	12.13 0 0 0 0 0 0 4697	14-15 0 0 0 0 0 0 4766
	WIND SPEED (KTS) 13	WIND SPEED (HTS) 14	HIND SPEED (KTS) 15	WIND SPEED (KTS) 16	WIND SPEED (KTS) 17	HIND SPEED (KTS) 18
Ì	TEMP (4C1 0-3 4-10 11-21 22-33 + 34	TENP (*C) 0-3 4-10 11-21 82-33 2 34	TERP (-C1 0-3 4-1 11-21 28-33 234)	TEMP (*C) 0-3 4-10 11-21 28-39 a 34	TENP (%) 0-3 4-10 11-2122-33 4 34	TERP (*C) 0-9 4-30 11-2122-39 2 24
H	32,33 0 + 0 0 0 30,31 6 3 1 0 0	34,35 + + 0 0 0 32,33 1 1 + 0 0	34,36 01 + 0 0 0 32,33 3 2 + 0 0	32.33 0 + 0 0 0 30.31 2 5 1 0 0	32.33 0 1 + 0 0 30.31 + 3 1 + 0	30.31 + 3 2 0 0 20.20 2 11 14 2 +
ļ	28.£9 19 33 5 + 0 26.27 9 19 3 0 0	30.31 7 6 1 0 0 20.20 22 27 6 1 0	30.31 9 10 1 0 0 29.26 16 30 6 + G	28.29 10 29 9 1 0 26.27 9 18 11 1 0	28.29 + 12 16 1 0 28.27 2 23 30 3 +	28.27 3 23 29 4 1
Ĭ	24.25 1 1 0 0	28.27 5 13 5 1 D 24.25 1 2 1 + D	28.27 6 10 4 0 0 24.28 + 2 + 0 0	24.28 • 1 2 0 0 22.23 + 0 0 0 0	28.63 U + + O O	20.21 0 0 0 0 0
ţ.	20.21 0 0 0 0 0	28.83 0 0 0 0	88.83 0 0 0 0 0	20.21 0 0 0 0 0	¥0.21 0 0 0 0 0	0 0 0 0 0
H	18.19 0 0 0 0 0 0 18.17 0 0 0 0 0	20.21 0 0 0 0 0 18.19 0 0 0 0 0	20.21 0 0 0 0 0 10.19 0 0 0 0 0	18.17 0 0 0 0 0 18.17 0 0 0 0 0	18:17 0 0 0 0 0	14.15 0 0 0 0
	14.15 0 0 0 0 0 12.15 0 0 0 0 0	16.17 0 0 0 0 0 14.15 0 0 0 0 0	18.17 0 0 0 0 0 0 14.18 0 0 0 0 0	14,15 0 0 0 0 0 12,15 0 0 0 0 0	14-18 0 0 0 0 0 12-13 0 0 0 0 0	12.13 0 0 0 0 0
١	346	739 23	249	HIND SPEED (KTS) 25	579	27
Ļ	KIND SPEED (KTS) 22 18HP (40) 0-3 4-10 11-21 22-33 34	WIND SPEED (KTS) 23	HIND SPEED (KTS) 24	TEMP (*C) 0-3 4-10 11-21 22-33 = 24	MIND SPEED (KTS) 26	HIND SPEED (KTS) 27
l	34.35 0 1 0 0 0	34.35 + + 0 0 0	90.91 1 0 0 0 0	20.20 0 1 0 + 0	20.20 0 + + 0 0	92.93 0 + 0 0 0
l	37,33 2 7 + 0 0 30,31 8 13 5 0 0	27,33 1 1 + 0 0 30,31 3 5 2 0 0	20.20 1 5 10 2 0 20.27 3 19 21 6 0	28,27 1 2 3 + 0 24,28 1 B 17 5 0	20:27 + 5 8 + 0 24:26 + 10 28 4 1	90.81 0 1 1 0 0 20.88 2 5 2 1 0
ł	20.20 10 26 11 1 +	20.20 8 25 17 2 4	24.25 1 7 15 7 0 22.23 0 1 0 C 0	27.23 2 9 25 15 1 20.21 0 1 5 2 +	22.25 + 11 27 B + 20.21 0 + 1 + 0	26.27 2 19 14 2 0 24.28 1 15 17 6 1
l	24.25 0 1 2 0 D 22.23 0 0 0 0 0	22.23 0 0 0 + 0	20.21 0 0 0 0 0 18.19 0 0 0 0 0	10.10 0 0 0 1 0	18.18 0 0 0 0 0 18.17 0 0 0 0 0	28.23 0 5 6 2 0
l	20.21 0 0 0 0 0 18.18 0 0 0 0 0	20.21 0 0 0 0 0 10.10 0 0 0 0 0	18-17 0 0 0 0 0 0 14-16 0 0 0 0 0	14.18 0 0 0 0 0 12.13 0 U 0 0 0	14-18 0 0 0 0 0 0 12-13 0 0 0 0 0	10.10 0 0 0 0 0
ł	18.17 0 0 0 0 0 14.18 0 0 0 0 0	10.17 0 0 0 0 0 14.16 0 0 0 0 0	. 12.13 0 0 0 0 0 0 10.11 0 0 0 0 0	10.11 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	10.11 0 0 0 0 0 0 9.0 0 0 0 0 0	14-15 0 0 0 0 0 12-13 0 0 0 0 0
ĺ	308	909	141	298	456	328
l	HIND SPEED (KTS) 31	HIND SPEED (KTS) 32	HIND SPEED (KTS) 33	HIND SPEED (KTB) 34	HIND SPEED (KTS) 35	HIND SPEED (KTS) 36
ı	TERP (*C) 0-3 4-10 11-21 22-33 2 34	TEMP (*C) 0-3 4-10 11-23 22-33 a 34	TEMP (*C1 0-2 4-10 11-21 22-33 a 34 24-25 0 + 0 0 0	TEMP (*C) 0-8 4-10 11-2122-33 a 34	TEMP (*C1 2-9 4-10 11-21 22-98 8 94 28.27 + 1 + 0 0	TEMP (*C1 0-5 4-10 13-21 22-33 + 34
Į	20.21 2 8 4 3 0	24.25 + 1 1 0 0	27,29 • 1 1 • 0	24.26 + 4 8 2 0	24.25 2 5 5 1 0	20.21 + 1 1 0 0
I	18.18 3 16 13 1 0 18.17 3 15 8 6 1	22.23 + 2 4 1 0 20.21 • 9 16 3 +	20.21 1 6 4 1 0 18.18 3 10 15 3 +	82:83 2 14 19 4 4 20:21 1 12 13 3 1	22 .23 4 14 22 3 2 20 .21 2 12 15 5 1	18.17 1 5 5 4 1
l	14.15 0 4 4 4 0 18.13 0 1 1 0 0	18.17 1 4 8 2 +	18,17 4 16 15 3 + 11,18 + 3 3 1 +	18.17 0 0 1 0 0	10.10 1 1 3 1 + 10.17 0 0 0 0 0	14:15 2 8 8 4 1 12:13 1 9 13 5 1
ł	10.11 0 0 0 0 0 0 •.• 0 0 0 0 0	14.15 + + + 0 0	12,13 0 + + + 1	14.15 0 0 0 0 0	14:18 0 0 0 0 0 0 12:19 0 0 0 0 0	10-11 + 4 8 J 1 0-0 0 + 1 Z +
ł	8.7 0 0 0 0 0 4.8 0 0 0 0 0	10-11 0 D 0 0 0 0.0 0 0 0 0	e.1 0 0 0 0 0 0 e.7 0 0 0 0 0	10.11 0 0 0 0 0 0.0 0 0 0 0	10:11 0 0 0 0 0 #:0 0 0 0 0	4.6 0 0 0 0 0
I	174	8.7 0 0 0 0 0 758	4.6 0 0 0 0 0	6.7 0 0 0 0 0 536	8.7 0 0 0 0 0 387	2.3 0 0 0 0 0
ı	WIND SPEED IKTS) 40	HIND SPEED (KTS) 41	HIND SPEED (KTS) 42	HIND SPEED (KTS) 43	HIND SPEED (KTS) 44	MIND SPEED (KTS) 45
Ì	TEMP (*C) 8-3 4-10 11-81 82-33 2 34	TEMP (*C) 0-5 4-10 11-81 22-33 4 34 20-21 0 0 0 0 0 0	TEMP (*C) 0-5 4-10 11-81 02-23 2 24			
Į	19.11 9 0 4 3 0 0.9 1 11 9 19 0	20,21 0 0 0 0 0	#4.25 0 + 0 0 0 0 ##.83 + + 0 0 0	20.21 O O O O O	14:18 0 0 0 3 1	14-18 0 0 + + 0 12-18 + 4 B B 2
	6.7 8 18 2 3 4.6 0 3 6 8 0	18.17 1 9 15 1 0 14.18 1 11 17 R 2	10.21 + 0 + 0 0 10.10 + 2 1 0 0	18.18 + 2 1 0 0 18.17 1 F 13 2 +	19-11 D U 4 D Q 0.9 O 4 8 7 2	0.11 + 5 22 17 2 0.9 0 2 12 11 2
	2.3 0 0 0 0 0	12:13 2 10 8 2 0 10:11 1 1 3 1 0	16.17 2 5 9 2 + 14.18 1 7 6 4 +	14.18 2 8 15 8 1 12.12 1 7 16 9 1	0.7 4 10 11 22 7 4.8 0 2 11 5 3	0.7 0 0 2 2 1 4.8 0 0 0 0 0
	-2,-1 0 0 0 0 0 -4,-2 0 0 0 0 0	0 0 0 0	12.13 2 11 13 6 4	10.11 0 • 3 3 1 •.• 0 0 0 0 1 0	0.1 0 0 0 0 0	2.3 0 0 0 0 0 0.1 0 0 0 0 0
	0.1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4.4 0 0 0 0 0	9.8 D D 2 • O	4.7 0 0 0 0 0	-1 0 0 0 0	·2 ·-1 0 0 0 0 0
	<u> </u>	2.3 0 0 0 0 0			-48 0 0 0 0 0 -48 0 0 0 0 0	-43 0 0 0 0 D
	109 0 0 0 0	1.3 0 0 0 0 0 0 0.1 0 0 0 0 0 0 270	4.8 0 0 0 0 0	2.3 0 0 0 0 0 292	-48 0 0 0 0 0 0 -48 0 0 0 0 0 0	-88 0 0 0 0 0 0 244

jective compilation of available data for specified areas without regard to suspected biases.

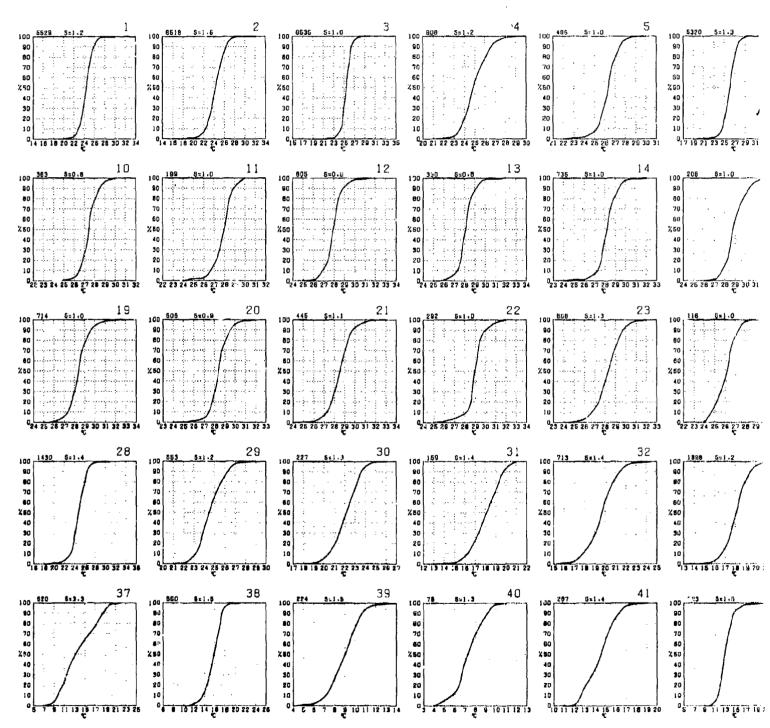
pposite page) are based on all available data subjectively adjusted where bias was evident.



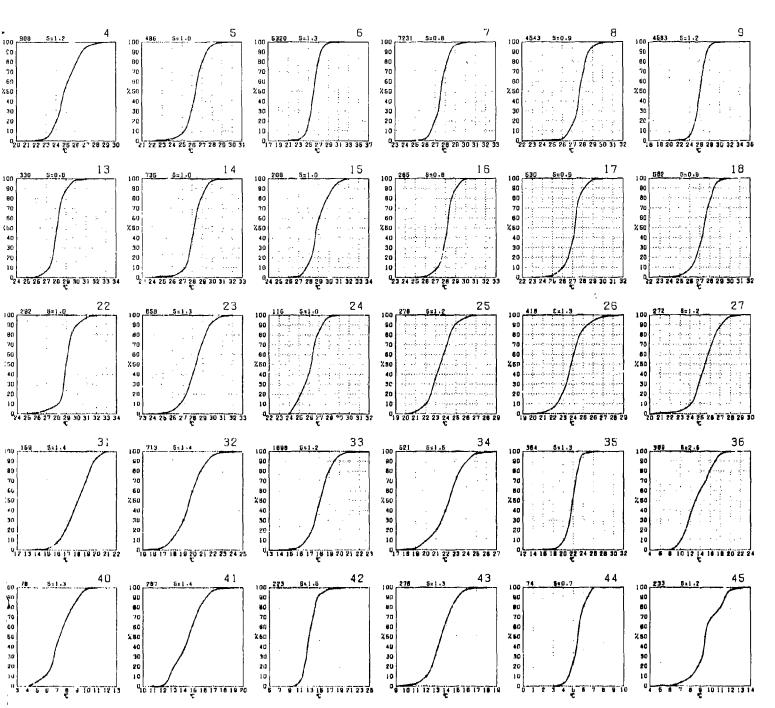
SEA SURFACE TEMPERATURE



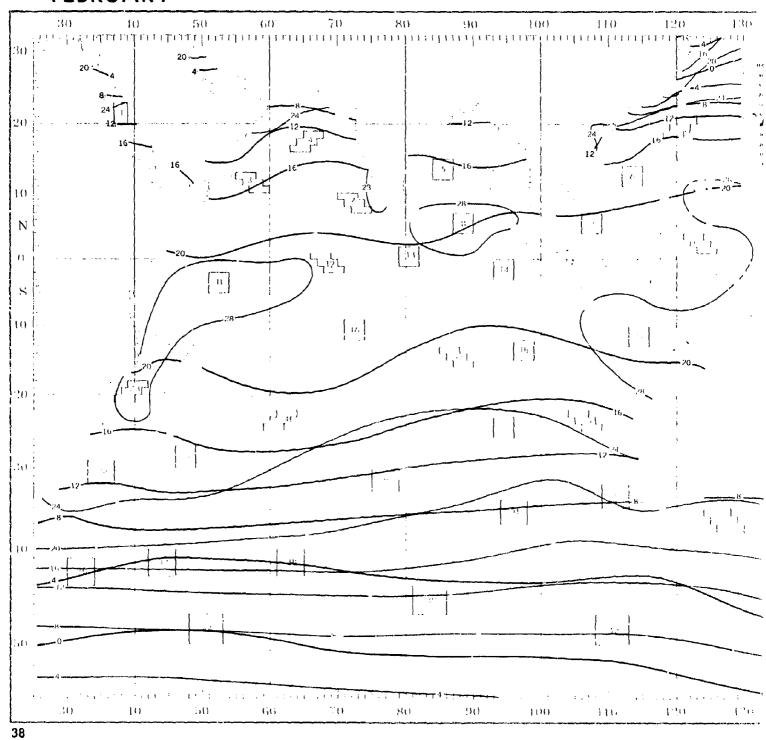
SEA SURFACE TEMPERATURE



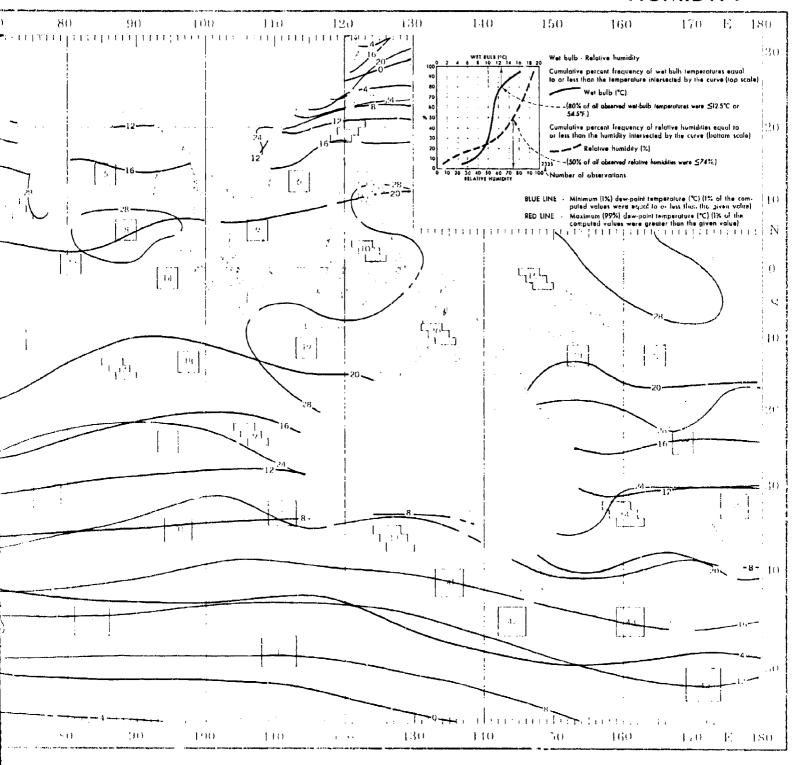
<u>Graphs</u> represent the objective compilation of available data for specified areas withon The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively ad



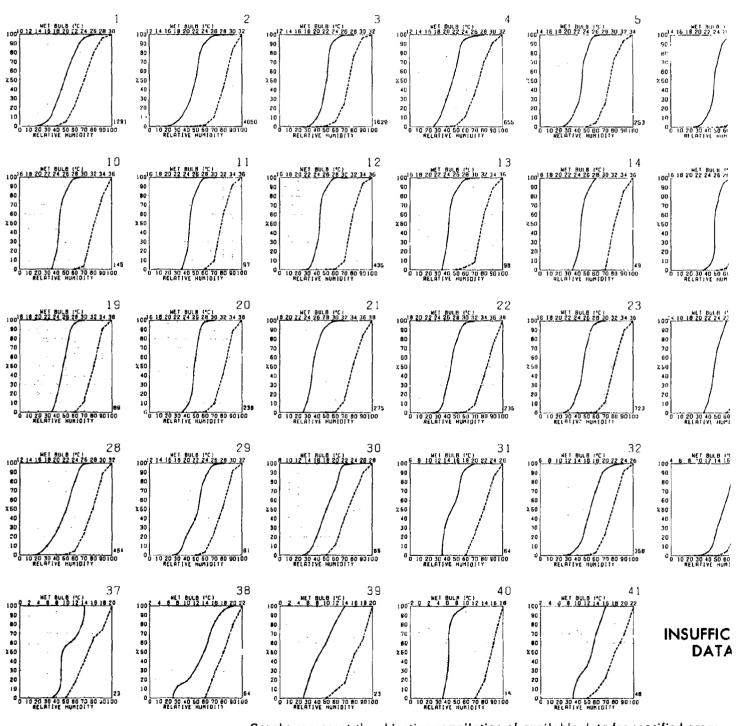
ictive compilation of available data for specified areas without regard to suspected biases.



HUMIDITY



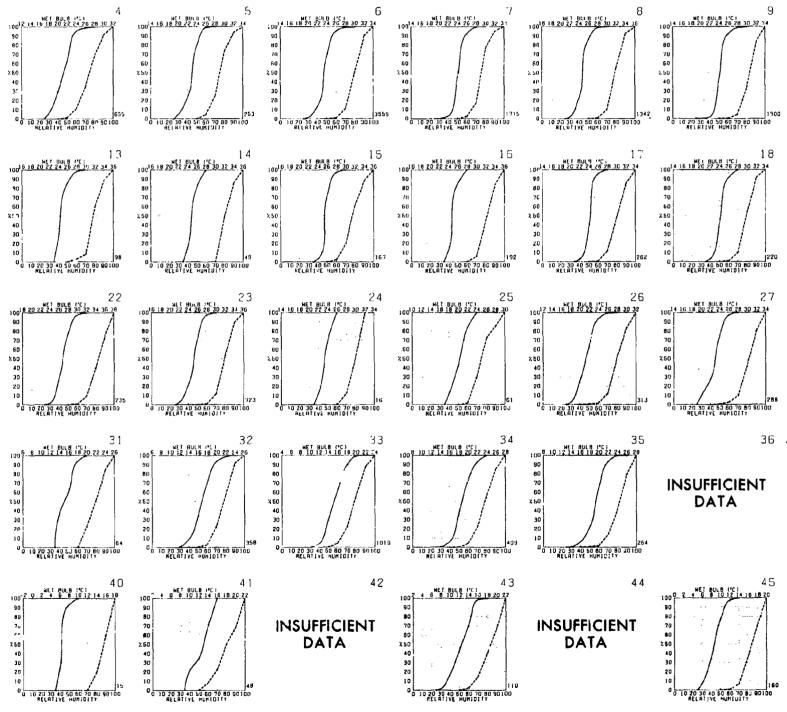
WET BULB AND RELATIVE HUMIDITY

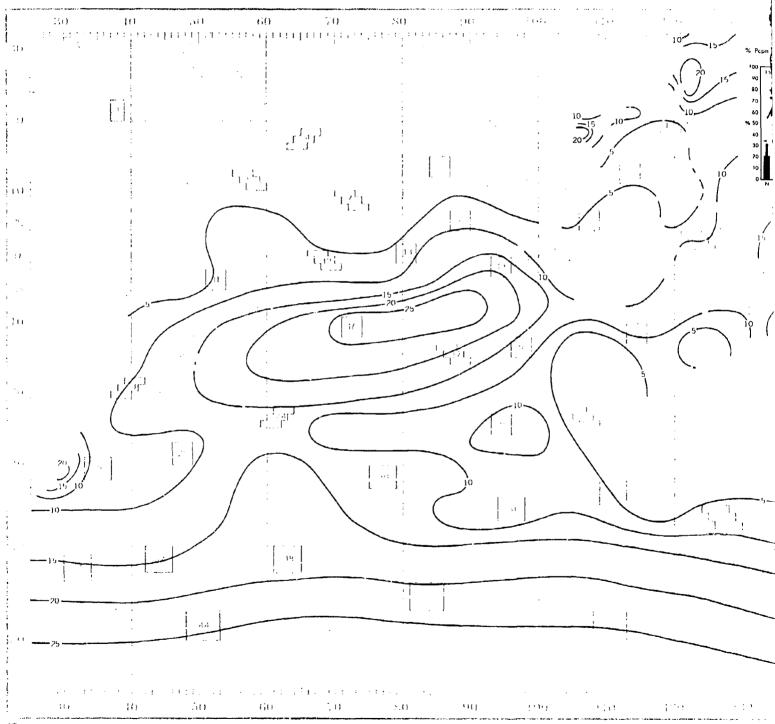


<u>Graphs</u> represent the objective compilation of available data for specified areas w The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively

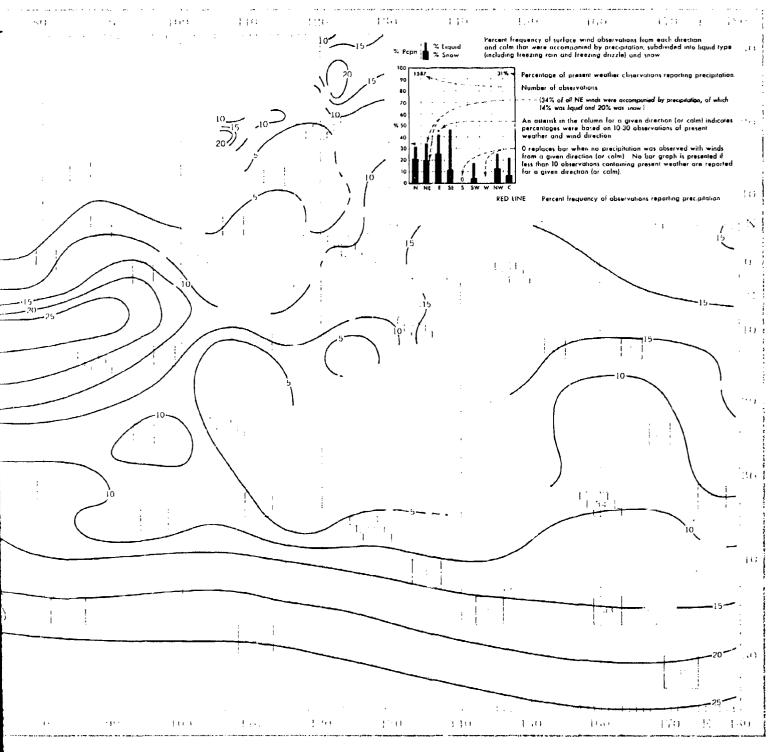
UMIDITY

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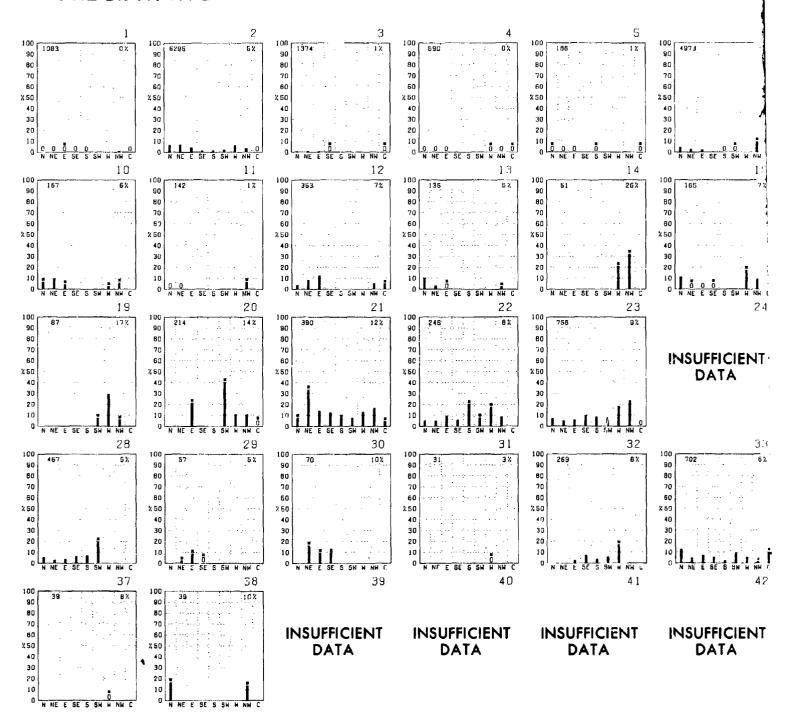




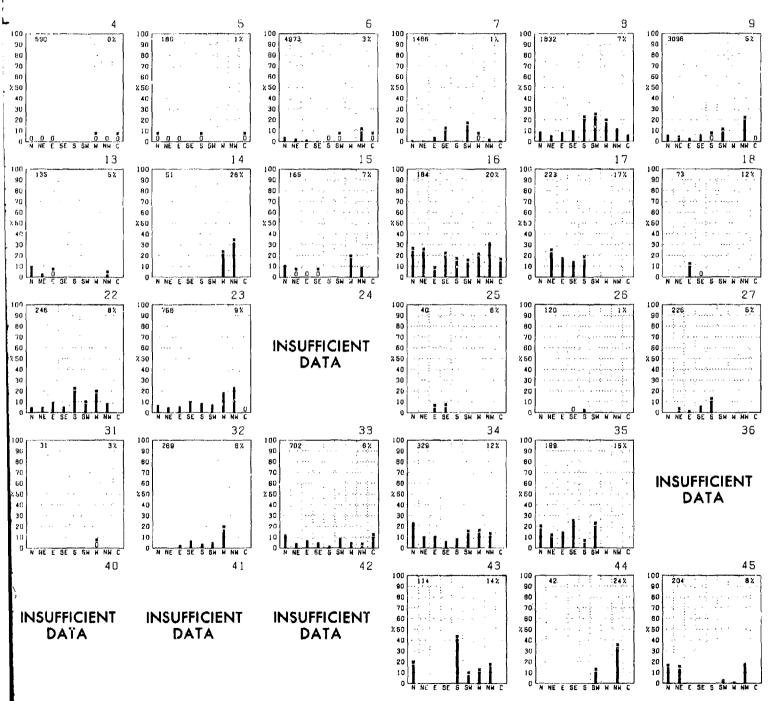
PRECIPITATION



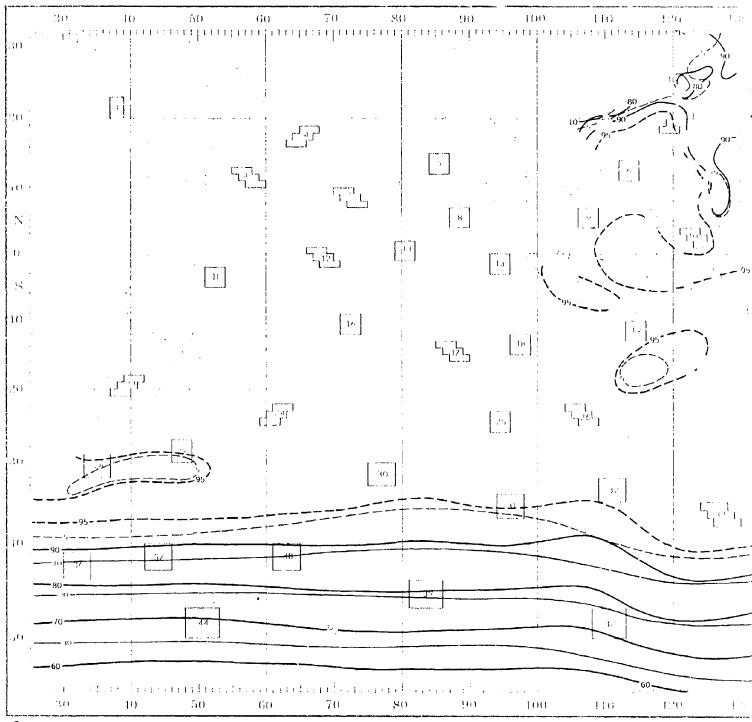
PRECIPITATION



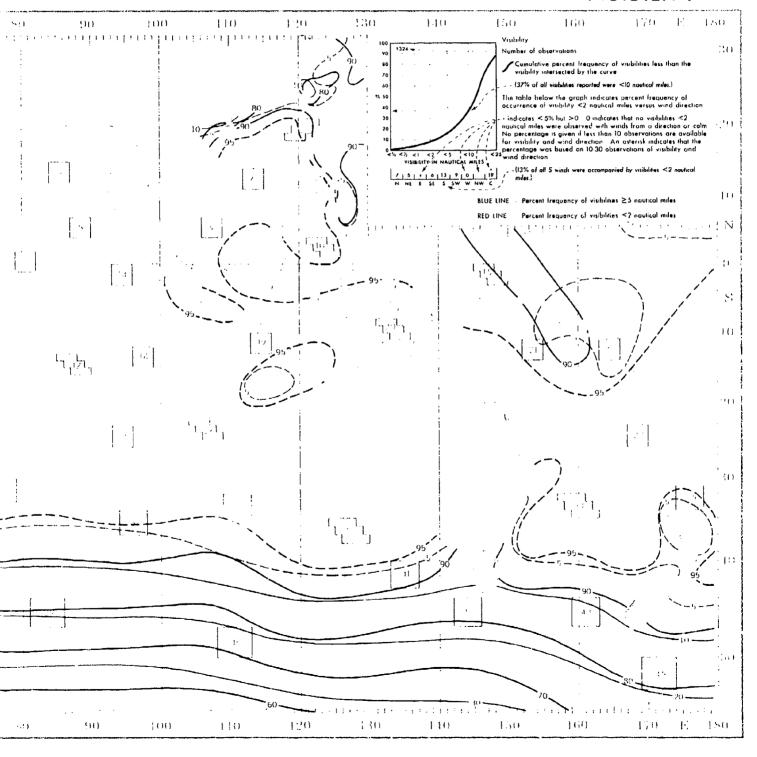
Graphs represent the objective compilation of available data for specified areas without re. The isopleth analyses (opposite page) are based on all available data subjectively adjusts



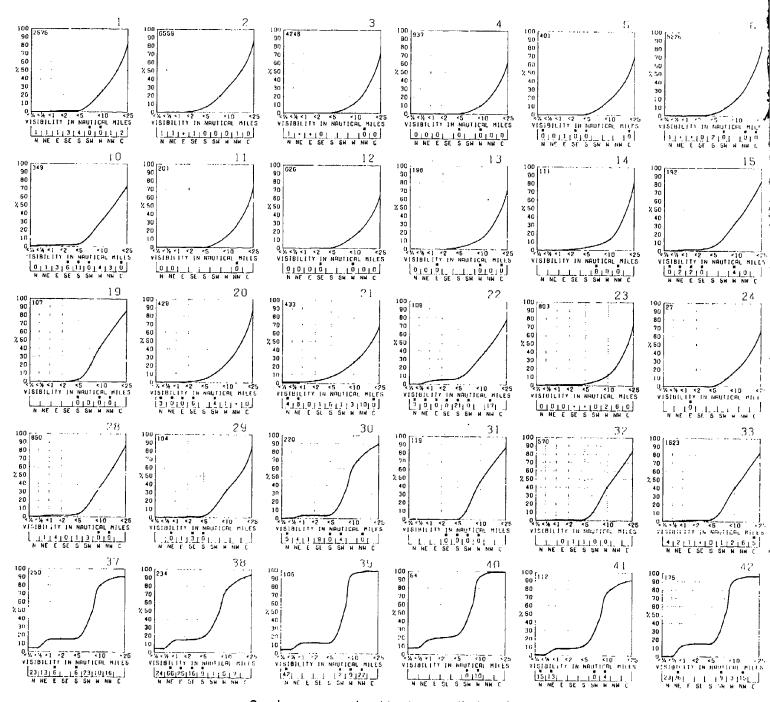
ctive compilation of available data for specified areas without regard to suspected biases. posite page) are based on all available data subjectively adjusted where bias was evident.



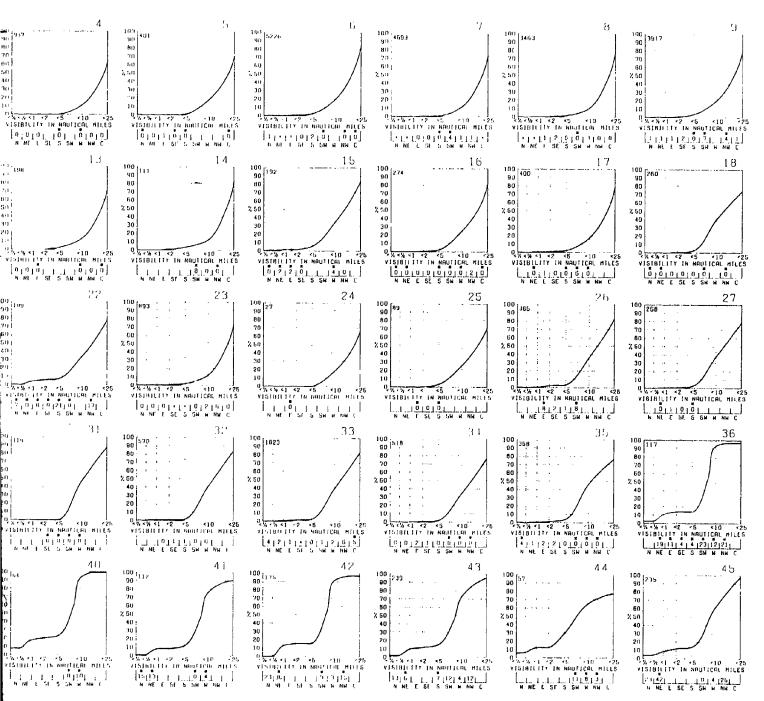
VISIBILITY



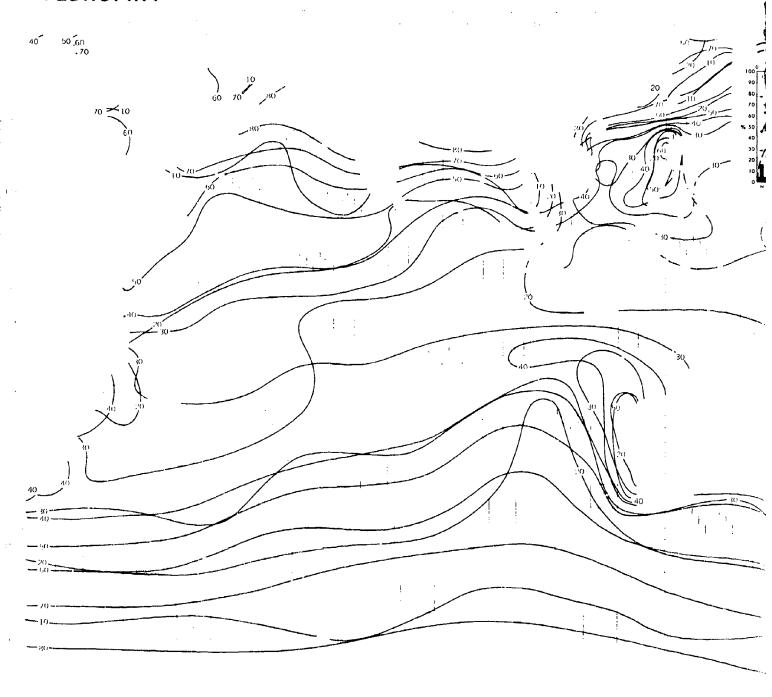
VISIBILITY



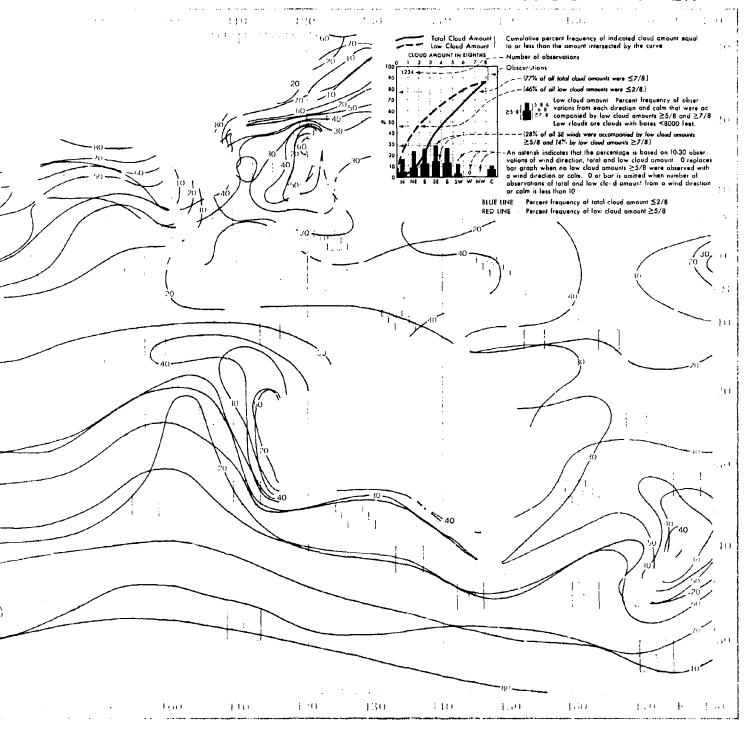
Graphs represent the objective compilation of available data for specified areas without reg The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjusted



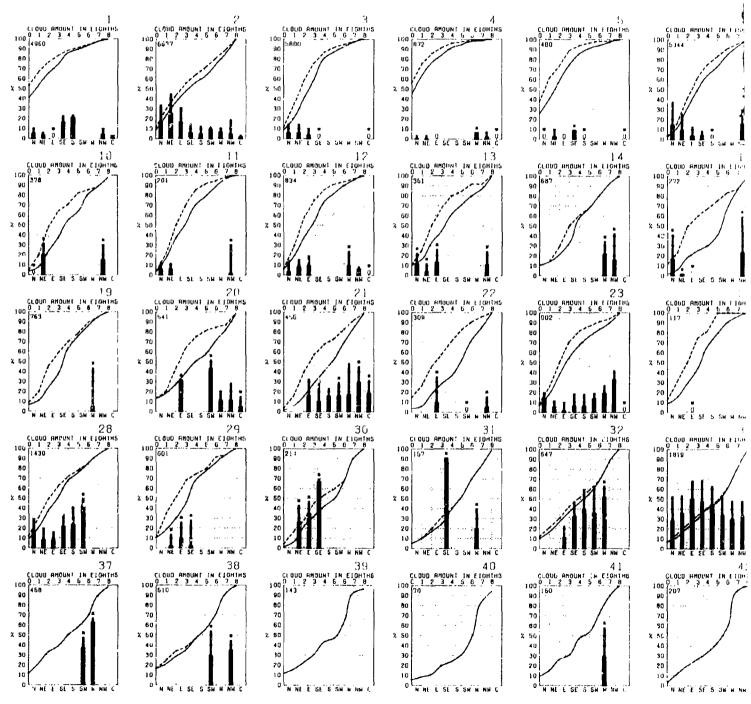
tive compilation of available data for specified areas without regard to suspected biases. osite page) are based on all available data subjectively adjusted where bias was evident.



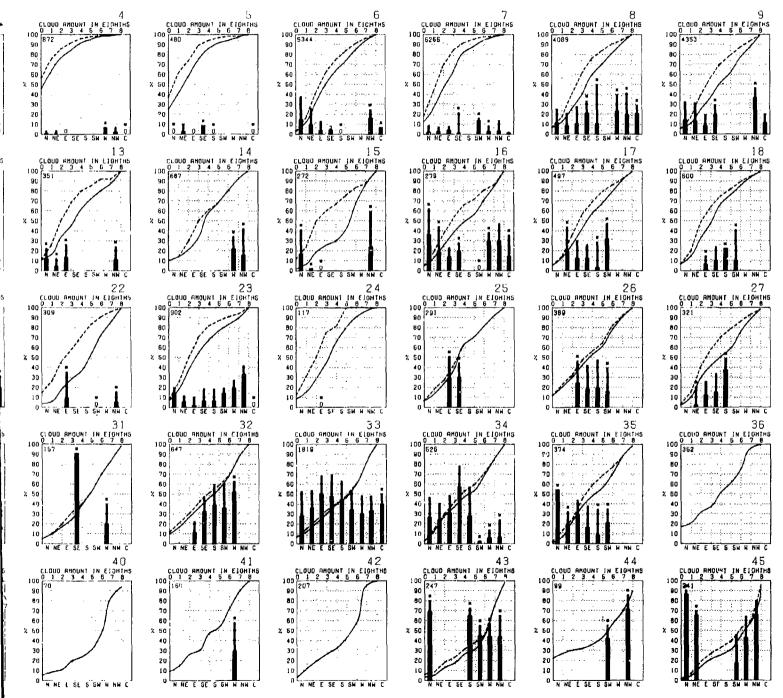
CLOUD COVER



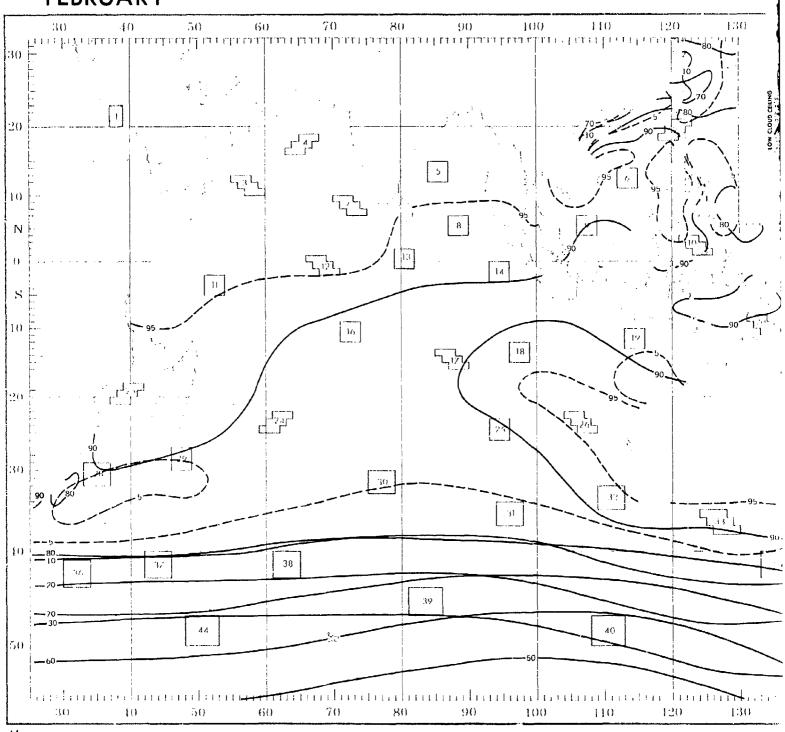
CLOUD COVER



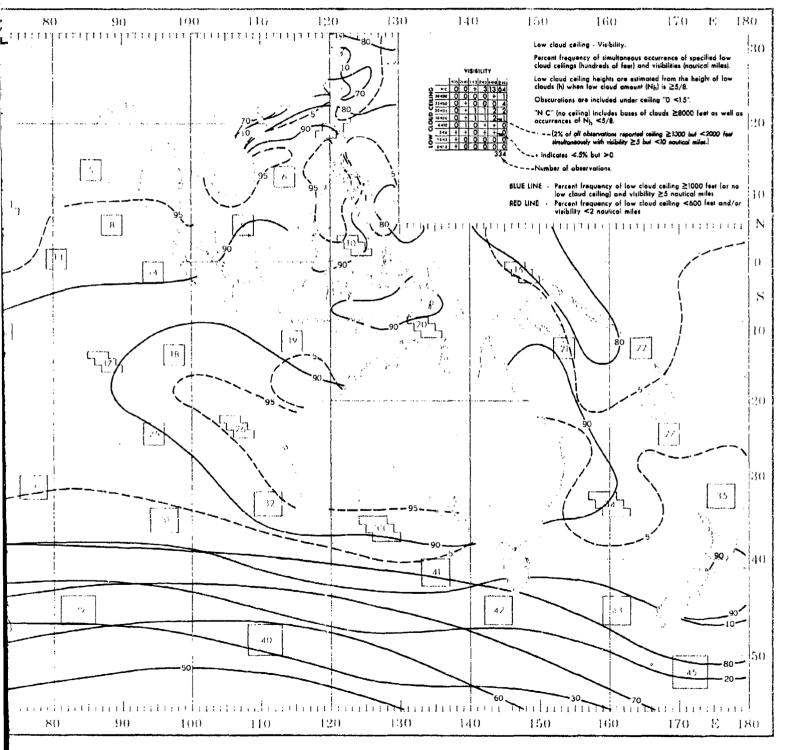
Graphs represent the objective compilation of available data for specified areas without The isopleth analyses (apposite page) are based on all available data subjectively adjusted.



objective compilation of available data for specified areas without regard to suspected biases. (opposite page) are based on all available data subjectively adjusted where bias was evident.



CEILING AND VISIBILITY



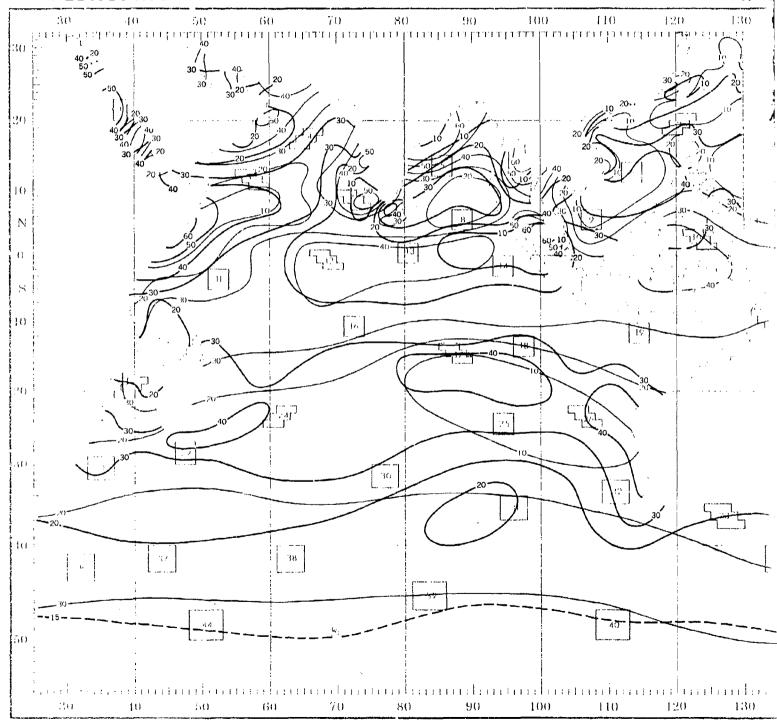
CEILING AND VISIBILITY

VISIBILITY	VISIBILITY ***********************************	VISIOILE (IT 3	VISIBILITY 4	VISIBILITY VISIBILITY AC 0 0 0 1 6 88 S3-40 0 0 0 0 0 0 1 6 88 S3-40 0 0 0 0 0 0 0 1 S 34-60 0 0 0 0 0 0 1 S 34-60 0 0 0 0 0 0 0 1 S 34-60 0 0 0 0 0 0 0 1 S 34-60 0 0 0 0 0 0 0 0 1 S 34-60 0 0 0 0 0 0 0 0 0 S 34-6 0 0 0 0 0 0 0 0 0 S 34-6 0 0 0 0 0 0 0 0 0 S 34-6 0 0 0 0 0 0 0 0 0 0 S 34-6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY
C C C C C C C C C C	10 10 10 10 10 10 10 10	*** *** *** *** *** *** *** *** *** **	**/** **/***	10-10 10 10 10 10 10 10	10-10 0 0 0 0 2 4 54 5-10 1-10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
VISIBILITY	VISIBILITY	VISIBILITY	VISIBILITY 1/4	VISIBILITY	VISIBILITY -17/ 17/41 12 24 54 10 10 -17/ 17/41 12 24 54 10 10 -17/ 17/41 12 24 54 54 10 10 -17/ 17/41 12 24 54 54 10 10 -17/ 17/ 17/ 17/ 17/ 17/ 17/ 17/ 17/ 17/
VISIBILITY 28	VISIBILITY 29 **/*********************************	VISIBILITY 30 -1/4	VISIBILITY 31 -1/4 [941] 1-2 2-8 3-10 110	VISIBILITY 32	VISIBILITY 33 -1/c 3/4 1/
VISIBILITY ATT PARTIES FAIGHTON AC 0 0 0 3 5 28 BOME 0 0 0 0 3 5 28 SEME 0 0 0 0 0 0 0 0 0 SEME 0 0 0 0 0 0 0 0 0 0 SEME 0 0 0 0 0 0 0 0 0 0 SEME 0 0 0 0 0 0 0 0 0 0 SEME 0 0 0 0 0 0 0 0 0 0 SEME 0 0 0 0 0 0 0 0 0 0 SEME 0 0 0 0 0 0 0 0 0 0 SEME 0 0 0 0 0 0 0 0 0 0 SEME 0 0 0 0 0 0 0 0 0 0 SEME 0 0 0 0 0 0 0 0 0 0 SEME 0 0 0 0 0 0 0 0 0 0 SEME 0 0 0 0 0 0 0 0 0 0 SEME 0 0 0 0 0 0 0 0 0 0 SEME 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0 0 0 0 0 0 0 0 0 0 SEM 0 0	No. No.	INSUFFICIENT DATA	INSUFFICIENT DATA	VISIBILITY 41	INSUFFICIENT DATA

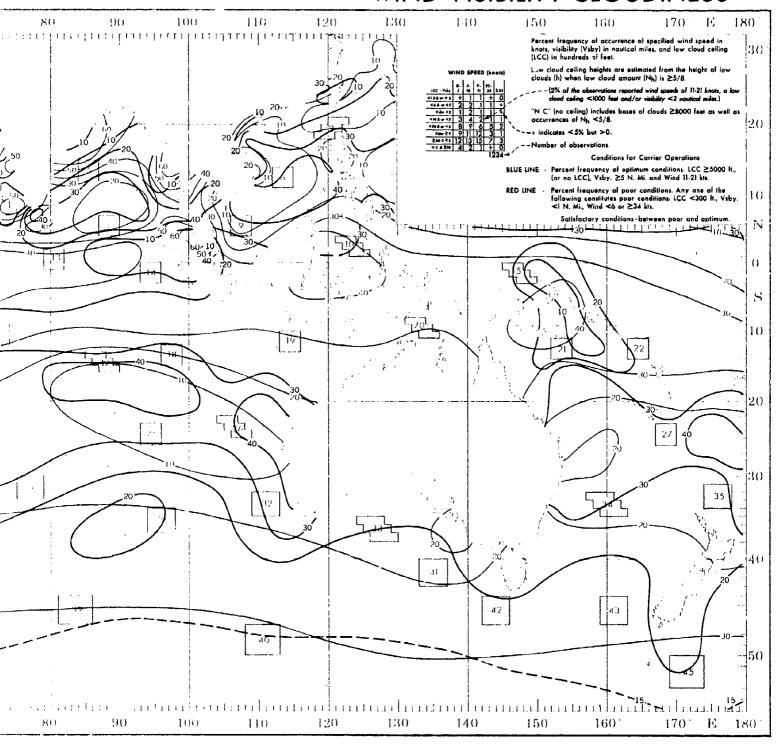
<u>Graphs</u> represent the objective compilation of available data for specified areas without regions to a linear specified areas without regions are based on all available data subjectively adjusted

VISIBILITY 4 **** *** *** *** *** *** ***	VISIBILITY ***********************************	VISIBILITY	VISIBILITY VISIBILITY AC	VISIBILITY	VISIBILITY C-1/2 1/
NC O 3 O O 6 66 6 6 6 6 6	NC 0 0 0 2 81	NC O O O O O O O O O	RC 0 0 0 0 0 2 49 G0-40 0 0 0 0 0 0 2 3440 0 0 0 0 0 0 0 2 3540 0 0 0 0 0 0 0 17 G10-20 0 0 0 0 0 17 G10-20 0 0 0 0 0 0 17 G10-20 0 0 0 0 0 0 0 0 A10 0 0 0 0 0 0 0 A11-5-3 0 0 0 0 0 0 0 G-1.5 0 0 0 0 0 0 0 0 A7	NC 0 0 0 0 4 53 50=80 0 0 0 0 0 1 4 50=80 0 0 0 0 0 1 13 50=80 0 0 0 0 0 1 13 50=80 0 0 0 0 1 0 7 50=80-38 1 0 0 1 0 0 0 3 60=10 0 0 0 0 0 0 3 60=10 0 0 0 0 0 0 2 1.5-3 0 0 0 0 0 0 0 61.5 0 0 0 0 0 0 0	MC 0 0 0 1 7 62 50 90 0 0 0 0 1 1 2 34 10 0 0 0 0 0 1 1 50 10 20 0 0 0 1 1 50 10 20 0 0 0 0 1 50 10 20 0 0 0 0 1 50 10 20 0 0 0 0 1 50 10 20 0 0 0 0 0 0 61 1.6-3 0 0 0 0 0 0 641 1.8 0 0 0 0 0 0 0 143
10 10 10 10 10 10 10 10	VISIBILITY 1-1/1 [1/1-1] 1-2 [1-6 [1-1] 1-10 1-1/1 [1/1-1] 1-2 [1-6 [1-1] 1-10 1-1/1 [1/1-1] 1-2 [1-6 [1-1] 1-10 1-1/1 [1/1-1] 1-2 [1-6 [1-1] 1-10 1-1/1 [1/1-1] 1-2 [1-1] 1-2 [1-1] 1-1/1 [1/1-1] 1-2 [1-1] 1-1/1 [1/1-1] 1-2 [1/1-1] 1-1/1 [1/1-1] 1-2 [1/1-1] 1-1/1 [1/1-1] 1-2 [1/1-1] 1-1/1 [1/1-1] 1-2 [1/1-1] 1-1/1 [1/1-1] 1-2 [1/1-1] 1-1/1 [1/1-1]	VISIBIL [1Y -1/2 1/4-1 1-5 2-6 3-10 110 -1/2 1/4-1 1-5 2-6 3-10 110 -1/2 1/4-1 1-5 2-6 3-10 110 -1/2 1/4-1 1-5 2-6 3-10 110 -1/2 1/4-1 1-5 2-6 3-10 110 -1/2 1/4-1 1-5 2-6 3-10 110 -1/2 1/4-1 1-5 1-5 1-5 -1/2 1/4-1 1-5 1-5 -1/2 1/4-1 1-5 1-5 -1/2 1/4-1 1-5 1-5 -1/2 1/4-1 1-5	VISIBILITY ***/****/***/****/******************	VISIBILITY Visibility Visi	INSUFFICIENT DATA
INSUFFICIENT DATA	VISIBILITY 4 1	INSUFFICIENT DATA	VISIBILITY 4 3 ***/*	VISIBILITY 4.4	VISIBILITY 45 ***********************************

bjective compilation of available data for specified areas without regard to suspected biases. opposite page) are based on all available data subjectively adjusted where bias was evident.



WIND-VISIBILITY-CLOUDINESS



LOW CLOUD CEILING-VISIBILITY-WIND

	0	0	,	Ē	
HIND SPEED (KNOTS)	2. WIND SPEED (KNOTS)	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	MIND SPEED (KNOTS)	6 WIND SPEED (KHOTS)
LCC - YEST 3 10 21 33 234	LCC - VBBY 3 10 21 33 434	LCC - VSST 0- 4- 11- 22- 3 10 21 33 134	LCC - Y68Y 0- 4- 11- 22- 3 10 21 33 334	LCC - V587 0- 1- 11- 22- 33 234	LLC V587 3 10 71 33 +34
1.540 *.5 0 0 0 0	41.54 OR 4.5 0 + + +	<1.54 QR = .6 D D O O O	1.6 4 OR * .5 0 0 0 0 0	*1.5 4 OR *.5 0 0 0 0 0	*1.5 & QR *.6 + + + 0
48 4 OR 42 0 0 0 0 0 0 V	<84 OR <2 0 + 1 1 + VSBY +2 0 + + 0	<8 ± 0R <2 0 0 + 0 0 V88Y <2 0 0 + 0 0	<64 OR <2	48 & OR <2 0 0 + 6 0 9887 42 0 0 0 0 0	*84 0R *2
<10 4 DR <2 0 1 1 0 0	410 4 OR 42 + 1 4 4 1	<10 4 0R <2 0 + 1 C D	<10 4 0 4 0 4 0 4 0	<10 4 GR <2 D D + O O	<10 L OR <2 + ! 4 2 +
*20 4 DR *5 0 1 3 + 0	*20 4 OR *5 + 2 12 12 1 VANY 25 3 20 41 26 3	<20 4 0R 46 0 3 3 + 0 V887 ≥6 3 53 42 1 0	420 4 OR 45 + 1 + + 0	<20 4 OR <5 1 1 0 0 V88Y ±6 18 64 17 0 0	420 4 OR 46 + 2 12 5 + V88Y A6 2 26 57 13 +
350 4 25 8 28 48 6 0	250 4 25 3 18 27 14 2	2 50 4 26 3 48 38 1 0	250 4 25 12 57 27 + 0	250 4 25 18 61 16 0 0	250 4 26 1 23 42 7
MC 4 t 10 7 25 45 E D	NC 4 a 10 3 15 22 10 1 5383	NC 4 > 10 3 47 34 1 0	MC 4 a 10	MC 4 = 10 15 59 14 0 0	MC L = 10 1 22 36 5 +
10	1 1	12	13	1 4	15
MIND SPEED (KNOTS)	WIND SPEED (MNOTS)	WIND SPEED (KNOTS)	AINO SPEED (KNOTS)	HIND SPEED (KNOTS)	WIND SPEED (KNOTS)
LCC - VSBY	LCC - V66Y	CCC - VERY 3 10 21 33 234	1.64 OR S.D 0 0 0 0 0	LCC - Y48Y 3 10 21 33 234	LCC - YARY 3 10 21 33 234
-0 ± 0R +2 0 2 0 0 0	48 & OR 42 0 0 0 0 0	<84 CM <2 1 0 0 0 0	<1.64 OR <2 0 1 0 0 0	48 4 DK +2 D D D D D	46 A DR 42 0 4 2 2 0
V887 -2 0 0 0 0 0	V887 42 0 0 0 0 0	V38Y =2 0 0 0 0 D	V85Y +2 0 0 0 0 0	V887 42 0 0 0 0 0	V68Y 42 0 0 0 2 0
410 4 0R 42 0 9 2 0 0	<10 4 OR 42	<10 4 0A <2 1 1 1 0 0 <20 4 0A <6 1 7 1 + 0	410 4 OR 42	<10 4 0R <2 0 4 0 0 0 0 = 4 0 0 0 0 = 4 0 0 0 0 0 0	410 4 OR 42 0 13 6 2 0
V667 25 11 48 41 0 D	VSBT 25 8 63 29 0 0	Vasy a5 13 71 15 + 0	VBBY 25 20 60 16 1 0	VBBT 45 13 63 19 2 0	VEGY »6 19 49 19 0 0
#C4>10 11 28 33 D U	HC4 a 10 8 48 22 0 0	NC 4 NC 12 62 13 0 0	980 4 95 16 51 14 1 D	950 4 36 10 40 15 0 0 MC 4 4 10 10 38 13 0 0	850 4 25 19 30 8 0 0 NC 4 2 10 19 25 8 0 U
54	107	372	112	52	53
19 HIND GPEED (KNOTS)	20 WIND SPEED (KNOTS)	21 WIND SPEED (KNOTS)	22 HIND SPEED (HNOTS)	23 WIND SPEED (KNOTS)	24 NINO SPEED (KNOTS)
LCC - YESY 9 10 21 29 294	LCC - VEBY 3 10 21 33 294	LCC - VBBY 3 10 21 33 234	LCC - V887 0- 4- 11- 22- 33 334	LCC - YEBY 3 10 21 33 234	LCC - V68Y 0- 4- 11- 22- 33 834
<1.54 M <.8 0 0 0 0 0	41.84 0R 4.8 0 0 0 U 0	4).8 4 0F 4.5 + + 1 0 0	-1.54 JR5 0 1 0 0 0	-1.5 L OR S 0 + 0 + 0	<1.5 4 OH <2.5
48 4 OR 42 0 0 0 0 0	46 4 OR 42 0 0 0 0 0	<84 0R 42 (+ 2 + 0 VBST 42 (+ 1 0 0	<8 4 OR <2 D 4 3 D 0	46 4 DR 42 D 1 + + + + + + + + + + + + + + + + + +	
*10 4 08 48 5 2 7 2 0	YBBY 42 0 0 0 0 0 0 0 0 410 4 0R 42 1 2 5 2 0	VBS7 42 0 + 1 0 0	YABY <2 0 3 3 0 0 <10 4 0R <2 0 6 4 0 0	<10 & OR <2 4 2 2 1 4	19 4 0R <2 0 0 0 13 0
420 4 98 48 5 5 16 2 0	<20 4 OR 46 2 5 10 2 1	*20 & 0R *8 4 9 10 4 0	-20 4 OR -6 D 15 9 D O	420 4 08 48 1 5 5 2 +	420 4 DR 45 0 U U 13 0
7487 28 9 40 44 5 D 280 426 5 37 28 2 D	veev as 18 37 37 4 6	VS\$T a5 20 47 20 3 0	V68Y 45 4 60 2B 0 0	V687 25 15 46 31 5 +	v58v 45 7 47 33 13 0 >50 4>6 7 47 27 0 0
MC 4 > 10 5 35 16 2 0	MC 4 a 10 15 30 25 2 0	NC 4 2 10 18 33 15 + 0	NC 4 & 10 4 40 21 0 0	NC 4 = 10 16 40 23 3 +	MC 4 a 10 7 47 27 U D
28	29	30	31	32	33
HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	WIND SPEED (KNOTS)	WIND SPEED (KNOTS)
LCC - VEBY 3 10 21 33 334	LCC - V481 0- 4- 11-172- 3 10 21 33 234	LCC - Y887 3 10 21 33 234	LCC - VAST 3 10 21 33 234	CCC - VBBY 3 10 21 33 254	LCC - V68Y 3 10 21 33 236
<1.8 4 08 <-B 0 0 0 0 0 0 0 0 48 4 08 <-B 0 0 0 0 0 0	<1.54.08 <.5	<1.5 4 QR <.5 0 0 0 0 0 0 0 46 4 DR <2 0 0 2 0 0	<1.64 OR <18	<1.5 & OR <.5 0 0 + 0 0 = 0 0	*1.5 4 0R * (8 0 + + 1) *8 4 0R * 2 + 1 1 + 0
V88Y 42 D D D D D	Y88Y <2 0 0 0 0 0	VERY 42 0 0 0 0 0	V88Y -2 0 0 0 0 0	VBBY 42 0 0 + 0 0	V887 42 0 0 0 0 0
<pre><10 LOR <2</pre>	-10 4 64 -2 0 2 4 2 0 -20 4 64 4 0 5 10 2 0	*10 4 0R *2 0 5 8 0 0 *20 4 0R *5 0 9 19 0 0	<10 4 0ft <2 0 0 2 B D	<:0 4 GR <2 0 1 4 + 0 <20 4 GR <5 1 5 15 6 0	-10 4 0R -2 1 4 4 1 + -20 4 0R -4 1 13 13 2 +
V667 aB 4 39 40 15 1	V&BT a5 0 39 59 2 0	VS81 45 5 41 50 3 0	VAST 85 11 50 30 9 8	V58Y N5 2 31 50 16 0	V687 28 6 43 42 7 0
250 4 25 4 32 29 8 +	E50 4 a S	a 50 4 a 5 3 23 27 2 0 MC 4 a 10 3 23 27 2 0	#60 4 #6 2 19 17 6 0 #C 4 # 10 2 15 15 6 0	#50 4 a B 1 18 28 7 0	250 4 25 4 20 19 4 19 MG 4 2 10 3 18 18 3 0 785
420	51	64	54	309	
37 WIND SPEED (KNOTS)	38 UST SPEED (KNOTS)	39	40	4 1 HIND SPEED (KNOTS)	42
LCC - YERY 0- 4- 11- 22- 1 10 21 33 334	U- 4- 11-82-			LCC - VARY 3 10 21 33 234	
41.84 dR 4.8 3 D 5 8 D	*1-8408 *.S 0 0 0 0 0			4)-84 00 4-8 0 0 0 0 0	
+8 4 0R <2 3 0 8 8 0 ▼88	*8 4 DR -2 4 0 2 2 0 VABT 0 0 0 2 0	INSUFFICIENT	INSUFFICIENT	46 4 5R 42 0 3 0 0 0 0 V887 42 0 0 0 0 0 0	INSUFFICIENT
<10 4 OR <2 3 3 5 10 0	410 4 0R 42 4 2 8 2 0	DATA	DATA	10 4 0M 12 0 3 0 0 0	DATA
420 4 DR 45 5 5 15 10 0	-20 4 0R -5 8 8 8 8 0			*20 4 OR *5 0 3 15 0 0 VBBY 25 0 32 59 3 0	
v44v as 8 23 31 21 0 as0 4 as 5 15 6 3 0	980 4 25 0 24 16 6 0			v88v as 0 32 59 3 0 a50 4 as 0 18 Z4 3 0	
MC 4 a 0 5 13 5 3 0	HC 6 2 10 0 24 12 b 0			HC 4 = 10 0 15 12 3 0	
	50			31	

<u>Graphs</u> represent the objective compilation of available data for specified areas without rego. The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjusted.

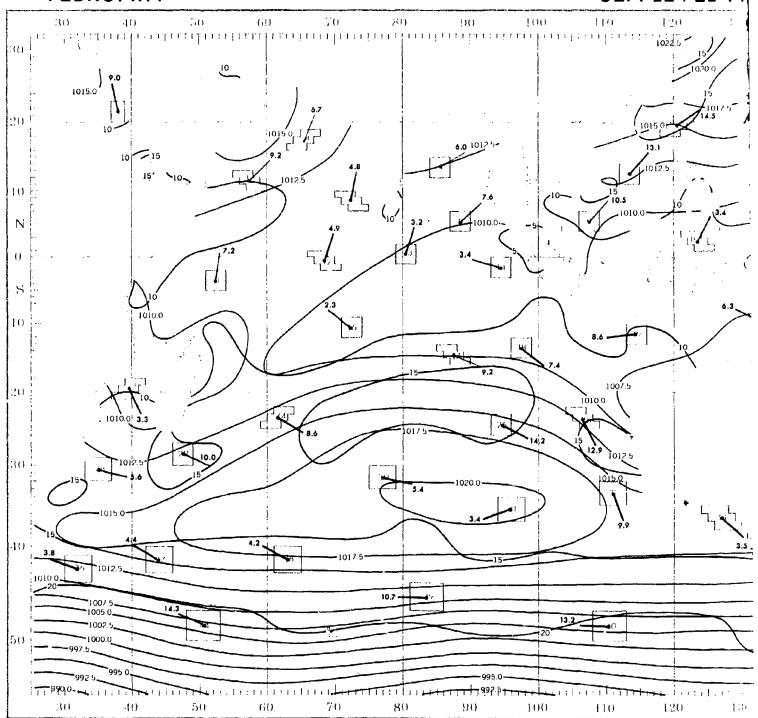
LITY-WIND

FEBRUARY

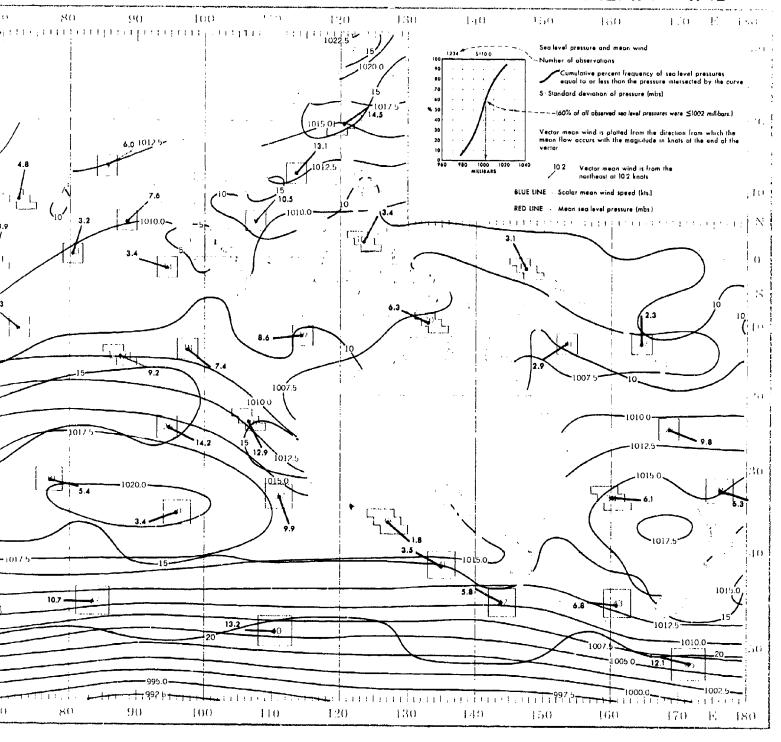
P HIND	4 SPEED (KNOTS)	S WIND SPEED (KNOTS)	HINO SPEED IMNOIS)	7 WIND SPEED (KNOTS)	HINO SPEED (KNOTS)	9 HIND SPEED (KNOTS)
*1.5 ¢ OR *.5 *8 ¢ OR *? *8 ¢ OR *? *8 ¢ OR *? *10 ¢ OR *? *20 ¢ OR *5 V86*15 1 250 ¢ 26 1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	LCC - VSSY		CC - V88Y 3 10 21 39 - 34 41.64 08 4.6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	*** C ********************************	CC - V887
*1.5 4 DM *.5 *1.5 4 DM *.5 *6 4 DR *? *558* *2 *10 4 DR *2 *10 4 DR *2 *20 4 DR *5 *258*	1 3 3 4 11 223 294 0 0 0 0 0 0 0 1 0 0 0 0 1 0 0 0 0 4 1 0 0 0 4 1 0 0 0 6 1 1 0 0 6 51 14 1 0 4 9 13 1 0	HIND SPEED (KNOIS) 1CC - V88Y	MINO SPEED (KNOTS) LCC - V88Y	HIND SPEED (KNOTS) LCC - V88Y	17 WIND SPEED (KNDTS) LCC - VBBY 3 0 4 11 22 3 3 3 3 4 *1.84 OR *.8 0 0 0 0 0 *5 4 OR *2 0 0 1 0 7 VBBT *2 0 0 1 6 1 4 *204 OR *8 0 6 14 2 1 VBBT *3 1 39 50 6 1 a\$0 4.8 1 31 34 3 0 HC 4 8 10 1 29 33 3 0 257	NIND SPEED (KNOTS)
LCC - Y88Y (*1.5 4 GR *2 *6 L GR *2 V887 *2 *10 4 GR *2 *20 4 GR *5 Y58Y 45	2 2 SPEED IKKNOTS1 2 4- 11- 23- 33- 34- 0 1 0 0 0 0 0 4 3 0 0 0 3 3 0 0 0 6 4 0 0 0 6 4 0 0 0 6 9 0 0 4 45 22 0 0 4 40 71 0 0 0 4	23 NINO SPEED (KNOIS) LCC - Year 0	2 4 WIND SPEED (XNOTS) LCC - VBBY 3 10 21 33 234 -1.5 4.08 -15 0 0 0 0 0 0 -84 08 -2 0 0 0 0 0 0 -10 4.08 -5 0 0 0 0 13 0 -10 4.08 -5 0 0 0 0 13 0 -10 4.08 -5 0 0 0 0 13 0 -10 4.08 -5 0 0 0 0 13 0 -10 4.08 -5 0 0 0 0 13 0 -10 4.08 -5 0 0 0 0 13 0 -10 4.08 -5 0 0 0 0 13 0 -10 4.08 -5 0 0 0 0 13 0 -10 4.08 -5 0 0 0 0 13 0 -10 4.08 -5 0 0 0 0 0 0 0 0 -10 4.08 -5 0 0 0 0 0 0 0 0 -10 4.08 -5 0 0 0 0 0 0 0 0 -10 4.08 -5 0 0 0 0 0 0 0 0 -10 4.08 -5 0 0 0 0 0 0 0 0 -10 4.08 -5 0 0 0 0 0 0 0 0 0 -10 50 4.06 7 47 27 0 0 0 -10 4.08 -5 0 0 0 0 0 0 0 0 0 -10 50 4.06 7 47 27 0 0 0 -10 4.08 -5 0 0 0 0 0 0 0 0 0 0 -10 50 4.06 7 47 27 0 0 0 -10 50 4.06 7 47 27 0 0 0	25 MIND SPEED (KNOTS) LCC - VSSY 0 - 4 - 11 - 125 - 134 41 - 5 - 4 - 6 - 7 - 7 - 7 - 7 - 7 - 7 41 - 5 - 7 - 7 - 7 - 7 41 - 5 - 7 - 7 - 7 41 - 5 - 7 - 7 41 - 5 - 7 - 7 41 - 5 - 7 41	26 MIND SPEED (KNOTS) LCC - V68Y	27 HIND SPEED (KNOTS) LCC - Y8BY G- 4- 51- 22- 3 10 21 33 334 -1.84 68 -15 0 0 0 0 -48 4 08 -2 0 0 0 0 -48 4 08 -2 0 0 0 0 -410 4 08 -2 0 0 6 1 -420 4 08 -5 1 2 15 6 0 -420 4 08 -5 1 2 15 0 -420 4 08 -5 1 2 15 0 -420 4 08 -5 1 2 15 0 -420 4 08 -5 1 2 15 0 -420 4 08 -5 1 2 15 0 -420 4 08 -5 1 2 15 0 -420 4 08 -5 1 2 15 0 -420 4 08 -5 1 2 15 0 -420 4 08 -5 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2
LCC - Y88Y 41-640R<-6 4640R<-2 Y88Y-7 -1040R<-2 -2040R-8 Y88Y-8 280428	3 3 5 5 5 5 5 5 5 5	32 MIND SPEED INNOTS LCC - VARY 0. 4- 11- 231- 334- 1.6 4 08 - 2 0 0 0 0 -64 08 - 2 0 0 0 0 -10 4 08 - 7 0 1 4 0 -10 4 08 - 8 1 15 16 6 0 -10 4 08 - 8 1 18 28 7 0 -10 4 0 10 1 17 26 7 0 -10 4 0 10 1 17 26 7 0 -10 4 0 10 1 17 26 7 0 -10 4 0 10 1 17 26 7 0	33 HIND SPEED (KNDTS) 1 CC - VBBV	34 HIND SPEED (KNDIS) LCC - V887 3 0- 4- 11-122- LCC - V887 3 10- 121-23- 344 (1.54 08 - 8 0 0 + 0 0 0 -64 08 - 2 0 0 + 1 0 + 0 -104 08 - 2 0 0 4 4 3 + 0 -104 08 - 5 11 16 5 + 0 -204 08 - 5 11 16 5 + 0 -204 08 - 5 3 20 27 4 0	35 HIND SPEED (KNOIS) LCC - VSSY	INSUFFICIENT DATA
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ective compilation of available data for specified areas without regard to suspected biases. posite page) are based on allavailable data subjectively adjusted where bias was evident.

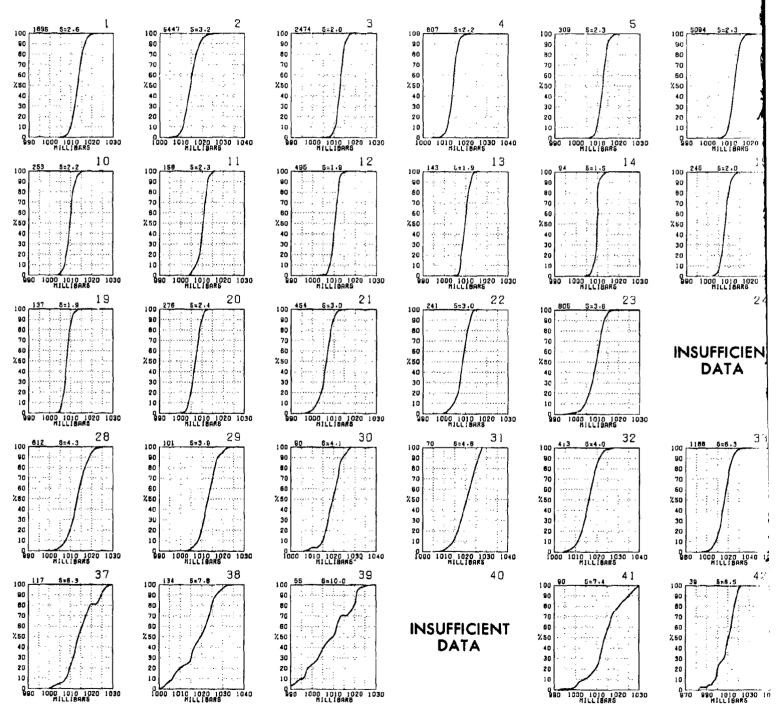
SEA LEVEL PR



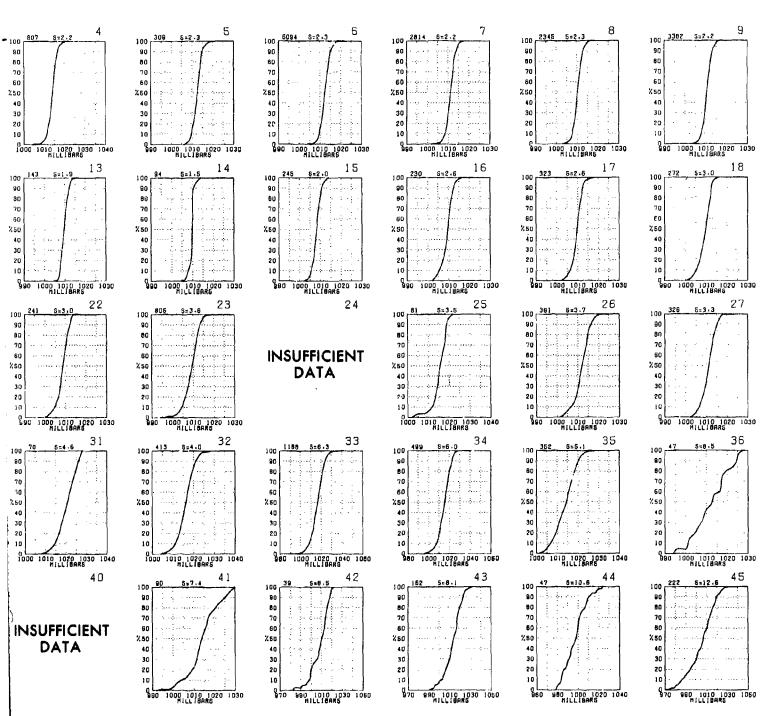
SEA LEVEL PRESSURE AND MEAN WIND



SEA LEVEL PRESSURE



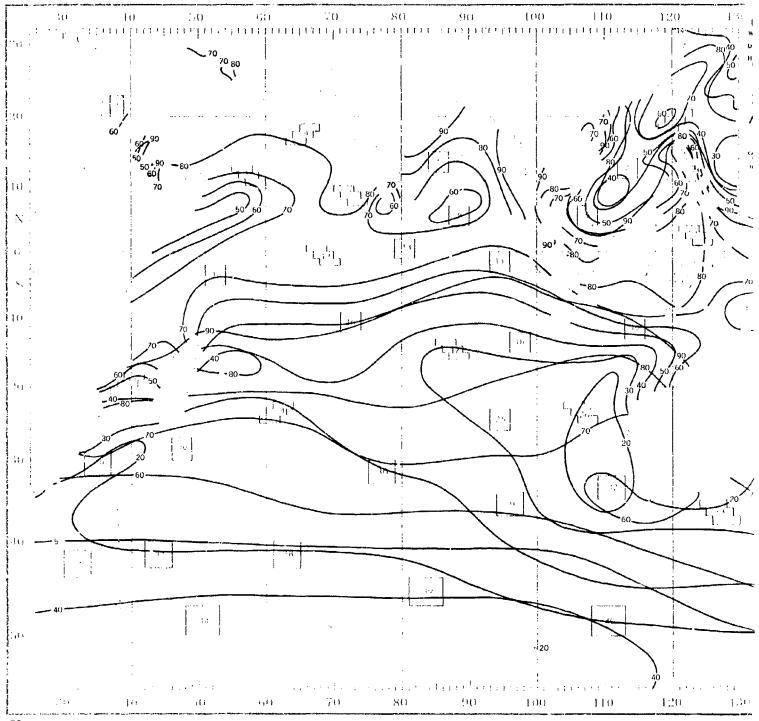
<u>Graphs</u> represent the objective compilation of available data for specified areas without The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjust



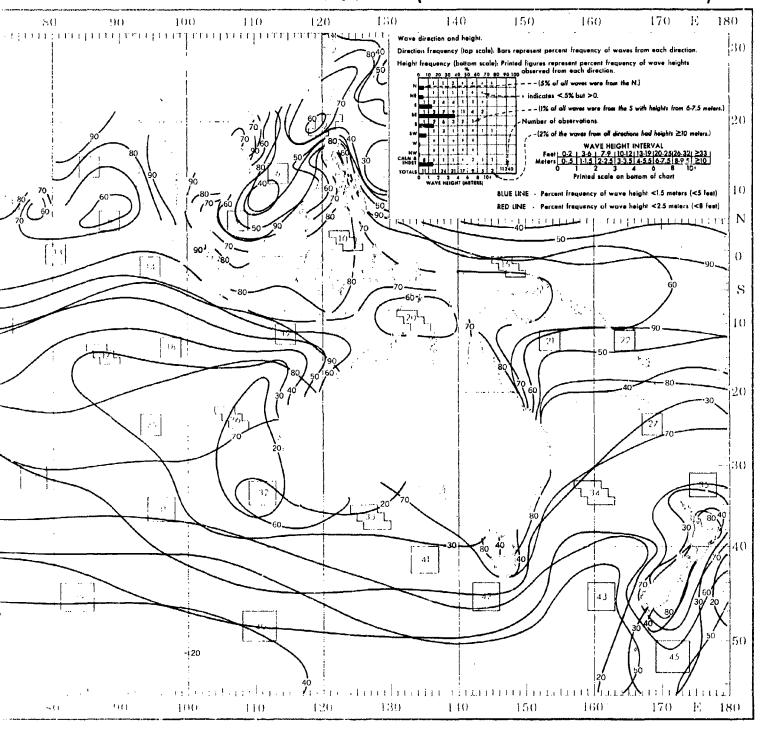
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Posite page) are based on all available data subjectively adjusted where bias was evident.

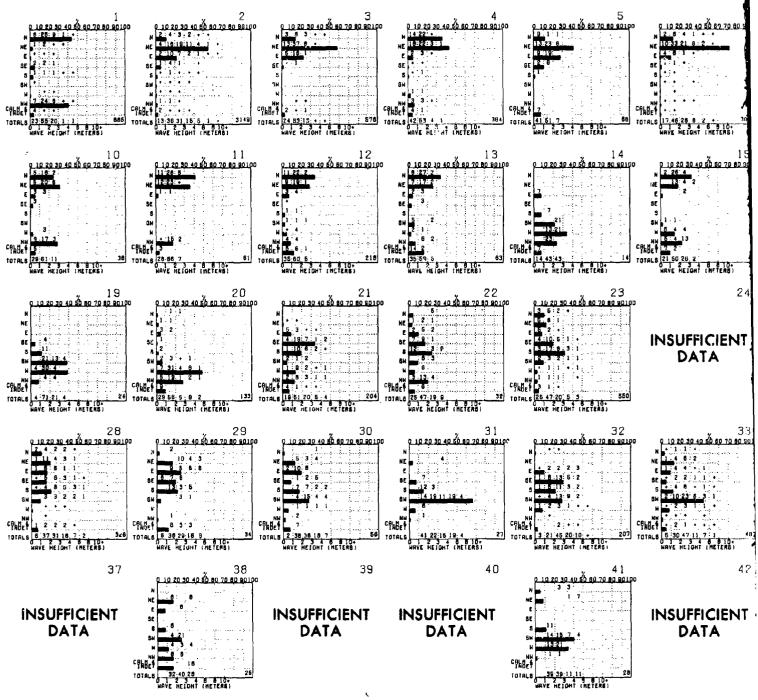
WAVES



WAVES (<1.5 AND <2.5 METERS)



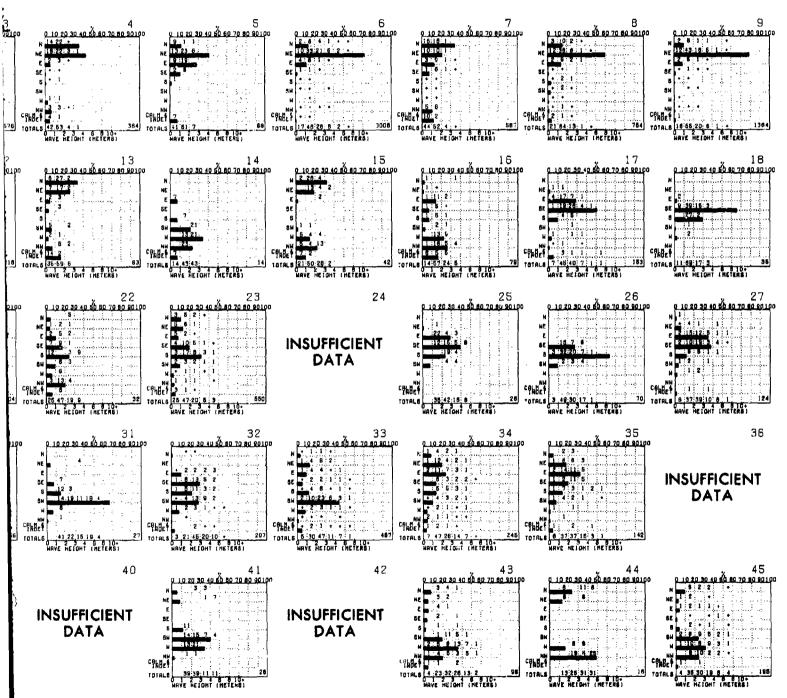
WAVE DIRECTION AND HEIGHT



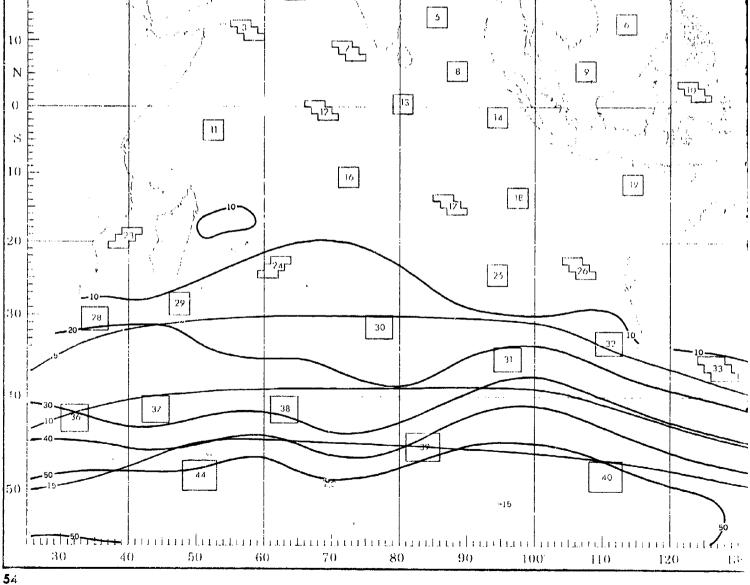
<u>Graphs</u> represent the objective compilation of available data for specified areas without re-The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjusted.

HGHT

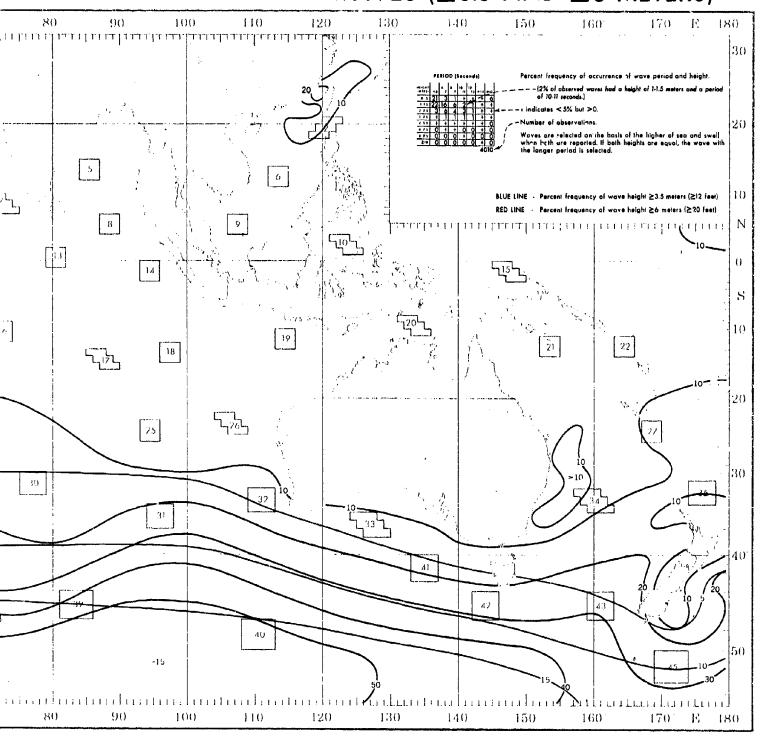
FEBRUARY



bjective compilation of available data for specified areas without regard to suspected biases. opposite page) are based on all available data subjectively adjusted where bias was evident.



WAVES (≥3.5 AND ≥6 METERS)



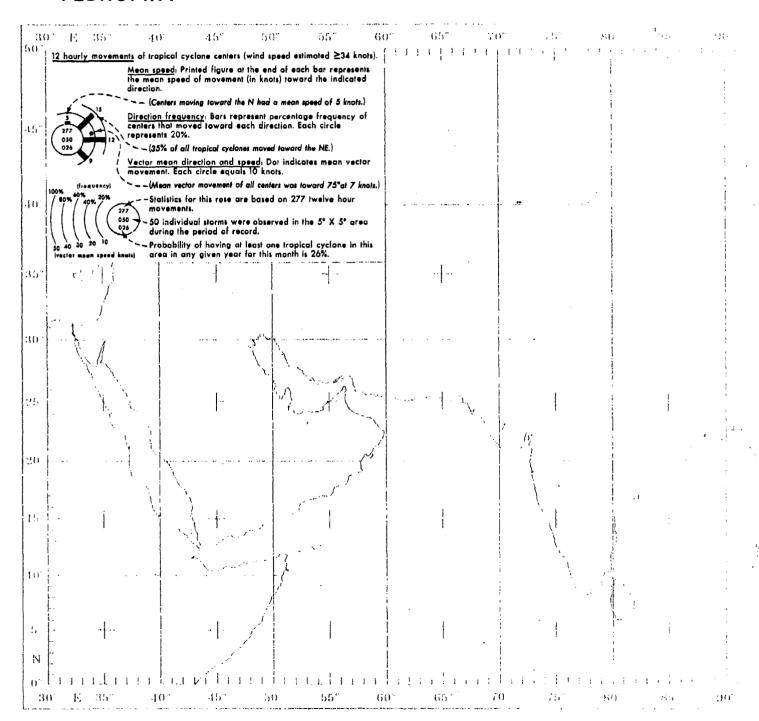
WAVE PERIOD AND HEIGHT

PERIOD I SECONDS 1	PERIOD (SECONDS) ***HEIGHT 6- 5- 18- 18- 18- (ATRES) 6- 7 6 18 18- 6- 5 1 1 - - 0 0 1-1-8 16 14 4 - - - 1-2-8 3 11 12 4 1 - 1-3-8 1 3 5 3 2 1 - 6-7-8 0 - - 1 1 1 1 - 6-7-8 0 0 - - - 0 318 0 0 0 0 0 0 3213	FREIOU (SECONDS) NELION 0 0 10 12 12 100 1 1 2 0 0 1 12 12 100 0 - 0 10 2 0 0 0 0 1 1 34 17 4 0 0 5 2 - 1 3 4 1 0 0 0 2 - 1 3 4 1 0 0 0 2 - 1 5 0 0 0 0 0 0 - 1 5 0 0 0 0 0 0 0 - 1 6 0 0 0 0 0 0 3 0 0 0 0 0 0 0 3 0 0 0 0 0 0 5 5 6 5 7 7 7 5 7 7 5 7 7 5 5	PERIOD (SECONOS) ***CLIGNT** ***INTRES** ***C. S. T. FERIOD (SECONDS) **ECONT 46	PERIOD (SECONU 6.7 8-16-11-1 0-6 15 2 - 0 0 1-1.6 21 16 5 - 0 2-8.3 3 9 10 3 3 - 0 2-8.6 0 2 3 2 1 1-1.5 2 1 1 1 1 1-1.5 0 0 0 0 0 0 1-1.6 0 0 0 0 0 0	
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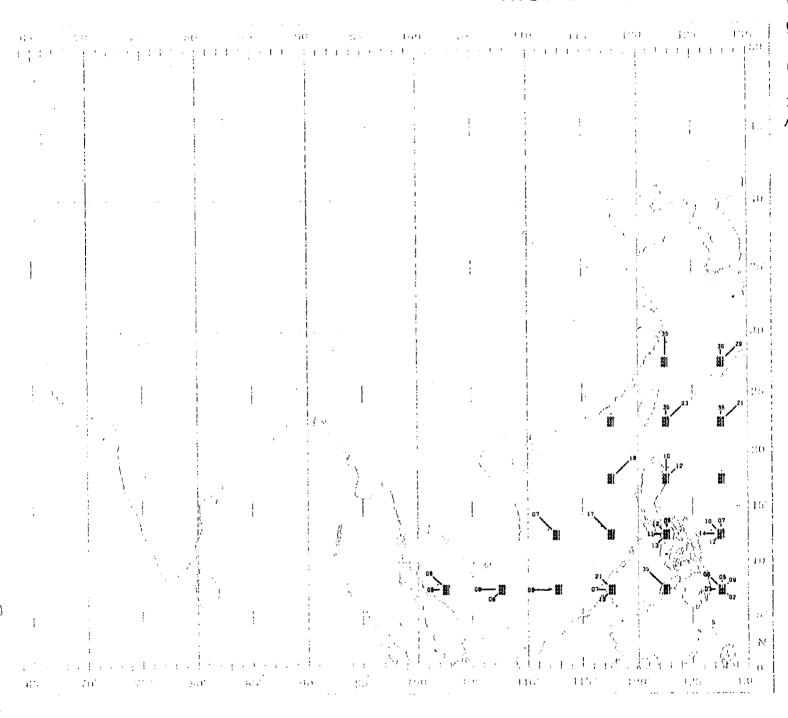
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### PERIOD (SECONDS) ***RIAN** ***	FERTION SECONDS	FERIOD ISECONOSI 10. 0. 10. 10. 10. 10. 10. 10. 10. 10. 1	7 PERIOD (SECONDS) PERIOD (8 PERIOD (SECONOS) SeconoS Se	9 PERIOD (SECONDS)
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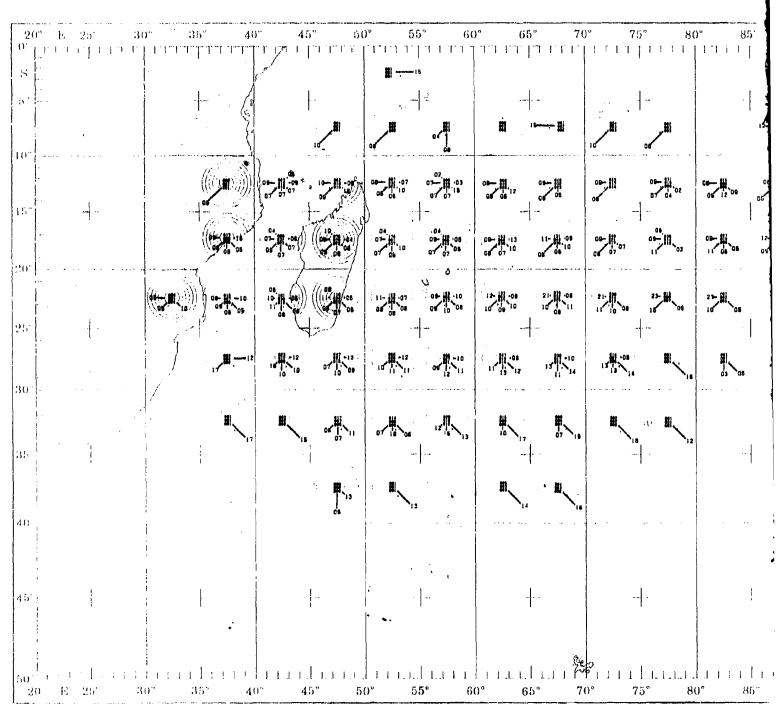
ctive compilation of available data for specified areas without regard to suspected biases, osite page) are based on all available data subjectively adjusted where bias was evident.



TROPICAL CYCLONE

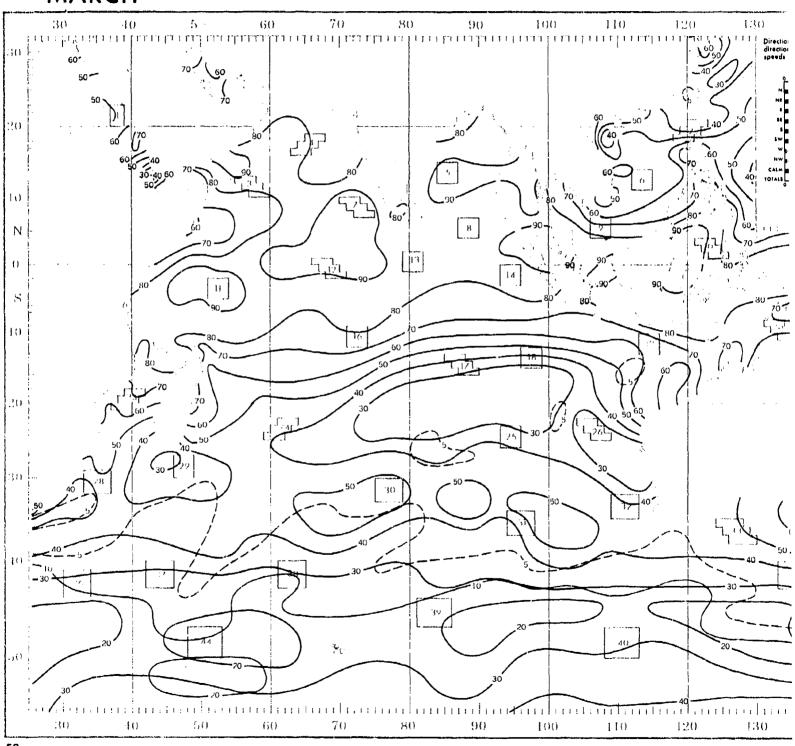


TROPICAL CYCLONE

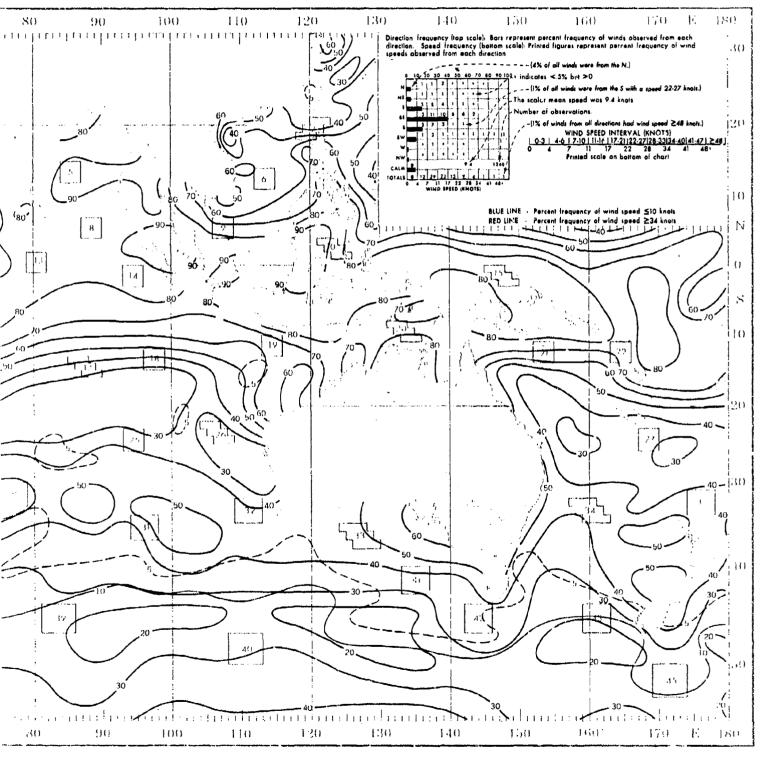


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09- HI -10	00-11-13 11-11-09 00-10-10	00-1111 00-1111 000	00-112 12-111-00 11 08 05 07 14 08	10-11 -05 05-11 04 11 07 05 15	14 00 10 10 00 00 00 00 00 00 00 00 00 00	05 08 07 09 H 07 15 08 07 08 08 08 08 09 08 08 09 08 08 09 08 08 08 08 08 08 08 08 08 08 08 08 08
04 10 04	12 H -00 21 H -00 11 10 00 11 10 00 11 11 10 11 11 11 1	21-11-10-08 18-09-11-11-11-11-11-11-11-11-11-11-11-11-11	05	13 or 06 11	0 0 0 10 0 15 11	07 H 07 H 08 H 08 H 08 H 08 H 08 H 08 H
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t	II . II . II			Mean s ihe me directio	speed: Printed figure at the e an speed of movement (in ki	and of each bar represents nots) toward the indicated d a mean speed of 5 knots.)
}	+			100% (frequency) (A 80% 20% 277 S 026 dd	15% of all tropical cyclones may mean direction and speed: tent. Each circle equals 10 k dean vector movement of all ce tatistics for this rose are bas- tovements. O individual storms were obsuring the period of record.	Dot indicates mean vector nots. nters was toward 75°at 7 knots.) 4 0 a d on 277 twelve hour
!!!!	0° 65° 7	0" 75" 80) 	(vactor mean speed knots) (I	rebability of having at least rea in any given year for th $105^{\circ}-1$	one tropical cyclone in this is month is 26%. 50° 10° 115° 120°

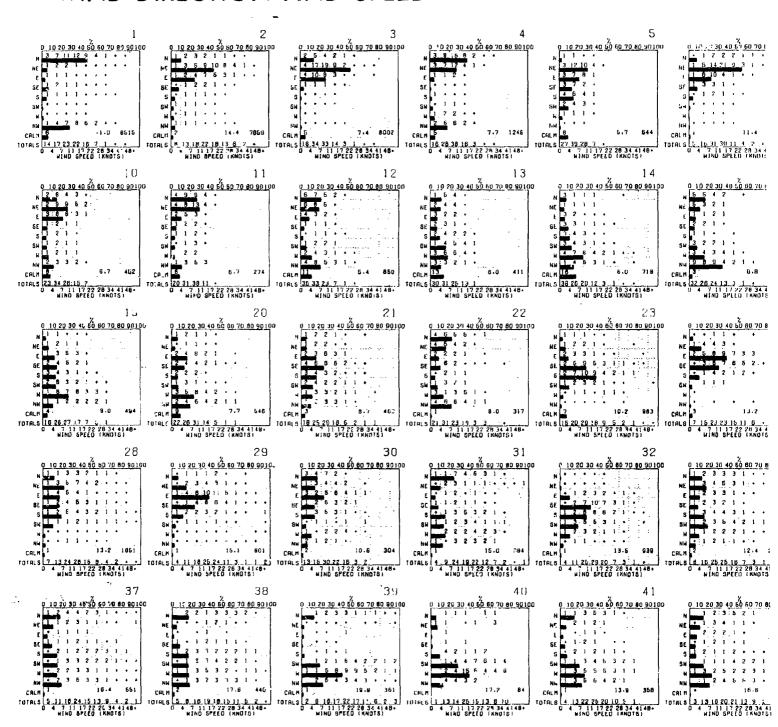
MARCH



SURFACE WINDS

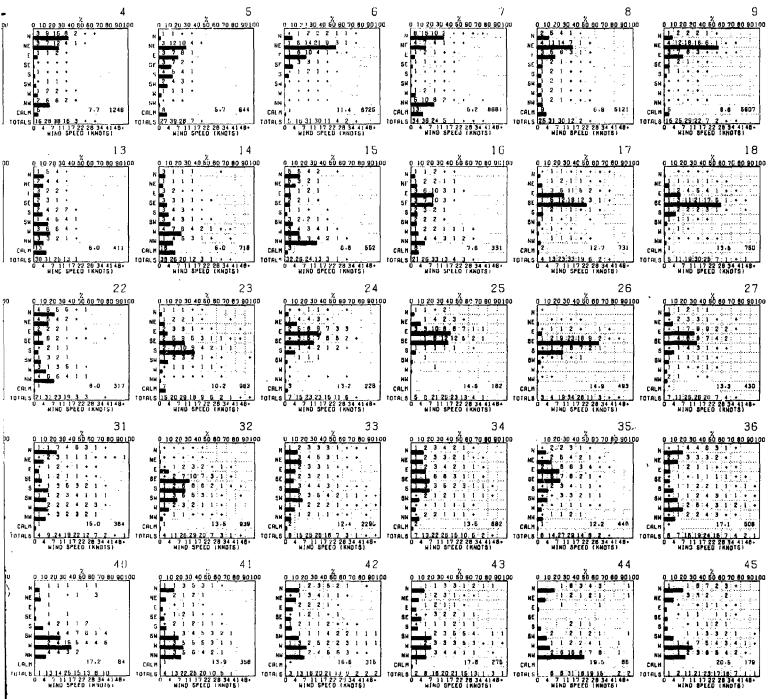


WIND DIRECTION AND SPEED



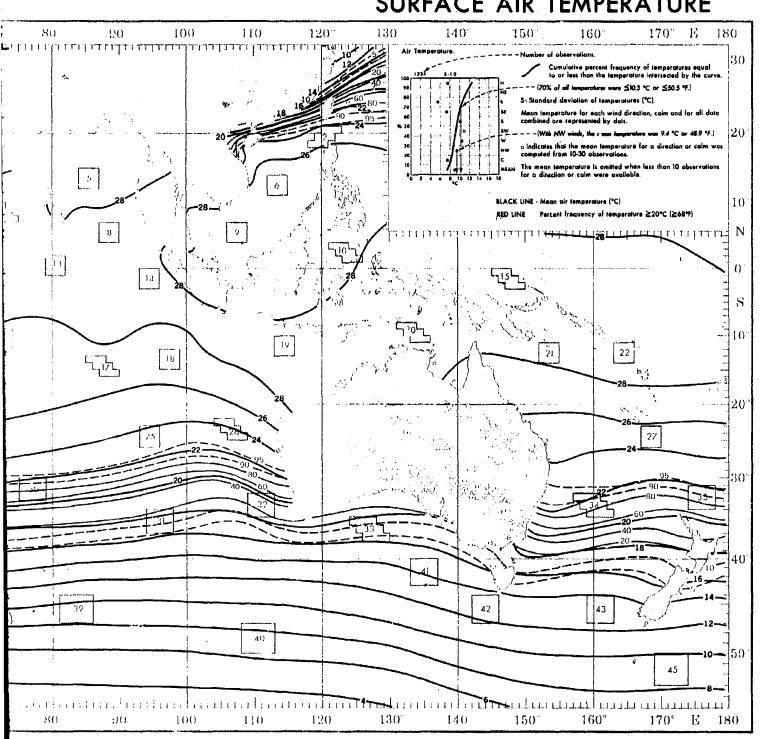
Graphs represent the objective compilation of available data for specified areas withou The isopleth analyses (opposite page) are based on all available data subjectively adju

MARCH

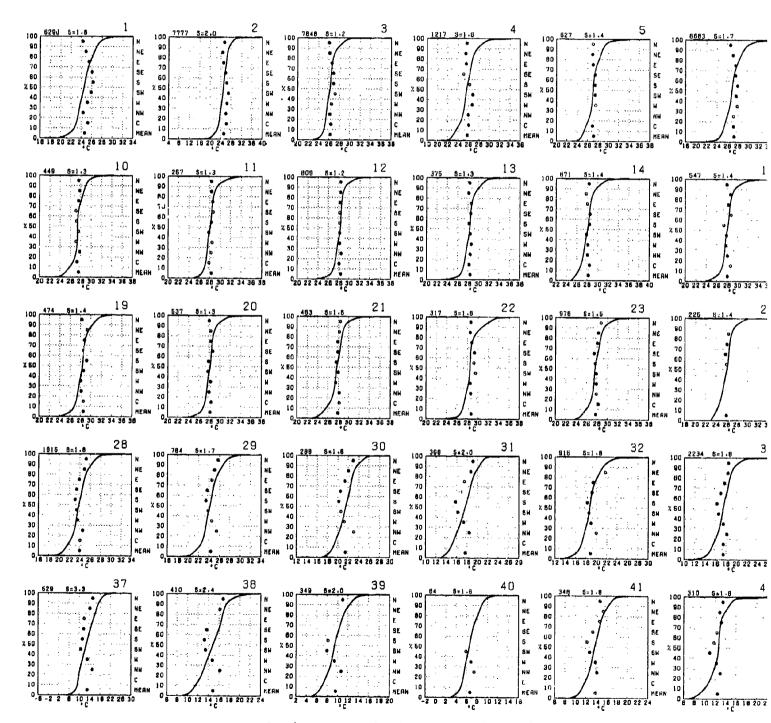


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SURFACE AIR TEMPERATURE

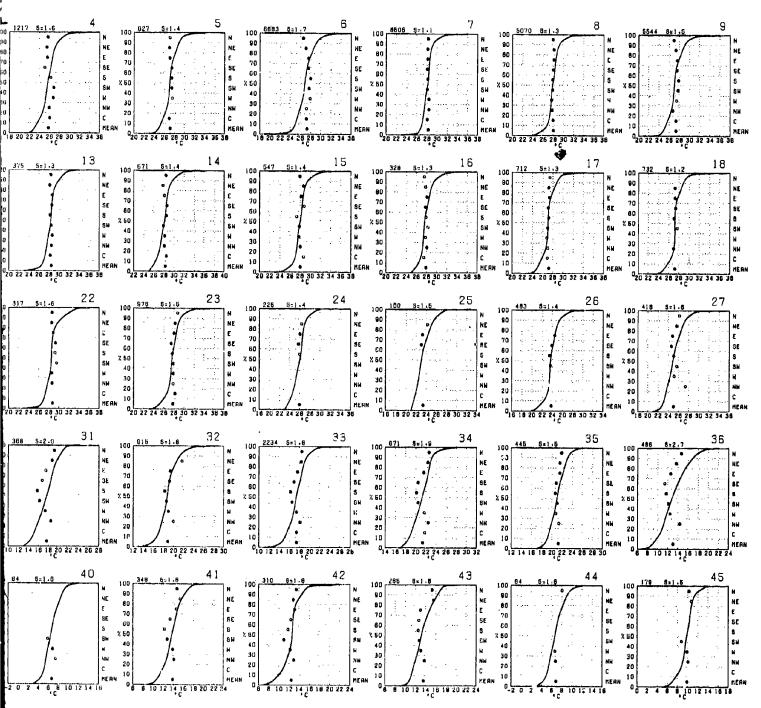


SURFACE AIR TEMPERATURE



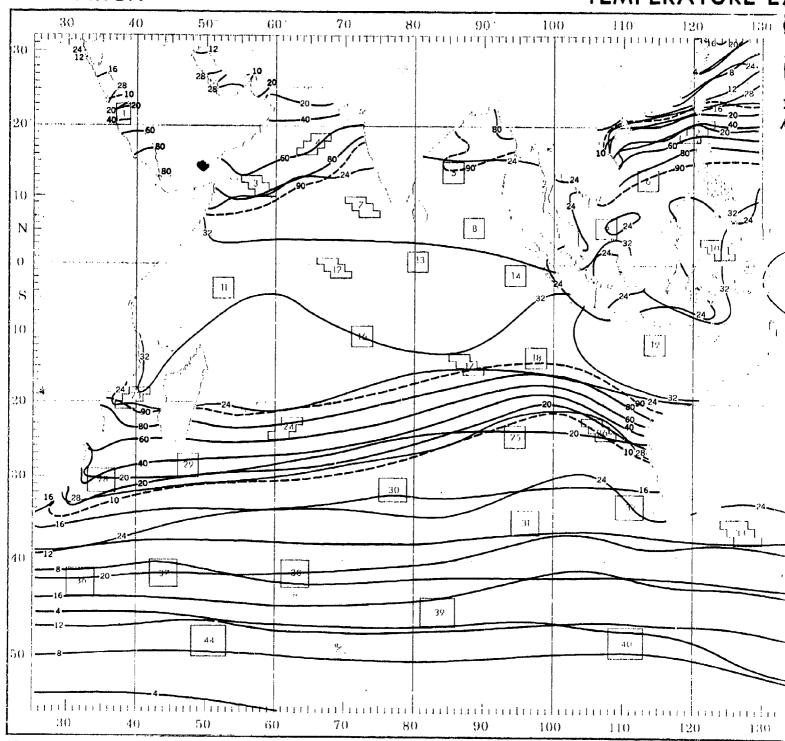
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MARCH

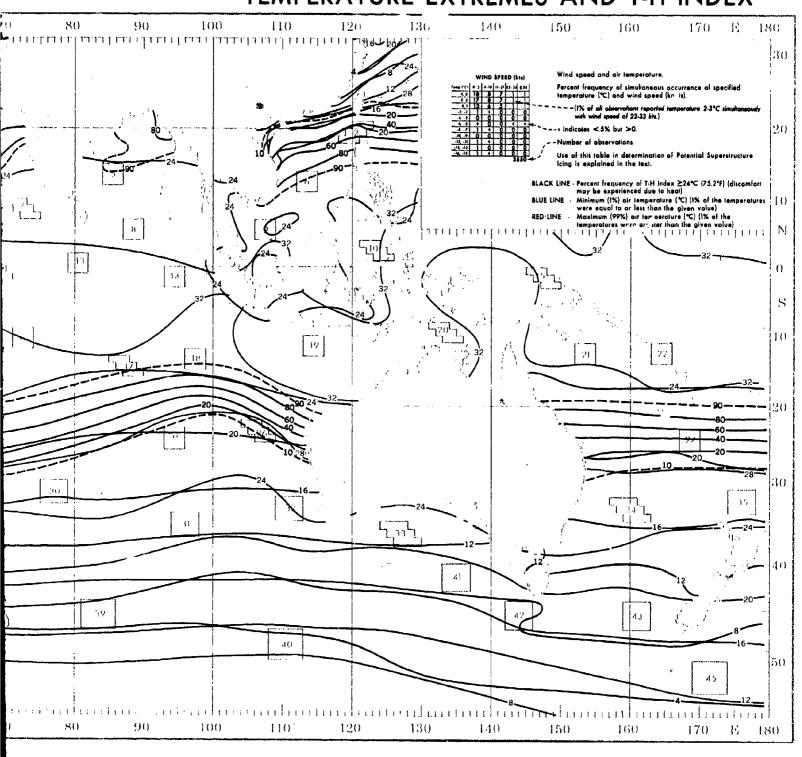


tive compilation of available data for specified areas without regard to suspected biases. ssite page) are based on all available data subjectively adjusted where bias was evident **MARCH**

TEMPERATURE E



TEMPERATURE EXTREMES AND T-H INDEX



WIND SPEED AND AIR TEMPERATURE

	·				
WIND SPEED (KTS)	HIND SPEED (KTS)	WIND SPEED (KTS) 3	HIND SPEED (KTS)	WIND SPEED (KTS)	WIND SPEED (K)
7EMP (*C) 0-9 4-10 11-21 22-33 = 34	TEMP (*C) 0-3 4-10 11-21 22-33 2 34		7LMP (*C) 0-3 4-10 11-21 22-33 2 34		
90,31 + + + 0 0	34.36 D + O O O 32.33 + + + O O	30.31 • 1 • 0 0 30.31 • 1 • 0 0	32.33 + + 0 0 0 0	38.53 1 + 0 0 0 30.31 2 2 0 0 0	34,35 + + + + 32.33 + 1 1
26.26 1 3 2 + 0 26.27 5 12 7 1 +	20.20 2 6 3 1 +	28.28 3 10 2 + +	28.29 2 8 2 0 0 26.27 6 29 7 0 0	28.29 10 22 2 0 0 28.27 13 38 4 0 0	30.31 + 4 3 20.20 2 16 32
24.28 6 18 17 4 + 22.29 2 6 11 3 +	28.27 3 14 14 3 + 24.26 2 9 15 6 1	#4.25 3 14 5 + 0 #2.29 + + + 0 D	24.26 6 24 8 + 0 22.23 1 3 1 0 0	24.23 0 0 0 0 0	24.25 + 3 4
80.81 + 1 2 + 0 10.10 + + + 0 0	21.23 + 1 B 6 1 20.21 + + 1 1 +	10,11 0 0 0 0 0	20.21 0 + 0 0 D	10.11 0 0 0 0 0	22.23 0 4 4
18.17 0 0 0 0 0 14.18 0 0 0 0 0	10.10 + + + + +	16-17 0 0 0 0 0 0 14-15 0 0 0 0 0	10-17 0 0 0 0 0 14-10 0 0 0 0 0	10.17 0 0 0 0 0	18,19 0 0 0
18.19 0 0 0 0 0	18.17	it. 1 0 0 0 0 D	12.13 0 0 0 0 0	12.13 0 0 0 0	16.17 0 0 0 14.18 0 0 0
	1 1	7868 HIND SPEED (KTS) 12	1226	1 /	
HIND SPEED (KTS) 10	MIND SPEED (KTS) 11	HIND SPEED (KTS) 12			MIND SPEED (K1
16HF (*C) 0-3 4-10 11-21 22-53 2 34 32:39 + 1 0 0 0 0	TEMP (*C) 0-3 4-10 11-21 22-33 2 34	32.33 + + + 0 0	72.39 1 1 + 0 0	TEMP (*C) 0-3 4-10 11-2122-39 24	92.33 2 1 0
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20,27 10 26 7 0 0 24,26 1 3 + 0 0	24,28 + 0 0 0 0	26.27 6 8 2 0 0	\$8.27 5 9 3 0 0 24.28 + 1 0 0	20.29 20 29 8 + 0 20.27 8 10 5 1 0	20.27 8 15 5
22.23 0 0 0 0	98.63 0 0 0 0 0	20,20 0 0 0 0 0	22.23 0 0 0 0 0	26.28 + 1 + 1 + 27.29 0 0 0 0 0	0 0 0 0
10.10 0 0 0 0	18.19 0 0 0 0 0	10.10 0 0 0 0	10-10 0 0 0 0	20.21 0 0 0 0 0	19-19 0 0 0
18:17 0 0 0 0 0 0 14:18 0 0 0 0 0 0 12:18 0 0 0 0 0	14.15 0 0 0 0 0 0 14.15 0 0 0 0 0	10-17 0 0 0 0 0 14-16 0 0 0 0 0	18:17 0 0 0 0 0 0 14:18 0 0 0 0 0	10.10 0 0 0 0 0 0 10.17 0 0 0 0 0 0 14.15 0 0 0 0 0	16,17 0 0 0 16,18 0 0 0
12:19 0 0 0 0 0 450	18.19 0 0 0 0 0 0 271	12.15 0 0 0 0 0 823	18-19 0 0 0 0 0 0 375	14,18 0 0 0 0 0	12.15 0 0 0
HIND BPEED (KTB) 19	HIND SPEED (KIS) 20	HIND SPEED (KTS) 21	HIND SPEED (KTS) 22	HIND SPEED (KTS) 23	WIND SPEED (KI
TEMP (40) 0-9 4-10 11-21 22-33 5 34	TENF (4C) 0-5 4-10 11-21 28-33 2 34	IEMP (*C) 0-3 4-10 11-21 22-38 a 94	TEMP (*C) 0-9 4-10 11-21 22-39 a 24	TEMP (PC) 0-3 4-10 11-21 22-33 2 54	TEMP (4C) 0-9 4-10 11-21
38:38 1 2 1 0 0 30:31 4 9 3 + 0	30.31 2 7 2 0 0	34.36 + 0 0 0 0 37.33 1 1 + 0 0	94.98 + + 0 0 0 0 98.98) 5 0 0 0	36,38 + + 0 0 0	\$0,31 0 0 + 20,28 + 4 7
28:29 9 33 16 4 0 28:27 2 8 5 2 0	20.29 14 38 12 1 0 26.27 4 11 4 1 0	10.31 3 3 3 + 0 20.20 8 32 13 2 0	90,31 B 9 3 0 0 89,88 13 30 13 2 +	30.31 3 5 1 + 0 20.26 10 24 9 2 0	26.27 3 24 21 24.28 2 10 10
24.25 O 1 + O O	##.## 1 1 + 0 0 ##.## 0 0 0 0 0	20.27 B 14 7 1 1 24.28 • 3 1 • 0	28.27 1 10 4 1 0	26,27 3 17 14 4 1 24,26 + 1 1 1 +	22.63 + 0 0 20.21 0 0 0
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14.14 0 0 0 0 0 18.13 0 0 0 0 0	14.16 0 0 0 0 0 18.19 0 0 0 0 0	16.17 0 0 0 0 0 14.15 0 0 0 0 0	10.17 0 0 0 0 0 0 14.18 0 0 0 0 0	14.14 0 0 0 0 0 0	18.19 0 0 0
478 28	538 20	458 역미	319	1005	
HIND SPEED (KTS) 28	HIND SPEED (KTS) 29	HIND SPEED (KTS) 30	HIND SPEED (KTS) 31	HIND SPEED (KTS) 32	NING SPEED (KT
20.21 + + 0 + 0	30.91 + + + 0 0	28.27 0 1 0 0 0	22:23 1 1 1 0	28.27 0 + 0 0 0	24.25 0 + +
20.20 1 1 1 + 0	28.29 + 2 2 + 0	24.28 3 8 2 + 0 27.23 6 15 17 1 0	80.81 1 7 5 2 0 10.18 1 12 17 7 1	24.28 + + 1 0 0 22.23 + 3 3 1 0	20.21 1 4 5
24.25 3 15 18 4 1 28.23 2 12 12 4 1	24.85 2 12 23 7 1 22.23 1 5 13 4 1	20.21 2 18 12 1 0 19.10 1 5 5 3 0	10.17 2 11 12 6 1 14.18 • 4 6 2 1	20,21 1 8 11 2 + 18,19 2 17 24 5 1	18.19 9 14 18 18.17 3 16 14
20.21 + 2 2 1 1 10.10 0 + + 0 0	20.21 0 1 1 1 1 10.19 0 0 0 0 0	18.17 + 0 1 0 0	18:13 1 0 1 0 0	16,17 1 5 9 2 + 14,18 + + 1 + +	14.18 1 4 5
18:17 0 0 0 0 0	10,17 0 0 0 0 0	12.13 0 0 0 0 0	9.0 C O O O O	12.13 0 + 0 0 0	10.11 0 + 0
12.19 0 0 0 0 0	18.13 0 0 0 0	0.0 0 0 0 0	4.6 0 0 0 0	0 0 0 0 J	6.7 0 0 0
16,11 0 0 0 0 0	10.11 D D D D 784	8.7 0 0 0 0 0 289	2.3 0 0 0 0 0 369	8.7 0 0 0 0 0 0 917	4.8 0 0 0
HIND SPEED (KTS) 37	WIND SPEED (KIS) 38	MIND SPEED (KTB) 39		HIND SPEED (KTS) 41	NIND SPEED INT
1EHP [40] 0-3 4-10 11-21 22-33 a 34		TEHP 1'C) 0-9 4-10 11-81 28-33 & 34	1EMP (4C) 0-3 4-10 11-2) 22-35 h 34		
\$0.81 0 + 1 1 0	22.23 0 0 + 0 0 20.21 + 1 0 1 0	14.18 0 0 3 1 0 12.13 + 3 6 5 1	70 ₄ 11 0 2 0 1 0 0.8 1 14 8 5 0	10,10 1 2 1 + C 10,17 + 5 7 2 C	20.21 0 + 0
18.16 + 2 5 1 1 18.17 2 3 5 4 1	18.17 1 8 10 8 3	10.11 0 7 13 7 3 0.0 2 9 13 10 9	6.7 0 11 24 8 6 4.6 0 0 8 7 4	14.18 1 16 20 4 0	19.19 0 0 0
14-15 + 7 8 3 1 12-19 1 5 9 4 1	14.15 2 B 10 4 1 12.13 1 B 9 5 1	0.7 0 1 4 5 3 4.6 0 0 1 + +	7.3 U 0 0 0 0 0.1 0 0 0 0 0	10.11 + 2 5 1 + 8.8 0 0 + 0 0	14.18 + 6 10 12.13 1 16 24
10.11 1 7 6 5 1 6.8 1 3 5 4 1	19:11 0 + 3 Z + 0:0 0 0 + 0 +	8.3 0 0 0 0 0 8.1 0 0 0 0 0	-2:-1 0 0 0 0 0 0 -4:-3 0 0 0 0 0	#.P 0 0 0 0 0 4.B 0 0 0 0 0	10.11 1 4 5 0.0 1 • 2
6.7 + 1 + 1 + 4.8 0 0 0 0 0	6.7 0 0 0 0 0 4.6 0 0 0 0 0	-11 0 0 0 0 0 -13 0 0 0 0 0	-0,-6 0 0 0 0 0	2.5 0 0 0 0 0	0.7 0 0 0
2.3 0 0 0 0 0	2.3 0 0 0 0 0	-00 0 0 0 0	-109 0 0 0 0	-11 0 0 0 0 0	2.3 0 0 0 2.3 0 0 0
529	410	349	84.	348	

<u>Graphs</u> represent the objective compilation of available data for specified areas with The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively as

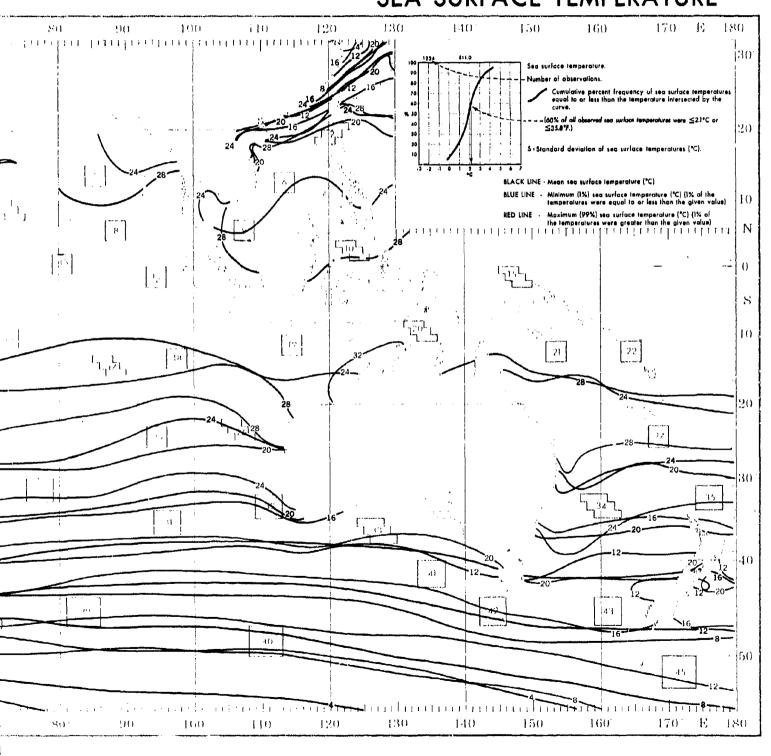
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MARCH

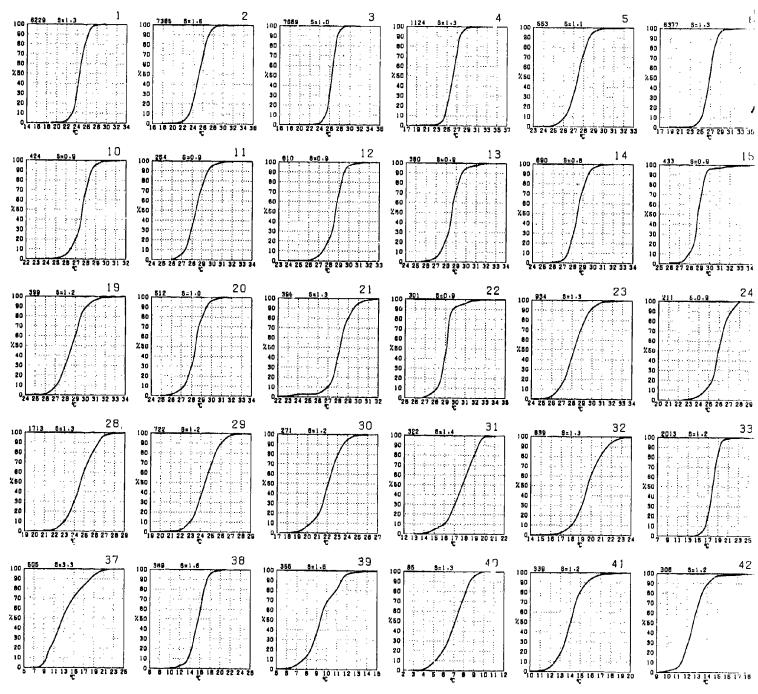
į					
- HIND SPEED (KTS) 4	HIND SPEED (KTB)	WIND SPEED (KTS)	WIND SPEED (KIS)	WIND SPEED (KTS) 8	MIND SPEED (KTS)
	TEMP (-C) 0-3 4-10 11-21 22-33 > 34		TEMP (4C1 0-3 4-10 11-21 22-33 3 34		TEMP (*C) 0-3 4-10 11-21 22-39 6 34
2.33 + + 0 0 0	38.33 1 + 0 0 0	34,36 + + + 0 0	34,36 + + + 0 0	34.35 0 0 0	36.37 0 + 0 + 0
0.31 • 1 • 0 0 8.29 2 8 2 0 0	90.31 Z 2 0 0 0 80.20 10 22 Z 0 0	38.33 + 1 1 + 0	32.33 + 1 + 0 0 30.31 4 6 1 0 0	32.33 • 1 • 0 0 30.31 2 6 1 0 0	34.35
4.27 6 29 7 0 0	26.27 13 38 4 0 0	20.20 2 16 12 1 0	20.20 23 43 4 + +	29.29 16 37 8 + 0	30.31 1 4 2 + 0
1.25 6 24 B + 0 2.25 1 5 1 0 0	22.83 0 0 0 0 0	#8:27 2 23 20 3 + #4:28 + 3 4 2 +	26.27 7 11 1 + 0	26.k7 7 15 3 + 0 24.25 + 1 + 0 0	28.29 6 21 9 + 0
0.21 0 + 0 0 0	E0.81 0 0 0 0	22.23 O + + + O	\$8.83 U + O O O	\$2.23 D + O O O	24,25 1 2 2 + +
0.10 0 0 0 0 0 0.17 0 0 0 0 0 0	19.19 0 0 0 0 0	10.10 0 0 0 0 0	20.21 0 0 0 0 0	10.10 0 0 0 0	##: ## + + + D
1.15 0 0 0 0 0	14.18 0 0 0 0 0 0 18.13 0 0 0 0 0	16.17 0 0 0 0 0 0 14.15 0 0 0 0 0	18-17 0 0 0 0 0 0 14-18 0 0 0 0 0	18-17 0 0 0 0 0 0 14-15 0 0 0 0 0	18-19 0 0 0 0 D 19-17 0 0 0 0 0
2.13 0 0 0 0 0	12.13 0 0 0 0 0	6585	8537	14.15 0 0 0 0 0 0 5094	5551
HIND SPEED (KTS) 13	HIND SPEED (KTS) 14	HIND BPEED (KTB) 15	HIND SPEED (KTS) 16	HIND SPEED (KTS) 17	HIND SPEED (KTS) 18
HIND SPEED (KTS)		TEMP (*C) 0-3 4-10 11-21 22-23 1 34	HIND SPEED (KTS)		TEMP (*C) 0-3 4-10 11-21 22-33 2 34
1.33 1 1 + 0 0	34.36 + + 0 0 0	32.53 2 1 0 0 0	38.93 1 1 + 0 0	38.35 0 + + 0 0	32.33 0 + 0 0
P-31 5 10 3 0 0	92.33 1 1 0 0 0	30.31 3 2 1 + 0	30.31 2 5 1 0 0	30.31 + 2 2 + 0	30,31 1 1 2 + 0
1.29 18 37 B O O	30.51 7 6 2 0 0 \$0.20 20 29 6 + 0	29.28 19 30 11 1 0 28.27 8 15 5 1 0	28.29 11 33 9 1 0 88.27 9 17 5 2 0	26.27 3 20 31 4 +	#8.28 2 10 20 5 · #6.27 2 18 30 4 1
125 + + 1 0 0	26,27 8 10 5 1 0	74.86 + 2 0 0	24.26 O 1 1 0 Q	24.26 1 9 2 1 +	84.25 + 2 2 + 0
1.23 0 0 0 0 0	29.23 0 0 0 0	20.21 0 0 0 0 0	88.83 0 0 0 0 0 80.81 0 0 0 0 0	20.21 0 0 0 0 0	0 0 0 0 0 0
0 0 0 0 0	20.21 0 0 0 0 0	19.18 0 0 0 0 0	10.10 0 0 0 0 0	18-18 0 0 0 0 0 0 18-17 0 0 0 0 0	10·10 0 0 0 0 0 10·17 0 0 0 0 0
0 0 0 0	18.17 0 0 0 0 0	14.35 0 0 0 0 0	14.15 0 0 0 0 0	14:15 0 0 0 0 0	14-18 0 D 0 D 0
13 0 0 0 0 0	14.15 0 0 0 0 0	12.13 0 0 0 0 0	18.19 0 0 0 0 0	18-19 0 0 0 0 0	38.13 0 0 0 0 0
. ,,,	23	2.4	25	26	37
HIND SPEED (KTS) 22	HIND SPEED (KTS) 23	HIND SPEED (KTS) 24	HIND SPEED (KTS) 25	HIND SPEED (KTB) 26	HIND SPEED (KTS) 27
	TEMP (*C) D-2 4-10 [1-2122-33 a 34			TEMP (*C) 0-3 4-10 11-81 88-99 a 94	
135 • • 0 0 0 133 1 5 0 0 0	34.38 + + 0 0 0 32.33 0 1 + 0 0	30,31 0 0 + 0 0 29,29 + 4 7 1 0	28.27 1 3 5 0 0 24.25 1 13 13 6 0	28-28 0 0 1 + 0	30.3i 0 + + 0 0 26.28 2 4 2 + 0
1.91 5 9 3 0 0	30.31 3 5 1 + 0	14.27 3 24 21 5 0	22.23 2 13 27 10 1	24.25 1 10 28 8 +	26.27 4 13 14 1 +
18 13 30 13 2 + 127 1 10 4 1 0	28.27 3 17 14 4 1	26.29 2 10 10 7 +	**************************************	28:83 1 10 24 7 0 20:21 0 1 2 + 0	24.26 1 15 23 8 0 22.23 0 5 G 1 0
.25 + + 1 0 0 .23 0 0 0 0 0	24.28 + 1 1 1 +	0 0 0 0 19.02 0 0 0 0 0 04.61	18.17 0 0 0 0 0 0 14.18 0 0 0 0 0	19-19 70 01 01 01	20.21 0 + 0 + + 10.10 0 0 0 0 0
iti 0 0 0 0	20-21 0 0 0 0	16.17 0 0 0 0 0	18.19 0 0 0 0	14-18 0 0 0 0 0	10.17 0 0 0 0
110 0 0 0 0 0 17 0 0 0 0 0	18-18 0 0 0 0 0 0 18-17 0 0 0 0 0	14.18 0 0 0 0 0 0 0 0 0 0 0	10.11 0 0 0 0 0 0.0 0 0 0 0 0	10-11 0 0 0 0 0	14-18 0 0 0 0 0 0 18-13 0 0 0 0 0
118 0 0 0 0	14.16 0 0 0 0	10.11 0 0 0 0 0	8.7 0 0 0 0 0	0.8 0 0 0 0	19-11 0 0 0 0
318	1005	225	160	463	418
HIND SPEED (KIS) 31		HIND SPEED (KTS) 33			HIND SPEED (HTG) 36
C) 0-3 4-10 11-2122-33 a 34	7EMP (*C1 0-3 4-10 11-2122-33 + 34	TEMP 1'C1 0-3 4-10 11-21 22-33 9 34		TENP (*C) 0-3 4-10 11-21 22-33 a 34	TEMP (*C) 0-3 4-10 11-21 22-33 5 34
23 1 1 1 1 0 21 1 7 5 2 0	28.27 0 + 0 0 0 24.26 + 1 0 0	24.25 0 + + + 0	26.27 1 1 + 0 0 24.28 1 4 4 1 0	26.27 0 1 1 0 0	20.21 0 1 1 + 0
10 1 12 17 7 1	28.23 + 3 3 1 0	20.21 1 4 5 1 4	22.23 3 14 17 4 +	22,25 2 13 17 2 0	18-17 1 4 8 2 +
17 2 11 12 6 1 18 · 4 6 2 1	19.10 2 17 24 5 1	10,17 3 18 14 4 +	18.18 1 6 7 4 •	18.10 + 6 3 1 0	12-15 1 7 11 5 1
13 1 0 1 0 0 11 0 0 0 0 0	18.17 1 5 9 2 ·	14.18 1 4 5 2 1 12.13 + 4 + +	18-17 0 + 1 + 0 14-18 0 0 0 0 0	16.17 0 0 + + 0 14.18 0 0 0 0 0	10.11 2 4 9 5 3 9.4 1 3 2 2 1
0 0 0 0 0	12.13 0 + 0 0 0	10.11 0 + 0 0 +	12.13 0 0 0 0	12.13 0 0 0 0 0	0.7 0 0 + + O
1.7 0 0 0 0 0 1.6 0 0 0 0 0	0 0 0 0 0 0 0	9.9 0 0 0 0 0 9.7 0 0 0 0 0	10-11 0 0 0 0 0 0 0-0 0 0 0 0 0 0	10.11 0 0 0 0 0 ••• 0 0 0 0 0	4.0 0 0 0 0 0 2.3 0 0 0 0 0
1.3 0 0 0 0 0	- •.• 0 0 0 0 0 0 •.7 0 0 0 0 0	4.5 0 0 0 0 0 4.6 0 0 0 0 0 0	0.0 0 0 0 0 0 0.7 0 0 0 0 0	0.0 0 0 0 0 0 0.7 0 0 0 0 0	0.1 0 0 0 0 0
369	917	2240	674	445	485
HIND SPEED (KTS) 40	HIND SPEED (KTS) 41	WIND SPEED (KTS) 42	HIND SPEED (KTS) 43	HIND SPEED (KTS) 44	HIND SPEED (KTS) 45
C1		TEMP (*C) 0-3 4-10 11-21 22-33 2 34		TEMP (*C1 0-8 4-10 11-21 22-98 a 54	7EMP (*G) 0-2 4-10 11-21 22-33 m 34
0 2 0 1 0 0 1 14 8 5 0	10.10 1 2 1 + 0	22 · 29 0 · 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	10,10 0 0 3 0 0	10:11 0 0 6 2 0 0.0 0 4 13 13 4	12.13 0 4 6 4 1 10.11 0 7 26 18 2
1.7 0 11 24 B 5	14.18 1 16 20 4 0	18.18 0 0 0 0 0 0 18.17 + 2 1 + 0	16,17 + 2 8 4 + 14,18 2 8 10 B 1 15,18 1 12 17 11 7	4.8 0 7 6 7 1	9.9 0 2 10 10 6 6.7 1 1 2 3 1
.3 0 0 0 0	12.13 1 13 11 5 1 10.11 + 2 5 1 +	14.16 + 6 10 3 1	18.19 1 12 17 11 Z 10.11 0 2 3 4 1	2.3 0 1 1 1 0	4.5 0 0 1 0 0
.i 0 0 0 0 0 0 0	6.8 0 0 + 0 0 6.7 0 0 0 0 0	12-13 1 16 24 15 1	8.9 0 + 0 + 0 8.7 0 0 0 0 0	0.1 0 0 0 0 0 -21 0 0 0 0 0	\$.8 0 0 0 0 0
1 1 -3 1 01 01 01 01 01	4.8 0 0 0 0 0	9.9 1 + 2 1 3	4.5 0 0 0 0 0	-4:31 01 01 01 0	-21 0 0 0 0
-8 0 0 0 0 0 0 -7 0 0 0 0 0	2,3 0 0 0 0 0 0 0.1 0 0 0 U 0	4.8 0 0 0 0 0	2.9 0 0 0 0 0 0.1 0 0 0 0 0	-0 -8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-43 0 0 0 0 0 0 -68 0 0 0 0 0
-9 0 0 0 0	-t1 0 0 0 0 0	2.3 0 0 0 0 0	-21 0 0 0 0 0	-100 0 0 0 0	-9,-7 0 0 0 0 0
84	348	310	266	84	179

ve compilation of available data for specified areas without regard to suspected biases. The page) are based on all available data subjectively adjusted where bias was evident.

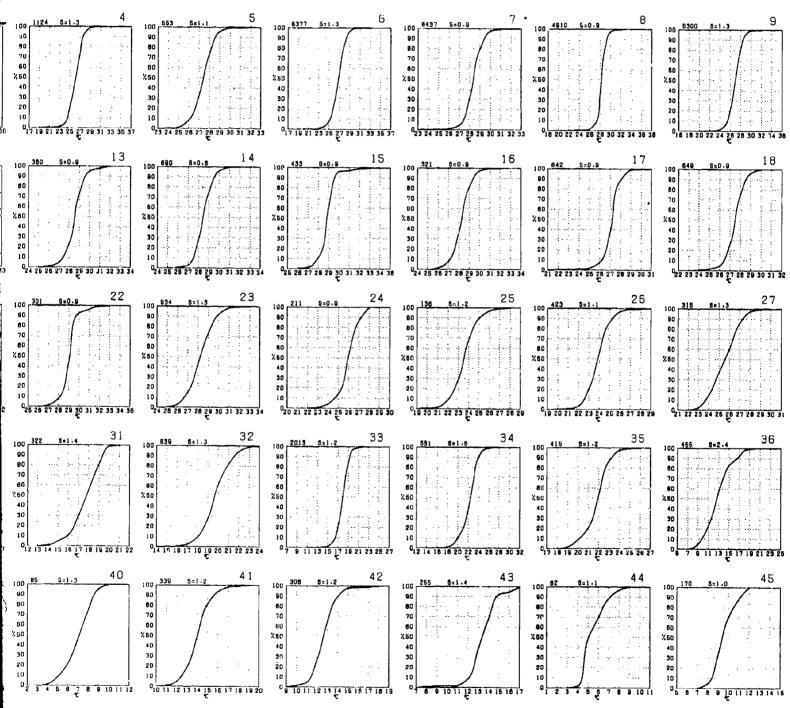
SEA SURFACE TEMPERATURE



SEA SURFACE TEMPERATURE

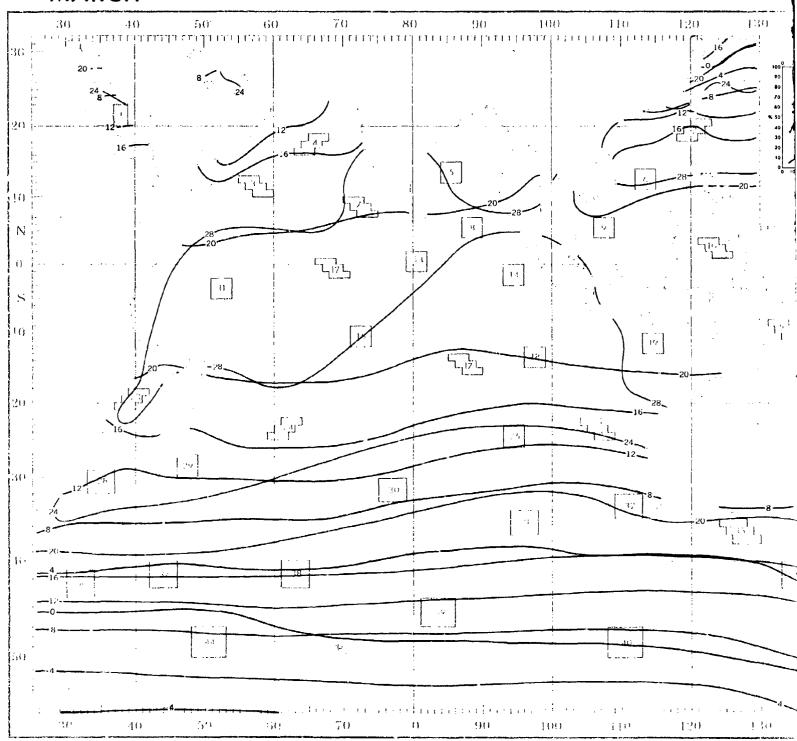


Graphs represent the objective compilation of available data for specified areas without the isopleth analyses (opposite page) are based on all available data subjectively adjust

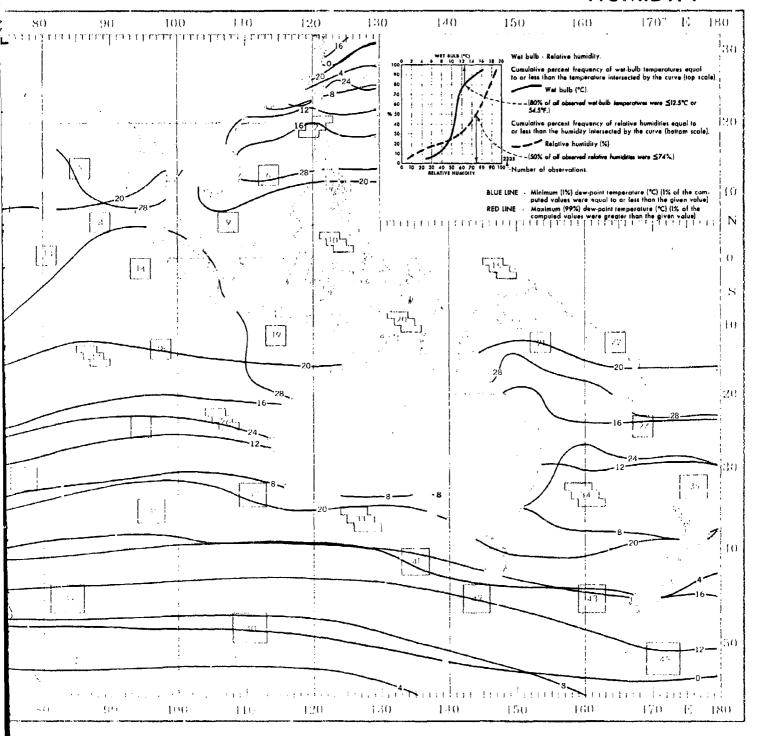


ejective compilation of available data for specified areas without regard to suspected biases.

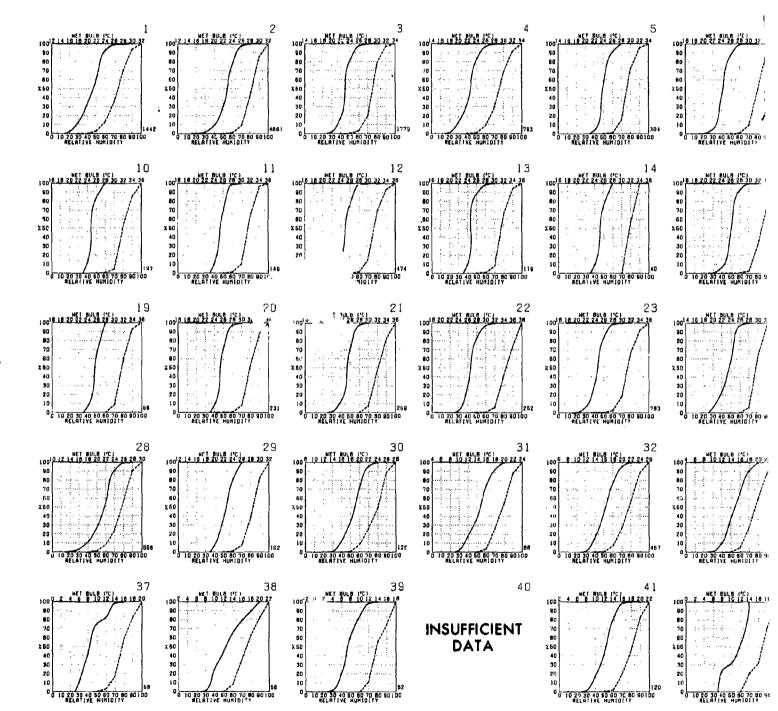
pposite page) are based on all available data subjectively adjusted where bias was evident.



HUMIDITY



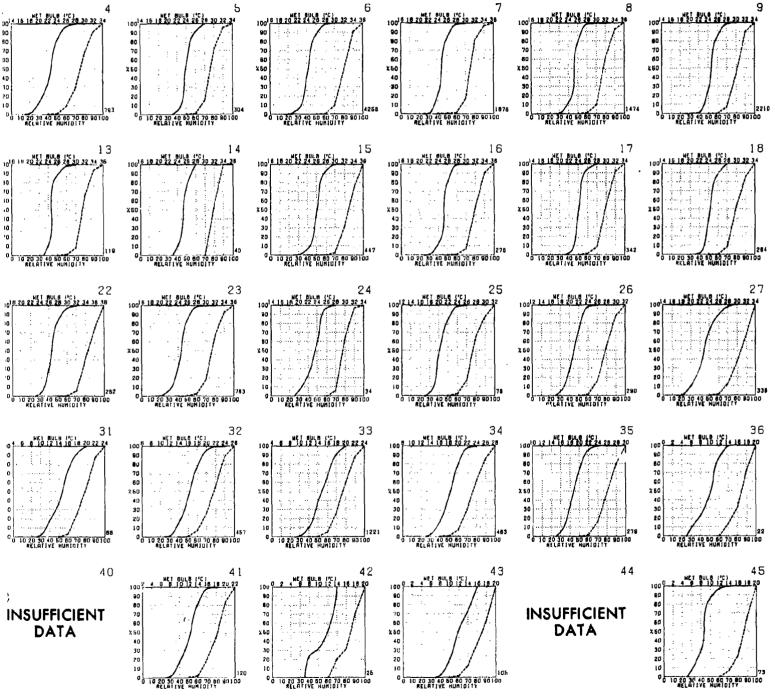
WET BULB AND RELATIVE HUMIDITY



<u>Graphs</u> represent the objective compilation of available data for specified areas without The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adj

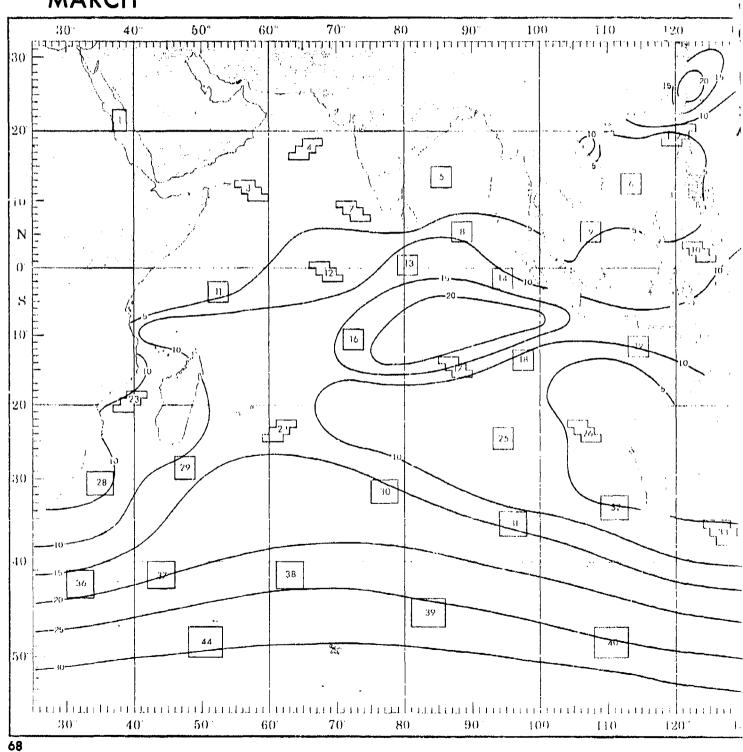
MIDITY

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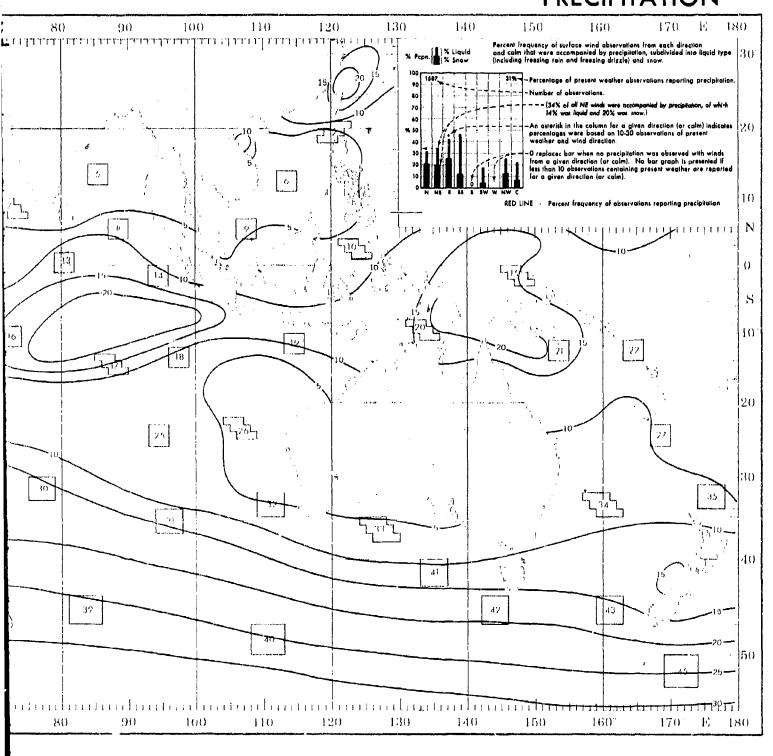


ctive compilation of available data for specified areas without regard to suspected biases.

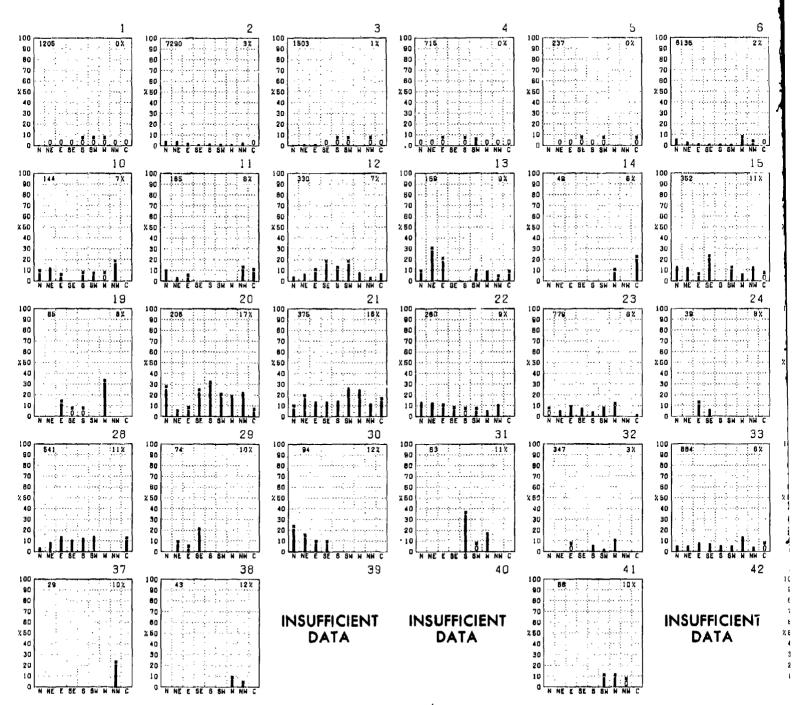
osite page) are based on all available data subjectively adjusted where bias was evident.



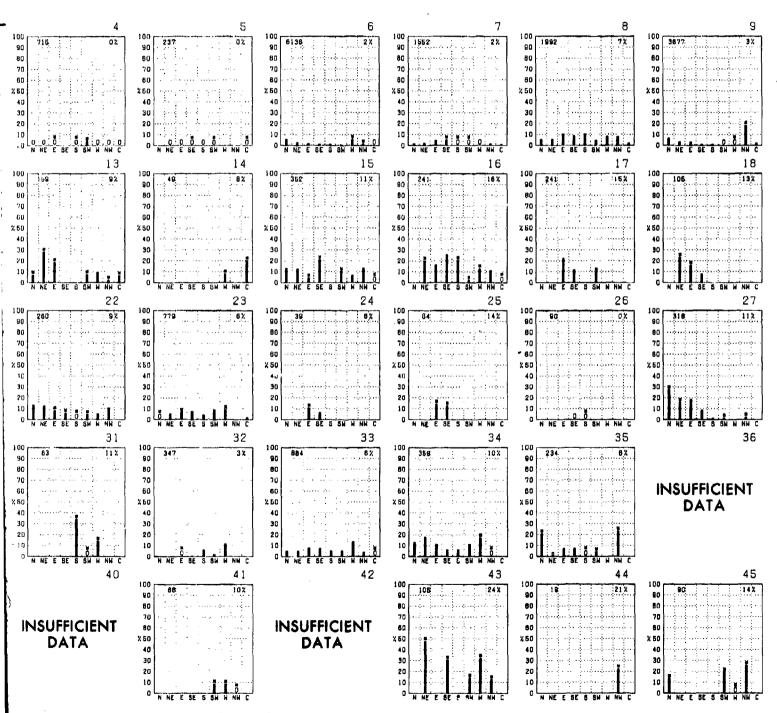
PRECIPITATION



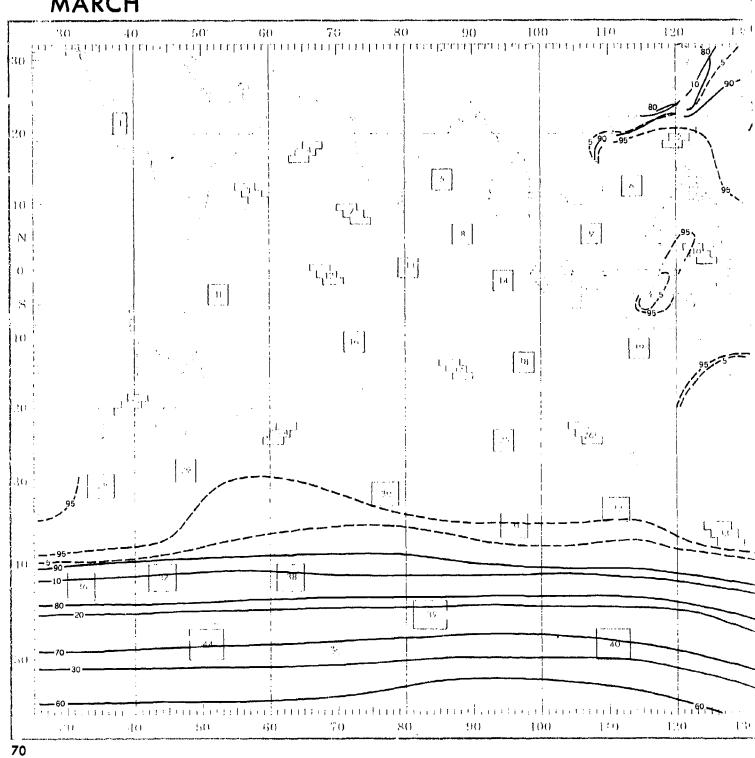
PRECIPITATION



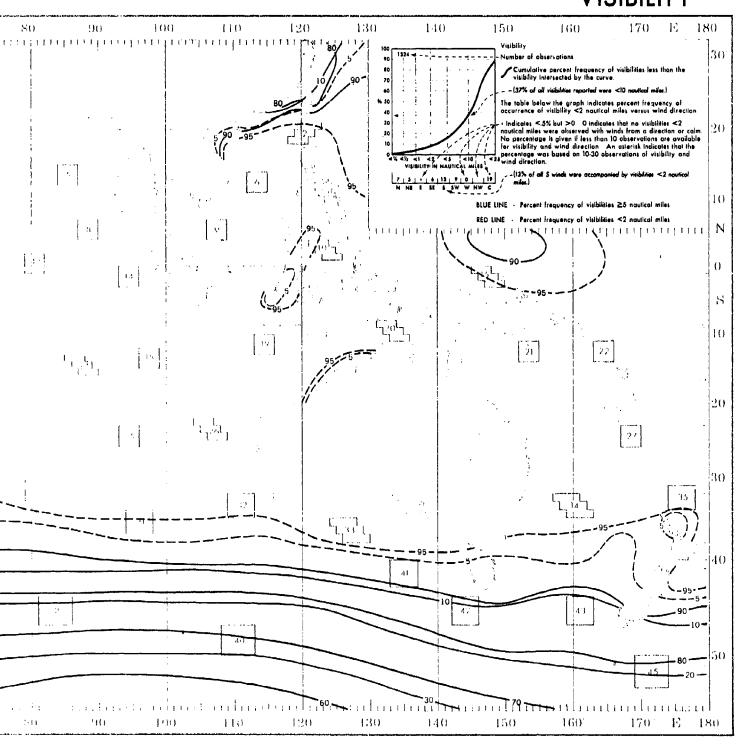
Graphs represent the objective campilation of available data for specified areas without regar. The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjusted w



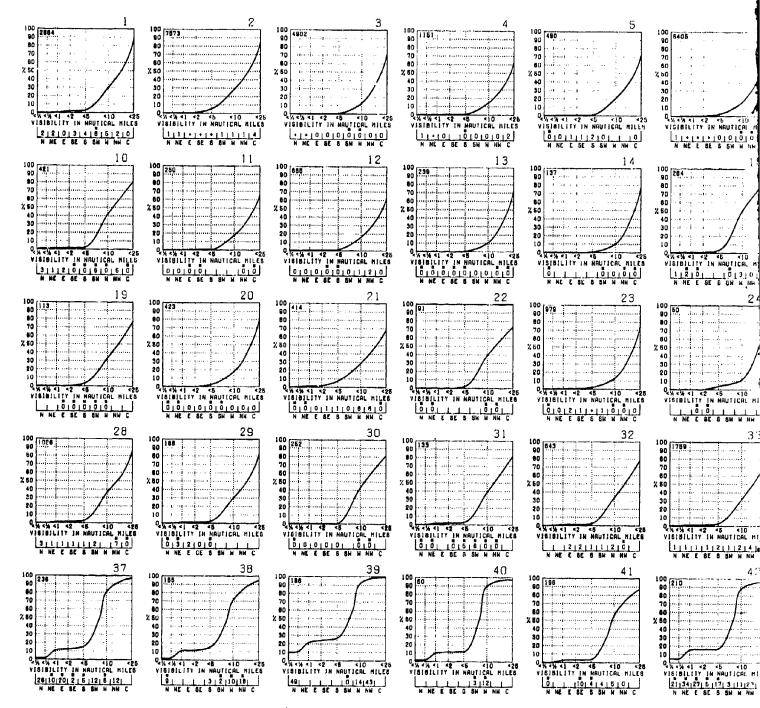
ective compilation of available data for specified areas without regard to suspected biases. posite page) are based on all available data subjectively adjusted where bias was evident.



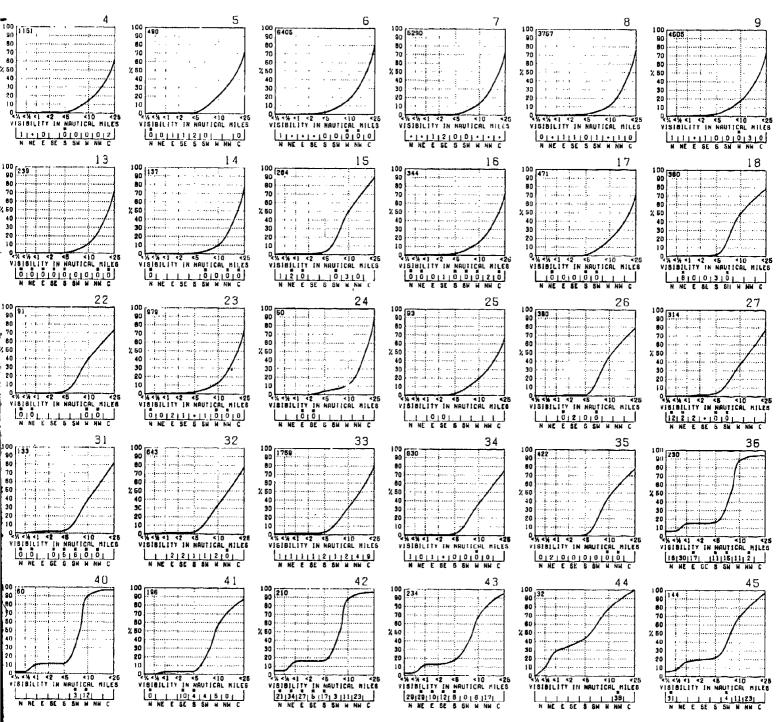
VISIBILITY



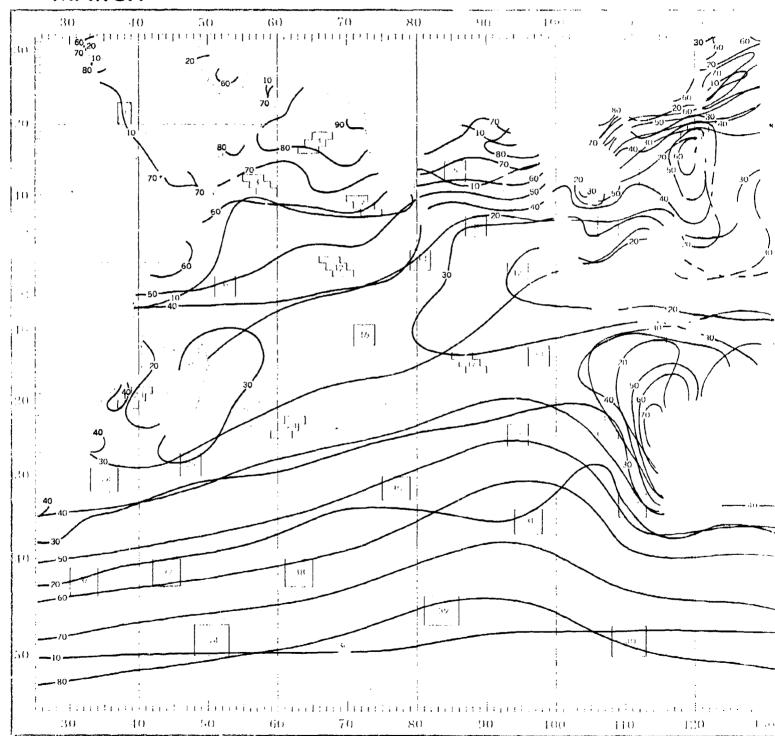
VISIBILITY



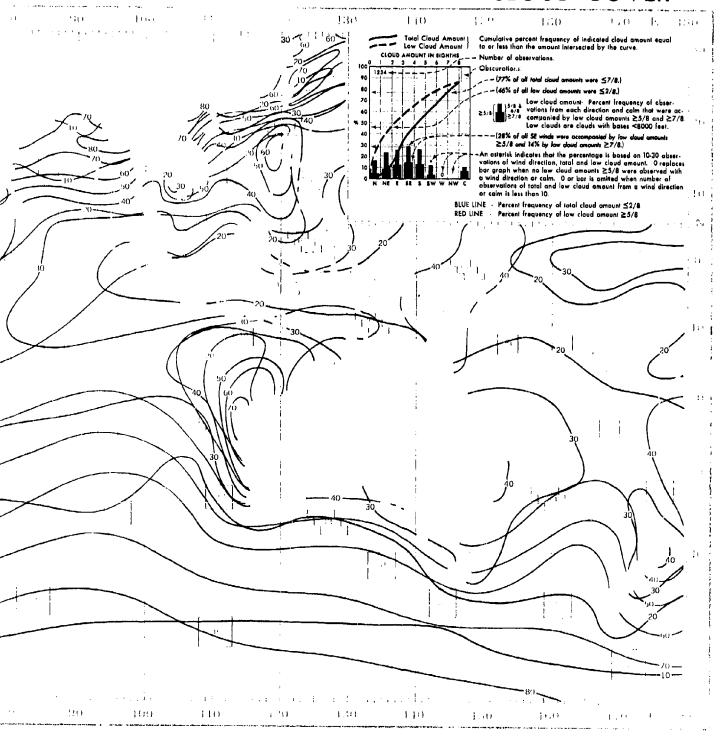
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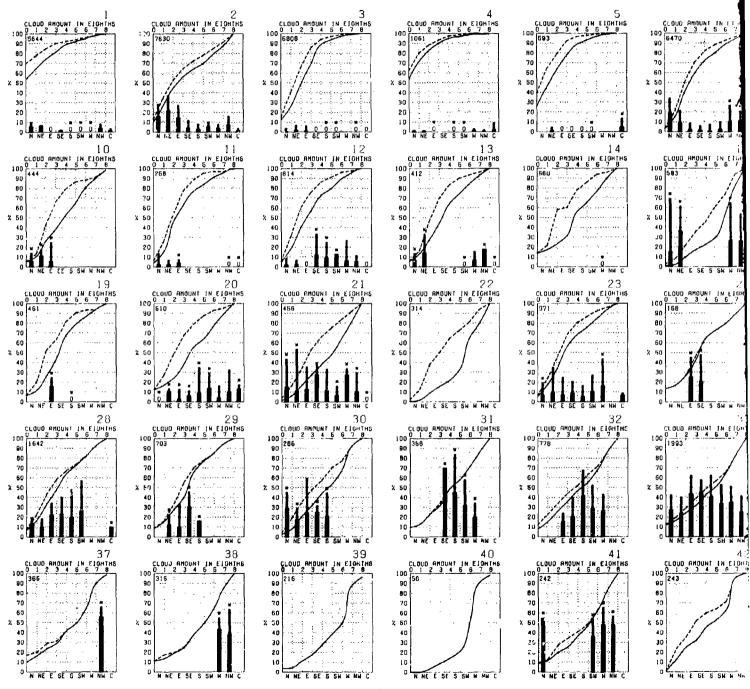
ctive compilation of available data for specified areas without regard to suspected biases. posite page) are based on all available data subjectively adjusted where bias was evident.



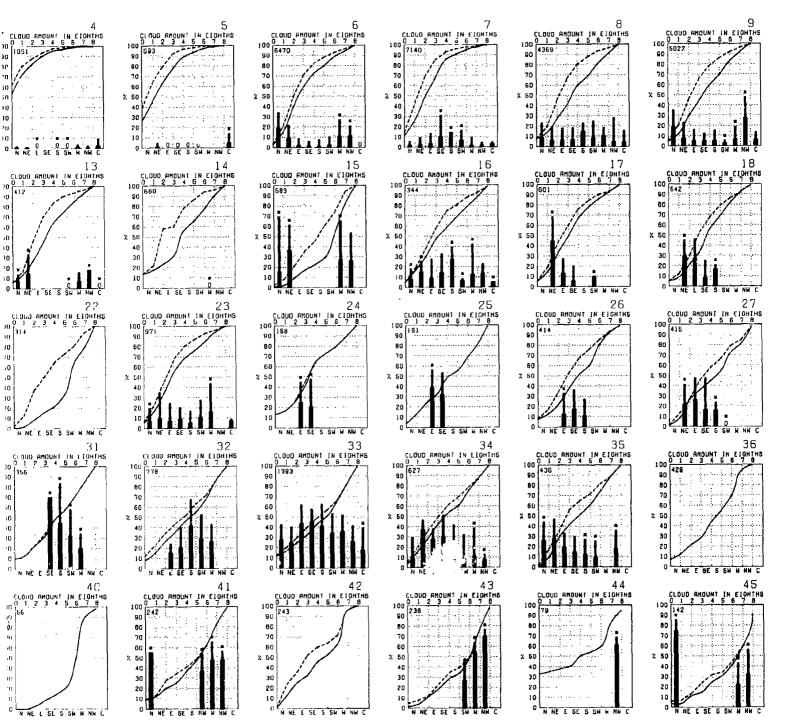
CLOUD COVER



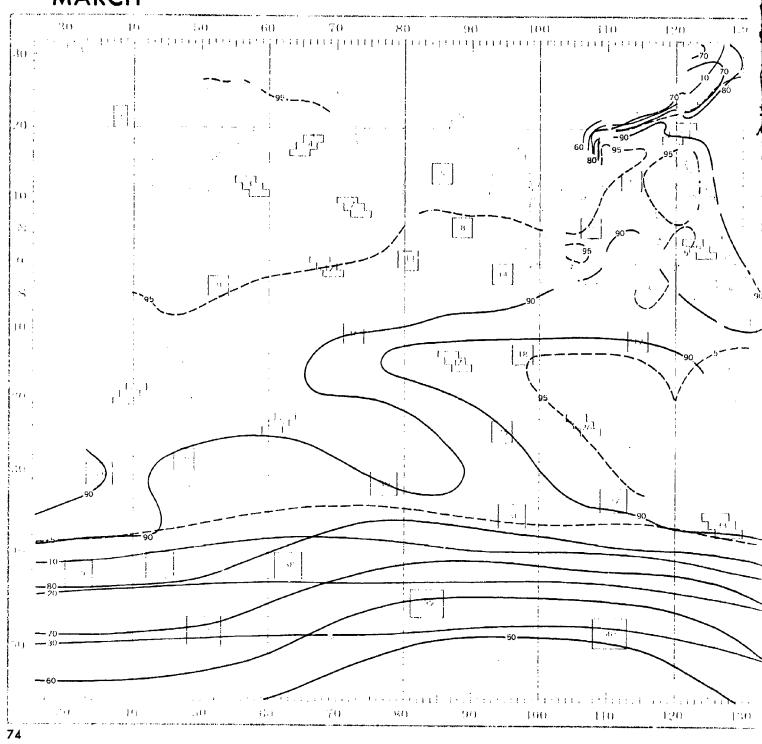
CLOUD COVER



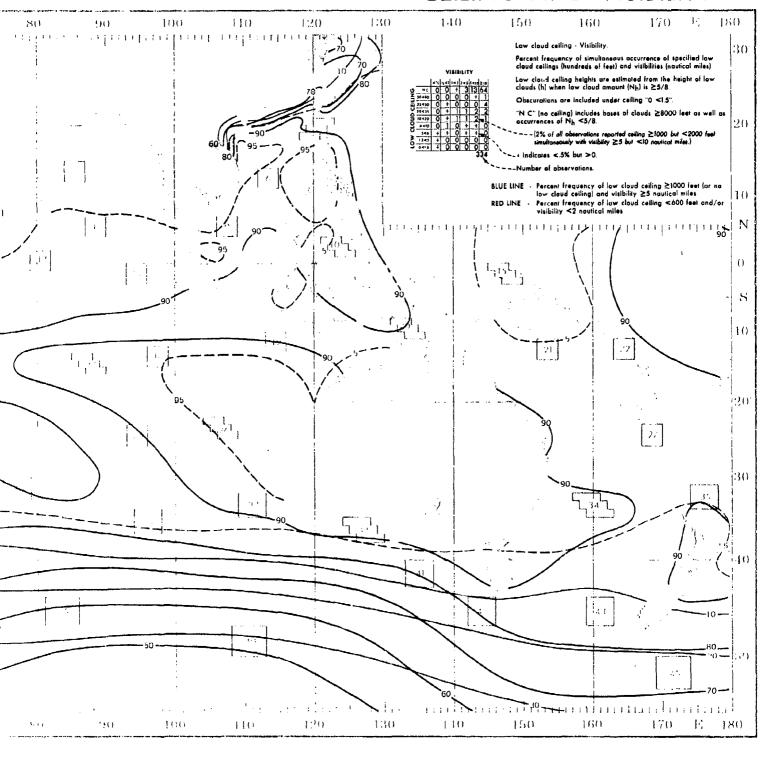
<u>Graphs</u> represent the objective compilation of available data for specified areas without The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjusted.



ive compilation of available data for specified areas without regard to suspected biases, site page) are based on all available data subjectively adjusted where bias was evident.



CEILING AND VISIBILITY



CEILING AND VISIBILITY

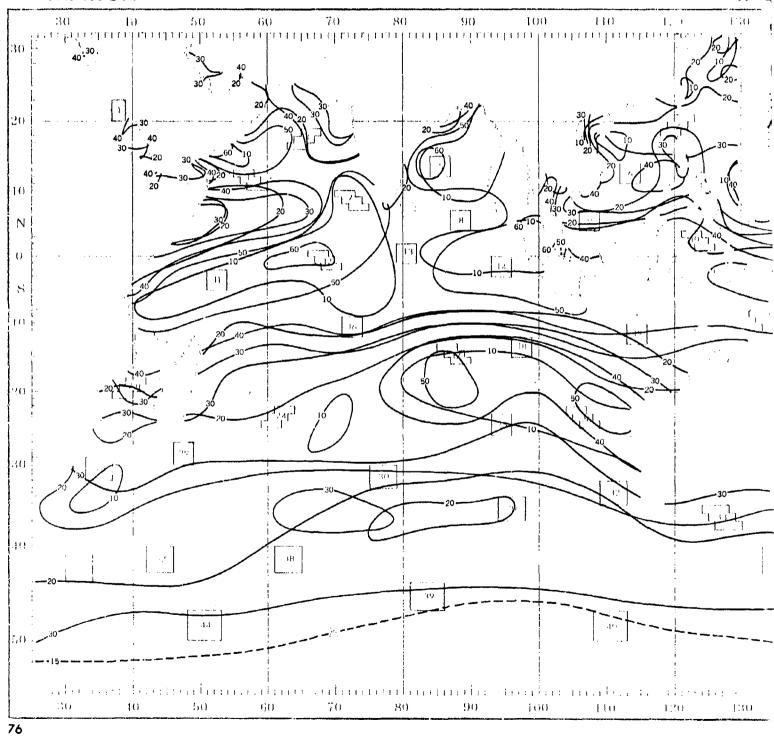
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VISIBILITY 1	VIBIBILITY 2	VISIBILITY 3 -1/2 -	VIBIBIL ITY 1/2 5/4-1 1-2 2-4 1-10 1-10 1/2 5/4-1 1-2 2-4 1-10 1-10 1/2 5/4-1 1-2 2-4 1-10 1-10 1/2 5/4-1 1-2 2-4 1-10 1-10 1/2 1/2 1-10 1-10 1/2 1/2 1-10 1-10 1/2 1/2 1-10 1-10 1/2 1/2 1-10 1-10 1/2 1/2 1-10 1-10 1/2 1/2 1-10 1-10 1/2 1/2 1-10 1-10 1/2 1/2 1-10 1-10 1/2 1/2 1-10 1-10 1/2 1/2 1-10 1-10 1/2 1/2 1-10 1-10 1/2 1/2 1/2 1/2 1/2 1-10 1/	VISIBILITY -1/4 7/441 1/2 2/48 5/410 410 -6C	VIS (BILL) -(1/2) (1/4) (1/2) NC
VISIBILITY 4 ¹ h / 1 ⁻¹ 1 ⁻¹ 2 ⁴ h 4 ¹ 10 10 KC	VISIBILITY 1 1 *** *** *** *** *** *** **	VISIBILITY 12 14/15 5/41 148 548 5410 110 160 0 0 0 0 1 55 1640 0 0 0 0 0 1 25 3480 0 0 0 0 0 1 26 1040 0 0 0 0 0 5 27 348 0 0 0 0 0 5 28 1040 0 0 0 0 0 5 28 1040 0 0 0 0 0 0 28 1040 0 0 0 0 0 0 378	VISIBILITY	VISIBILITY 1 4 1 4 (1)	VISIBILI
VIBIBILITY	VISIBILITY 2 0	VIBIBILITY (1/	VISIBILITY 22 -1/2 7/2 1/2 2/2 2/2 2/2 -1/2 7/2 1/2 2/2 2/2 2/2 -1/2 7/2 1/2 2/2 2/2 2/2 -1/2 1/2 1/2 1/2 2/2 2/2 -1/2 1/2 1/2 1/2 1/2 1/2 -1/2 1/2 1/2 1/2 1/2 1/2 -1/2 1/2 1/2 1/2 1/2 1/2 -1/2 1/2 1/2 1/2 1/2 1/2 -1/2 1/2 1/2 1/2 1/2 1/2 1/2 -1/2 1/2 1/2 1/2 1/2 1/2 1/2 -1/2 1/2 1/2 1/2 1/2 1/2 1/2 -1/2 1/2 1/2 1/2 1/2 1/2 1/2 -1/2 1/2 1/2 1/2 1/2 1/2 1/2 -1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 -1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 -1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 -1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 -1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 -1/2 1/	VISIGILITY 2 3 101/2 F/161 121 248 8410 110 10	VISIBIL: (1/g) (744) (12) (1/g) (744) (12) (1/g) (744) (12) (1/g) (744) (12) (1/g) (1/g) (1/g) (1/g) (1
VIBIBILITY 28 **** **** **** **** **** ***** **** ******	VISIBILITY 29	VISIB:CLTY 3	VISIBILITY 31	VISIBILITY 32 **** **** **** **** **** ***	W(SISILI ***/** Fyets 1+2 1 1 2 1 1 1 1 1 1
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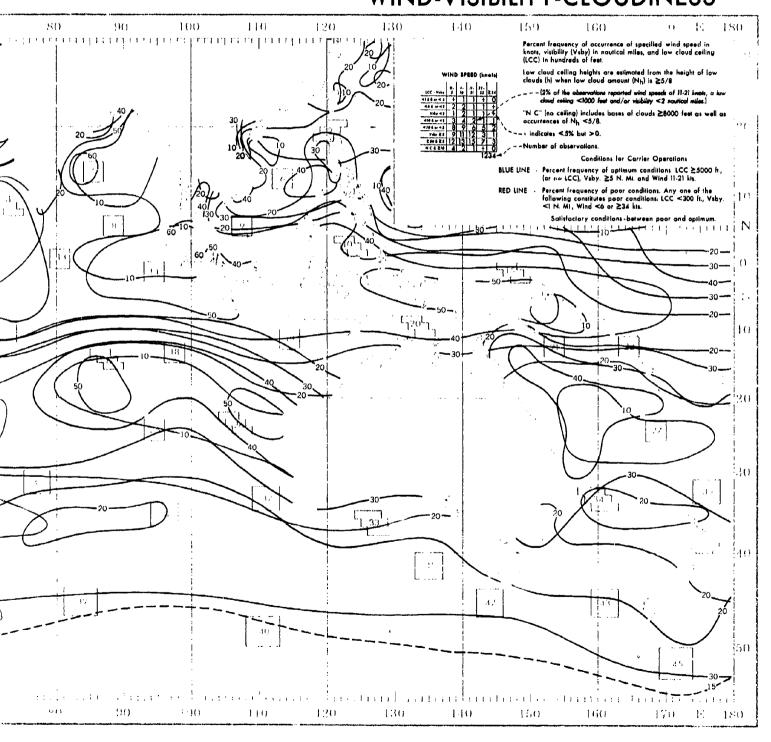
Graphs represent the objective compilation of available data for specified areas will The isopleth analyses (opposite page) are based on all available data subjectively

VISIBILITY 4 VISIBILITY MG 0 0 0 + 5 03 S0-80 0 0 0 0 0 0 0 S0-80 0 0 0 0 0 0 0 10-93 0 0 0 0 0 0 1 10-93 0 0 0 0 0 0 1 610 0 0 0 0 0 0 0 1 4.13 0 0 0 0 0 0 0 0 779	VIBIOIL TY	VISIBILITY 6	VISIBILITY ***/* ***	VISIBILITY R	VISIBILITY (4/x)						
VIBIBILITY	V S B L TY	VISIBILITY 1 5	VISISILITY **/** 7/** 1 ** 2 ** 3 ** 0 10	VISIBILITY 17	VISIBILITY						
VISIBILITY 22 ****/***/*** **********************	VISIBILITY **/** /** **	## 1816 LTY 24	VISIBILITY 4-7x 7-4-1 -2 2 -6 6 -10 3-10	VISIBILITY VISIBILITY NC 0 0 0 0 0 4 84 See 0 0 0 0 0 0 4 84 See 0 0 0 0 0 0 0 3 See 0 0 0 0 0 0 1 4 See 0 0 0 0 0 0 1 4 See 0 0 0 0 0 0 1 4 See 0 0 0 0 0 0 1 4 See 0 0 0 0 0 0 1 4 See 0 0 0 0 0 0 1 4 See 0 0 0 0 0 0 0 1 See 0 0 0 0 0 0 0 1 See 0 0 0 0 0 0 0 0 1 See 0 0 0 0 0 0 0 0 1 See 0 0 0 0 0 0 0 0 1 See 0 0 0 0 0 0 0 0 0 1	VISIBILITY - (-/x) -/x	VIBIBILITY 3	VISIBILITY 32	VISIBILITY 33 -1/2 free 1 2 2 3 3 4 3 3 -1/2 free 1 2 3 3 3 4 3 -1/2 free 1 2 3 3 4 3 3 -1/2 free 1 2 3 3 4 3 -1/2 5 5 5 5 5 5 5 5 -1/2 5 5 5 5 5 5 -1/2 5 5 5 5 5 -1/2 5 5 5 5 5 -1/2 5 5 5 5 -1/2 5 5 5 5 -1/2 5 5 5 -1/2 5 5 5 -1/2 5 5 5 -1/2 5 5 5 -1/2 5 5 5 -1/2 5 -1/2 5	VISIBILITY 3 4	VISIBILITY 35	VIBIBILITY 36 **12 **14 **16 **16 **10 **10
INSUFFICIENT DATA	VISIBILITY 4 1	VIBIBILITY 4 Z	## 10 0 0 0 7 28 ## 10 0 0 0 7 28 ## 10 0 0 0 0 2 0 ## 36-60 0 0 0 0 0 2 5 ## 10-60 0 0 0 0 5 8 ## 10-60 0 0 0 0 5 8 ## 10-60 0 0 0 0 5 8 ## 10-60 0 0 0 0 5 8 ## 10-60 0 0 0 0 5 8 ## 10-60 0 0 0 0 5 8 ## 10-60 0 0 0 0 5 6 8 ## 10-60 0 0 0 0 5 6 8 ## 10-60 0 0 0 0 0 0 0 0 ## 10-60 0 0 0 0 0 0 0 0 ## 10-60 0 0 0 0 0 0 0 0 ## 10-60 0 0 0 0 0 0 0 0 0 ## 10-60 0 0 0 0 0 0 0 0 0 ## 10-60 0 0 0 0 0 0 0 0 0 ## 10-60 0 0 0 0 0 0 0 0 0 ## 10-60 0 0 0 0 0 0 0 0 0 0 ## 10-60 0 0 0 0 0 0 0 0 0 0 ## 10-60 0 0 0 0 0 0 0 0 0 0 0 0 ## 10-60 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 ## 10-60 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY 4 4 -4/2 [7/21] 1-2 [248 [8/10] 110 MC 0 0 0 0 0 5 21 80-80 0 0 0 0 0 0 6 38-90 0 0 0 0 0 18 0 10-80 0 0 0 0 18 0 10-80 0 0 0 0 0 18 0 10-80 0 0 0 0 0 0 0 2 3-8 0 0 0 0 0 0 0 1 8-8 0 0 0 0 0 0 0 1 8-8 0 0 0 0 0 0 0	VIBIBILITY 45 -1/2						

tive compilation of available data for specified areas without regard to suspected biases. osite page) are based on all available data subjectively adjusted where bias was evident.



WIND-VISIBILITY-CLOUDINESS



LOW CLOUD CEILING-VISIBILITY-WIND

1	2	3	4	5	
MIND SPEED (KNOTS)	WIND SPEED (KNOTS)	NIND SPEED (KNOTS)	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	WIND SPEED (x
LCC - VSBY 3 10 21 33 234	LCC - VBBY 3 10 21 33 234	LCC - VSBY 3 10 21 33 254	LCC - VORT 0- 4- 11- 22- 33 834	LCC - VSST 3 10 21 33 334	LCC - Y88Y 3 10 21
41.6 4 OR 4.6 D + D O D	<1.5 i DR <.8 + + + + D	-1-84 OR -18 0 0 0 0 0	<1.54 0R < .5 0 0 + 0 0	<1.64 OR <-6 0 0 0 0 0	*1.5 t OR <.5 O + +
<64 OR <2 0 + 0 0 +	<8 4 DR 42 + 1 1 +	46 4 OR 42 0 0 0 0 0	48 4 OR 42 O + + O O	46 6 08 42 0 0 0 0 0	48 4 08 42 + + 1
Y887 49 0 + 0 0 +	V88Y <2 + + + +	0 0 0 0 9» reav	YABY 42 0 0 + 0 0	V867 42 0 0 0 0 0	¥607 42 □ +
410 4 0M 42 0 + 1 0 +	<10 4 OR <2 + 1 3 3 +	410 A 98 42 4 4 4 0 0	<10 4 0R <2 + + + D 0	410 4 9R 42 0 0 0 0 0	<10 4 OR <2 + 1 3
420 4 DR 48 + 1 3 + +	420 4 0A 45 1 3 8 B 1	420 4 SR 45 + 2 1 + 0	420 & OR 46 + 1 + 0 O	420 4 OR 45 + 2 + 0 0	420 4 OR 45 + 4 7
veev >s 11 31 47 8 + >s0 4 >s 11 30 44 9 +	V68Y 28 7 30 41 16 1	VSSY 35 12 68 18 + 0	VSBY 35 16 64 20 + 0	#89 4 4 5 27 68 5 0 0	VSST 36 4 46 41 380 435 4 42 33
AC 4 a 10 8 24 39 7 +	280 4 28 7 26 30 8 1 MC 4 2 10 5 22 24 5 0	NC4+10 11 64 16 + 0	MC 4 2 10 14 80 19 + 0	MC4 = 10 22 65 4 0 0	MG 4 a 10 3 39 28
1156	6271	1499	761	252	
10	1 1	12	13	. 14	
MIND SPEED (KNOTS)	WIND SPEED (KNOTS)	MIND SPEED (KNOTS)	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	MIND SPEED EN
LCC - V687 3 10 21 33 234	LCC - VSSY 3 10 21 33 234	LCC - VBBY 3 10 21 33 234	LCC - YABY 3 10 21 33 294	LCC - VSSY 3 10 21 33 334	LCC - VABY 0- 4- 11-
«1.84 OH «.B O O O O	«1.840R«.8 0 0 0 0 0	41.8 4 OR 4.8 0 0 0 0 0	41-54 08 4-5 0 0 0 0 0	*1.84 0A *18 0 0 0 0 0	41.8 4 UP 4.8 D U D
46 4 OR 42 0 0 0 0 0	46 L DR 42 0 1 0 0 0	<8 4 0R 42 + 0 1 0 0	48 4 OR 42 0 1 1 0 0	46 6 DR 42 0 0 0 0	48 4 OR 42 0 0 2
V887 <2 0 0 0 0 0	Y48Y -R 0 1 0 0 0	A88A 45 0 0 4 0 0	V887 <2 0 0 0 0 0	VBBY <# 0 0 0 0 0	V48Y 4F 0 0 0
410 4 0R 42 0 2 3 0 0 420 4 0R 45 0 5 5 0 0	410 4 OR 48 0 2 1 0 0	<10 4 0R <2 1 1 1 0 0 <20 4 0R <8 3 4 2 0 0	*10 4 GR 42 0 3 2 0 0	<10 4 OR <2 3 0 8 0 0	<10 4 0R <2 0 11 7
Vent as 18 52 32 0 0	V867 26 21 86 12 0 0	VERY 25 33 60 6 0 0	V687 35 22 80 19 0 0	7487 a5 34 43 20 0 9	VASY 46 20 52 25
3 50 4 35 16 40 28 0 0	250 6 25 18 60 10 0 0	a 50 4 a 5 29 55 4 0 0	a 50 4 as 21 48 14 0 0	360 4.46 31 37 6 0 0	. 60 4 a 16 16 B
MC & A 10 16 39 24 0 0	MC L a 10 18 57 9 0 0	MC 4 a 10 29 53 4 0 0	MC 4 = 10 20 45 13 0 0	NC 4 = 10 31 97 3 0 0	MC 4 2 10 16 11 7
62	146	362	139	36	
19	20	21	22	23	
WIND SPEED (KHOTS)	WIND SPEED (KNOTS)	WIND SPEED (KNOTS)	WIND SPEED (KNOTS)	MIND SPEED (KNOTS)	WIND SPEED (K/
LCC - VSOT 3 10 21 33 234	LCC - VSSY 3 10 21 33 294	LCC - V867 3 10 21 33 214	LCC - YEBY 9 10 21 98 254	LCC - Year 3 10 21 33 a34	LCC - VBBY 3 10 21
41.54 OR 4.5 0 0 0 0 0 0	48 4 0R 42 0 0 0 0 0 0	41.84 OR 4.8 0 0 0 0 0	<1.8408<.8 0 0 0 0 0 0	<1.84 OR <16 0 0 0 0 +	<1.84 0R <.6 0 0 0 <64 0R <2 0 0 0
V887 42 0 0 0 0 0	Y68Y 4E 0 0 0 0 0	VSSY 12 . O O	V887 -E 0 0 0 0 0	V887 42 0 + 0 0 +	V88Y +2 0 0 0
410 £ 0R 42 D D 2 D D	410 4 OR 42 1 3 2 1 0	<10 & OR <2 + 7 5 2 0	410 4 0F 42 0 7 0 2 0	*10 4 SP 42 + 3 2 1 1	410 & GR 42 0 0 3
*20 4 DR 45 0 7 2 U 0	420 4 DR 45 3 7 4 2 0	-20 4 OR -5 2 14 11 2 0	420 4 0R 46 0 26 7 2 0	-20 4 dR -6 1 6 4 3 1	<20 4 SR <6 0 3 24
V807 a5 12 67 19 0 0	YEEY 35 21 69 15 2 0	V68Y AS 13 48 28 3 0	V887 a5 13 61 22 2 0	Y88Y AS 18 46 25 8 +	VSSY a6 3 26 47
280 4 28 12 52 14 0 0 HC 4 2 10 12 45 14 0 0	#64 a 10 18 45 11 2 0	a \$0 4 a \$ 12 34 19 2 0 MC 4 a 10 1 27 18 1 0	MC 4 > 10 13 35 13 0 0	#80 4 #8 17 38 21 4 0 MC 4 h 10 16 37 21 4 0	a 50 4 a 8 3 2 4 2 6 HC 4 a 10 3 2 4 2 6
42	195	211	46	740	100 3 24 20
. 28	29	30	31	32	
HIND SPEED (XNOTS)	HIND SPEED (KNOTS)	HIND BPEED (KNOTS)	HIND SPETO (KNOTS)	NIND SPEED (KNOTS)	WIND SPEED (K)
LCC - VBBT 0- 4- 11- 22-	LCC - VARY 0- 4- 11- 22- 3 10 21 35 234	LCC - Year 9 10 21 99 294	LCC - VBBY 0- 4- 11- 22- 34	LCC - VANY 3 10 21 33 334	LCC - YEBY 0- 4- 11-4
41.64.08 4.8 0 0 + 0 +	41.84084.8 0 0 0 0 0	-1-54 0M 5 0 0 0 0 0	41.64084.6 0 0 0 0	41.5 6 OR 4.8 0 0 0 0 0	41-64 OR 4-6 + + D
-64 08 -z + 1 1 D 1	<84 OR <2 0 0 0 0 0	46 4 DR 42 D D D D D	48 A CR 42 D G G G D	48 4 OR 42 O + 1 + C	-6 4 GR -2 + 1 +
*10 4 OR *2 1 3 5 1 1	VBBT 42 G O O C O	VØDT 42	VSSY -2 0 0 0 0 0 0 -	VBBY 4P 0 9 0 D 0	V88Y 42
420 4 08 46 2 7 12 3 1	410 k DR 42 0 0 2 5 0	<10 4 0R <2 1 1 6 2 0	410 4 0R 42 1 1 0 0 0 0 420 4 0R 48 4 17 19 1 0	<10 4 OR 42 + 1 3 2 1 <80 4 OR 46 1 7 13 5 1	410 4 0R 42 1 3 5 420 6 0R 48 1 10 12
VBBY as 6 36 47 7 1	1887 as 2 31 53 14 0	V68Y 25 3 51 38 7 0	V607 3E B 44 39 9 D	VBST 25 4 35 48 10 1	V68Y 38 5 41 43
2 60 4 25 5 27 33 4 D	a 60 4 a 5 2 2 6 3 7 6 0	2 50 4 25 2 40 14 4 0	3 18 22 5 O	440 4 26 3 20 28 4 -	250 625 3 21 23
HC 4 A 10 4 26 32 3 0	HG 4 2 10 2 28 37 5 0	MC 4 8 10 2 38 13 9 0	MC 4 + 10 3 17 19 3 0	HC 4 2 10 3 18 23 3 +	MC 4 a 10 2 18 20
540	81	104	77	379	
37 HIND SPEED (KNOTS)	38 HIND SPEED (KNOTS)	HIND SPEED (KNOTB)	40	4 1 WIND SPEED (KNOTB)	HIND SPEED (KN
10-14-1:5-100-1	0- 4-1:1-122-1			10-14-111-199-1	المرابد المرابد
LCC - VBBY 3 10 21 33 224					
48 6 0R 42 0 0 0 0 0	41.8 £ 08 4.8 0 0 0 2 0	46 4 DR 4E 0 5 5 5 0	INICHIEFI CIENT	<1.54 0H = .5 0 0 0 0 0 0 0 = 84 0H = 2 0 0 1 0 0	<1.54 OR <.5 0 0 0
V487 48 D D D D D	VSEY *E 0 0 0 2 0	V897 -R 0 5 5 5 0	INSUFFICIENT	V897 42 0 0 0 0 0	V897 <2 0 0 0
-10 4 GR -2 D D 7 D D	410 4 08 42 D 2 5 7 D	410 4 0R 4F 0 10 14 5 0	DATA	<10 4 0R <2 0 10 4 1 1	<10 4 0R <2 0 0 0

5 24 29 10 0 5 5 5 10 0

V687 #6

D 41 32 14 D

0 18 11 2 0

160 4 18

<u>Graphs</u> represent the objective compilation of available data for specified areas without The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adj

0 0 10 0 14 57 1 0 10 43 1

150 4 15

0 42 38 15 4

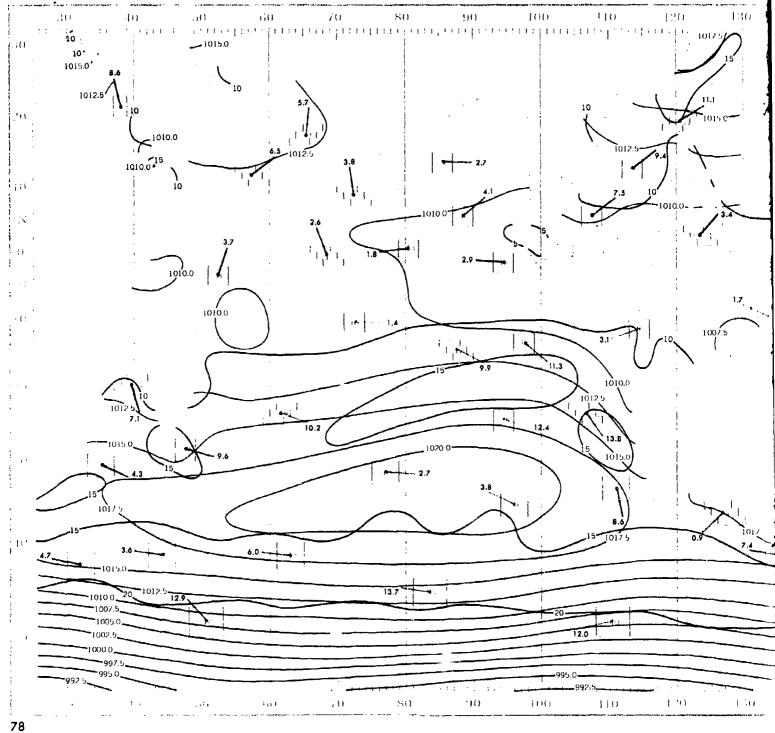
ITY-WIND

MARCH

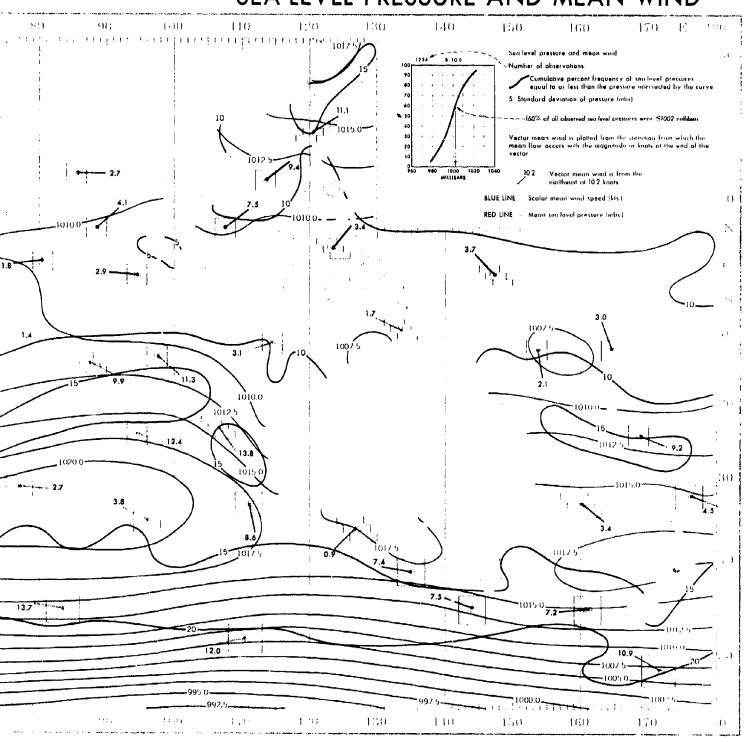
, L 4	5	6.	7	8	9
NIND SPEED (KNDTS) LCC - VERY 0 4 - 11 - 22 - 1 - 23 - 134	MIND SPEED (XNOTS) LCC - V007	HIND SPEED (KNOTS) LCC - VBBY 9 10 81 193 234	MIND SPEED 1KNOTS) LCC - V8BY	HIND SPEED (KNOTS) LCC - VBBY	HIND SPEED INNOTS) LCC - VASY
420 4.08 45	*20 4 08 *5	**************************************	**************************************	**GO 4.08 45 2 8 4 0 0 0 **V68Y NS 19 80 20 + 0 ***SO 4.8 16 49 15 0 0 ***MC 4.8 10 16 46 14 0 0 1510	VBBY 95 1 8 8 1 + VBBY 95 13 50 33 2 + >BG L 95 11 42 23 1 + MC 4 = 10 11 38 19 + + 2480
13	14 HIND SPEED (KNOTS)	15 HIND SPEED (KNOTS)	16 HIND SPEED (KNOTS)	. 17 WIND SPEED (KNOTS)	18 Wind Speed (KNOTS)
1 1 2 2 2 3 2 3 2 3 2 3 2 3 3	**************************************	N(AU S) 0 4 11 12 23 33 34	CC - VBBY 0 4 - 11 - 22 - 23		CC - V889 0 1 1 1 2 2 1 2 2 2 2
22	23	24	25	26	27
MIND SPEED IXNOTS) LCC - VBB*	HIND BPEED (ANDIS) LCC - Y887	NINO SPEED (MNOTS) LCC - V887	HIND BPEED (INDSE) LCC - VABAY	HIND SPEED LENGTS	HIND SPEED (KNOTS) LCC - VBSY 0 4 11 12 13 13 134 11.6 4.08 < 5 0 0 1 2 1 0 48.4 08 < 9 0 1 2 1 0 VBSY < 2 0 0 1 0 0 480.4 08 < 8 0 10 16 8 0 VBSY
46	740	34	68	171	180
3 MIND SPEED (MIND S) MIND SPEED (MIND S) MIND SPEED (MIND S) MIND S) MIND S MIND	32 HIND SPEED (KNOTS) LCC - 9887	### A PROPERTY OF THE PROPERTY	34 HIND OFFEC (KNDTS) LCC - VARY 9 10 81 33 384 41.84.08 4.8 0 0 0 0 0 0 0 46.08 42 0 1 0 0 0 0 0 0 410.408 42 0 2 3 3 2 420.408 5 1 6 12 7 2 V887 8 7 33 42 14 2 880.4 8 6 25 25 6 6 0 MC(48.10 0 25 23 5 0	35 HIND SPEED (KNDTS) LCC - VERY	36 HIND SPEED (NOTE) LCC - VBBY
40	4]	42	43	44 HIND SPEED (KNOTS)	45
NSUFFICIENT DATA	MIND SPEED I MINDES LCC - V487	HIND SPEED (KNOTS) LCC - VABY	MIND SPEED (KNDTS) LCC - VABY	CCC - YEBY G = 11-1-12-13-13-13-13-13-13-13-13-13-13-13-13-13-	LCC - V88Y 0 3 10 21 39 384

tive compilation of available data for specified areas without regard to suspected biases. site page) are based on all available data subjectively adjusted where bias was evident.

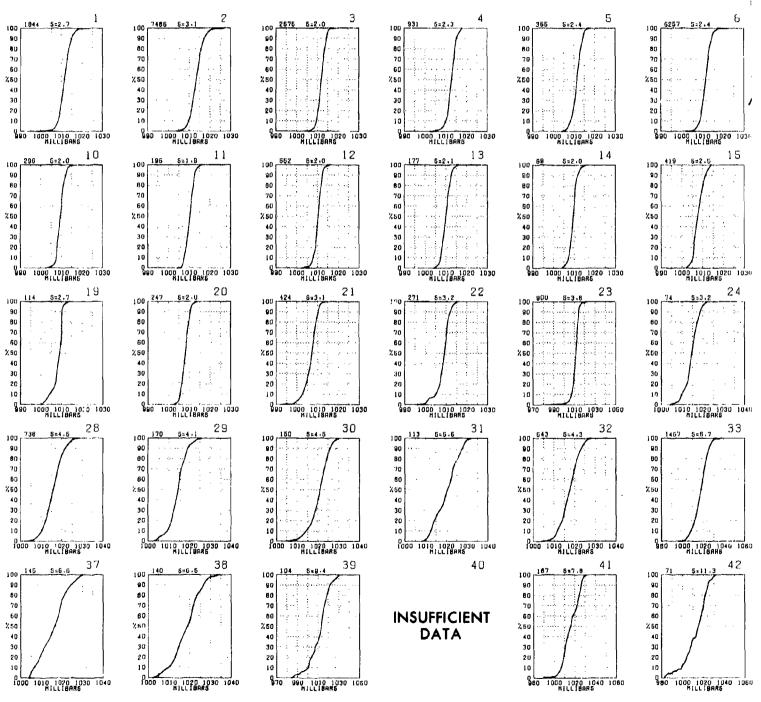
SEA LEVEL PRE



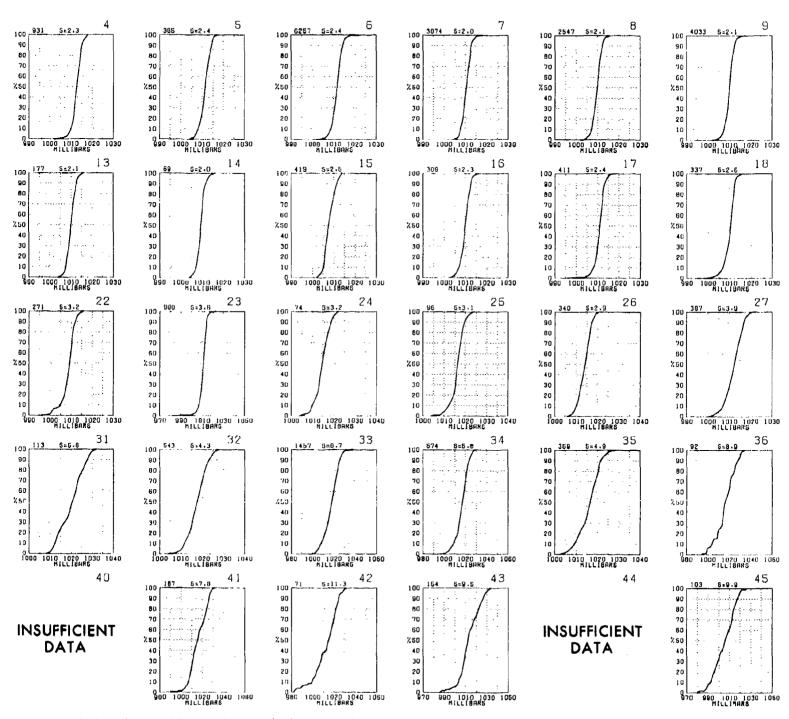
SEA LEVEL PRESSURE AND MEAN WIND



SEA LEVEL PRESSURE

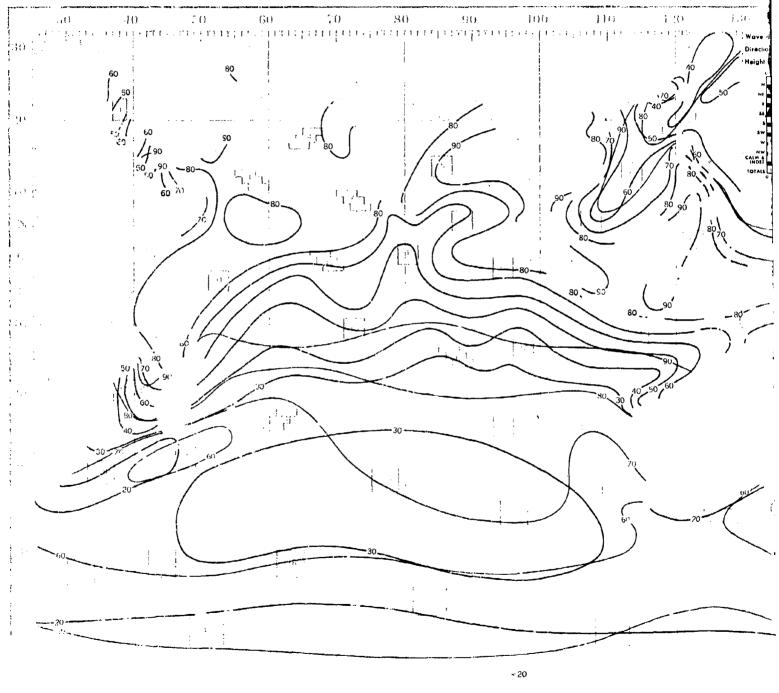


Graphs represent the objective compilation of available data for specified areas without re The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjuste

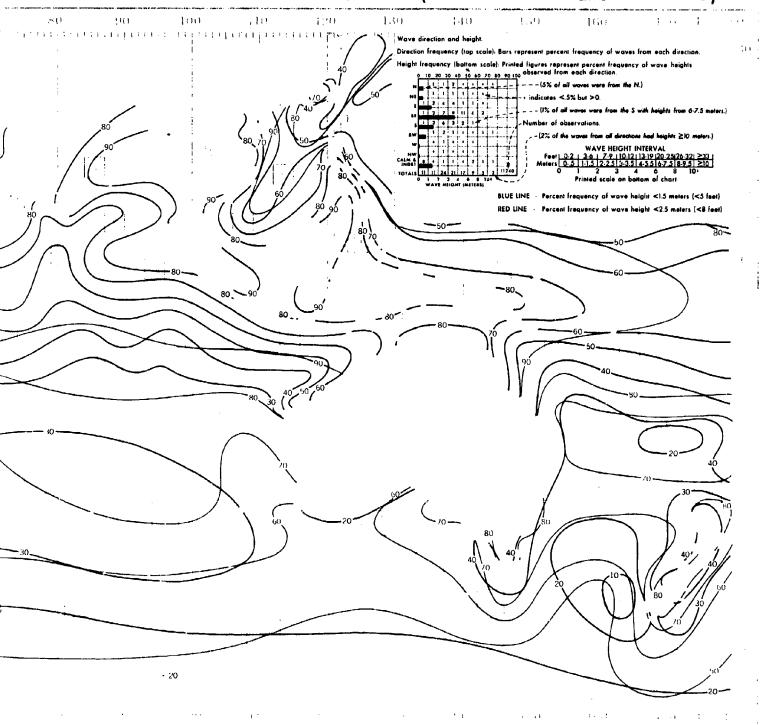


objective compilation of available data for specified areas without regard to suspected biases. (opposite page) are based on all available data subjectively adjusted where bias was evident.

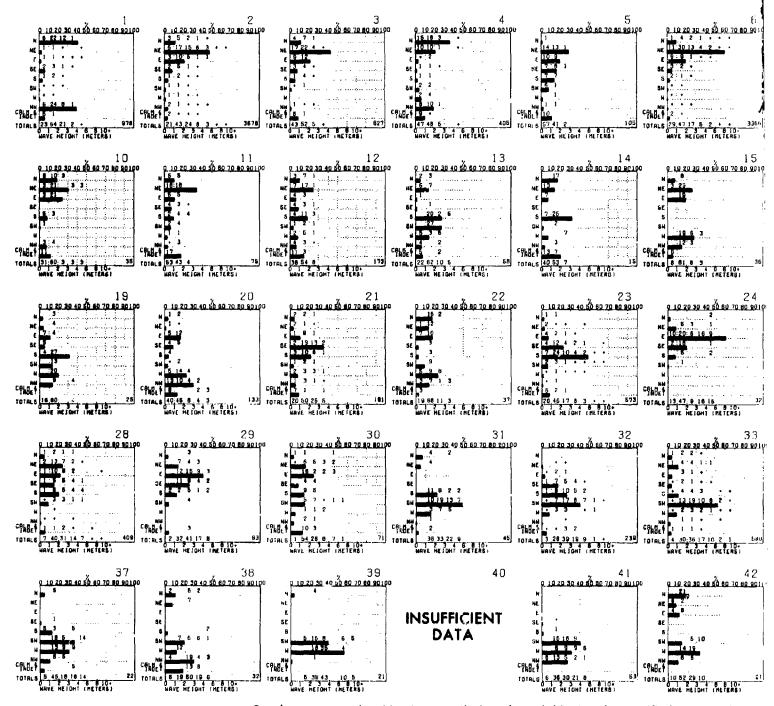
WAVES



WAVES (<1.5 AND <2.5 METERS)



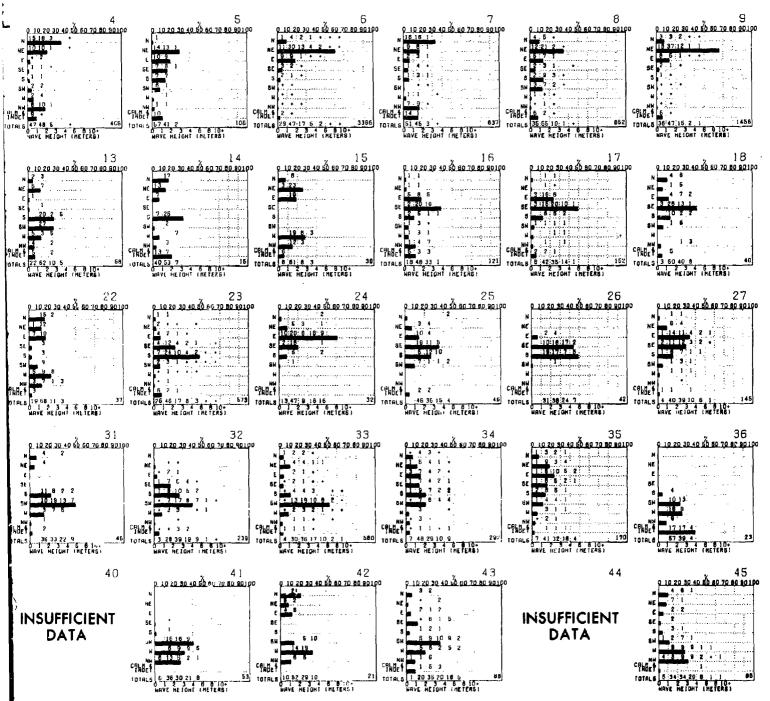
WAVE DIRECTION AND HEIGHT



<u>Graphs</u> represent the objective compilation of available data for specified areas without re The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjusted

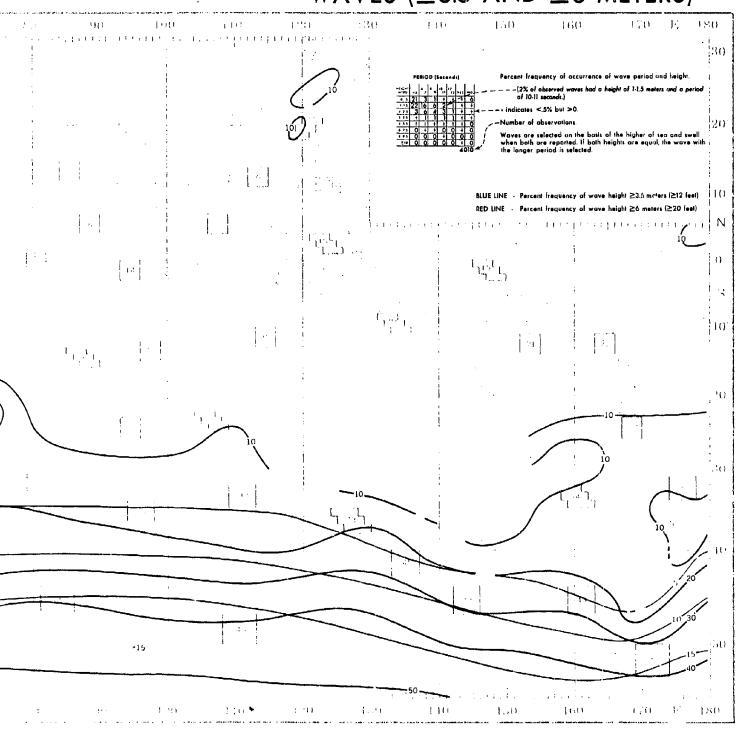
GHT

MARCH



ctive compilation of available data for specified areas without regard to suspected blases. osite page) are based on all available data subjectively adjusted where bias was evident. **MARCH** WAVE the particular and the particular tensor of a few tau -15

WAVES (≥3.5 AND ≥6 METERS)



WAVE PERIOD AND HEIGHT

PERIOD (SECONDS) 1	PERIOD (SECONDS) (C)	PERIOD (SECONDS) 10 10 10 10 10 10 10 10 10	PERIOD (SECONDS) 1	PERIOD (SECONDS) 1	PERIOD ISECON 1
TERIOD (SECONDS)	1 1 1 1 1 1 1 1 1 1	1 2 PERIOD (SECONDS) Notice 1	1 3 PERIOD (SECONDS) 100 101 111 110 110 111 110 110 111 110 110 111 110	INSUFFICIENT DATA	FERIOD (SECON 1
19	PERIOD (SECONDS) ***PERIOD (SECONDS) **PERIOD (SECONDS) **PER	PERIOD (SECONDS) PERIOD (SEC	PERIOD (SECONDS) HEIDEN 48 6-7 8-10-11-11-113 Ind 146 7 8-11-11-11-113 Ind 147 8-11-11-11-11-11-11-11-11-11-11-11-11-11	PERIOD I SECONDS No. 100 1	PERIOD (SECON 10.10 1.0 1.0 1.0 10.10 1.0 1.0 10.10 1.0
28 PERIOD (SECONDS) (61-2) (48	PERIOD (SECONDS) NC16417 4 5	PERIOD (SECONDS)	31 NETION 18 19 19 18 19 19	32 NECEST PERTOD (SECONDS) NECEST N	NC10n1 N
37 PERIOD (SECONDS) ***INSM** 48 6	## PERIOD (BECONDS) ME (BMT) 4 5 6 19 15 13 18 18 O-8 8 0 0 0 0 0 0 I-1.8 9 0 8 0 0 0 3 S-2.8 3 8 38 3 0 0 0 S-3.8 3 8 3 0 0 0 0 S-3.8 3 3 6 0 3 0 3 S-3.8 3 3 6 0 3 0 3 S-3.8 3 0 0 0 0 0 0 0 S-3.8 0 0 0 0 0 0 0 0 S-3.8 0 0 0 0 0 0 0 0 S-3.8 0 0 0 0 0 0 0 0 S-3.8 0 0 0 0 0 0 0 0 0 S-3.8 0 0 0 0 0 0 0 0 0 S-3.8 0 0 0 0 0 0 0 0 0	#ERIOD (SECONDS) #EINT 1- 6 10- 12- 13 19 0-14 0 0 0 0 0 0 0 1-1.5 0 5 0 0 0 0 0 1-1.5 0 5 0 0 0 0 5 1-3.5 0 10 28 0 0 0 5 1-3.5 0 0 0 0 0 0 0 1-3.5 0 0 0 0 0 0 0 1-4.5 0 0 0 0 0 0 0 1-3.5 0 0 0 0 0 0 1-3.5 0 0 0 0 0 0 1-3.5 0 0 0 0 0 0 1-3.5 0 0 0 0 0 0 1-3.5 0 0 0 0 0 0 1-3.5 0 0 0 0 0 1-3.5 0 0 0 0 0 1-3.5 0 0 0 0 0 1-3.5 0 0 0 0 0 1-3.5 0 0 0 0 0 1-3.5 0 0 0 0 0 1-3.5 0 0 0 0 0 1-3.5 0 0 0 0 0 1-3.5 0 0 0 0 0 1-3.5 0 0 0 0 1-3.5 0 0 0 0 1-3.5 0 0 0 0 1-3.5 0 0 0 0 1-3.5 0 0 0 0 0 1-3.5 0 0 0 0 1-3.5 0 0 0 0 1-3.5 0 0 0 0 1-3.5 0 0 0 1-3.5 0 0 0 0 1-3.5 0 0 0 0 1-3.5 0 0 0 0 1-3.5 0 0 0 0 1-3.5 0 0 0 0 1-3.5 0 0 0 0 1-3.5 0 0 0 0 1-3.5 0 0	INSUFFICIENT DATA	#ER*OD (SECONDS)	FERIOD (SECONC 18 18 18 18 18 18 18 18

<u>Graphs</u> represent the objective compilation of available data for specified areas witho The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adj

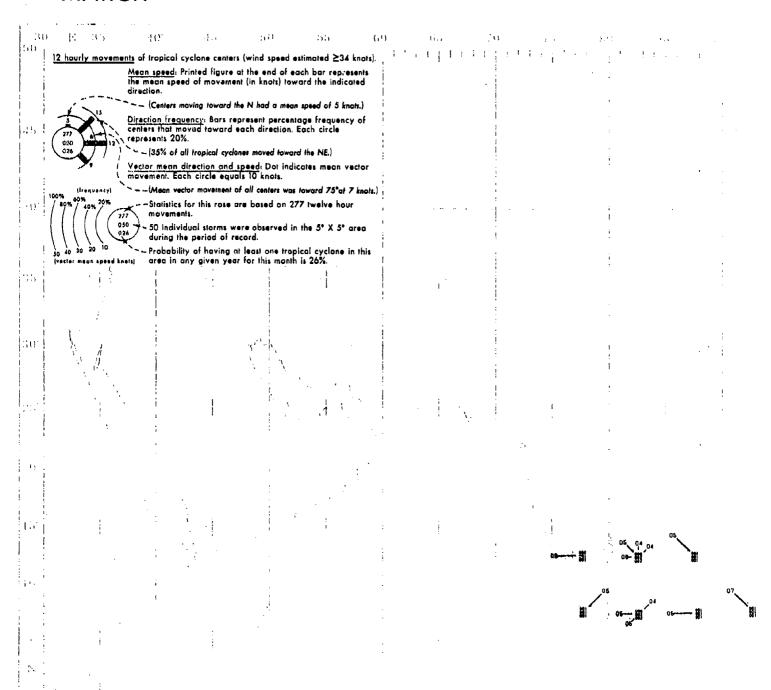
MARCH

PERIOD (SECONOS) **E10**1	PERIOD (SECONDS) **ELONI 0 - 1 0 - 1 10 - 11 13 13 150 0 - 6 48 5 1 0 0 0 12 1 - 1 - 8 23 8 1 1 0 0 0 2 - 1 - 8 1 0 1 0 0 0 0 2 - 1 - 8 0 0 0 0 0 0 0 4 - 8 0 0 0 0 0 0 0 6 - 7 - 8 0 0 0 0 0 0 0 3 - 1 - 8 0 0 0 0 0 0 3 - 1 - 8 0 0 0 0 0 0 3 - 1 - 8 0 0 0 0 0 0 3 - 1 - 8 0 0 0 0 0 3 - 1 - 8 0 0 0 0 0 3 - 1 - 8 0 0 0 0 3 - 1 - 8 0 0 0 0 3 - 1 - 8 0 0 0 3 - 1 - 8 0 0 0 3 - 1 - 8 0 0 0 3 - 1 - 8 0 0 3 - 1 - 8 0 0 3 - 1 - 8 0 0 3 - 1 - 8 0 3 - 1	PERIOD (SECONOS) **EIO**I	PERIOD (SECONDS) **ELOHI	PENIOD (SECONDS) PENIOD (SEC	PERIOD (SECONDS) MC16m7 48 7 8 10 12 13 14 (R188) 48 7 8 10 12 13 14 6-4 30 2 1 0 0 0 1-1 1 23 14 3 1 + 0 0 2-8 3 8 3 1 + 0 0 2-9 4 1 1 1 1 1 2-3 4 1 1 1 1 1 2-3 4 1 1 1 1 1 2-3 4 1 1 1 1 1 2-3 4 1 1 1 1 1 2-3 4 1 1 1 1 1 2-3 4 1 1 1 1 1 2-3 4 1 1 1 1 2-3 4 1 1 1 1 2-3 4 1 1 1 1 2-3 4 1 1 1 1 2-3 4 1 1 1 1 3-4 1 1 1 1 3-5 1 1 1 3-5 1 1 1 3-5 1 1 1 3-5 1 1 1 3-5 1 1 1 3-5 1 1 1 3-5 1 1 3-5 1 1 3-5 1 1 3-5 1 1 3-5 1 1 3-5 1 1 3-5 1 1 3-5 1 1 3-5 1 1 3-5 1 1 3-5 1
13	INSUFFICIENT DATA	S S S S S S S S S S	FERTOD (SECONDS) 16 17 18 18 18 18 18 18 18	17	18 PERIOD (SECONDS)
PERIOD (SECONDS) **Clost	23 PERIOD (SECONDS) PERIOD	PERIOD (SECONDS) **Closty 6 7 8 10 12 13 13 186	PERIOD (SECONDS) PERIOD (SEC	PERIOD (SECONDS) PITON	PERIOD (SECONDE) 10 10 10 10 10 10
31 PERIOD (SECONDE)	32 FERTION	## FERIOD (SECONDS) FERIOD (SECONDS)	34 FERTIOD (SECONDS) MC1041 18 18 18 18 18 18 18	35 PERIOD (BECONDS) PERIOD	36 PERIOD [SECONDS]
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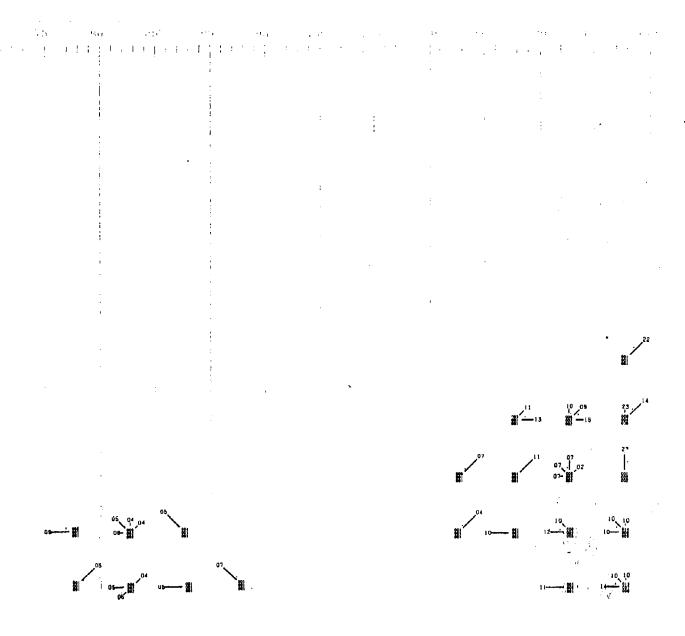
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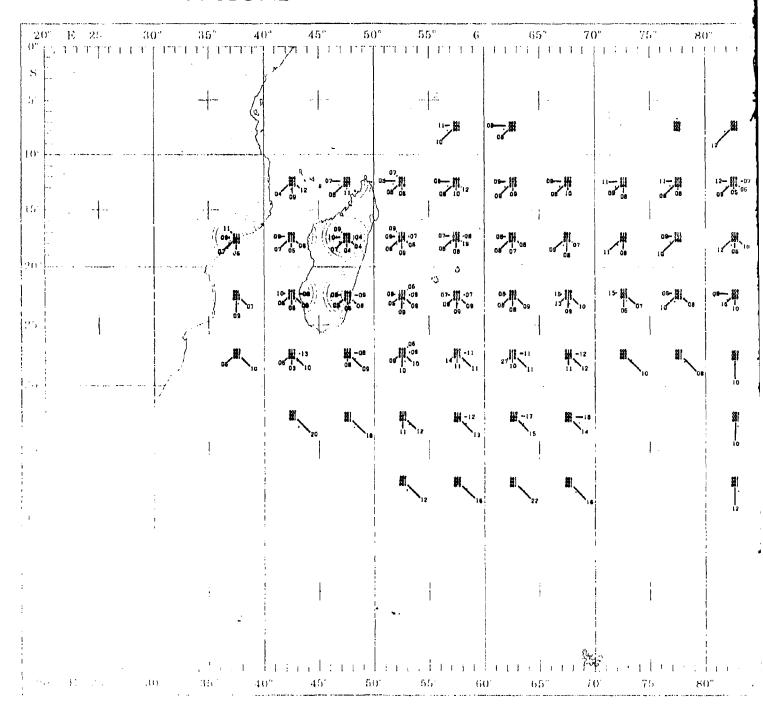
MARCH



TROPICAL CYCLONE

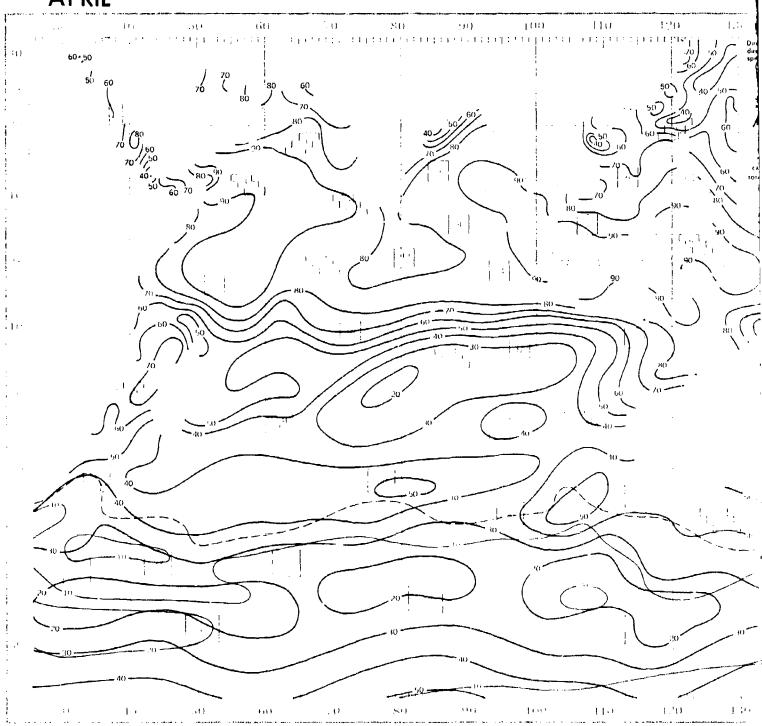


TROPICAL CYCLONE

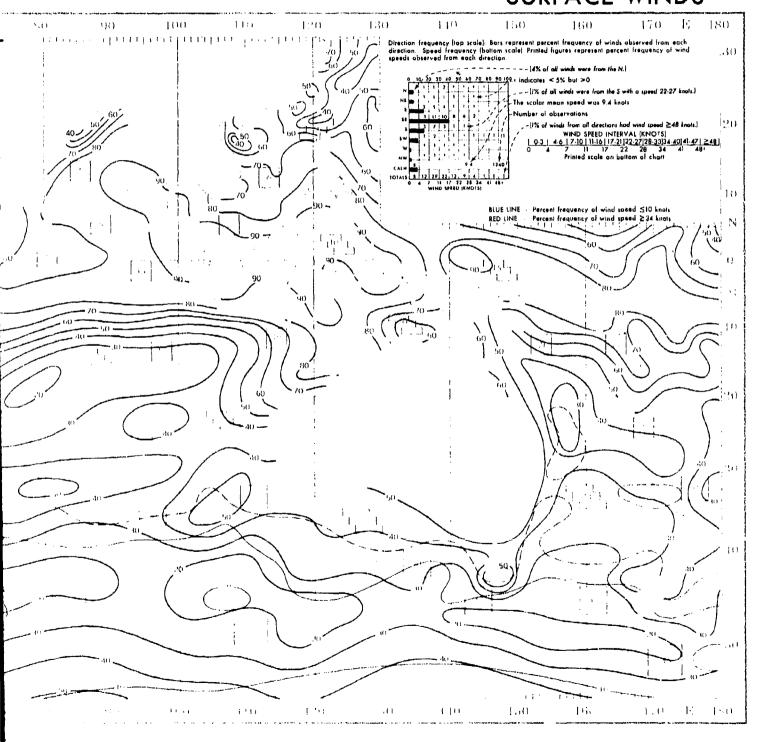


MARCH

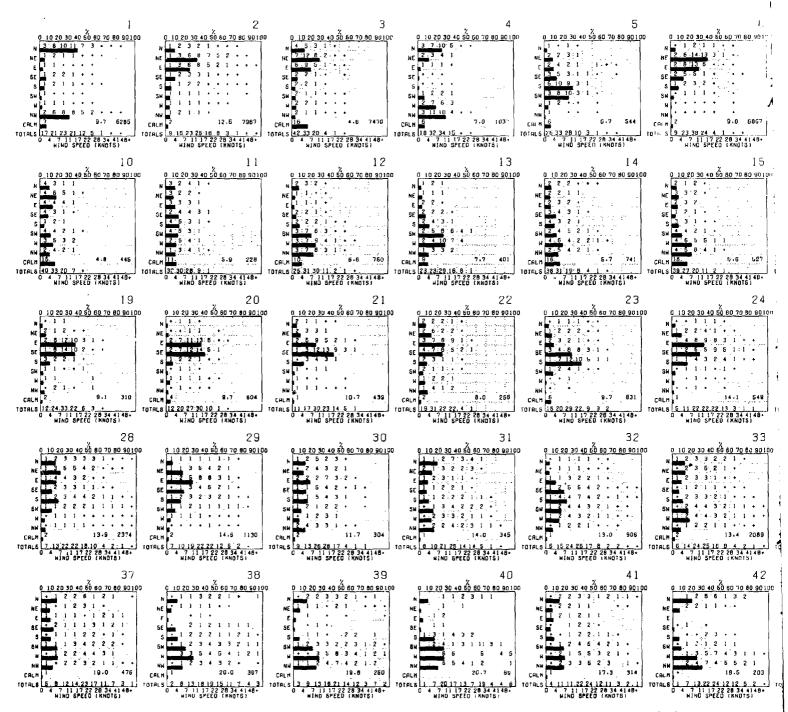
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12 hourly movements of tropical cyclone centers (wind speed estimated ≥34 knoth the mean speed of movement (in knots) toward the indicated direction. Direction frequency: Bars represent percentage frequency of centers that moved toward each direction. Each circle represents 20%.	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	54 10 11 11 12 15	W ae		14 13
13 15 16 16 17 18 18 18 18 18 18 18 18 18 18 18 18 18					HI. HI. HI.
Mean speed: Printed figure at the end of each bar represents the mean speed of movement (in knots) toward the indicated direction. 12 Mean speed: Printed figure at the end of each bar represents the mean speed of movement (in knots) toward the indicated direction. Centers moving toward the N had a mean speed of 5 knots.) Direction frequency: Bars represent percentage frequency of centers that moved toward each direction. Each circle represents 20%.	13 .	15	!	10	15 14 16 21 16 24
Direction frequency: Bars represent percentage frequency of centers that moved toward each direction. Each circle represents 20%.	Ш	H H	· :	数 	12 hourly movements of trapical cyclone centers (wind speed estimated ≥34 knots). Mean speed: Printed figure at the end of each bar represents the mean speed of movement (in knots) toward the indicated
OSO Propresents 20%.	16	, ,	•	(12	(Centers moving toward the N had a mean speed of 5 knots.) 3 Direction frequency: Bars represent percentage frequency of
			;		030 12 represents 20%.
movement. Each circle equals 10 knots.	;	;			movement. Each circle equals 10 knots.
movements. 050 020 - 50 individual storms were observed in the S° X 5° area during the period of record.	;	!	1 1 1		movements. 030 - 50 individual storms were observed in the 5° X 5° area during the period of record.
So to 20 10 —— Probability of having at least one tropical cyclone in the fruster mean speed knowled area in any given year for this month is 26%. 20 55 70 5.5 80 85 90 95 100 105 110 115					Tractor mean speed knowled ured in any given year for this month is 26%.



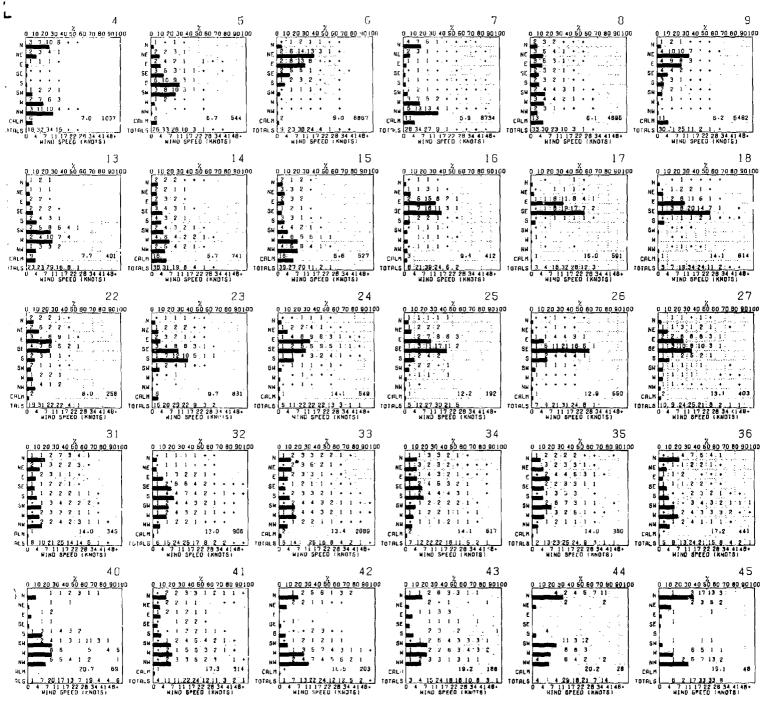
SURFACE WINDS



WIND DIRECTION AND SPEED



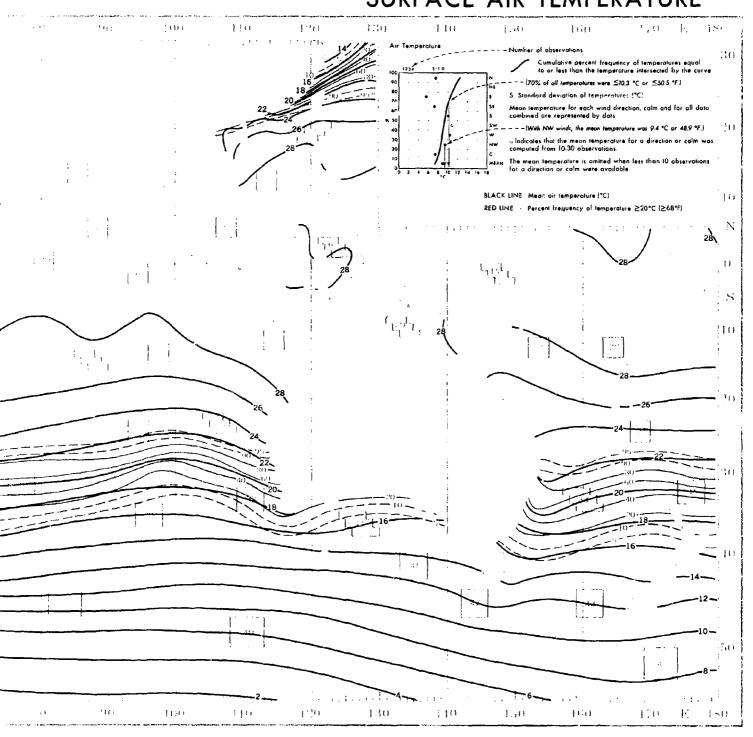
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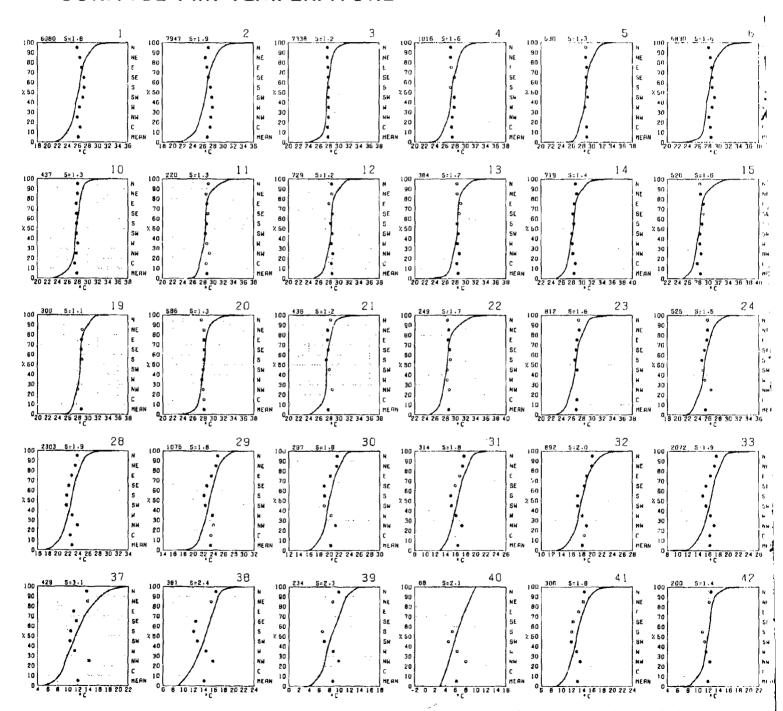
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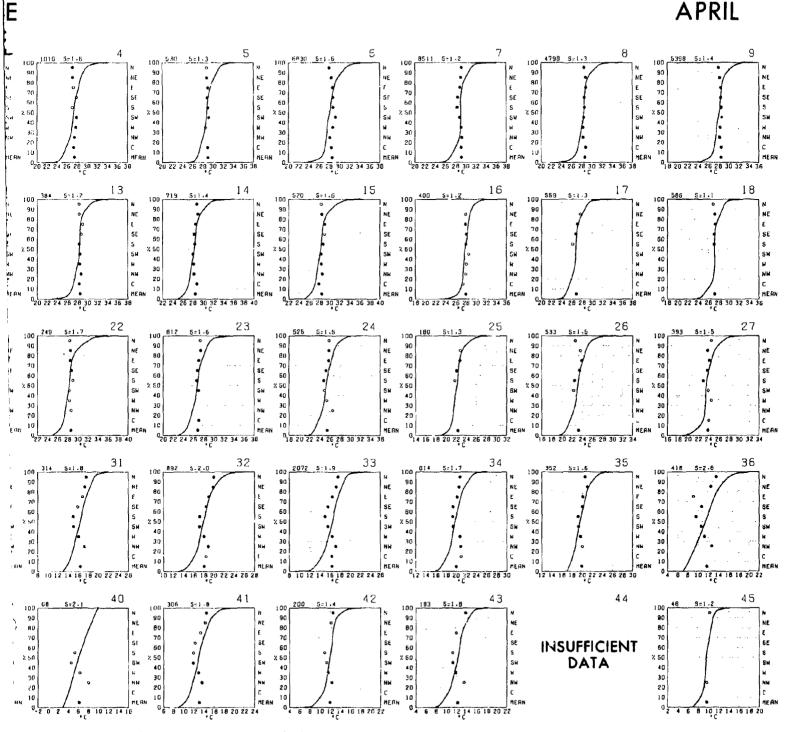
SURFACE AIR TEMPERATURE



SURFACE AIR TEMPERATURE



<u>Graphs</u> represent the objective compilation of available data for specified areas without re The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjuste

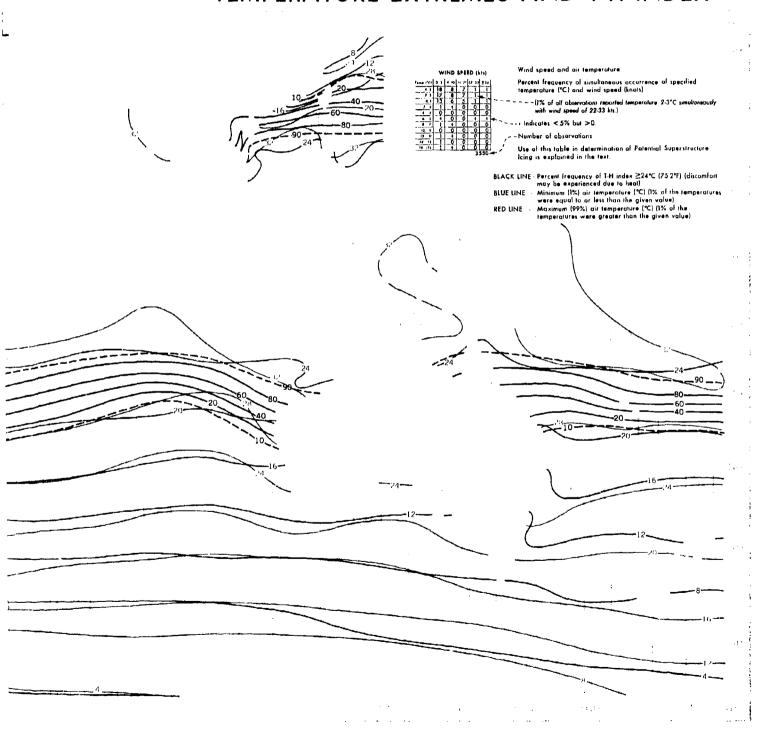


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TEMPERATURE EX



TEMPERATURE EXTREMES AND T-H INDEX



WIND SPEED AND AIR TEMPERATURE

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HIND SPEED (KIS)	WIND SPEED (KIS) 2	WIND SPEED (KTS) 3	HIND SPEED 'KIS)	WIND SPEED (KTS) 5	WIND SPEED CKT
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HIND SPEED (KIS) 28	HIND SPEED (KTS) 29			HIND SPEED (KTS) 32	NIND SPEED INTS
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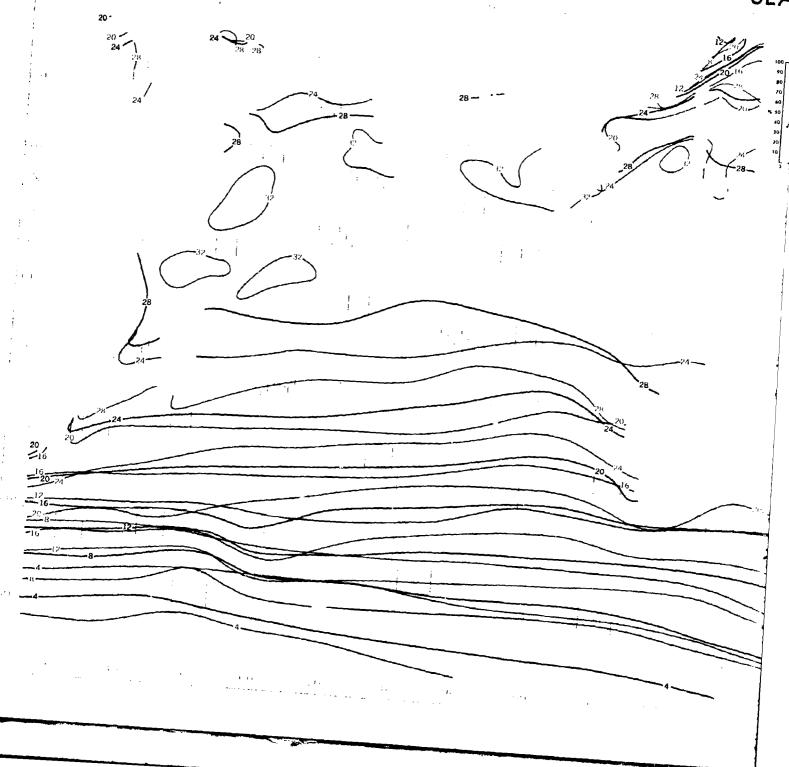
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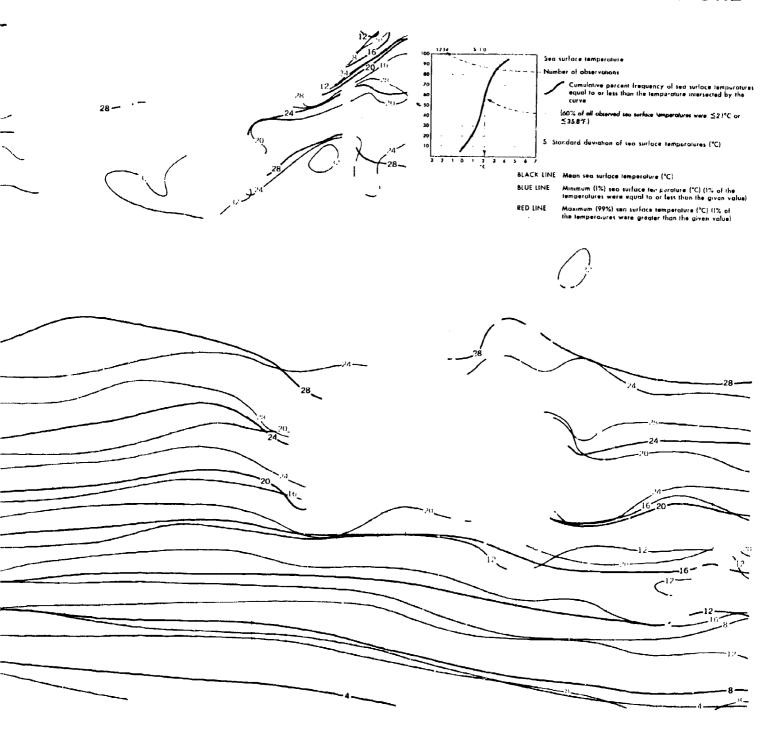
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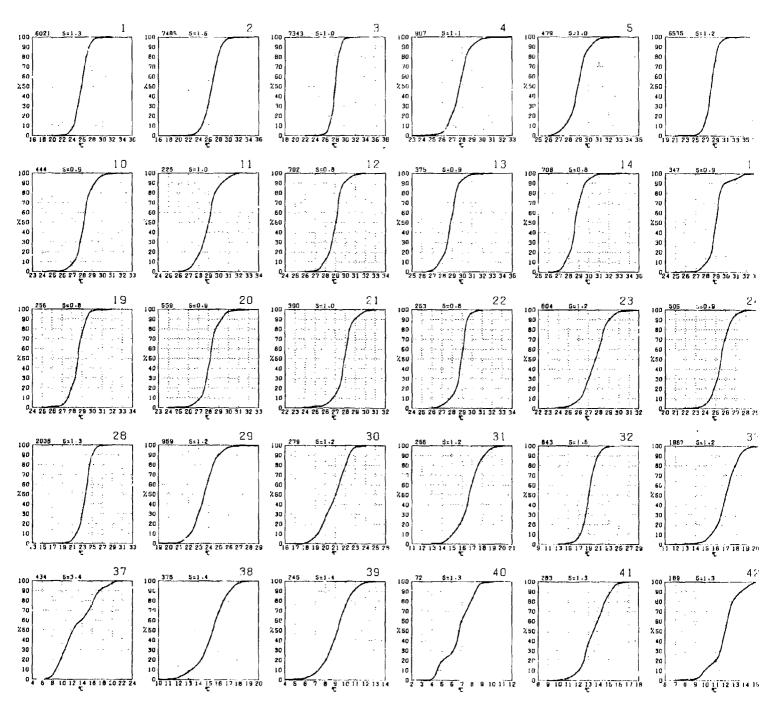
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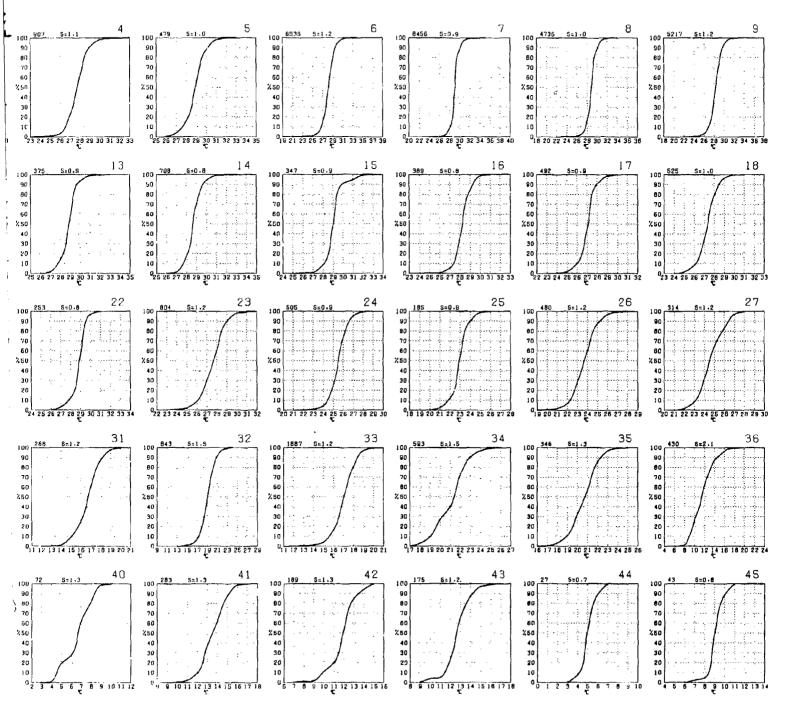
SEA SURFACE TEMPERATURE



SEA SURFACE TEMPERATURE

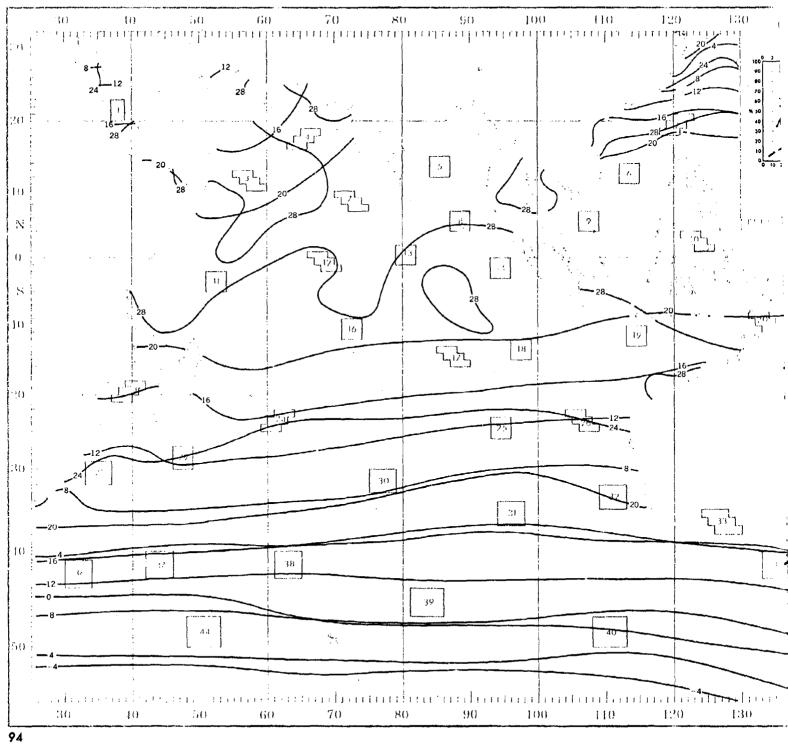


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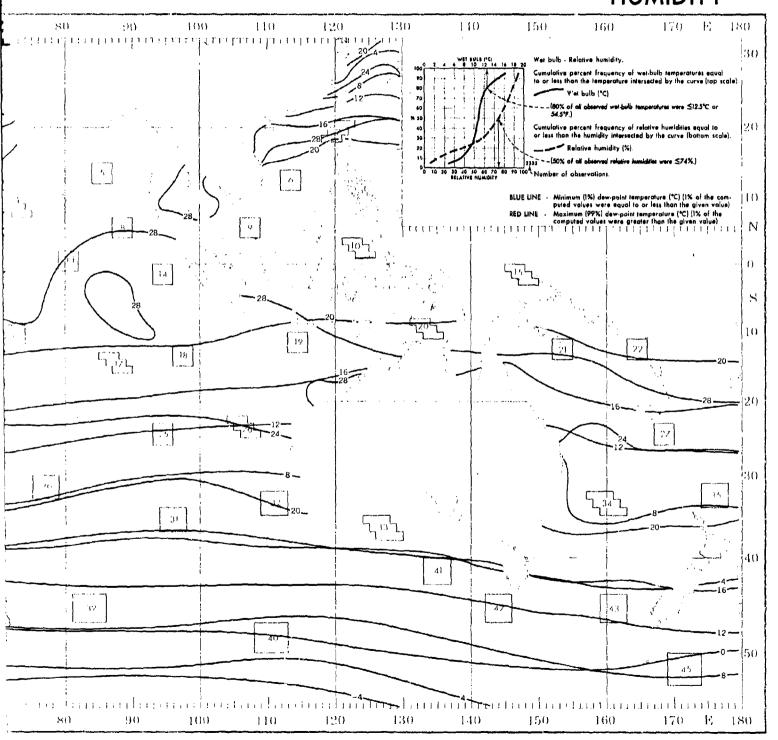


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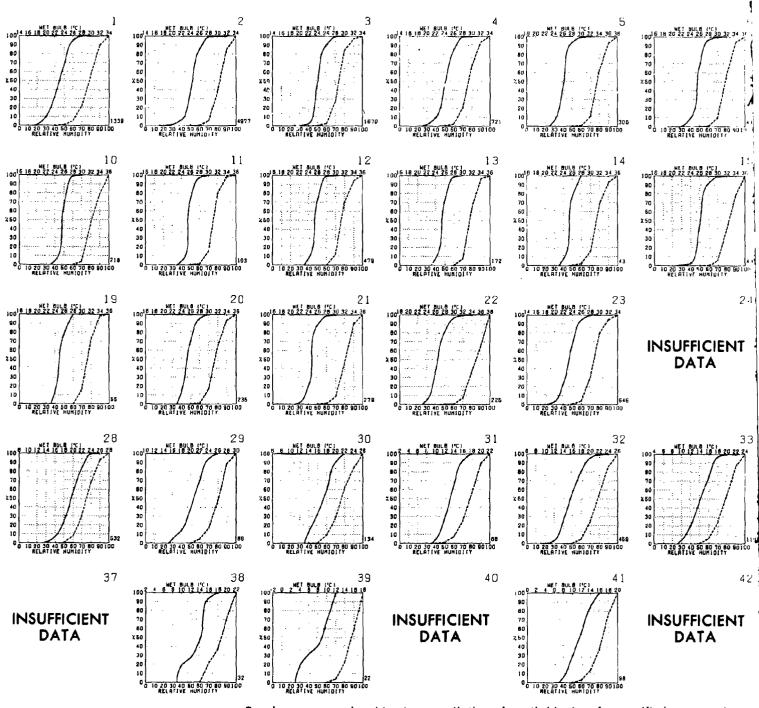
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HUMIDITY

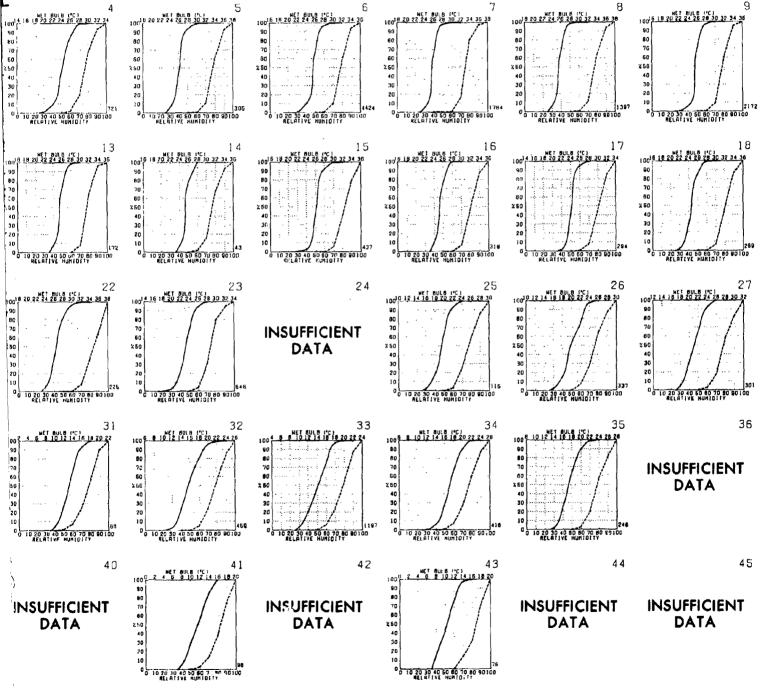


WET BULB AND RELATIVE HUMIDITY

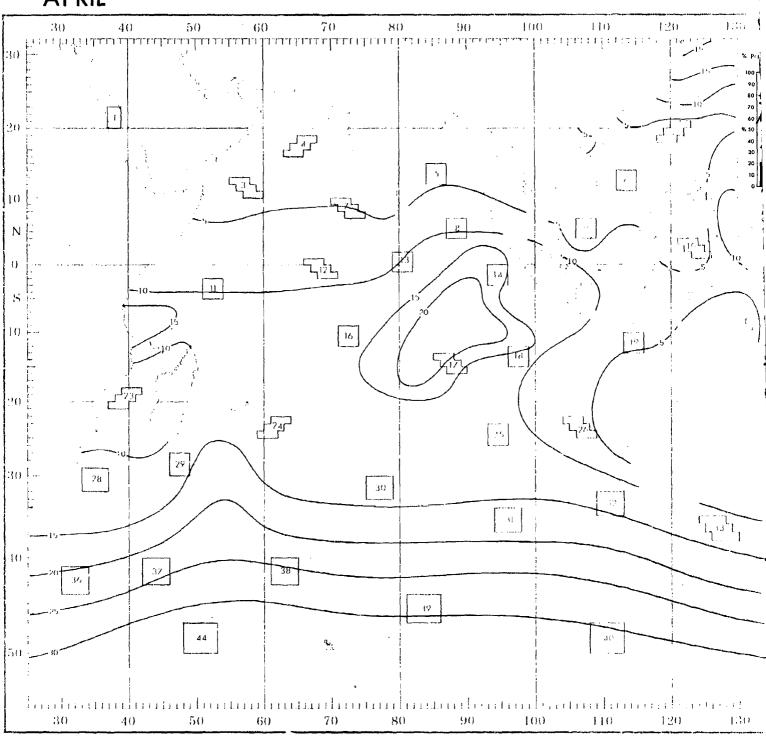


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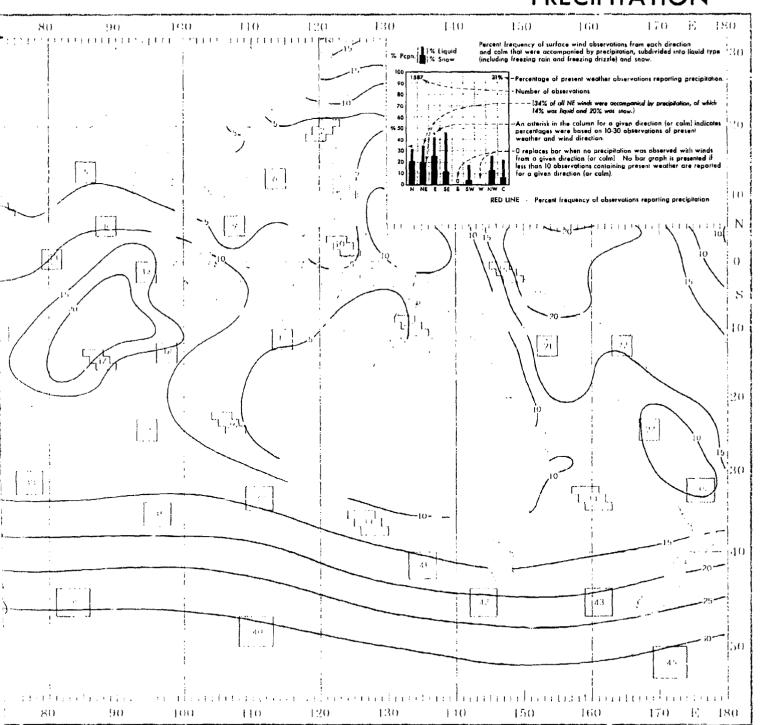




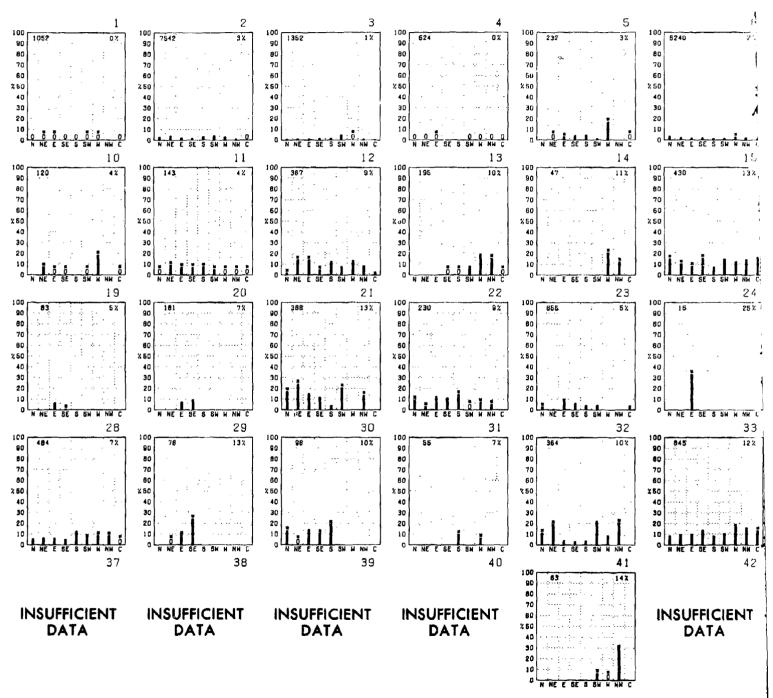
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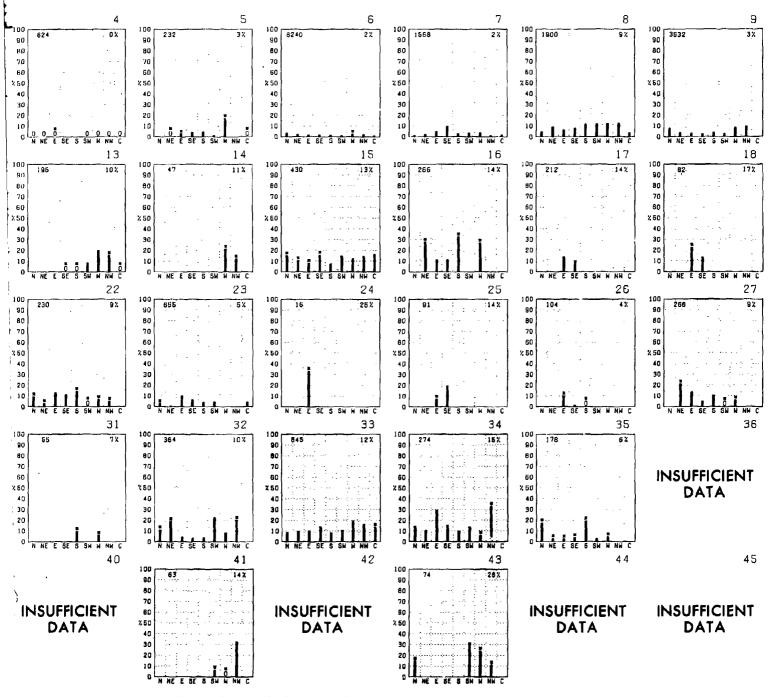
PRECIPITATION



PRECIPITATION

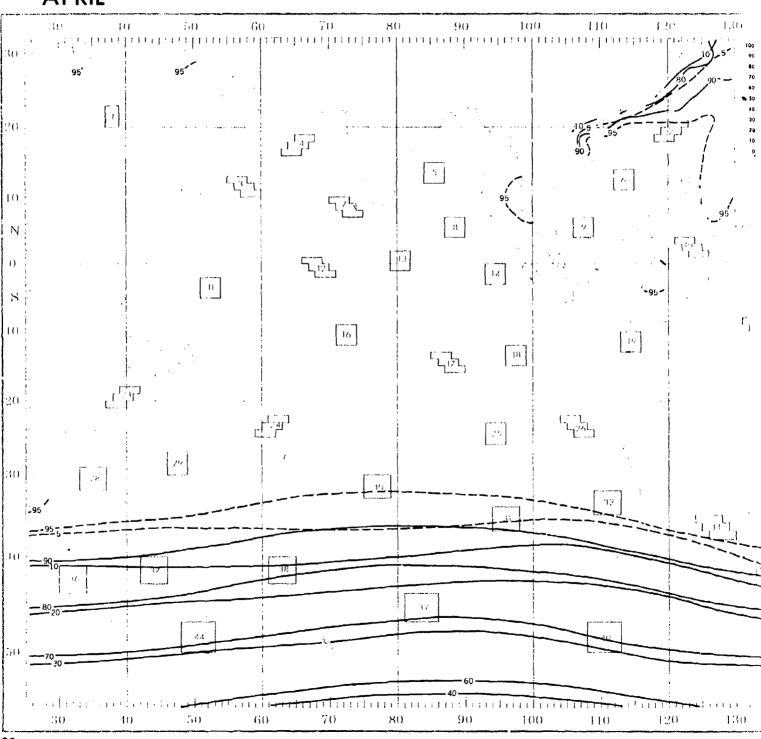


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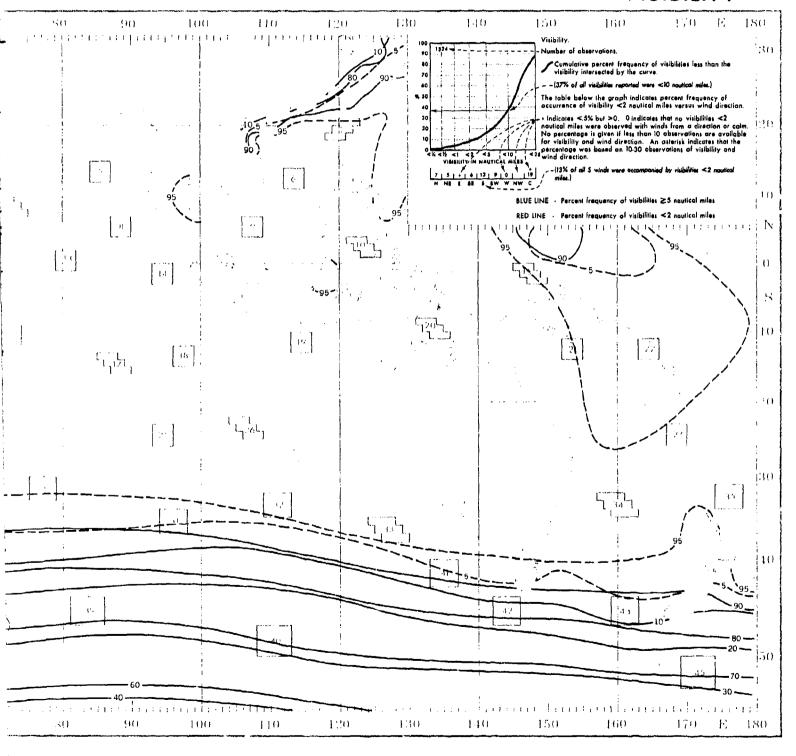


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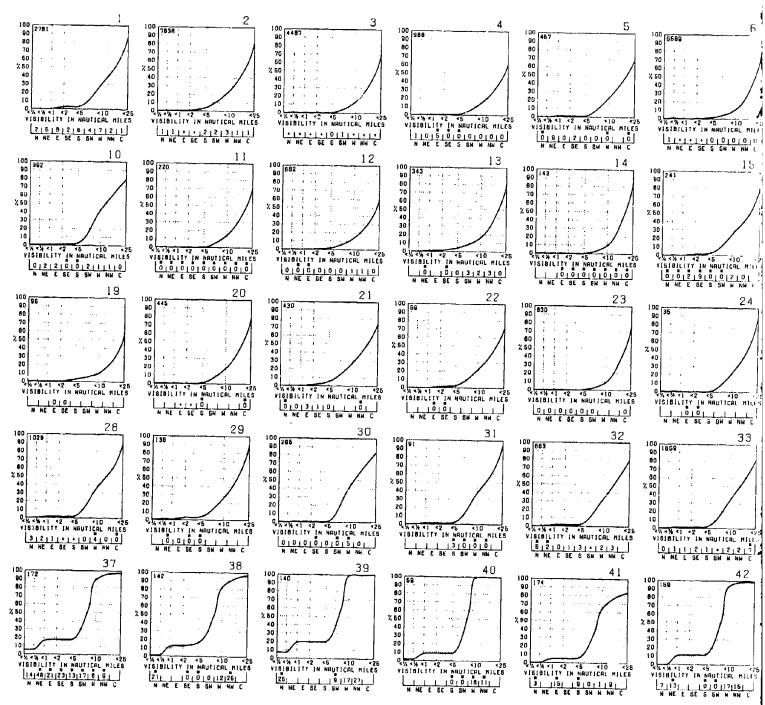
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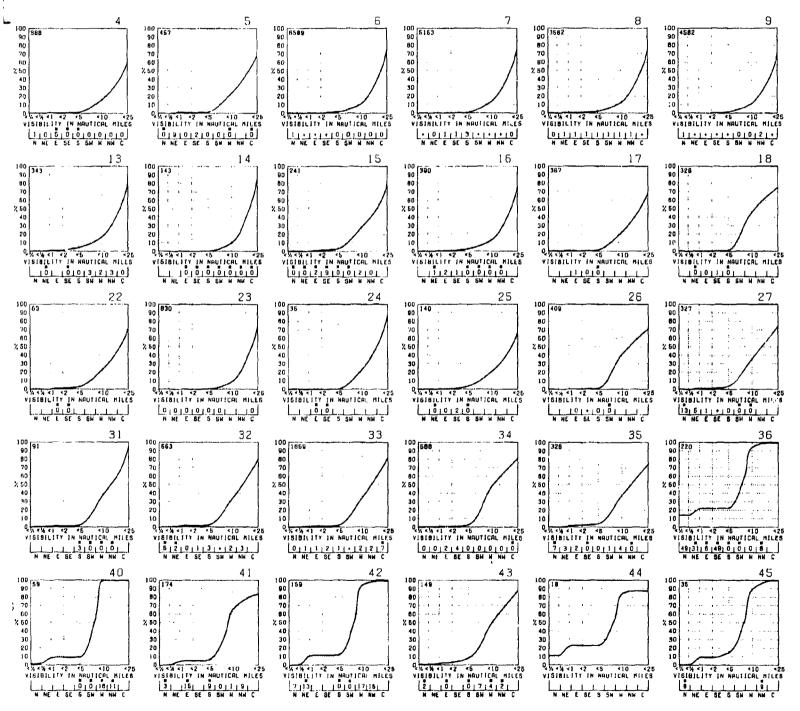
VISIBILITY



VISIBILITY

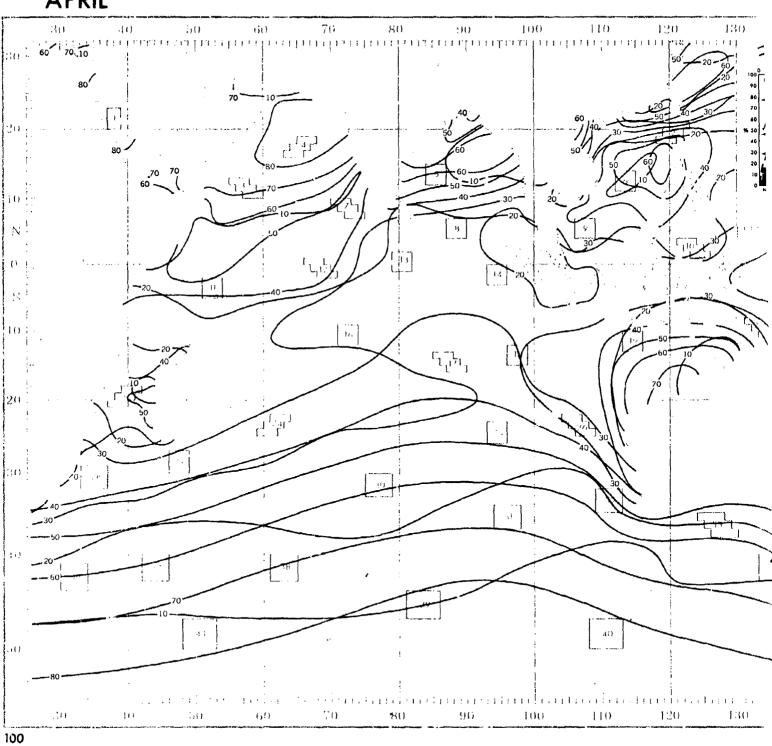


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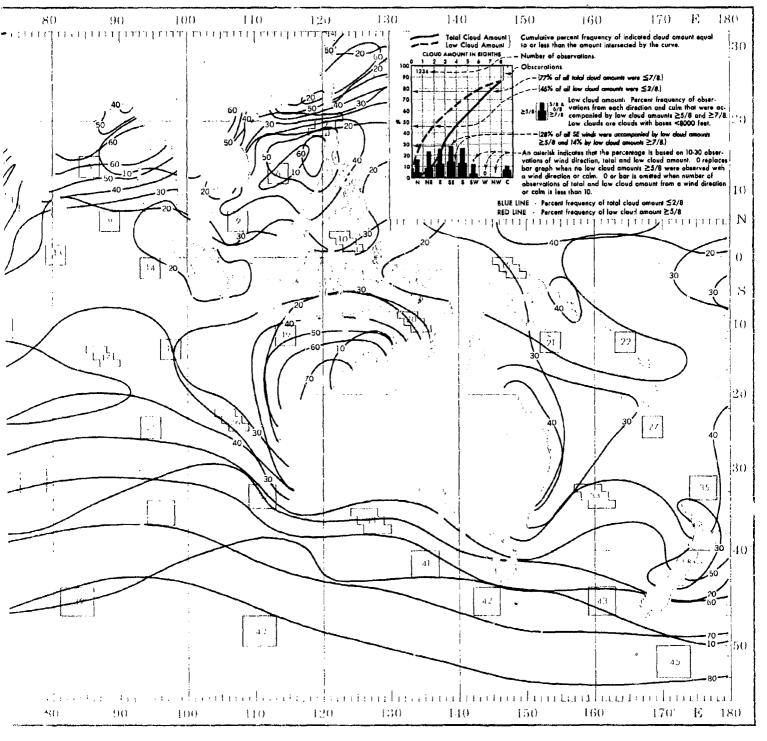


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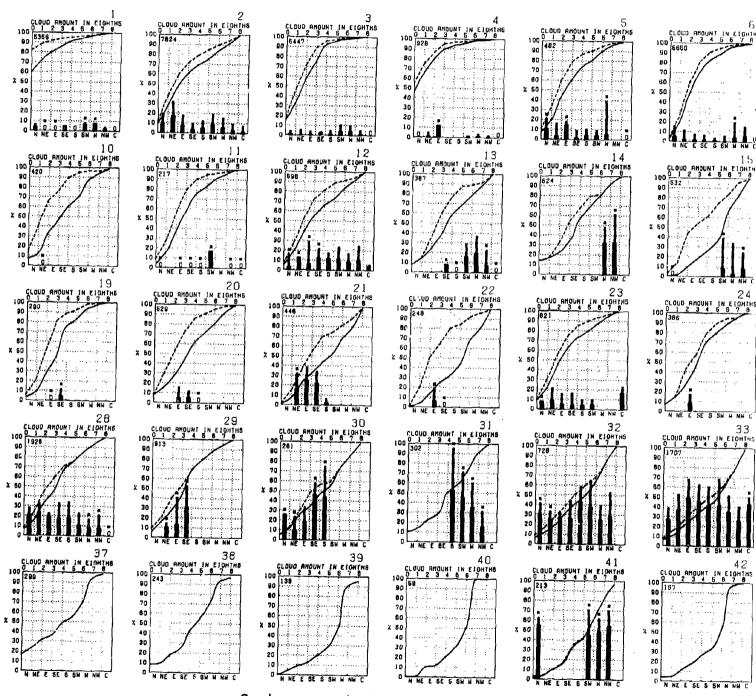
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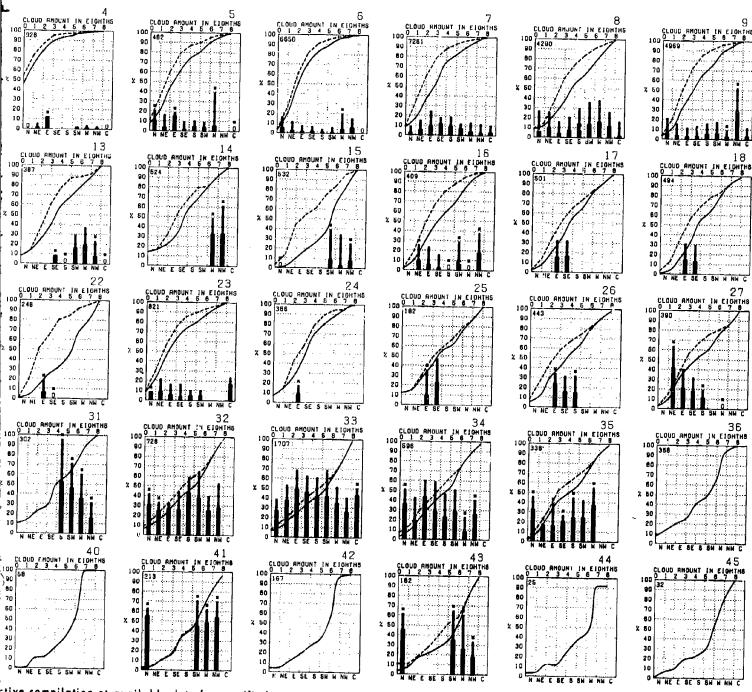
CLOUD COVER



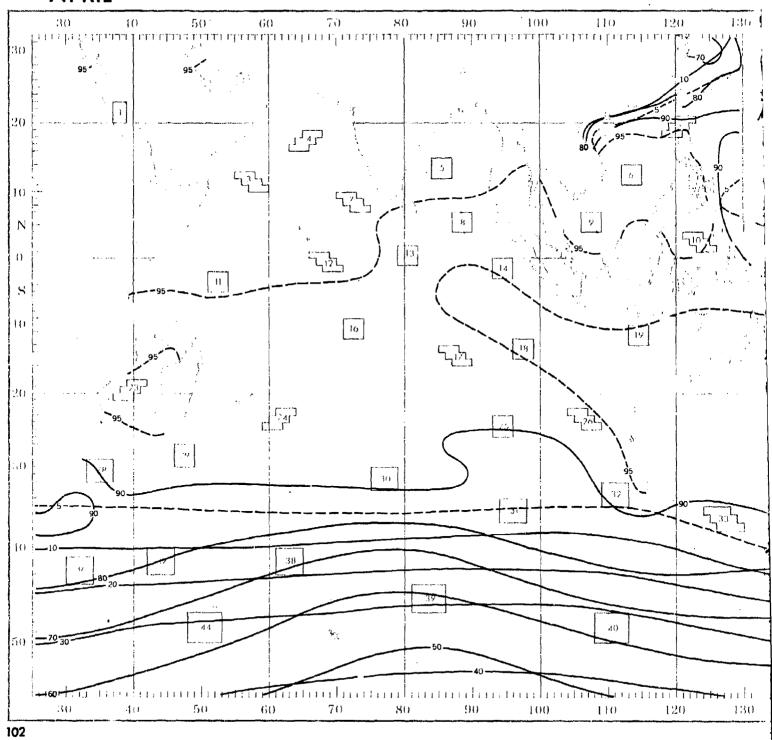
CLOUD COVER



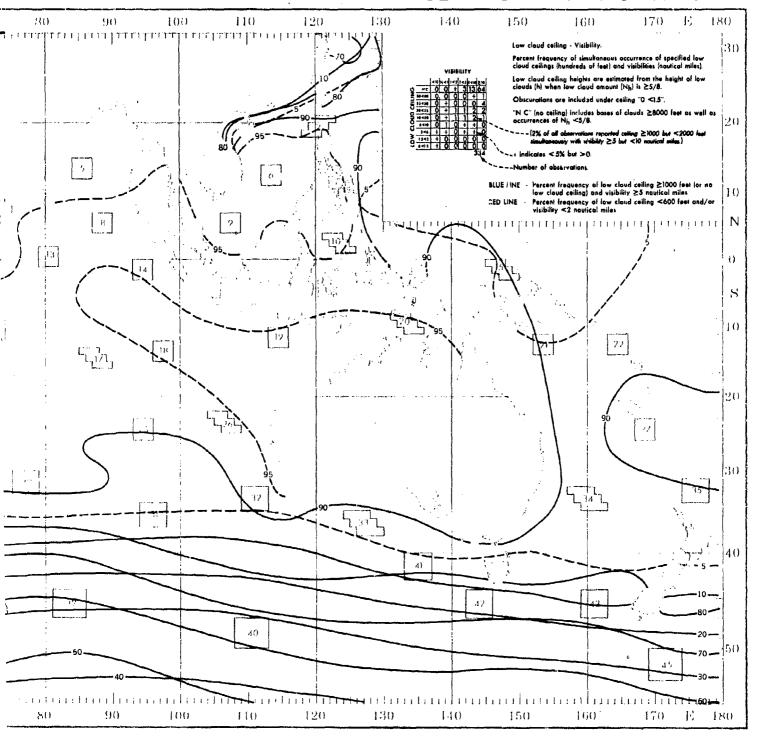
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CEILING AND VISIBILITY



CEILING AND VISIBILITY

VISIBILITY 1 4*/x 7** 1 1* 2*4 \$=10 \$10 WC + 0 0 1 0 0* 50 000 0 0 0 0 50 000 0 0 0 50 000 0 0 0 50 000 0 0 0 50 000 0 0 0 50 000 0 0 0 50 000 0 0 50 000 0 0 50 000 0 0 50 000 0 0 50 000 0 50 000 0 0 50 00	VISIBILITY 2/17 7/21 1-2 2-5 3-10 110 MC	VISIBILITY 4'78 [741] 1-2 [748 [8-10] 110 KC 0 0 0 0 0 2 94 50-40 0 0 0 0 0 0 0 38-40 0 0 0 0 0 0 0 20-38 0 0 0 0 0 0 1 30-40 0 0 0 0 0 0 0 1 30-40 0 0 0 0 0 0 0 0 30-40 0 0 0 0 0 0 0 0 30-40 0 0 0 0 0 0 0 0 30-40 0 0 0 0 0 0 0 0 30-40 0 0 0 0 0 0 0 0 30-40 0 0 0 0 0 0 0 0 30-40 0 0 0 0 0 0 0 0 30-40 0 0 0 0 0 0 0 0 30-40 0 0 0 0 0 0 0 0	VISIBILITY -1/2 1/4 1/2 2/4 5/10 1/0 -1/2 1/4 1/2 2/4 5/10 1/0 -1/2 1/4 1/2 2/4 5/10 1/0 -1/2 1/4 1/2 2/4 5/10 1/0 -1/2 1/4 1/2 1/4 5/10 1/0 -1/2 1/4 1/4 1/4 1/4 1/0 -1/2 1/4 1/4 1/4 1/4 1/4 -1/2 1/4 1/4 1/4 1/4 -1/2 1/4 1/4 1/4 1/4 -1/2 1/4 1/4 1/4 -1/2 1/4 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 -1/	VISIBILITY	VISIBILITY
VISIBILITY *****	VIGIBILITY *'/# */**	VISIBILITY 1 2 1/24	VISIBILITY 1-1-	VISIBILITY -1/2 7/4 7/4 1/2 2/2 5/4 0/4 0/4 -1/2 7/4 1/2 2/2 5/4 0/4 0/4 -1/2 7/4 1/2 2/2 5/4 0/4 0/4 -1/2 7/4 1/2 2/2 5/4 0/4 -1/2 7/4 1/2 2/2 5/4 0/4 -1/2 7/4 1/2 2/2 5/4 0/4 -1/2 7/4 1/2 2/2 5/4 0/4 -1/2 7/4 1/2 2/2 5/4 0/4 -1/2 7/4 1/2 2/2 5/4 0/4 -1/2 7/4 1/2 1/2 1/2 -1/2 7/4 1/2 1/2 1/2 -1/2 7/4 1/2 1/2 1/2 -1/2 7/4 1/2 1/2 1/2 -1/2 7/4 1/2 1/2 -1/2 7/4 1/2 1/2 -1/2 7/4 1/2 1/2 -1/2 7/4 1/2 1/2 -1/2 7/4 -1/2 7/4 1/2 -1/2 7/4 1/2 -1/2 7/4 1/2 -1/2 7/4 1/2 -1/2 7/4 1/2 -1/2 7/4 1/2 -1/2 7/4 1/2 -1/2 7/4 1/2 -1/2 7/4 1/2 -1/2 7/4	VISIBILITY 4 1/2 7/4 1 4 2 2 4 8 5 10 210
VISIBILITY -(-/	VISIBILITY 2 0 **********************************	VISIBILITY 21	VISIBILITY 22 -1/1 f/4+ 142 f-8 8-10 -10 NC 0 0 0 0 0 4 78 5-490 0 0 0 0 0 0 0 25-50-50 0 0 0 0 0 0 10-20 0 0 0 0 0 4 2 6-10 0 0 0 0 0 0 4 7-10 0 0 0 0 0 0 0 0 10-20 0 0 0 0 0 0 0 0 10-20 0 0 0 0 0 0 0 0 10-20 0 0 0 0 0 0 0 0 10-20 0 0 0 0 0 0 0 0 10-20 0 0 0 0 0 0 0 0 10-20 0 0 0 0 0 0 0 0 10-20 0 0 0 0 0 0 0 0 10-20 0 0 0 0 0 0 0 0	VISIBILITY 23 (1) (VISIBILITY 2 4 -1/2 FACI 1-1/2 2-1/2 1-1/2
VISIBILITY 28 4 1/2 7 1 28 2 5	VISIBILITY 29 **V*********************************	VISIBILITY 3 0	VISIBILITY **** **	VISIBILITY AC 0 0 0 0 0 2 48 See 0 0 0 0 0 0 2 48 See 0 0 0 0 0 0 1 5 See 0 0 0 0 0 0 1 5 See 0 0 0 0 0 0 1 5 See 0 0 0 0 0 0 1 5 See 0 0 0 0 0 0 1 5 See 0 0 0 0 0 0 1 5 See 0 0 0 0 0 0 1 5 See 0 0 0 0 0 0 1 1 See 0 0 0 0 0 0 1 1 See 0 0 0 0 0 0 0 1 See 0 0 0 0 0 0 0 0 1 See 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 See 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY 3 3 3 3 3 4
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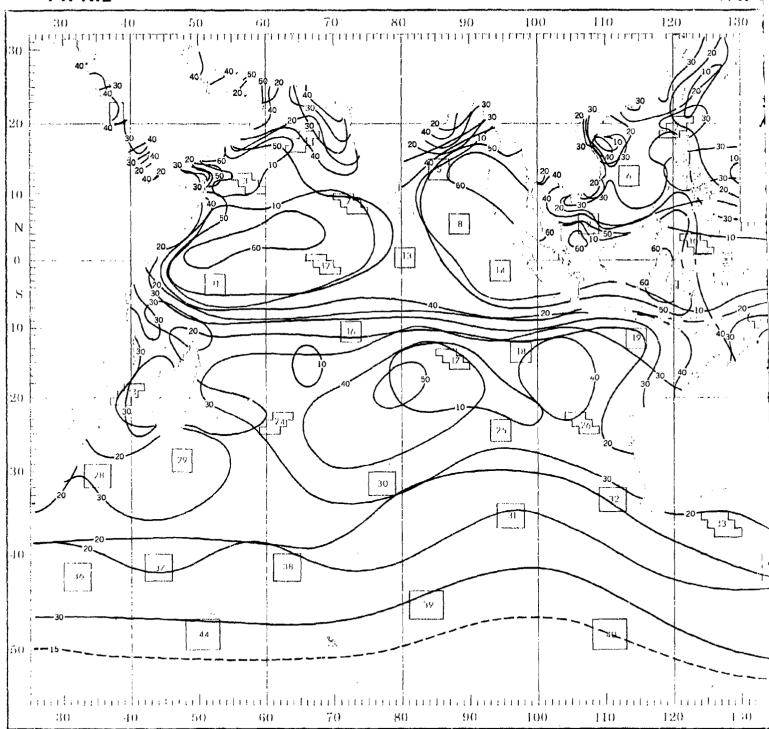
Graphs represent the objective compilation of available data for specified areas without rec The isopleth analyses (apposite page) are based on all available data subjectively adjusted

8-10 0 0 0 0 3 10

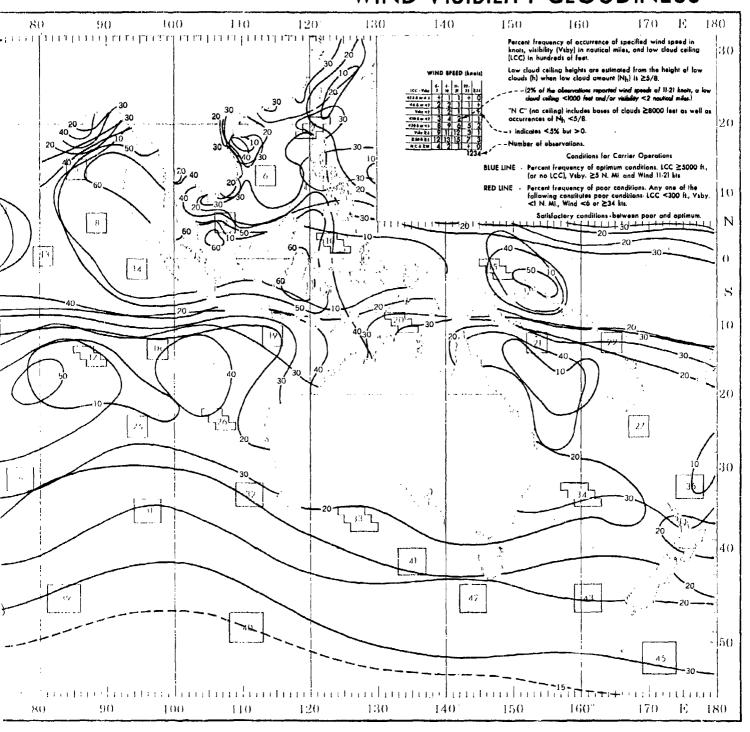
VISIBILITY ACC 0 1 8 88 BU-80 0 0 0 0 0 0 0 0 35-60 0 0 0 0 0 0 1 - 10-20 0 0 0 0 0 0 1 - 11-20 0 0 0 0 0 0 0 1-5-3 0 0 0 0 0 0 0 1-5-3 0 0 0 0 0 0 0 1-5-3 0 0 0 0 0 0 0 1-5-3 0 0 0 0 0 0 0 704	VISIBILITY 5 **/vg /4e1 1=2 2=6 8=10 10 NC	VISIBILITY 6 1-1/2 1/4 1/4 1/4 2 2 2 2 2 3 3 1 1 1 10 10 10 1 1 1 2 2 2 2 3 3 1 10 10 10 10 10 10 1 10 10	YISIBILITY VISIBILITY VISIBILITY ACC + 0 0 0 + 3 06 50-00 0 0 0 0 0 + 1 30-00 0 0 0 0 0 + 2 10-20 0 0 0 0 0 + 4 1.4-3 0 0 0 0 0 0 0 0 1.4-3 0 0 0 0 0 0 0 0 1512	VISIBIL 17Y	VISIBILITY
VISIBILITY VISIBILITY AC 0 0 0 1 2 74 S040 0 0 0 0 0 0 0 0 S18450 0 0 0 0 0 0 1 4 2015 0 0 0 0 0 1 4 G1020 0 0 0 0 0 1 4 G1020 0 0 0 0 0 2 3 6 G100 0 0 0 0 0 1 2 3 T 345 0 1 1 0 0 0 0 G115 0 0 0 0 0 0 0 0 G115 0 0 0 0 0 0 0 0 0 T 345 0 1 1 0 0 0 0 T 345 0 1 1 1 0 0 0 0 G115 0 0 0 0 0 0 0 0 0 0	VISIBILITY 1 4	VISIBILITY ***********************************	VISIBILITY **/** **/** 1 ** 2 ** 3 ** 0 **	1 7 7 7 7 7 7 7 7 7	V S S L V S S L V S S S L V S S S L V S S S L V S S S L V S S S S S S S S S S S S S S S S S
VISIBILITY	VISIBILITY 23 NC 0 0 0 0 0 2 04 S0 00 0 0 0 0 1 S0 00 0 0 0 0 1 S0 00 0 0 0 0 1 S0 00 0 0 0 0 0 1 S0 00 0 0 0 0 0 1 S0 00 0 0 0 0 0 0 S0 00 0 0 0 0 0 0 S0 00 0 0 0	VISIBILITY 24	VISIBILITY 25 -1/2 1/4 1/4 2 2 5 1/4 1/4 -1/2 1/4 1/4 2 2 5 1/4 1/4 -1/2 1/4 1/4 2 2 5 1/4 1/4 -1/2 1/4 1/4 2 2 5 1/4 -1/2 1/4 1/4 2 2 5 1/4 -1/2 1/4 1/4 1/4 2 2 5 -1/2 1/4 1/4 1/4 1/4 -1/2 1/4 1/4 1/4 1/4 -1/2 1/4 1/4 1/4 1/4 -1/2 1/4 1/4 1/4 1/4 -1/2 1/4 1/4 1/4 1/4 -1/2 1/4 1/4 1/4 -1/2 1/4 1/4 1/4 -1/2 1/4 1/4 1/4 -1/2 1/4 1/4 1/4 -1/2 1/4 1/4 1/4 -1/2 1/4 1/4 1/4 -1/2 1/4 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 1/4 -1/2 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 -1/2 1/4 1/4 -1/2 1/4 1/4 -1/2 1/4 -1/2 1/4 1/4 -1/2 1	VISIBILITY Z S	VISIBILITY 27
VISIBILITY 31	VISIBILITY 32 ***	**************************************	VISIBILITY 3 4 ***	VISIBILITY 355 NC 0 0 1 0 1 59 50-60 0 0 0 0 0 0 2 25-60 0 0 0 0 0 0 3 50-60 0 0 0 0 0 0 0 2 50-60 0 0 0 0 0 0 0 3 50-60 0 0 0 0 0 0 0 3 50-60 0 0 0 1 0 0 0 3 50-60 0 0 0 1 0 0 0 0 3 50-60 0 0 0 1 0 2 9 6-10 0 0 0 0 2 2 13 50-60 0 0 0 0 1 1 0 6-10 0 0 0 0 0 0 0 0 186	INSUFFICIENT DATA
INSUFFICIENT DATA	# 10410	INSUFFICIENT DATA	VISIBILITY 4 3 *** *** *** *** *** *** ***	INSUFFICIENT DATA	INSUFFICIENT DATA

ctive compilation of available data for specified areas without regard to suspected biases.

osite page) are based on all available data subjectively adjusted where bias was evident.



WIND-VISIBILITY-CLOUDINESS



LOW CLOUD CEILING-VISIBILITY-WIND

MC A P 10

V887 k8 0 25 36 25 0

0 13 13 6 0

MIND SPEED (KNOTS)	2 NIND SPEED (KNDTS) LCC - VARY	MIND SPEED (XNOTS)	HIND SPEED (KHDTS) LCC - VABY	HIND SPEED (KNOTS) LCC - VORT 9 10 21 33 344 -1.8 & GR - 18 0 0 0 0 0 0 -44 GR - 2 0 1 0 0 0 VARY - 2 0 0 0 0 0 -13 & GR - 2 0 0 0 0 -13 & GR - 2 0 0 0 0 -13 & GR - 2 0 0 0 0 -13 & GR - 2 0 0 0 0	HIND SPEED (KNOTS LCC - V447 3 10 21 33 5 41.4 4.04 - 1.5 0 0 0 0 48.4 04 - 2 0 0 0 0 V887 - 2 0 0 0 0 - 10 4.08 - 2 0 1 3 0 - 10 4.08 - 2 0 1 3 0 - 10 4.08 - 2 0 1 3 0 - 10 4.08 - 2 0 1 3 0 - 10 4.08 - 2 0 1 3 0
VABY 48	VARY AS 8 37 41 0 + A50 4 NB 8 34 32 5 + MC 4 N 10 7 29 27 4 + B 407 1 1 HIND SPEED (KNDTS) LCC - Y88Y 0 1 0 21 33 234 -1.64 OR 4.5 0 0 0 0 0 0 VARY 42 0 0 0 0 0 0	VBBY + S	V88Y 18 18 65 16 4 0 2	VBBY AS	VSST-88
410 4 04 *2	10 4 08 42 1 2 1 0 0 0	10 4 08 - 92	*10 4 04 *2	-10 4 08 42 0 4 0 2 0 -20 4 04 48 2 13 2 2 0 -20 4 04 18 19 67 12 2 0 -20 4 04 18 19 67 12 2 0 -20 4 04 18 19 67 12 2 0 -20 4 04 18 19 67 12 2 0 -20 4 04 18 19 67 12 2 0 -20 4 04 18 19 67 12 2 0 -20 4 04 18 18 18 18 18 18 18 18 18 18 18 18 18	410 4 08 42 0 3 0 0 1 120 4 08 45 1 1 0 7 0 1 121 43 15 0 1 121 43 15 0 1 121 43 15 0 1 121 43 15 0 1 121 43 15 0 1 121 43 15 0 1 121 43 15 0 1 121 43 15 0 1 121 43 15 0 1 121 43 15 0 1 121 43 15 0 1 121 43 15 0 1 131
*** 4 00 *** 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-94 - 64 - 62	-6 4 08 -2	-5 & OR -2 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-6 1 08 -2	44 4 08 *2
CCC - V66Y 8 0 4 11 27 39 384 1.6 4 08 4-8 0 + U 0 0 0 18 4 08 4-8 1 1 1 1 0 V88Y 48 0 0 0 0 0 0 0 10 4 08 4-8 1 2 3 2 1 420 4 18 4 6 1 7 8 4 1 V68Y 98 7 37 43 10 2 850 4 38 5 30 32 5 1 MC 4 1 0 5 29 32 4 1 MC 4 1 0 5 29 32 4 1 3 7	CCC - V887		CC - V68x 3 0 1 11 27 27 3 324 4 1 1 1 3 324 4 1 1 1 3 324 4 1 1 1 1 1 1 1 1	CC - V88Y 3 10 21 33 284 41-8 4 08 4-8 0 + 0 0 0 0 48 4 08 4-7 0 0 0 0 0 V88Y 47 0 0 0 0 0 0 40 4 08 47 0 0 2 3 3 1 420 4 08 45 0 13 6 1 V88Y 88 6 4 22 11 2 550 4 8 4 4 25 19 4 1 MC 4 8 10 4 23 16 3 1 392	LCC - VSSY
INSUFFICIENT DATA	MIND SPEED (KNOTS) LCC - VSSY	INSUFFICIENT DATA	INSUFFICIENT DATA	4 1 MIND 6PEED (KNOT8) LCC - V667 9 10 21 35 35 4 4 1 1 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	INSUFFICIENT DATA

Graphs represent the objective compilation of available data for specified areas without re The Isopleth analyses (opposite page) are based on all available data subjectively adjuste

3 19 56 19 0 0 4 26 4 0 0 4 25 4 0

V681 MB 2 80 4 BE

NC 4 = 10

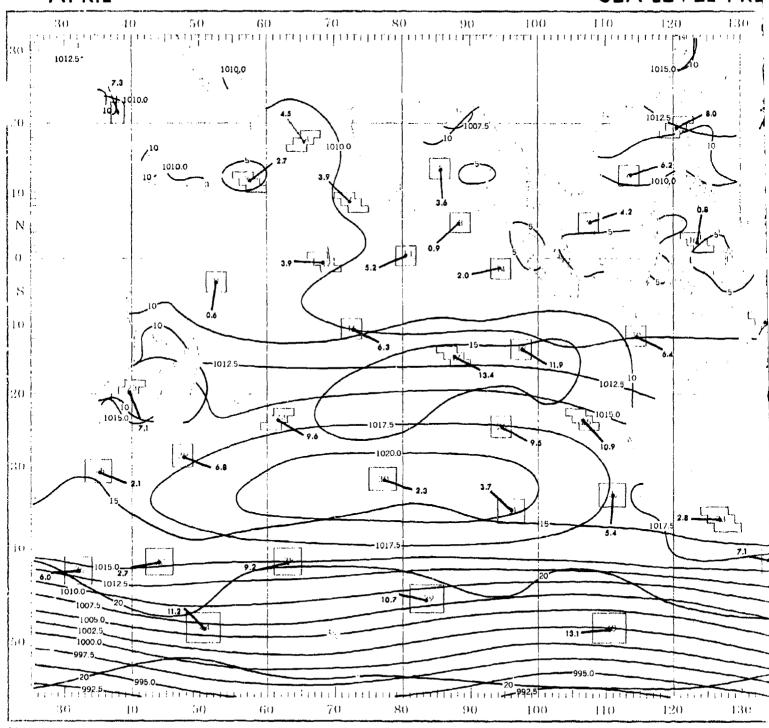
LITY-WIND

APRIL

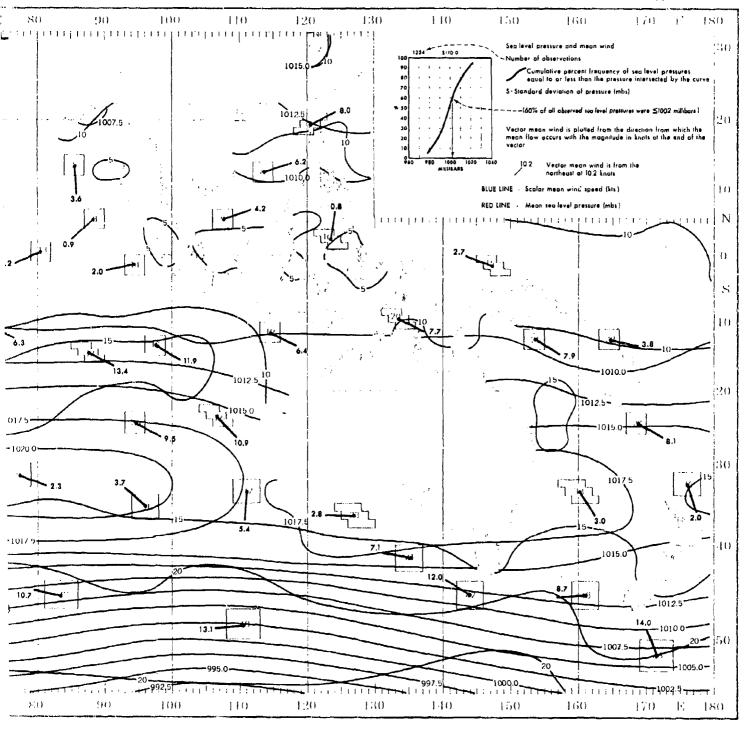
HIND SPEED (KNDTS) LCC - V887 3 10 77 37 37 38 4 11-18-1 38 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	WIND SPEED (KNOTS) UCC - VSSY 3 10 21 33 334 *1.54 08**.5 0 0 0 0 0	6 WIND SPEED (KNOTS) LCC - VNNY 3 10 21 35 334 11.6404 - 6 0 9 9 9 9 0	77 WIND SPEED (KNOTS) LCC - VORY 9 10 21 39 394 41.8167.41 0 0 0	MIND SPEED (KNOTS) LCC - Y88Y 9 10 17 39 344	HIND SPEED (MNOTS)
-84 08 -2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-64 OR -72 0 1 0 0 0 VARY -2 0 + 0 0 0 -104 OR -2 + 2 0 0 + -204 OR -3 1 4 0 1 4 VARY -8 26 65 6 2 4 -504 A6 24 50 6 1 0	-64 GR -2	*66 58 *2	- 64 08 - 27 + 1 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	**E 4 08 *2
1 3 HIND SPEED (KNOTS)	MC 4 = 10 19 59 5 1 0 239 1 4 WIND SPEED (KNOIS)	MG 4 + 10 7 53 23 + 0 5399 1 5 WIND SPEED (KNOTS)	MC4 = 10 24 54 B 0 0 1466 1 6 HIND SPEED (KND15)	MC4+10 27 37 5 0 0 1455 1 7 MIND SPEED (MNOTS)	18
CCC - VARY 9 10 61 39 394 11 61 39 394 11 61 39 394 11 61 61 61 61 61 61 6	CC - VBBY 9 10 71 39 394 *1.8 4 0R *.6 0 0 0 0 0 0 0 *8 4 0R *2 0 0 0 0 0 0 *10 4 0R *2 0 4 0 2 0 *10 4 0R *2 2 0 4 0 2 0 *20 4 0R *2 2 0 4 0 2 0 *20 4 0R *2 2 0 4 0 2 0 *20 4 0R *2 4 0 2 0 *20 4 0R *2 4 0 4 0 2 0 *20 4 0R *2 4 0 4 0 2 0 *20 4 0R *2 4 0 4 0 2 0 *20 4 0R *2 4 0 4 0 2 0 *20 4 0R *2 4 0 4 0 2 0 *20 4 0R *2 4 0 4 0 2 0 *20 4 0R *2 4 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	LCC - VBBY 3 - 1 - 1 - 1 - 22 - 3 - 3 - 3 - 4 - 1 - 3 - 3 - 5 - 3 - 4 - 3 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5	CC - V88Y 0-4 11 27 3 3 3 3 3 4 4 5 4 6 7 7 1 0 0 0 0 0 0 0 0 0	CC - VESY 3 6 1 28 33 34	CC - VBBY 0- 4- 11- 21- 31- 34- 34- 31- 31- 31- 31- 31- 31- 31- 31- 31- 31
26 37 11 1 0 167 27 22 WIND SPEED (MNDIS)	MC4410 13 42 4 0 0 52 73 WIND SPEED INNOTS!	MEC 10 14 39 17 0 0 70 2 4 MIND SPEED (KNOT6)	MC4*10 9 45 20 + 0 294 25 MIND SPEED (KNOTS)	2 22 37 2 0 267 26 MIND SPEED (KNOTS)	MC 6 8 10 3 21 37 5 0 131 27 HIND SPEED (KNOTS)
CCC + VBBY 3 10 21 33 394	CC - VASI 9 O C 11 127 13 334 14 14 14 15 15 15 15 1	CCC - VBSY 73 10 41 13 134	CCC - VSBV 3 10 21 33 344 -1.54.08 < 2 0 0 0 0 0 -1.54.08 < 2 0 0 0 0 0 -1.54.08 < 2 0 0 0 0 0 -1.54.08 < 2 0 0 0 0 0 -1.54.08 < 2 1 2 4 1 0 -1.54.08 < 5 1 7 18 1 0 -1.54.08 < 5 1 7 18 1 0 -1.54.08 < 5 3 25 30 3 0 -1.54.08 < 6 3 25 30 3 0 -1.54.08 < 6 3 25 30 3 0 -1.54.08 < 7 3 23 27 3 0 -1.54.08 < 7 3 23 27 3 0 -1.54.08 < 7 3 23 27 3 0 -1.54.08 < 7 3 23 27 3 0 -1.54.08 < 7 3 23 27 3 0 -1.54.08 < 7 3 23 27 3 0 -1.54.08 < 7 3 23 27 3 0 -1.54.08 < 7 3 23 27 3 0 -1.54.08 < 7 3 23 27 3 0 -1.54.08 < 7 3 23 27 3 0 -1.54.08 < 7 3 24 24 24 24 24 24 24	CC - V8BY 3 0 21 33 244 -1.8 4 0R 4.8 0 0 0 0 0 0 0 -8 4 94 -2 0 1 0 0 0 0 -10 1 0 0 0 0 0 -10 1 0 1 0 0 0 -10 1 0 1 0 1 2 2 0 -10 1 0 1 0 1 2 2 0 -10 1 0 1 0 1 0 0 0 -10 1 0 1 0 1 0 1 0 0 0 -10 1 0 1 0 1 0 1 0 0 0 -10 1 0 1 0 1 0 1 0 0 0 -10 1 0 1 0 1 0 1 0 0 0 -10 1 0 1 0 1 0 1 0 0 0 -10 1 0 1 0 1 0 1 0 0 0 -10 1 0 1 0 1 0 1 0 0 0 -10 1 0 1 0 1 0 1 0 0 0 -10 1 0 1 0 1 0 1 0 0 0 -10 1 0 1 0 1 0 1 0 0 0 -10 1 0 1 0 1 0 0 0 0 -10 1 0 1 0 1 0 0 0 -10 1 0 1 0 0 0 0 0 -10 1 0 1 0 0 0 0 0 -10 1 0 1 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -10 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	CC - V68Y 8 10 81 33 344
31	32	33	34	35	36
HIND SPEED 1 KNOTS) LCC - Y88Y 9 10 21 752 224 13.8 4 00 4.8 0 0 0 0 0 -16 4 06 47 0 0 0 0 0 -10 4 06 47 2 9 3 2 0 -20 4 06 -6 2 23 11 2 0 V687 16 6 55 29 11 0 340 4 17 0 18 9 6 0 10 4 4 10 0 17 9 5 0	HIND SPEED (KNOTS) LCG - V68T 3 10 21 33 314 11.8 4.08 - 5 0 0 0 0 0 48 4 98 - 7 0 0 0 0 0 410 4.08 - 7 0 0 0 0 0 410 4.08 - 7 0 2 3 3 1 -20 4.08 - 5 6 40 42 11 2 450 4.56 4 25 19 4 1 8C4 4.10 4 23 18 3 1 382	MIND SPEED (KNDTS) LCC - Y48Y	HIND SPECO (KNOIS) LCC - VSSY 3 10 21 33 244 11.84 SS 4.8 0 0 + 0 0 18.08 2 0 0 + 0 0 18.08 2 0 0 0 0 0 10.40 2 + 5 4 3 2 10.40 2 + 5 4 3 2 10.40 2 + 5 4 3 2 10.40 3 6 1 1 1 1 2 4 10.40 4 6 6 1 2 3 6 4 10.40 4 6 6 1 2 3 6 4 10.40 4 6 6 1 2 3 6 4 10.40 4 6 6 1 2 3 6 4 10.40 4 6 6 6 6 6 6 6 6 6 10.40 4 6 6 6 6 6 6 6 6 6 10.40 4 6 6 6 6 6 6 6 10.40 4 6 6 6 6 6 6 6 10.40 4 6 6 6 6 6 6 10.40 4 6 6 6 6 6 10.40 4 6 6 6 6 6 10.40 4 6 6 6 6 10.40 4 6 6 6 10.40 4 6 6 6 10.40 4 6 6 10.40 4 6 10.40	HIND SPEED (KNOTE) LCC - VS87 3 10 11 32 324 41.8 4 08 4.8 0 0 0 0 0 0 0 44 6 08 42 0 11 1 1 0 1 450 4 08 42 0 4 12 1 1 450 4 08 43 1 31 85 10 1 V887 88 1 31 85 10 1 550 4 5 1 21 34 6 0 MC 4 10 1 20 34 6 0	INSUFFICIENT DATA
40	41	42	43	4 4	45
INSUFFICIENT DATA	NIND SPEED (KNOIS) LCC - VBST 0	INSUFFICIENT DATA	HIND SPEED (INDIS) LCC - VBBY 9 10 E1 89 294	INSUFFICIENT DATA	INSUFFICIENT DATA

ctive compilation of available data for specified areas without regard to suspected biases. josite page) are based on all available data subjectively adjusted where bias was evident.

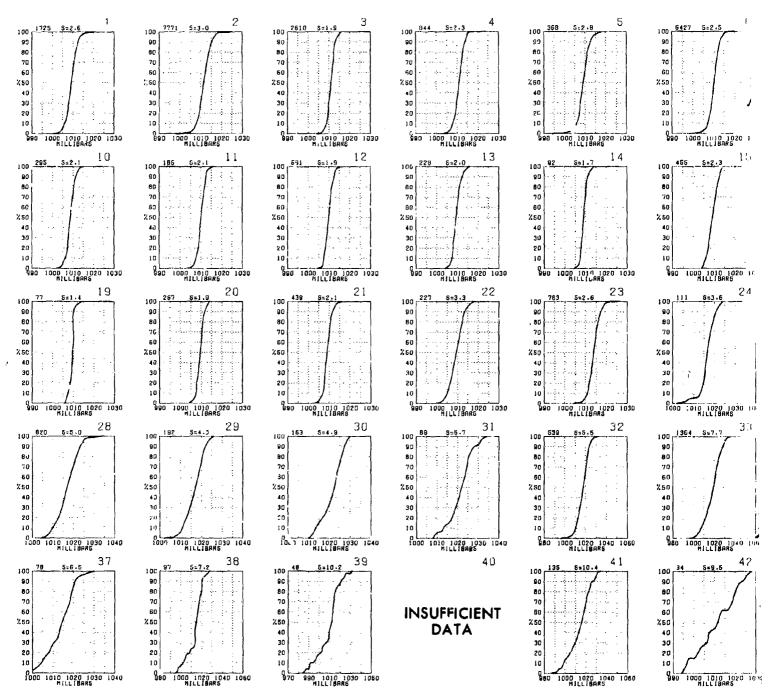
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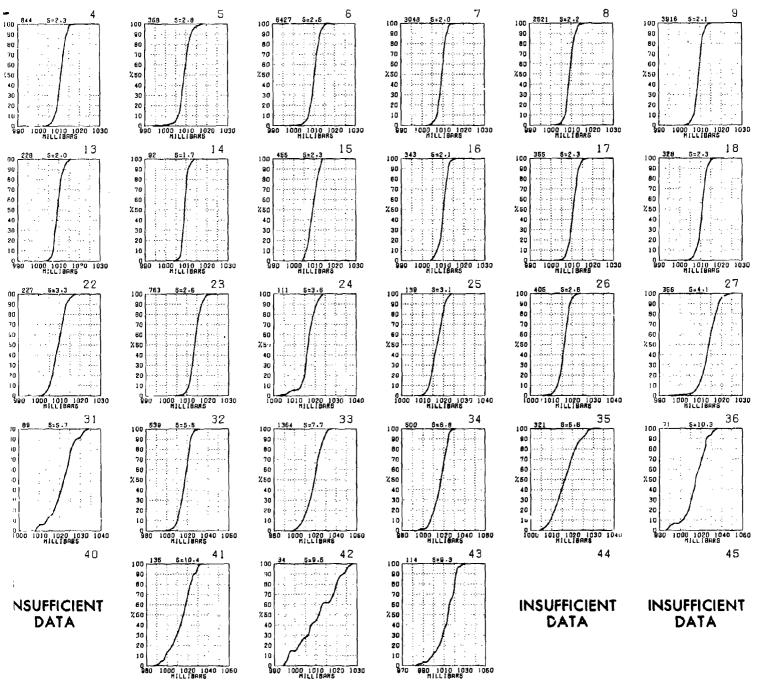
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SEA LEVEL PRESSURE

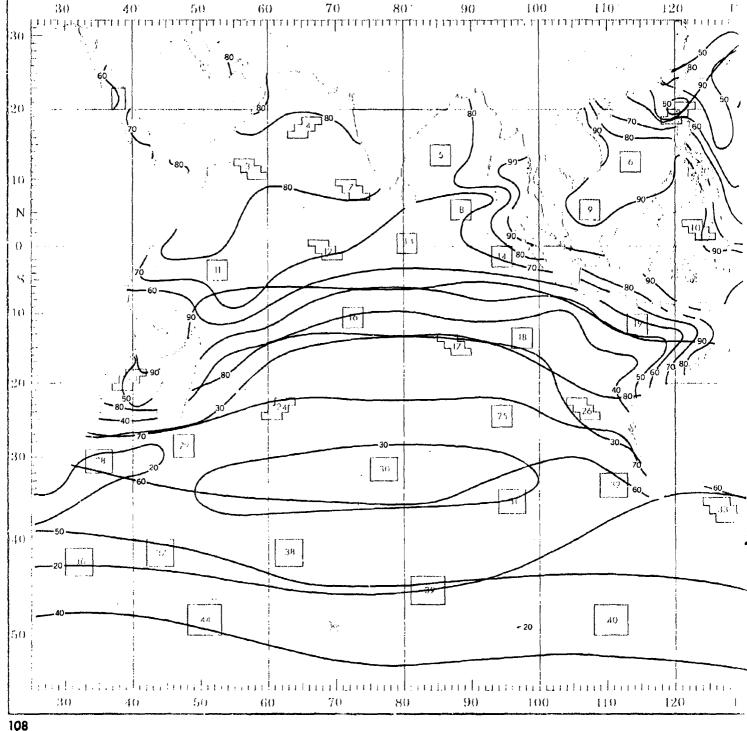


Graphs represent the objective compilation of available data for specified areas without in the isopleth analyses (opposite page) are based on all available data subjectively adjust

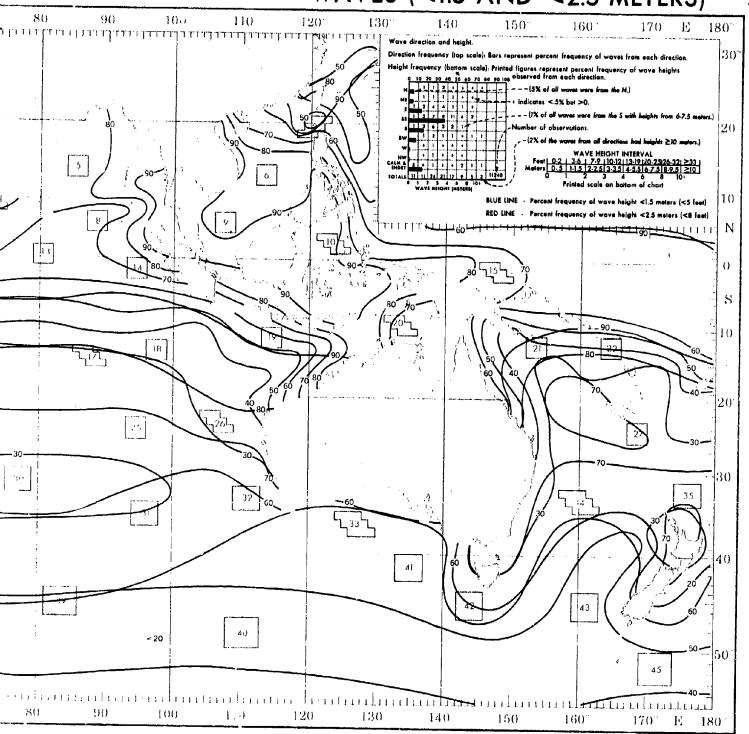


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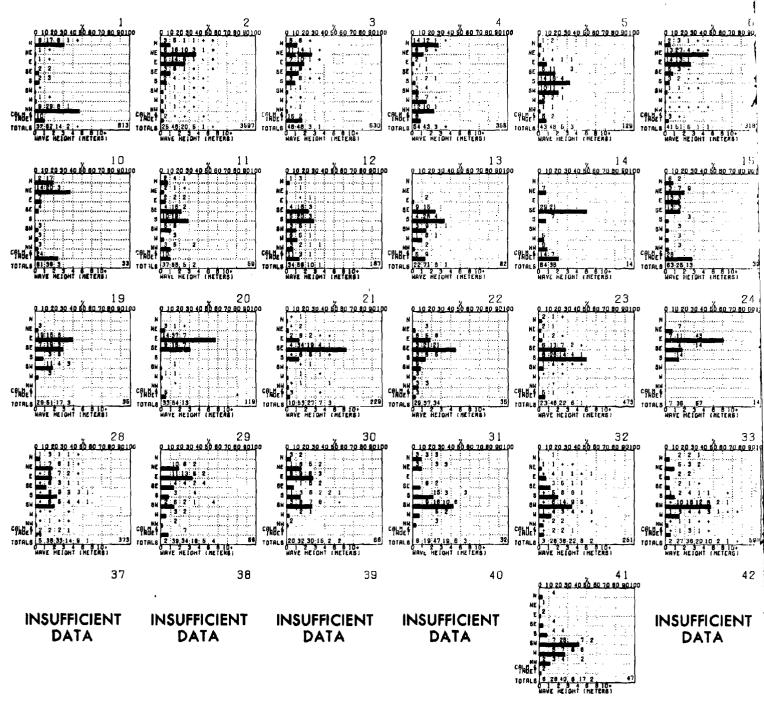
WAVE



WAVES (<1.5 AND <2.5 METERS)

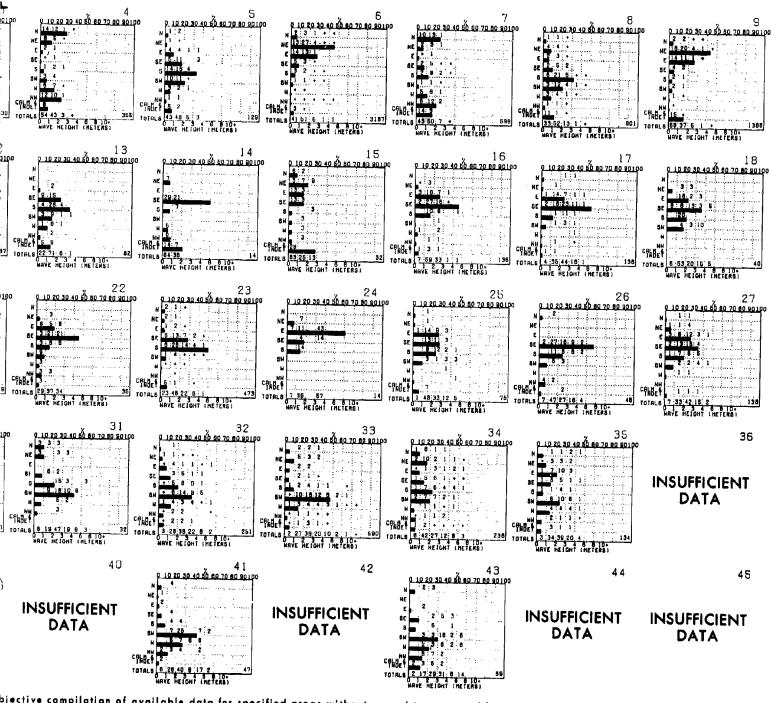


WAVE DIRECTION AND HEIGHT



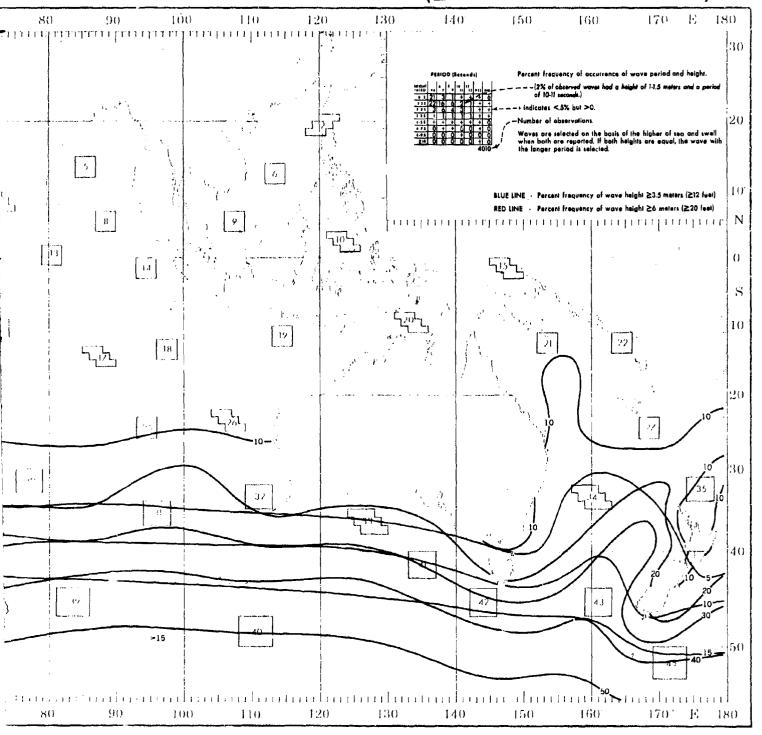
<u>Graphs</u> represent the objective compilation of available data for specified areas without re The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjusted IGHT

APRIL



bjective compilation of available data for specified areas without regard to suspected biases. opposite page) are based on allavailable data subjectively adjusted where bias was evident.

WAVES (≥3.5 AND ≥6 METERS)



WAVE PERIOD AND HEIGHT

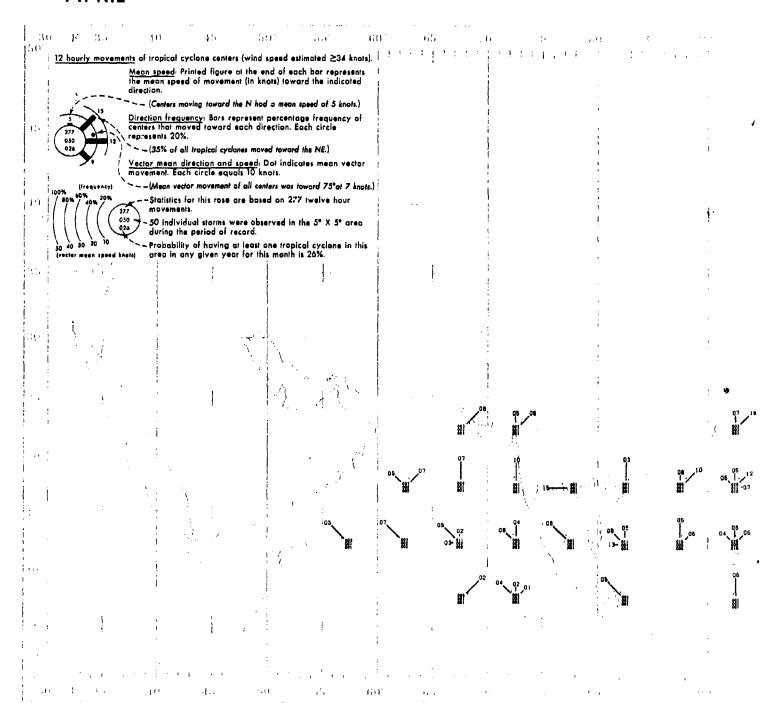
PERIOD (SECONDS) PERIOD (SECONDS) PERIOD (SECO	PERIOD (SECONDS)	FERJOD (SECONDS) **Esem 6	PERIOD (SECONDS) **Closed 6-7 6-1 16-1 18-1 1800	PERIOD (SECONDS) NET 100	PERIOD I SECONDS: 10 10 10 10 10 10 10
8-3-6	3-9.8 • 1 2 1 • • • • • • • • • • • • • • • •	6-1.6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1-3.8 · 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1-1:0 0 2 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	15.16
PERJOD (SECONDS) INTER: 44 8- 8- 18- 18- 12	PERIOD (SECONDS) (KIRR) 4- 7 - 8 - 10- 15- 15- 15- 15- 15- 15- 15- 15- 15- 15	12 PERIOD (SECONDS) 12 16 16 16 16 16 16 16	1 3	INSUFFICIENT DATA	PERIOD SECONOS
PERIOD [SECONDS] PARISO 16 10 13 13 13 PARISO 16 10 13 13 13 PARISO 16 7 6 10 13 13 13 PARISO 16 7 6 11 13 13 13 PARISO 16 14 0 6 0 3 PARISO 16 14 0 6 0 3 PARISO 16 14 0 6 0 3 PARISO 17 17 17 17 PARISO 17 17 17 17 PARISO 17 17 17 PARISO 18 18 18 18 PARISO 18 18 18 18 PARISO 18 PARI	PERIOD (SECONDS) ***RECONT 6 - 10 - 12 - 13 15 160	PERIOD (SECONDE)	22 PERIOD (SECONDS) PERIOD (## Clong Feriod (SECONDS) Feriod (SECONDS) Feriod (SECONDS) Feriod PERIOD (SECONDS) 1 1 1 1 1 1 1 1 1	
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<u>Graphs</u> represent the objective compilation of available data for specified areas without r The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjust

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3 INSUFFICIENT DATA	#ERIOD (SECONDS) #ERIOD (SECONDS) ###################################	INSUFFICIENT DATA	## ## ## ## ## ## ## ## ## ## ## ## ##	INSUFFICIENT DATA	INSUFFICIENT DATA

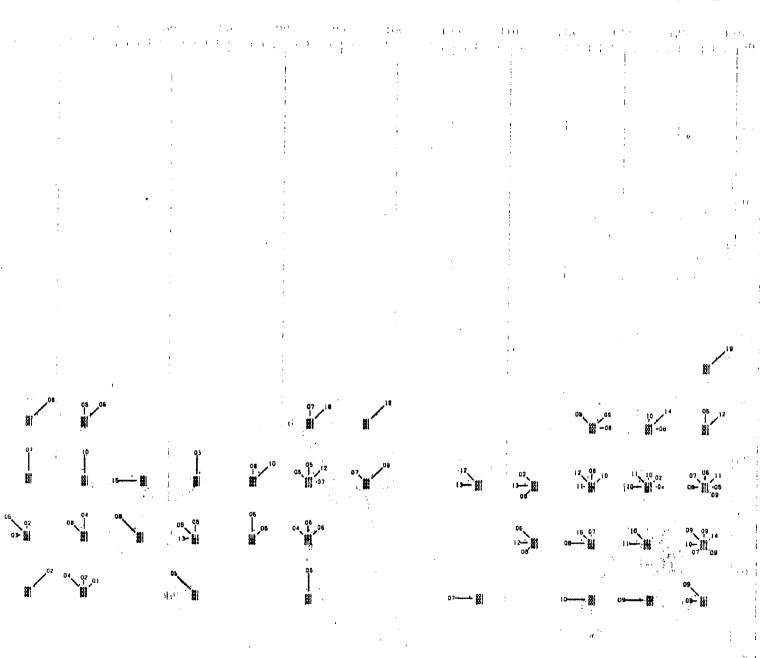
tive compilation of available data for specified areas without regard to suspected biases.

Issite page) are based on all available data subjectively adjusted where bias was evident.



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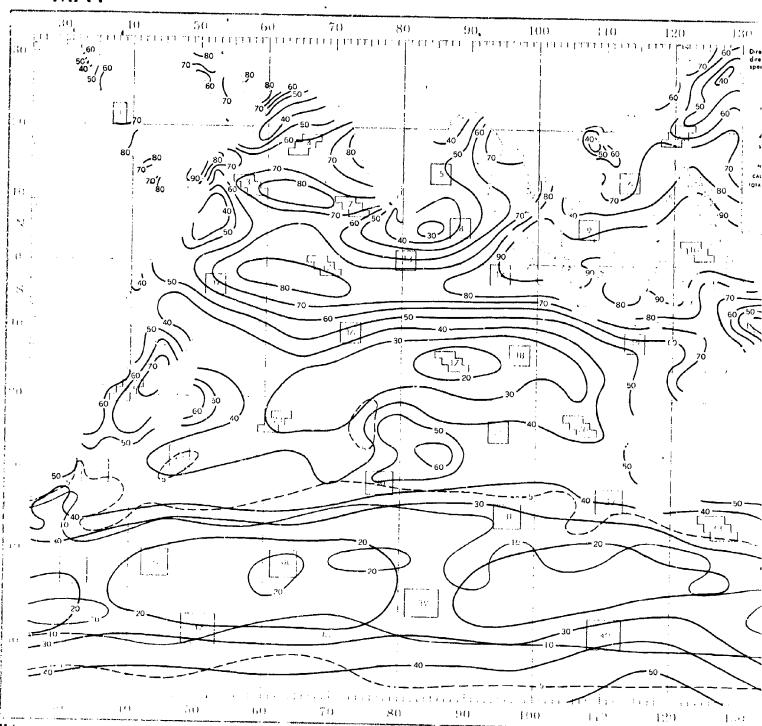
TROPICAL CYCLONE



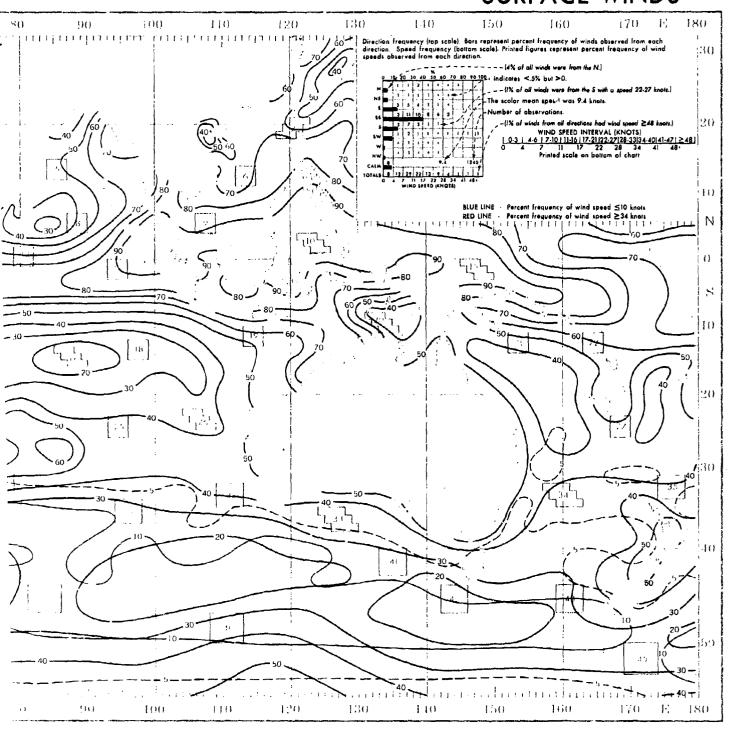
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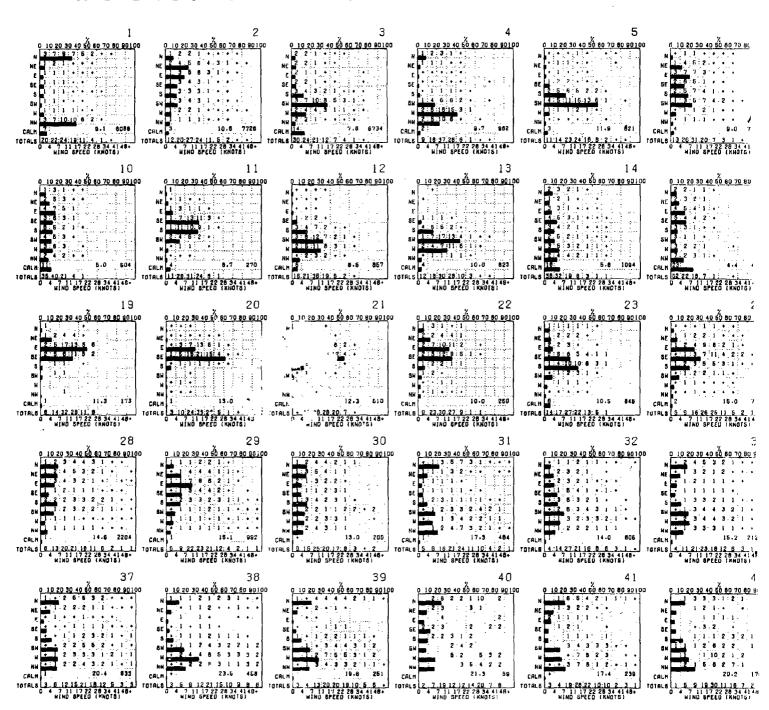
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SURFACE WINDS

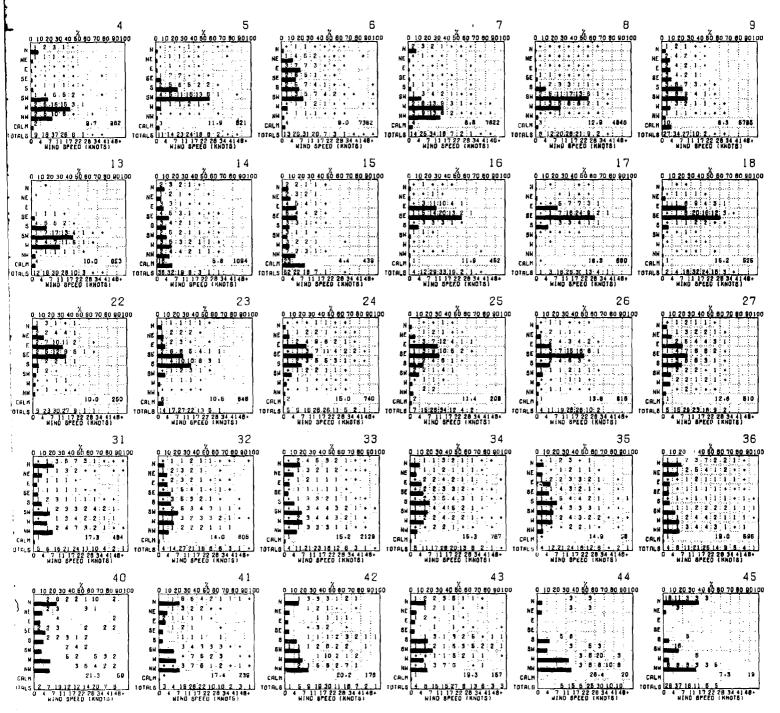


WIND DIRECTION AND SPEED



Graphs represent the objective compilation of available data for specified areas without. The isopleth analyses (opposite page) are based on all available data subjectively adjust

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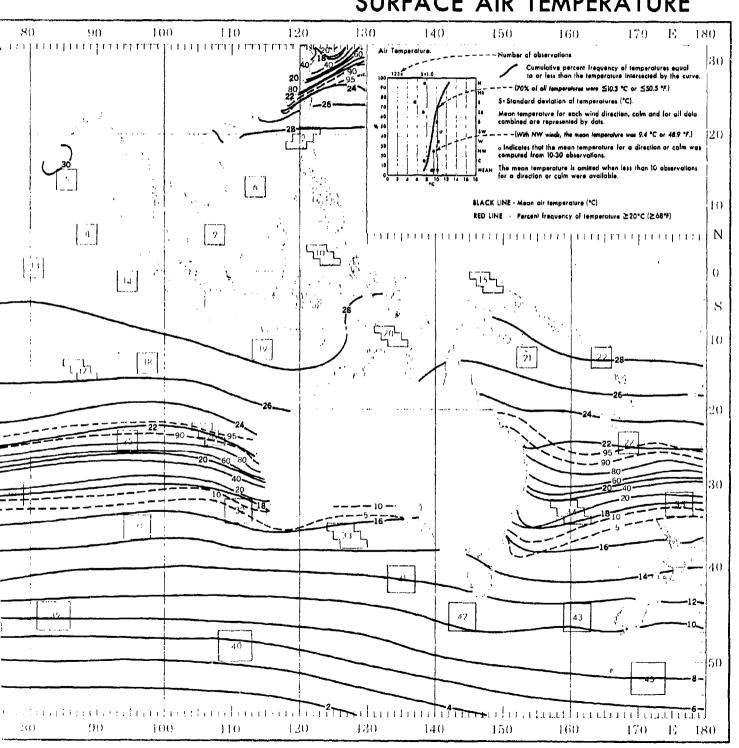


ective compilation of available data for specified areas without regard to suspected biases.

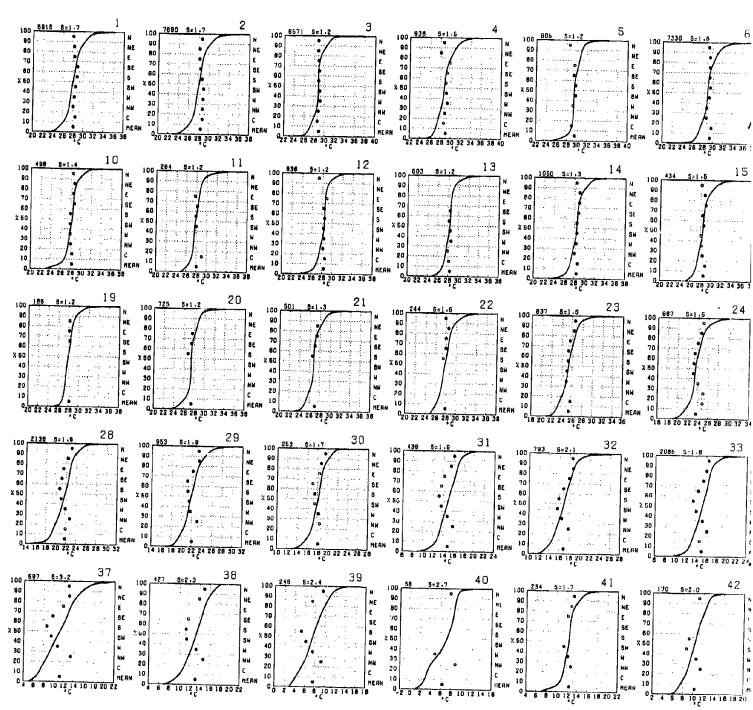
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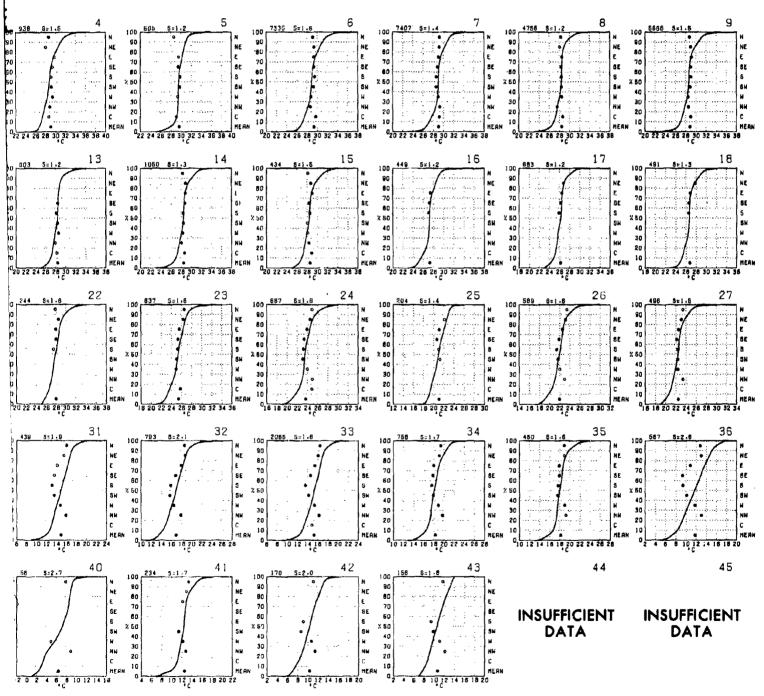
SURFACE AIR TEMPERATURE



SURFACE AIR TEMPERATURE

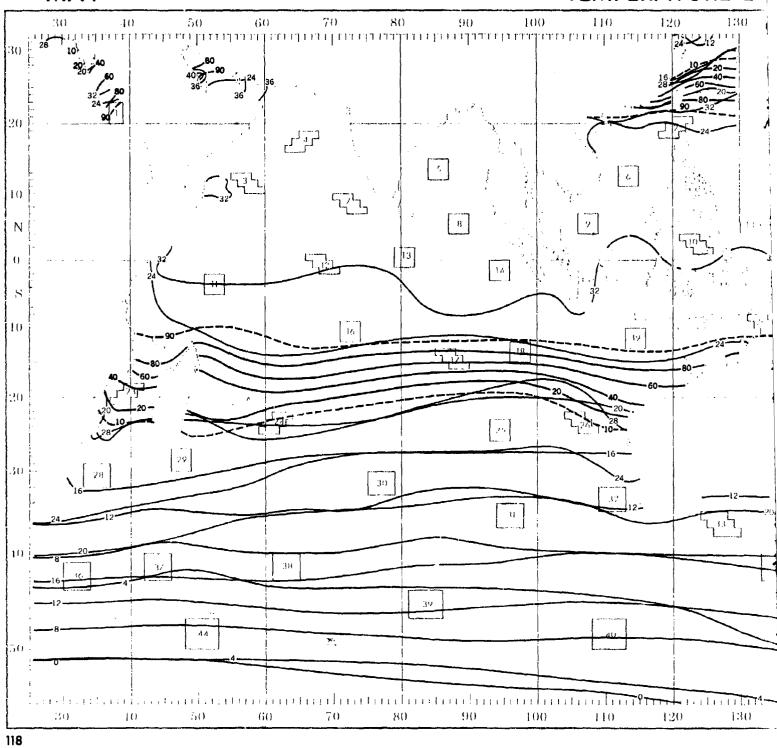


Graphs represent the objective compilation of available data for specified areas without The isopleth analyses (opposite page) are based on all available data subjectively adjust.

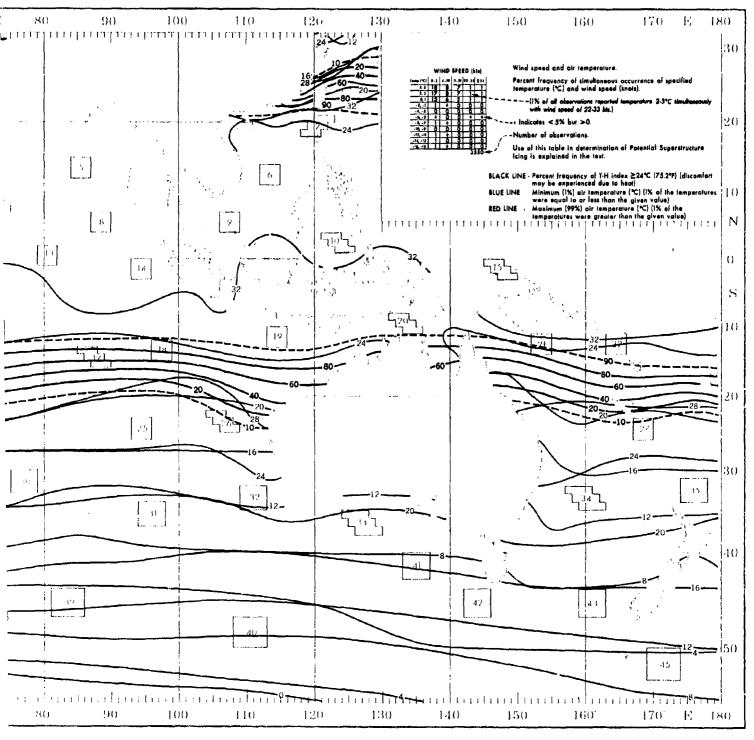


tive compilation of available data for specified areas without regard to suspected biases.

TEMPERATURE EX



TEMPERATURE EXTREMES AND T-H INDEX



WIND SPEED AND AIR TEMPERATURE

WIND SPEED (KTS)	NIND SPEED (KIS) 2	WIND SPEED (KTS) 3	WIND SPEED (KIS)	WIND SPEED (KIS) 5	WIND SPEED (KT
TEMP (90) 0-3 4-10 11-21 22-33 4 24	TERP (*C) 0-3 4-10 11-21 22-39 2 34	TEMP (*C) 0-3 4-10 11-21 22-33 & 34	18HP (*C) 0-3 4-10 11-21 22-33 3 34	TEMP (*C) 0-9 4-10 11-21 22-33 a 34	TEMP (*C) 0-3 4-10 11-212
38,37 0 + 0 0 0 34,36 + + + 0 0	36.37 0 + 0 0 34.36 + 0 0 0	38.37 + + + 0 0	34,35 + 1 + 0 0	34.35 + + + 0 0	38.37 · · · · · · · · · · · · · · · · · · ·
32.33 1 1 1 + 0 30.31 4 8 4 + 0	92.93 2 + 0 30.91 3 1 6 1 +	32,32 1 1 1 0 0	30.31 2 13 10 1 + te.te 4 31 19 1 +	20.31 4 16 23 5 0 20.29 6 18 15 3 +	32.53 1 4 2 30.31 4 19 8
20.20 0 21 13 2 0 20.27 5 13 11 2 U	29.26 7 24 17 3 + 20.27 2 9 9 3 +	28.27 2 2 1	28.27 2 7 2 0 0	26.27 4 4 1 4 4	20.20 7 30 13 20.27 1 4 2
24.25	24.25 + 1 1 1 + 22.23 + + + 0 0	24.28 + + + + 0	22,23 0 0 0 0 0 0 20,21 0 0 0 0 0	20.21 0 0 0 0 0	24.25
20.21 0 0 0 U	89.81 0 0 0 0	20.21 0 0 0 0	18.18 0 0 0 0 0	10.10 0 0 0 0	20.21 0 0 0
18.19 0 0 0 0 0 18.17 0 0 0 0 0	10-10 0 0 0 0 0 0 10-17 0 0 0 0 0 0	20.21 0 0 0 0 0 10.10 0 0 0 0 0 10.17 0 0 0 0 0	18-18 0 0 0 0 0 0 16-17 0 0 0 0 0 0 14-18 0 0 0 0 0 0	26.43 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	10.10 0 0 0 10.17 0 0 0
HIND SPEED (KTS) 10	NIND SPEED (KTS) 11	HIND SPEED (KTS) 12	942	HIND SPEED (KTS) 1 4	
TERP (*C) 0-0 4-10 11-21 12-30 34	MIND SPEED (KTS)		TEMP (*C) 0-3 4-10 11-21 22-33 4 34	15HP ('C) 0-1 4-10 11-21 22-21 34	HIND SPEED (KT)
32.33 1 1 + 0 0 30.31 3 7 + 0 0	18.33 0 Z 1 0 0 30.31 3 4 Z 0 0	92.99 0 + + 0 0	32,39 4 1 1 0 0 30,31 2 6 4 0 0	34,38 0 + 0 0 0	32.33 3 2 0
20.29 23 39 2 0 0	20.20 6 30 16 1 0	30.21 3 8 3 + 0 20.29 12 40 16 1 0 24.27 2 9 5 1 0	80.80 5 35 27 2 +	30.31 7 9 1 0 0	20.20 31 24 5
20.27 6 12 2 0 0 24.28 1 1 + 0 0	£4.68 0 + + 0 0	24.26 0 1 0 0	26.27 2 5 6 1 0 24.26 0 1 + + +	20:20 24 34 7 1 0 20:27 4 6 3 1 0	26.27 B B 2 24.26 1 0 0
#0.#1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	88.83 0 0 0 0 0 0 0 0 0 18.09	20.21 0 0 0 0	#2.23 0 0 0 0 0 0 #0.21 0 0 0 0 0 10.10 0 0 0 0 0	24:24 + 1 + + 0 22:23 0 0 0 0 0	\$6.\$1 0 0 0 \$6.\$3 0 0 0
10,17 0 0 0 0 0	19.17 0 0 0 0 0 19.17 0 0 0 0 0	10.17 0 0 0 0 0	18-17 0 0 0 0 0	20:21 0 0 0 0 0 18:19 0 0 0 0 0	18-10 0 0 0 16-17 0 0 0
14.15 0 0 0 0 0 18.19 0 0 0 0 0	14-15 0 0 0 0 0 12-13 0 0 0 0 0	14.16 0 0 0 0 0 0 18.13 0 0 0 0 0	14.15 0 0 0 0 0 12.13 0 0 0 0 0	18,17 0 0 0 0 0 14,18 0 0 0 0 0	14-18 0 0 0 18-13 0 0 0
503	284	842	603	1052	
HIND SPEED (KTS) 19	MIND SPEED (KTS) 20 18HP (+C) [0-3 [4-10]11-21 22-33 234	HIND SPEED (KTS) 21	MIND SPEED (KTS) 22	WIND SPEED (KTS) 23	WIND SPEED CKTS
32.33 0 1 0 0 0	34-38 0 0 + 0 0 32-39 0 1 1 0 0	32,33 0 + 0 0 0 30,31 1 2 2 0 0	32.33 0 3 0 0 0	32,33 + 0 0 0 D	30,31 + + +
30-31 1 5 4 1 0 26-88 3 21 25 6 0	30.31 + 2 1 0 0	28,29 2 15 13 2 0	26.29 5 25 18 1 0	20.20 2 4 3 + 0	28.28 + + 1 26.27 1 3 5
20.27 3 18 10 0 0 24.28 0 0 0 0 0	20.27 1 15 27 3 +	24.25 + 4 4 1 0	24.25 4 1 3 0 0	26,27 5 18 12 2 0 24,26 5 20 15 3 0	24.28 2 11 18 22.23 1 8 24
20.21 0 0 0 0 0 10.19 0 0 0 0 0	24.28 0 1 2 + 0 22.29 0 + 0 0 0	20.21 U U O O O	22.23 0 0 0 0 0 0 20.21 0 0 0 0 0 30.10 0 0 0 0 0	22.23 1 2 3 1 0 80.21 0 0 + 0 0	20.01 + 1 2 10.18 0 0 0
18:17 0 0 0 0 0	20.21 U O O O O O	10:10 0 0 0 0 0 10:17 0 0 0 0 0	18.17 0 0 0 0 0	18.19 0 0 0 0 0 16.17 0 0 0 0 0	18.17 [] [] [] [] [] [] [] [] [] [] [] [] []
14.18 Q Q Q Q Q Q	18.17 0 0 0 0 0 14.18 0 0 0 0 0	14.16 0 0 0 0 0 12.19 0 0 P 0 0	16:17 0 0 0 0 0 0 14:16 0 0 0 0 0 12:13 0 0 0 0 0	18.17 0 0 0 0 0 14.18 0 0 0 0 0 12.13 0 0 0 0 0	12.13 0 0 0 10.11 0 0 0
165	725	503	244	852	
WIND SPEED (KIS) 28	HIND SPEED (KTS) 29 TEMP (PC) 0-3 4-10 11-81 22-39 34	HIND SPEED (KTS) 30	MIND SPEED (KTS) 31	WIND SPEED (KTS) 32	WIND SPEED (KTS
20 20 + + + 0 0	20.81 0 + + 0 0	88-85 + O 1 O O	20.21 + 0 0 + 0	24.28 0 + + 0 0	20.21 + + +
26:27 • 1 1 • • 24:26 1 5 6 3 •	20.25 0 + + 0	#0.21 2 9 7 2 0 10.10 5 22 17 5 0	19.19 0 1 4 · · · 18.17 1 5 18 9 1	22.23 0 1 1 + 0	18,19 + 4 5 18,17 1 12 17
22:23 3 13 18 5 1 20:21 3 11 10 4 1	24.25 2 6 7 3 +	18.17 1 9 10 3 2 14.18 1 2 2 4 + 12.19 0 0 0 0 +	14.18 2 10 17 7 2 12.13 2 5 6 3 2	10.10 1 11 12 4 1 16.17 2 16 13 4 1	14.16 2 11 13 12.13 1 5 5
18.10 1 3 3 3 2 19.17 • • • • • •	20.21 1 8 14 6 1 18.15 4 2 3 1 1	10.11 0 0 0 0	10.11 1 1 + 2 0 0.0 0 0 0 0 0 +	14.18 1 8 6 4 1	10,11 0 + 1 8.9 0 0 0
14.18 + 0 + D O	10.17 0 C 0 0 + 14.16 0 0 0 0 0	0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4.8 D D D D D	10.11 0 0 0 0 0 0.0 0 0 0 0 0	6,7 0 0 0 4,8 0 0 0
11.15 + 0 + 0 0 12.15 0 0 0 0 0 10.11 0 0 0 0 0 6.5 0 0 0 0 0	14.18 0 0 0 0 0 0 12.13 0 0 0 0 0 10.31 0 0 0 0 0	6.9 0 0 0 0 0 0 6.7 0 0 0 0 0 0 4.8 0 0 0 0 0 0 2.3 0 0 0 0 0 0	6.7 0 0 0 0 0 0 4.6 0 0 0 0 0 0 8.8 0 0 0 0 0 0 0.1 0 0 0 0 0 0	0.7 0 0 0 0 0 4.6 0 0 0 0 0	2.3 0 0 0 0.1 0 0 0
2147	. 954	286	HIND SPEED (KTS) 40	795	
HIND SPEED (KTS) 37			MIND SPEED (RTS) 10-10 11-21 22-33 2 34		HIND SPEED (KTS)
20.21 0 + 1 0 0 19.19 0 0 1 1 +	18-19 0 0 + + + 18-17 2 4 8 4 3	12:13 0 + 1 3 1 10:11 0 3 7 7 2	10.11 0 2 2 5 0 6.8 0 3 7 19 5	18.17 0 0 0 0 0 0 0 0	14,16 0 0 2
10.17 0 1 3 2 1	10-15 1 8 10 10 4 18-13 0 3 8 7 7	4.8 2 6 13 7 2 6.7 1 4 11 8 2	6.7 2 14 5 2 0 4.8 0 3 3 7 2	14.18 + 5 13 3 3	10.11 0 5 18 (
18-19 2 5 8 7 3	10.11 + 2 5 4 5	4.6 4 3 8 3 3	2.3 0 3 5 2 8	12.13 1 13 20 9 1 10.11 1 5 5 5 1	8.7 0 1 6 2 4.8 0 0 0 1
10.11	6.7 0 0 + 0 +	0.1 0 0 0 0 0	-2,-1 0 0 0 0 0	0.7 0 0 0 1 0	8.3 0 0 0 C
4.6 0 0 1 0 1	2.3 0 0 0 0 0	-43 0 0 0 0 0	-05 0 0 0 0 0	2.3 0 0 0 0	0,1 0 0 0 C -2,-1 0 0 0 C
0:1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.1 0 0 0 0 0 -11 0 0 0 0 0	-66 0 0 0 0 0 -67 0 0 0 0 0	-07 0 0 0 0 0 -109 0 0 0 0 0	0.1 0 0 0 0 0 -21 0 0 0 0 0	-43 0 0 0 0 -85 0 0 0 0

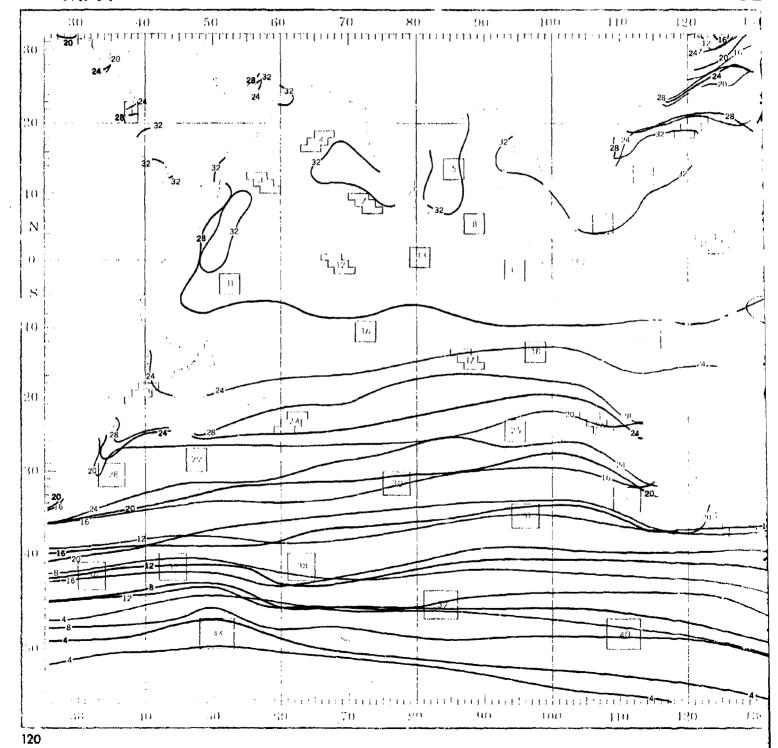
<u>Graphs</u> represent the objective compilation of available data for specified areas withouthe <u>isopleth</u> analyses (apposite page) are based on all available data subjectively adjusted.

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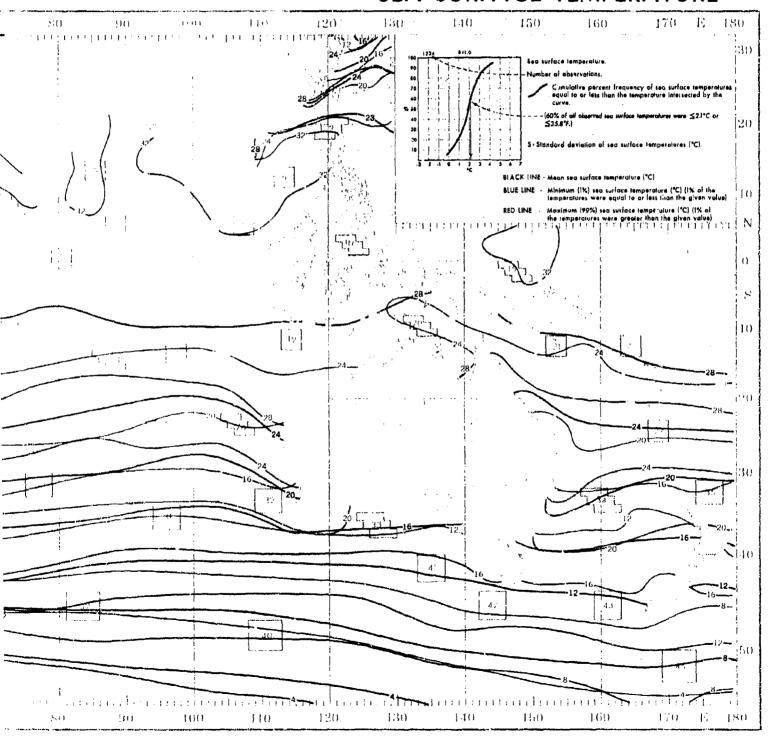
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HIND SPEED (HTS)	WIND SPEED (KTS) 5	WIND SPEED (KTS)	HIND SPEED (KTS)	HIND SPEED (KTS)	HIND SPEED (KTS)
MP (*C1 D-3 4-10 11-21 22-33 a 34	TEMP (*C) 0-3 4-10 11-21 22-33 = 34	1ERP (1C) 0-3 4-10 11-21 22-39 4 34	TEMP (4C) 0-3 4-10 11-21 22-39 2 34	1EMP (4C) 0-3 4-10 11-21 22-33 a 34	TEMP (4C) 0-3 4-10 11-21 22-33 = 34
34,35 + 1 + 0 0	34.38 + + + 0 0	30,37 + + + 0	56.37 0 + 0 0	34.35 0 + + 0	30.37 + + 0 0 0
32.33 1 3 3 0 0	32.33 1 2 2 + 0 30.31 4 15 23 5 0	34.35 + 1 + + 0 32.33 4 2 + 0	34.38 + + + 0 0 32.33 1 2 1 + 0	32.33 + + 1 + 0	34.35
30.31 2 13 10 1 + 20.20 4 31 19 1 +	90.20 G 1B 15 3 +	30,31 4 19 6 1 4	30.31 5 19 7 + +	28.20 6 22 33 8	30:31 6 14 3 + 0
28.27 2 7 2 0 0	28.27 + + 1 + +	20.20 7 30 13 2 +	20.20 7 33 14 1 +	26.27 1 4 7 2 +	20.20 17 37 6 + 0
24.25 0 0 + 0 0	24.21 0 + 0 + 0	26,27 1 4 2 1 4	26.27 1 4 3 1 •	24,28 + + 1 + 0	24.25 + 1 + + 0
22.23 0 0 0 0 0 0 20.21 0 0 0 0 0	20.21 0 0 0 0 0	24.25 + + + 0	24.25 • • • • •	22.23 0 + + + 0	22.23 + + + 0
0 0 0 0	10.10 0 0 0 0	20.21 0 0 0 0	20.21 0 0 0 0	10.10 0 0 0 0	\$0.21 0 0 0 0
16.17 0 0 0 0 0	18-17 0 0 0 0 0	19.19 0 0 0 0 0 16.17 0 0 0 0 0	18.19 0 0 0 0	10.17 0 0 0 0 0	10-10 0 0 0 0
14.16 0 0 0 0 0	14-15 0 0 0 0 0	10.17 0 0 0 0 0	10.17 0 0 0 0 0	14.15 0 0 0 0 0	18-17 0 0 0 0 0
947	610	/341	/418	4703	0000
WIND SPEED (KIS) 13	HIND SPEED (KTS) 14	WIND SPEED (KTS) 15	HIND SPEED (KTS) 16	HIND SPEED (KTS) 17	WIND SPEED (KTS) 18
10 1161 0-3 4-10 11-21 22-33 2 34	TEMP (*C) 0-3 4-10 11-21 22-33 = 34	TEMP (*C) 0-3 4-10 11-21 22-33 1 34	TEMP (1C1 0-3 4-10 11-21 22-33 = 34	TERP 1001 0-3 4-10 11-E1 EE-39 a 94	TEMP (*C) 0-3 4-10 11-2122-39 - 34
38,33 4 1 1 0 0	34.38 0 + 0 0 0	32,33 3 2 0 0 0	32.33 0 0 + 0 0	30.31 0 • 1 • 0	90.31 + + 1 1 0
30.31 2 6 4 0 0	32.33 1 1 + 0 0	30.31 8 5 + 1 0	30.31 0 2 2 0 0	20,28 . 2 8 2 0	20.20 + 6 12 2 0
20.20 8 35 27 2 +		20.29 31 24 5 0 0		26.27 1 12 38 11 +	26.27 1 16 37 13 + 24.26 0 1 6 3 0
76,87 2 5 6 1 0 74,25 0 1 + + +	26.89 24 34 7 1 0 26.87 4 6 3 1 D	28,27 9 8 2 0 U 24,28 1 0 0 0 0	26.27 2 24 29 2 0	24.25 1 5 14 3 1 22.23 0 0 1 1 +	24.86 0 1 6 3 0 28.23 0 0 + + 0 20.21 0 0 0 0 0
12.23 0 0 0 0	24:28 + 1 + + D	22.23 0 0 0 0 0	22.23 0 0 0 0 0	20.21 0 0 0 0 0	80.81 0 0 0 0
70.21 0 0 0 0	22.53 0 0 0 0 0	20.21 0 0 0 0 0	20.21 0 0 0 0	10-10 0 0 0 0	10.10 0 0 0 0
18.18 0 0 0 0 0 0 18.17 0 0 0 0 0	20,21 0 0 0 0 0 10,10 0 0 0 0 0	18-19 0 0 0 0 0	18.18 0 0 0 0 0 0 18.17 0 0 0 0 0 C	1\$,17 0 D 0 0 0 14,18 0 0 0 0 0	18.17 0 0 0 0 0 14.18 0 0 0 0 0 0
14.18 0 0 0 0 0 0 0 12.19 0 0 0 0 0	13-17 0 0 0 0 0	14.16 0 0 0 0	14.16 0 0 0 0 0	12:13 0 0 0 0 0	14:16 0 0 0 0 0 0 12:13 0 0 0 0 0 10:11 0 0 0 0
12,13 0 0 0 0	14-15 0 0 0 0 0	12.13 0 0 0 0 0	12.13 0 0 0 0 0	10.11 0 0 0 0 0	10.11 0 0 0 0 0
803	1052	438	450	666	491
HIND SPEED (KTS) 22	HIND SPEED (KTS) 23	HIND SPEED (KTS) 24	HIND SPEED (KTS) 25	NIND SPEED (KTS) 26	HIND SPEED (KTS) 27
P (*C) G-3 4-10 11-21 22-33 2 34	TERP (*C) 0-3 4-10 11-21 22-33 x 34	TEHP 1901 0-3 4-10 11-21 22-33 = 34	TEMP (*C) 0-3 4-10 11-21 22-99 2 34	TERP (40) 0-3 4-10 11-21 22-33 & 34	TEHP (*C) 0-3 4-10 11-E 22-33 34
32,33 0 3 0 0 0	32.33 + 0 0 0 0	30.31 + + 0 0	24,25 0 2 2 0 0	20.29 + + + 0 0	28.20 + + 0 0 0
30.39	30.31 + + + 0 0	20:28 + + 1 + 0	22.23 4 17 16 1 D 20.21 5 18 20 4 0	26,27 + 1 1 0 0 24,26 1 5 6 1 0	26.27 • 2 1 + 0
78.29 5 25 18 1 0 26.27 3 16 13 1 0	28-29 2 4 3 + 0 28-27 5 18 12 2 0	26.27 1 3 5 1 0 24.26 2 11 19 8 1		24,25 1 5 6 1 0 22,29 3 14 27 6 0	24.25 + 8 6 1 0 22.23 4 24 23 7 0
24.26 + 1 3 0 0	24.28 6 20 15 3 0	12,25 1 9 24 6 2	18.19 + 2 8 + 0 16.17 0 0 0 0 0 0 14.15 0 0 0 0 0 0 12.13 0 0 0 0 0	20.21 1 8 18 5 0	20.21 + 7 10 2 0
22.23 0 0 0 0 0	22.23 1 2 3 1 0	20.21 + 1 2 1 +	14.15 0 0 0 0 0		19:19 0 1 + 1 0 16:17 0 0 0 0 0
20.21 0 0 0 0 0	20.21 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	10.10 0 0 0 + 0 10.17 0 0 0 1 0	12.13 0 0 0 0 0 0 10.11 0 0 0 0 0	18-17 0 + 1 0 0 14-16 0 0 0 0 0	18-17 O O O O O
18.17 0 0 0 0 0	15.17 0 0 0 0 0	14.16 0 0 0 0 0	0.0 0 0 0	12.13 0 0 0 0 0	12.13 0 0 0 0 0
14.15 0 0 0 0 0	14.18 0 0 0 0 0	12.13 0 0 0 0 0	6.7 0 0 0 0 D	10-11 0 0 0 0 0 0 0.0 0 0 0 0 0	10-11 0 0 0 0 0 0 0.0 0 0 0 0 0
12.13 0 0 0 0 0	12.13 0 0 0 0 0	10-11 0 0 0 0 0	4.6 0 0 0 0 0	0.0 0 0 0 0 0 591	0 0 0 0 0
	32	33	34	35	36
HIND SPEED IKTS 31	WIND SPEED (KTS) 32	WIND SPEED (KIS) 33	WIND SPEED (KTS) 34	WIND SPEED (KTS) 35	WIND SPEED (KTS) 36
11°C) 0-3 4-10 11-21 22-33 2 34 20,21 + 0 0 + 0		1EHP (*C) 0-3 4-10 11-2122-33 a 34	*tm# (*C) 0-3 4-10 11-21 22-33 > 34	TEHP (*C) 0-5 4-10 (1-21 22-53 & 94	TEMP (*C) 0-3 4-10 11-8188-93 8 34
20,21 + 0 0 + 0	24,26 0 + + 0 0		ZE123 1 2 1 1 1 1		
18.17 1 6 18 9 1		10.10 + 4 51 21 +1		22.23 4 1 2 0 0	18-17 0 2 4 2 1
14.18 2 10 17 7 2	20,21 1 4 3 + +	10.10 + 4 5 2 + 10.17 1 12 17 8 1	20.21 1 5 10 2 1 18.16 3 13 20 8 1	20.21 • 4 6 2 • 10.10 2 18 23 8 1	18.17 0 2 4 2 1 14.18 1 4 12 4 1
	10.10 1 11 12 4 1	14:17 1 12 17 U 1 14:16 2 11 13 6 1	#0.21 1 5 10 2 1 18.16 3 13 20 9 1 18.17 1 7 13 6 1	20.21	16:17 0 2 4 2 1 14:16 1 4 12 4 1 12:13 1 5 15 7 3
12.13 2 6 5 3 2	10.10 1 11 12 4 1 10.17 2 16 13 4 1	1w:17 1 12 17 W 1 14:16 2 11 13 6 1 1z:13 1 5 5 3 1	\$0.21 1 5 10 2 1 18.16 3 13 20 9 1 18.17 1 7 13 6 1 14.18 0 1 1 1 1 +	20.21	16,17 0 2 4 2 1 14,18 1 4 12 4 1 12,13 1 5 13 7 3 10,11 1 4 11 4 2
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12.13 2 6 5 3 2 10.11 1 1 2 2 0	16,10 1 11 12 4 1 16,17 2 16 13 4 1 14,16 1 8 6 4 1 12,18 0 1 2 1 +	10-17 1 12 17 8 1 14-16 2 11 13 6 1 12-13 1 5 5 3 1 10-11 0 + 1 + +	### 1	20.21	16.17 0 2 4 2 1 16.18 1 4 12 4 1 17.18 1 5 15 7 3 10.11 1 4 11 4 2 10.11 1 4 11 4 2 10.11 1 3 5 4 1 10.11 2 1 2 1 2
12.13 2 6 5 3 2 10.11 1 1 2 2 0	16,10 1 11 12 4 1 16,17 2 16 13 4 1 14,16 1 8 6 4 1 12,18 0 1 2 1 +	10-17 1 12 17 8 1 14-16 2 11 13 6 1 12-13 1 5 5 3 1 10-11 0 + 1 + +	20.21 1 6 10 2 1 15.16 3 3 3 20 9 1 16.17 1 7 13 6 1 16.17 1 7 13 6 1 16.18 0 1 1 1 1 1 1 1 1 1	20.21	16.17 0 2 4 2 1 14.18 1 4 12 4 1 12.13 1 5 13 7 3 10.11 1 4 11 4 2 6.0 1 3 5 4 1 6.7 0 + 2 1 2 4.8 0 0 0 0 0 4 5.3 0 0 0 0 0
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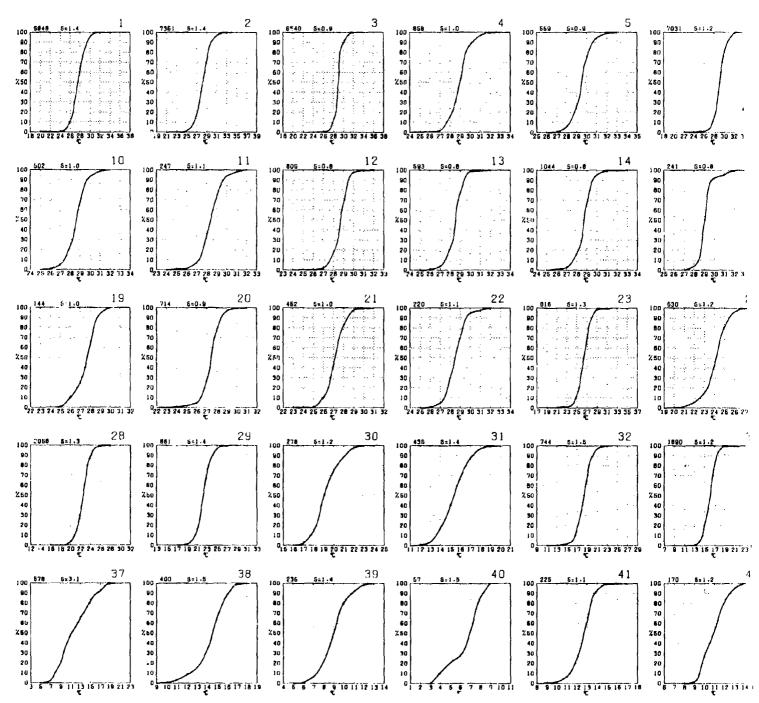
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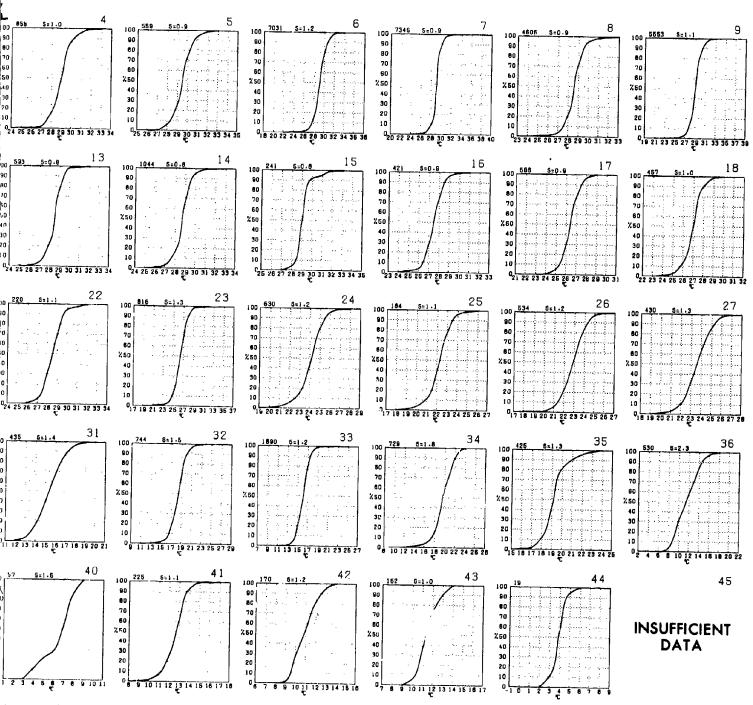
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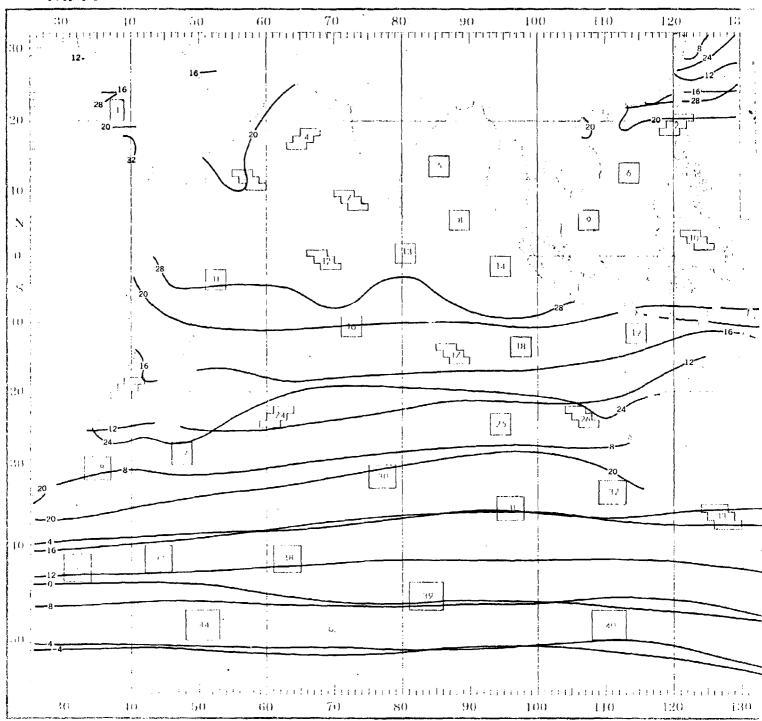
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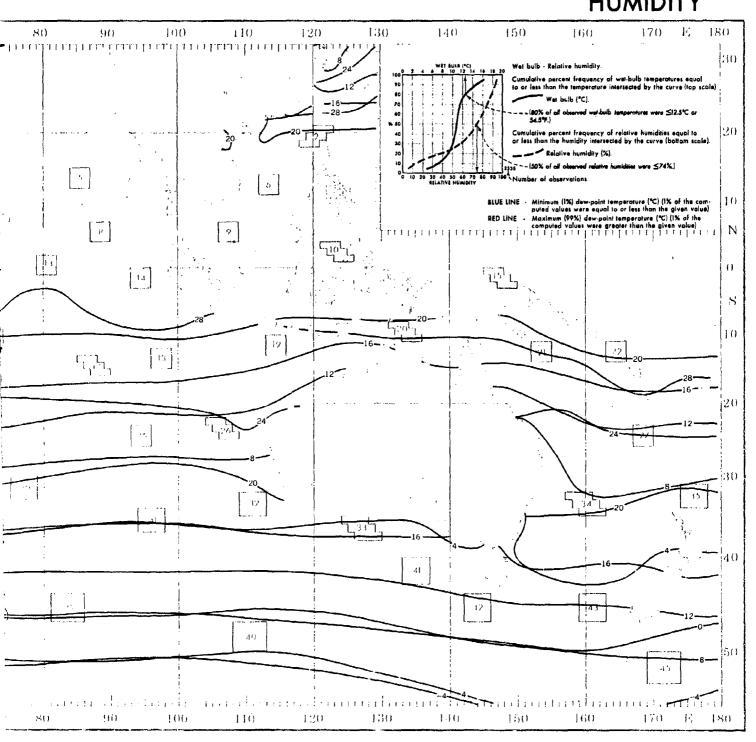
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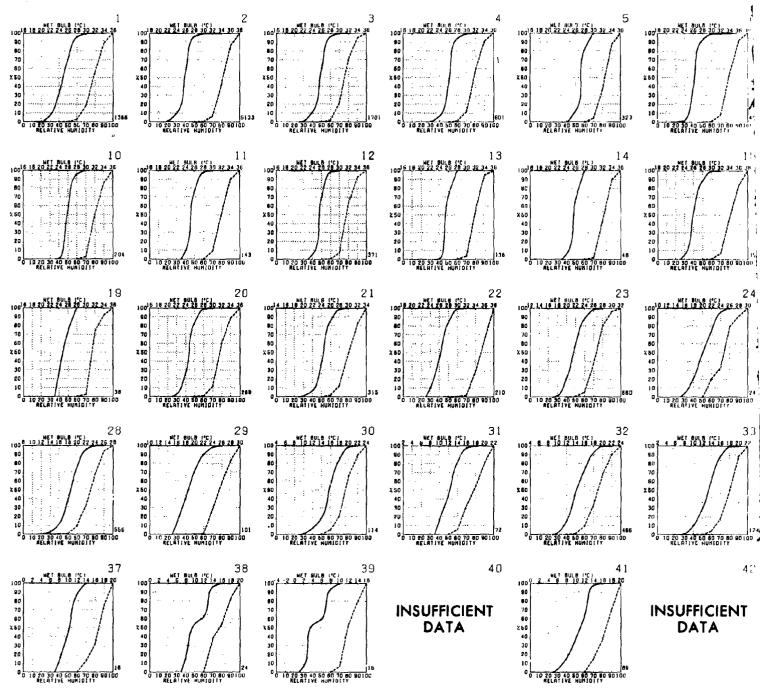
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HUMIDITY

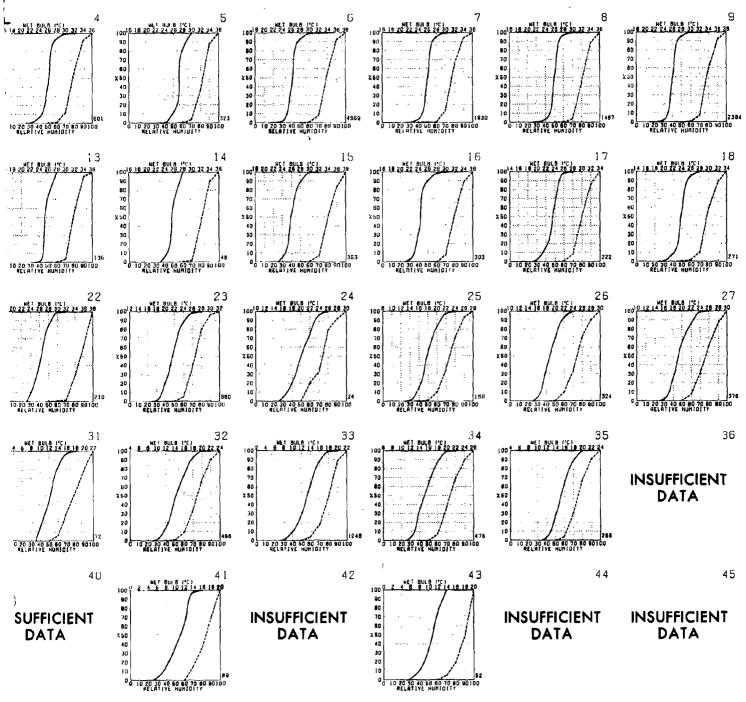


WET BULB AND RELATIVE HUMIDITY

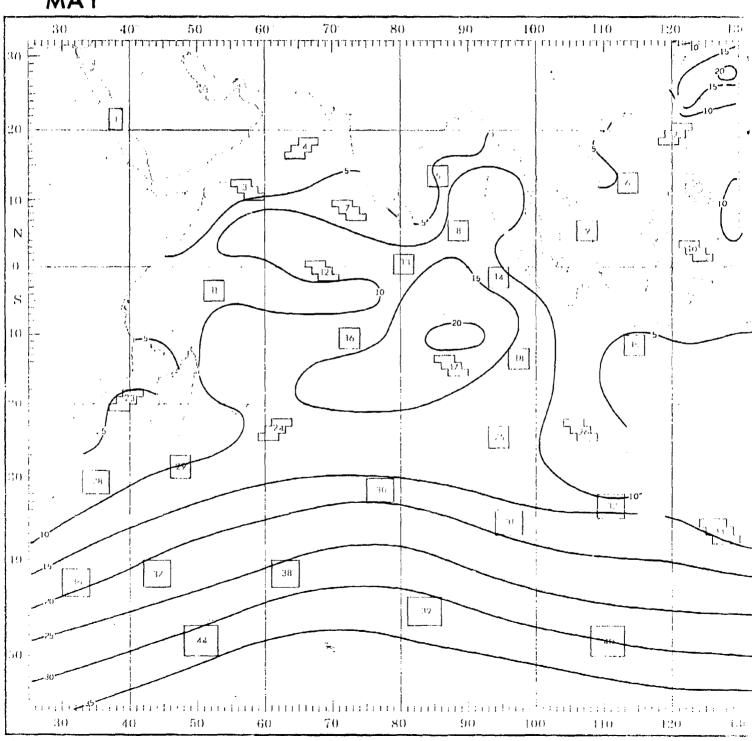


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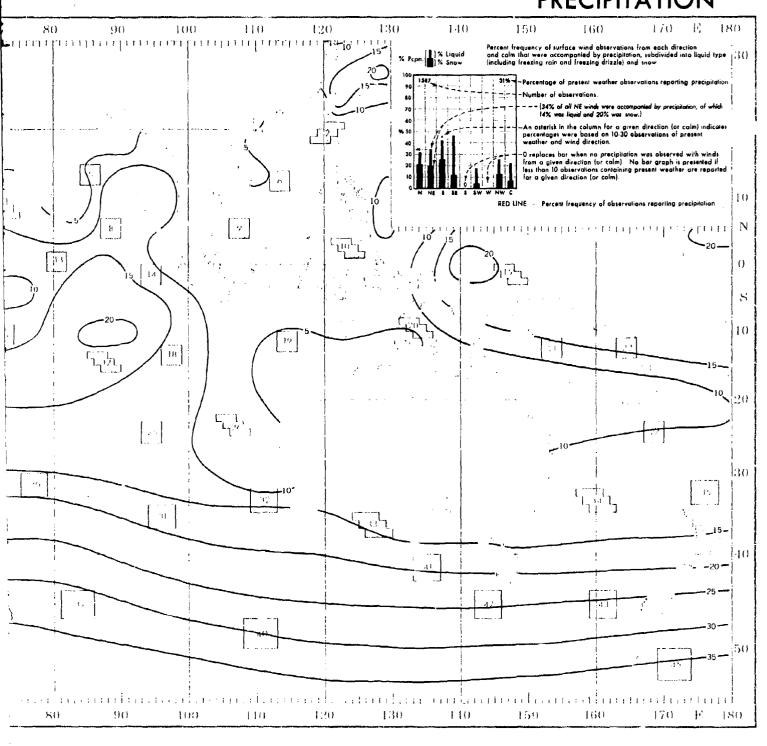




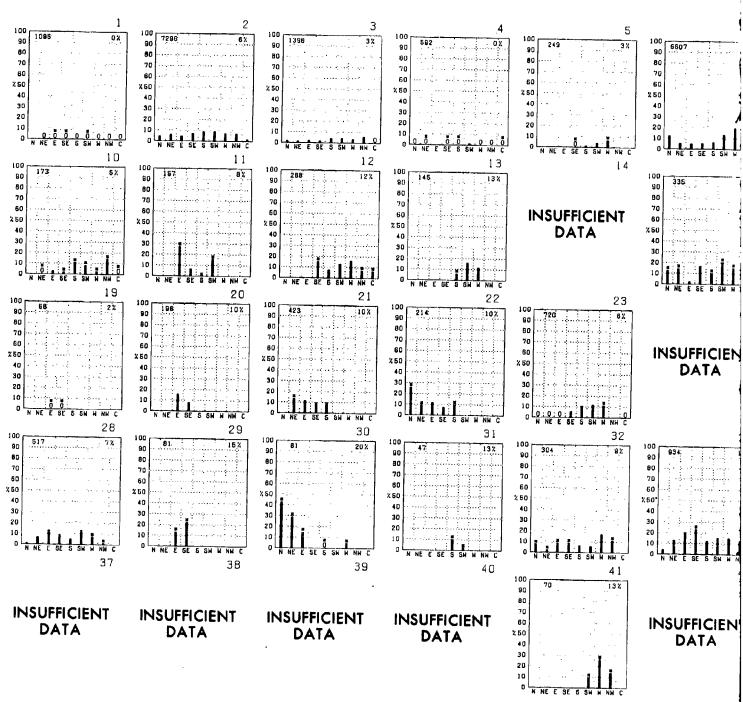
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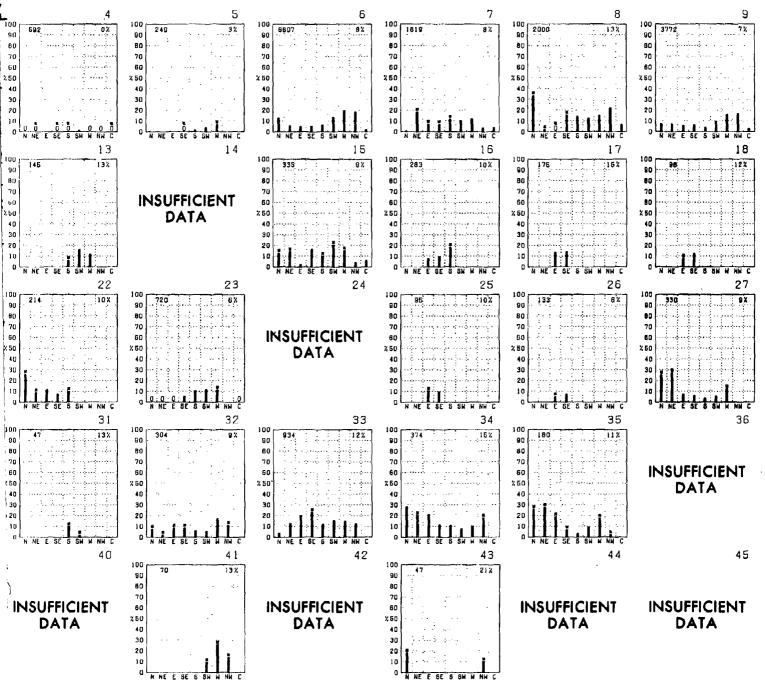
PRECIPITATION



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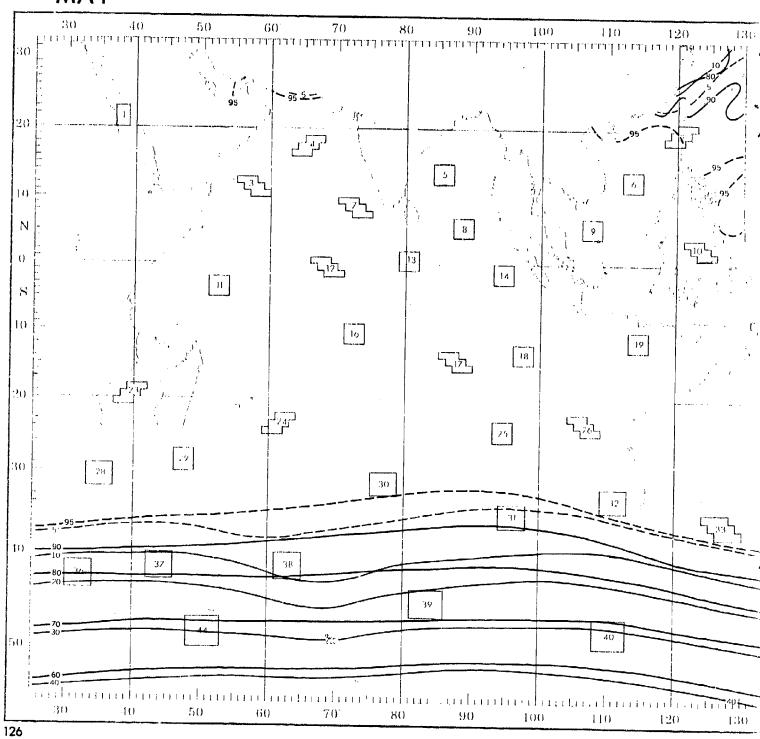


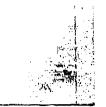
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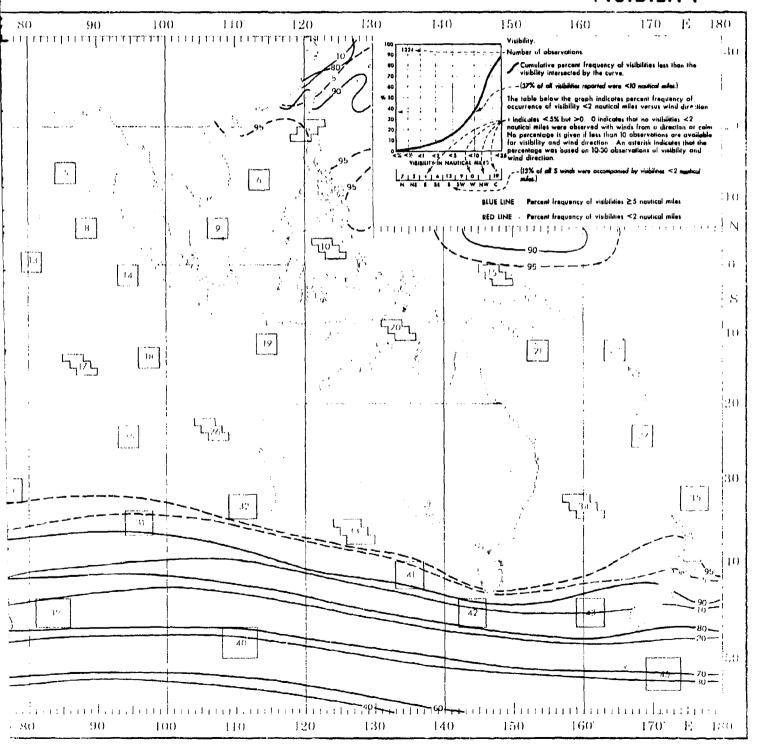
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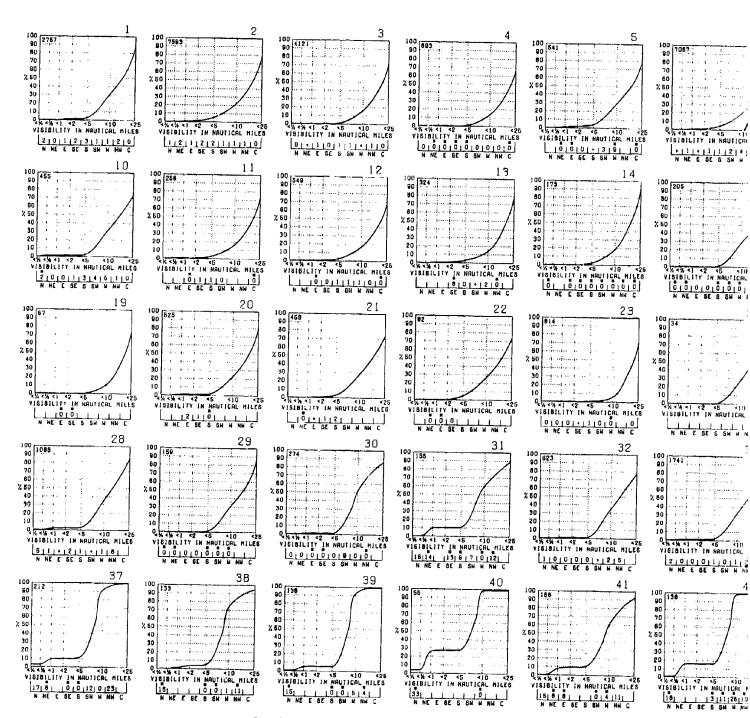




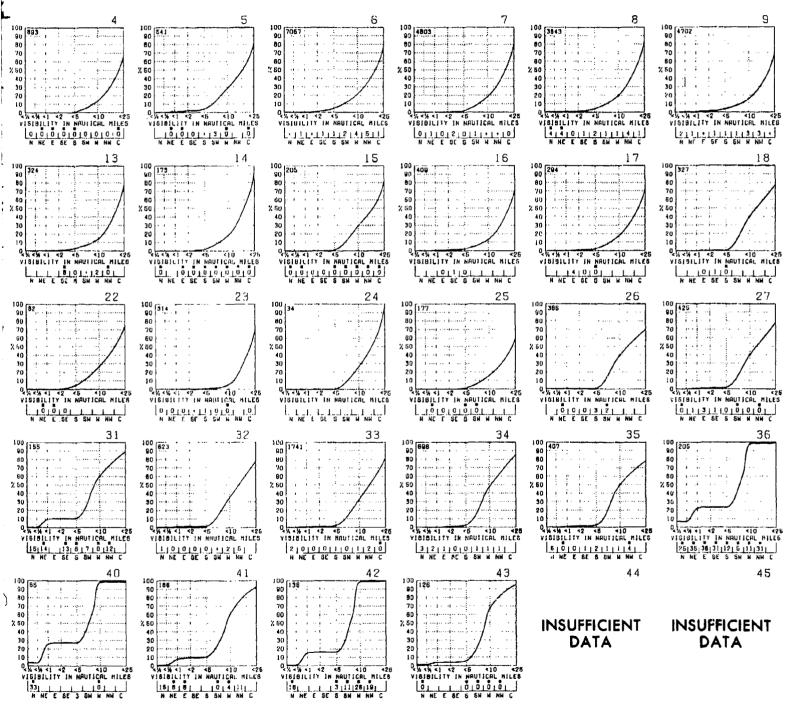
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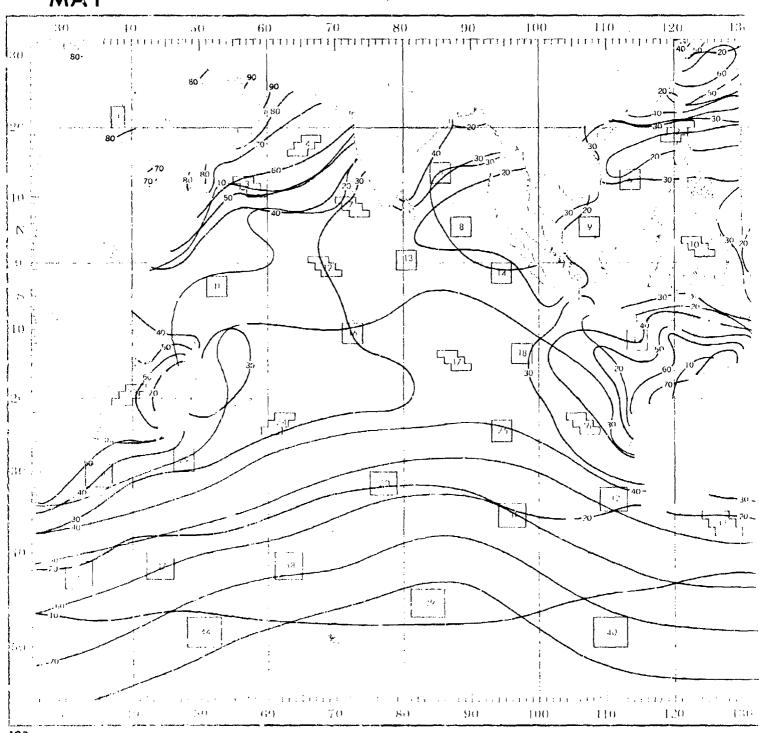
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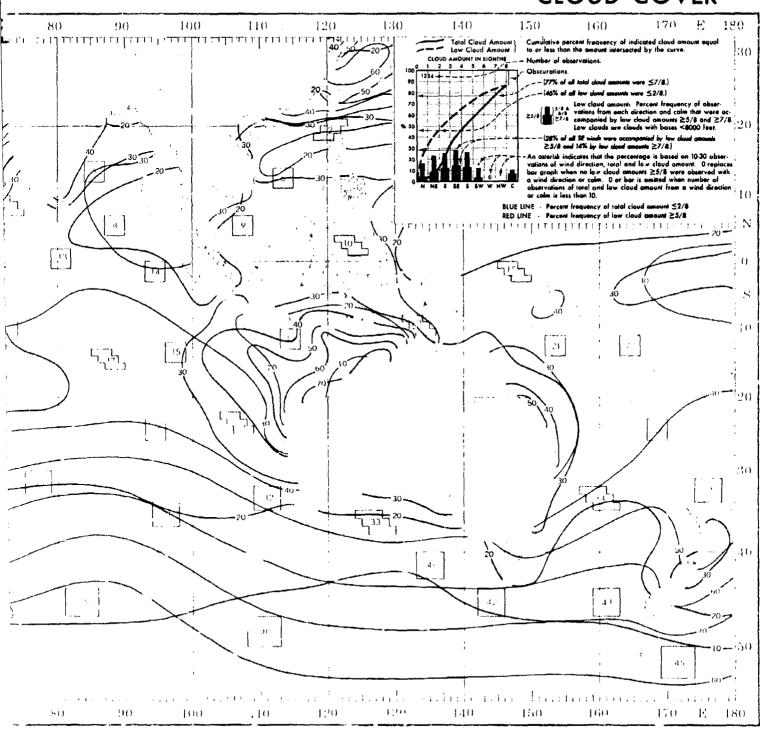
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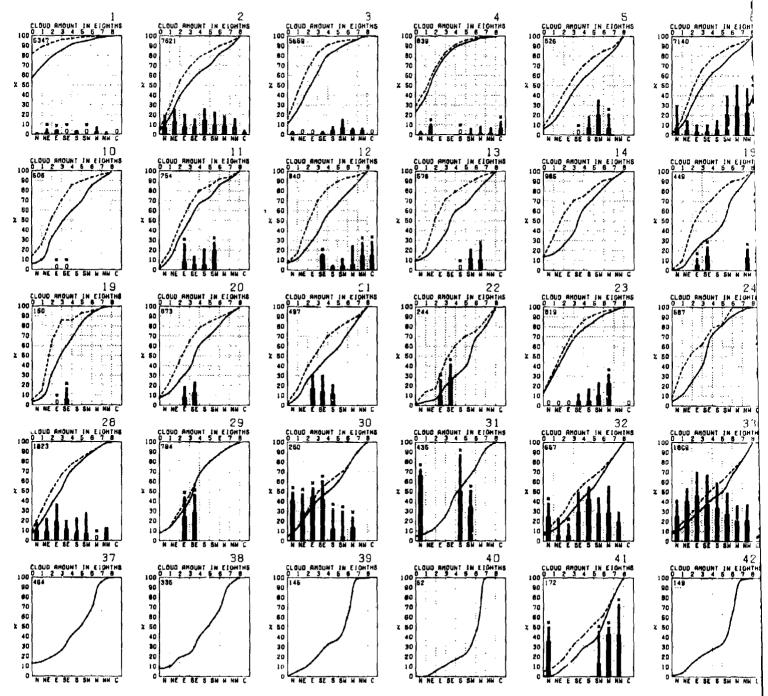
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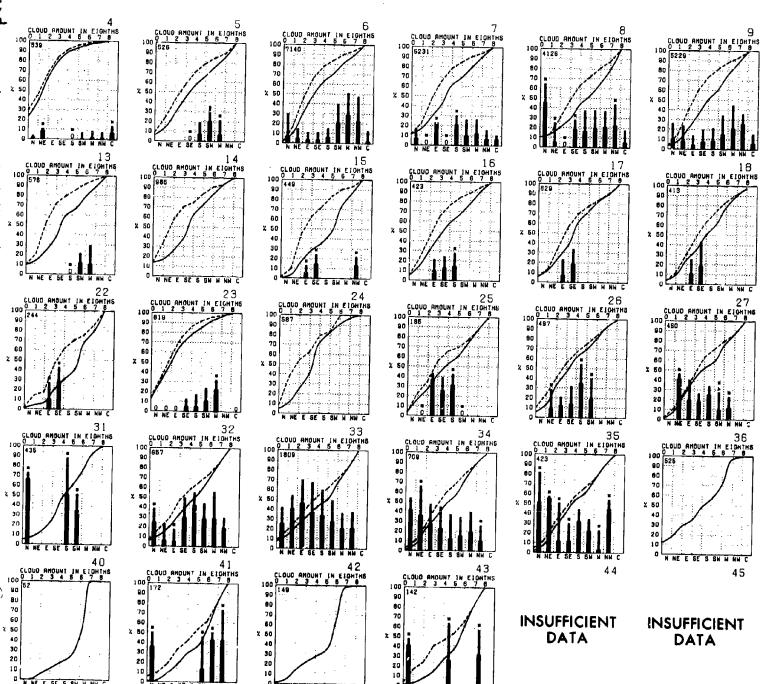
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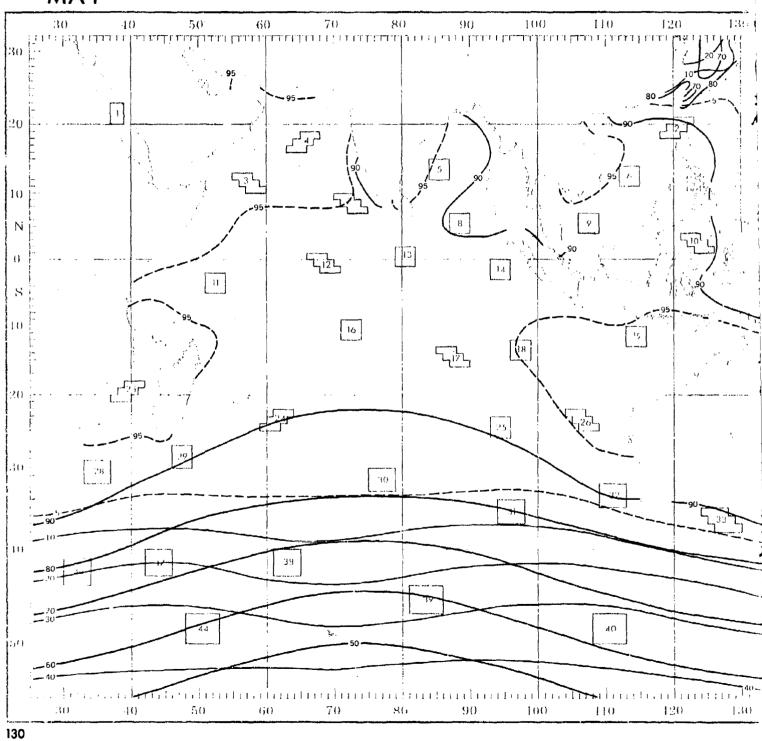
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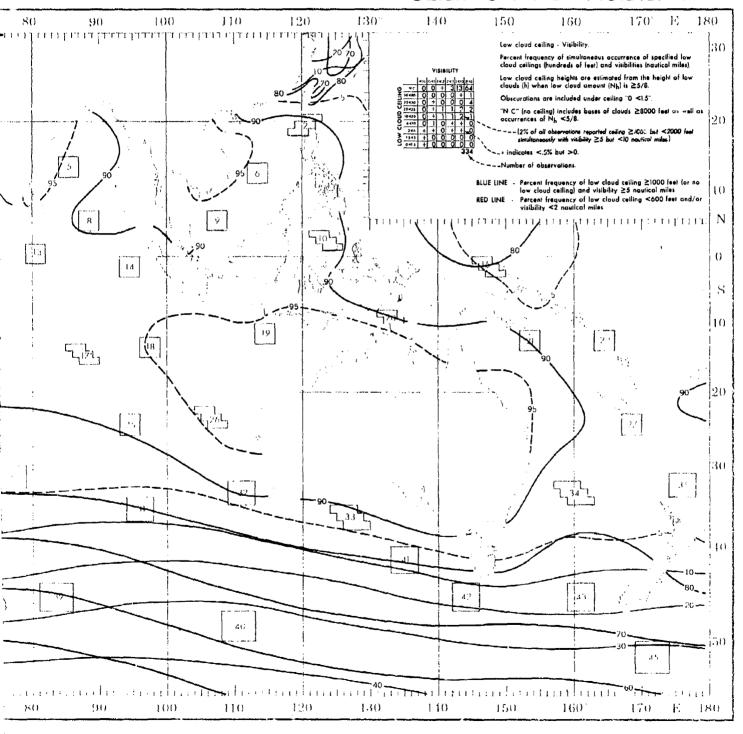
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CEILING AND VISIBILITY

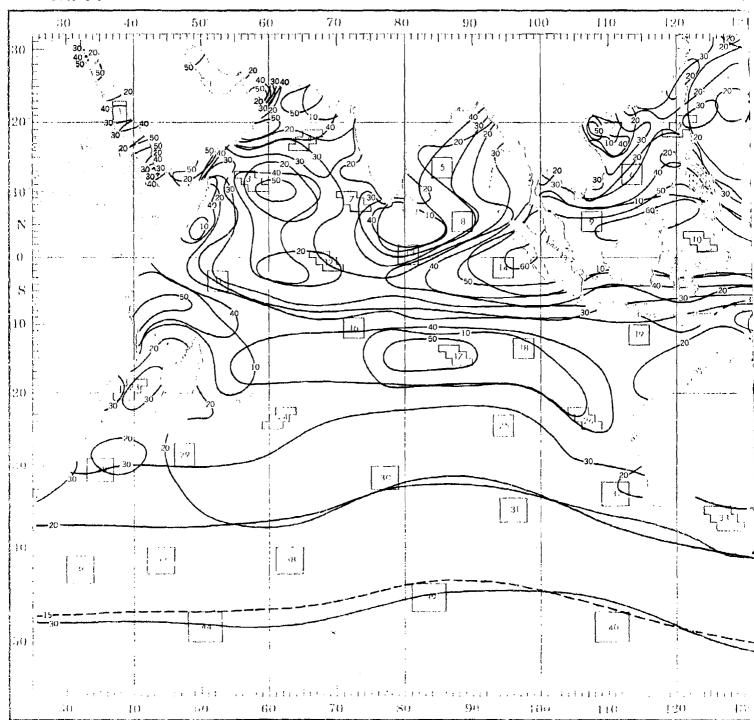
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VISIBILITY 28 *'A*	VISIBILITY 29	VISIBILITY 30 **/** */** ** ** ***	VIBIBILITY 31	VIBIBILITY 32	VISIBILITY Column
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Graphs represent the objective compilation of available data for specified areas without. The isopleth analyses (apposite page) are based on all available data subjectively adjust

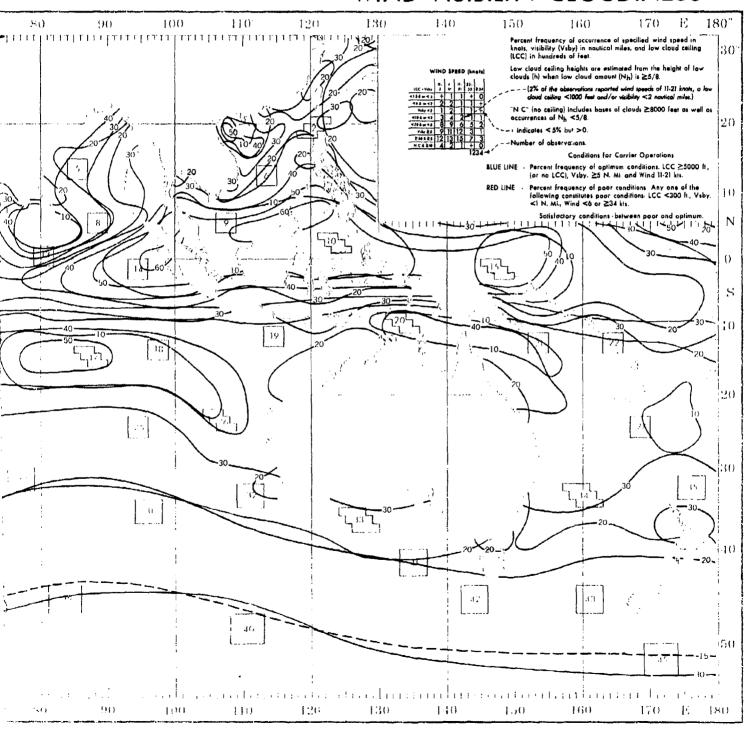
VISIBILITY 4 VISIBILITY 4 4 0 0 0 0 + 7 85 50-90 0 0 0 0 0 1 20-35 0 0 0 0 0 0 1 20-35 0 0 0 0 0 0 0 1 20-35 0 0 0 0 0 0 0 1 20-35 0 0 0 0 0 0 0 1 3-46 0 0 0 0 0 0 0 1 3-54 0 0 0 0 0 0 0 0 1-54 0 0 0 0 0 0 0 0 1-55 0 0 0 0 0 0 0 0 0-1.55 0 0 0 0 0 0 0 0 502	VISIBIL 17Y e ¹ /2 f'/4 1 = 2 2 + 5 1 = 10 2 + 0	VISIBILITY **/**	VISIBILITY ***********************************	VISIBILITY e ¹ / ₂ f/ ₄ f/ ₄ 1 e E 2 e E 10 10	VISIBILITY VISIBILITY 14 /2 7 /4 1 /2 2 /5 5 10 310 80 0 0 0 0 0 0 0 1 1 50 /40 0 0 0 0 0 0 1 1 20 /45 0 0 0 0 0 0 0 1 1 20 /45 0 0 0 0 0 0 1 2 7 610 0 0 0 1 1 1 3 6 /40 0 0 0 1 1 1 3 6 /40 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
VISIBILITY **/* **/* 1 **/* 2 **/* 8 **10 **10 **(*) 0 0 0 2 6 71 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 1 1 6 **(*) 0 0 0 0 0 1 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 0 **(*) 0 0 0 0 0 **(*) 0 0 0 0 0 **(*) 0 0 0 0 0 **(*) 0 0 0 0 0 **(*) 0 0 0 0 0 **(*) 0 0 0 0 0 **(*) 0 0 0 0 **(*) 0 0 0 0 **(*) 0 0 0 **(*) 0 0 0 **(*) 0 0 0 **(*) 0 0 **(*) 0 0 **(*) 0 0 **(*) 0 0 **(*) 0 0 **(*) 0 0 **(*) 0 0 **(*) 0 0 **(*) 0 **(*) 0 0 **(*) 0 *	VISIOIL TY 1 4 **C*********************************	VISIBILITY 1 5 **/** **** 1 = 2 2 + 6 8 - 10 a 0	**************************************	VISIBILITY 1 7 -1/2	VISIBILITY *** *** *** *** *** *** ***
VISIBILITY 22 (**)*	VISIBILITY VISIBILITY NC 0 0 0 0 0 2 88 50460 0 0 0 0 0 0 1 50460 0 0 0 0 0 0 1 50460 0 0 0 0 0 0 1 50460 0 0 0 0 0 0 1 50460 0 0 0 0 0 0 1 50460 0 0 0 0 0 0 1 50460 0 0 0 0 0 0 1 50460 0 0 0 0 0 0 1 6410 0 0 0 0 0 0 1 6410 0 0 0 0 0 0 0 1.8-3 0 0 0 0 0 0 0 01.5 + 0 0 0 0 + 0	VISIBILITY 24 *** *	VIS.BIL.ITY 25	VISIBILITY 26 ******	VISIBILITY 27 4 1/2 74 1 1 1/2 2 4/2 5 1 1 0 1 0 NC
VISIBILITY 31	VISIBILITY 32 1/16	VISIBILITY 4/2 [A41] 142 [448 [410] 100 100 4 0 0 0 0 0 0 0 1 100 3040 0 0 0 0 0 0 1 100 3040 0 0 0 0 1 1 6 100 100 0 0 0 1 1 6 100 100 0 0 0 0 1 1 6 100 100 0 0 0 0 0 0 0 100 100 0 0 0 0	VISIBILITY -/0/[/14] -12 [F48 [8-10]-10] NC	VISIBILITY 35 VISIBILITY	INSUFFICIENT DATA
INSUFFICIENT DATA	VISIBILITY 41 -1/2 [44] 1-2 [44	INSUFFICIENT DATA	WISISILITY NC 0 0 0 0 0 47 Social 0 0 0 0 0 0 0 0 34-40 0 0 0 0 0 0 0 0 34-40 0 0 0 0 0 0 0 0 34-40 0 0 0 0 0 0 0 0 34-40 0 0 0 0 0 0 0 0 4 18-60 0 0 0 0 0 0 4 18 4 10 0 0 0 0 1 0 0 0 4 18-60 0 0 0 0 0 0 0 4 18-60 0 0 0 0 0 0 0 4 18-60 0 0 0 0 0 0 0 4 18-60 0 0 0 0 0 0 0 4 18-60 0 0 0 0 0 0 0 5 18-80 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 6 18-80 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	INSUFFICIENT DATA	INSUFFICIENT DATA

ective compilation of available data for specified areas without regard to suspected biases.

posite page) are based on all available data subjectively adjusted where bias was evident.



WIND-VISIBILITY-CLOUDINESS



LOW CLOUD CEILING-VISIBILITY-WIND

<1 - 5 4 OR + - 5

420 4 0R 48 420 4 0R 48

V687 47

+ 60 4 ±6

INSUFFICIENT

DATA

1	2	3	4	5	
HIND SPEED (KNOTS)	NIND SPEED (KNOTS)	WIND SPEED (KNOTS)	MIND SPEED (KNOTS)	HIND SPEED IKNOTS)	MIND SPEED (KNO
LCC - YABY 3 10 21 33 254	LCC - YABY 3 10 21 33 234	LCC - VBBY 3 10 21 33 324	LCC - YARY 3 0 21 33 54	LCC - VARY 3 10 21 33 234	0- 4- 11- 27 CC - YEST N 10 23 33
<1.546R <. 5 0 + 0 0 0	41.6 6 OR 4.6 + + + 0	41.64 DR 4.5 0 + 0 B 0	41.5 A OR 4.6 0 0 0 0	41.5 4 OR 4.5 0 0 0 0 0	17.54 OR 1.5
48 4 OR 42 0 + 0 0 0	46 4 OR 12 + 1 2 + +	*6 4 GR <p +="" 0="" 0<="" td=""><td>46 4 OR 42 0 0 0 0 0</td><td>48 4 DR -Z</td><td>*6 t 02 <2 1 2 </td></p>	46 4 OR 42 0 0 0 0 0	48 4 DR -Z	*6 t 02 <2 1 2
410 4 0R 42	Y887 *2 0 + 1 + + + *10 4 08 *2 + 2 4 1 +	V88Y <2 0 + + 0 0 <10 4 08 <2 + 1 1 + 0	Y58Y *2 0 0 0 0 0 *10 4 0R *2 0 1 + + 0	VBBY 42 0 0 0 0 0 0	Y581 42 + 1 1 -
<20 4 0R <5 + 1 1 + 0	<10 4 0R <2 + 2 4 1 + 420 4 0R <6 1 5 8 3 +	<90 4 08 <5 + 1 3 1 +	<20 4 0R <5 + 2 2 + D	<10 4 GM <2 0 1 3 1 0 4 GM <5 + 5 13 3 U	-10 4 08 -2 + 3 4 1 -20 4 08 -5 1 6 9 :
V887 36 12 40 40 6 C	VSBY 35 11 45 33 6 ·	V88Y 35 25 48 21 6 1	V887 26 9 51 38 1 +	V68Y 26 10 38 43 6 0	V887 a6 12 54 26
860 4 86 12 39 39 6 0	260 4 25 10 39 26 3 +	PRG 4 45 24 45 17 4 +	2 50 4 25 8 49 35 1 +	*50 4 *5 9 30 29 2 D	250 4 25 11 48 18 ;
HC 6 a 10 10 33 34 4 0	NC 4 a 10 9 34 22 2 +	HC4 > 10 23 44 16 4 ·	MC 4 2 10 8 45 31 1 +	HC 4 a 10 7 28 26 1 0	NC 43 10 10 43 15 1
1075	6357	1382	589	245	!
10	1 1 HIND SPEED (KNOTS)	12 MIND SPEED (KNOTS)	13 HIND SPEED (KNOTB)	14 HIND SPEED (XNOTS)	HIND SPEED (KNO
100 100 111- 22-	10-14-11-199-1	[[] [] [] [] []	10-14-111-122-1	0-14-111-122-1	10-14-111-122
CC - V887 3 10 21 39 194	LCC - Year 3 10 21 33 034	CC - VARY 3 10 21 39 254	CC - Year 5 10 81 33 254	LCC - Y88Y 3 10 21 33 274	CG - YEBY 3 10 21 33
48 6 0R 48 0 0 0 0 0	46 4 OR 42 D D O O O	*8 4 OR <2 0 + 0 0 0	-64 OR -2 0 0 2 0 0	-5 4 OR 48 0 U O 0 0 A 8 + NO 4 8+	-118 GR -12 0 0 0 0
Y887 42 0 0 0 0 0	V88Y 42 0 0 0 0 0	VERY 42 0 + 0 0 0	VEDT 42 0 0 0 0 0	VSBT 42 0 0 0 0 0	VS97 +2 0 0 0 0
410 4 98 42 2 2 0 0 0	410 4 OR 42 2 2 2 0 0	410 4 0m 42 0 1 1 0 0	<10 4 OR <2 0 1 8 0 0	410 4 9R 42 0 5 0 0 0	410 4 BH 42 5 3 2 D
420 4 0R 45 2 7 2 0 0	420 4 OR 45 2 9 5 0 0	420 4 0R 45 + 6 5 + D	420 4 0R 46 0 5 13 0 0	420 4 68 45 0 5 0 2 D	470 4 OR 46 5 12 5 ()
V667 aB 28 67 5 0 0	280 435 7 43 30 1 0	VSBY 25 11 56 29 1 0 2 1 0 2 1 0 2 1 0 2 1 0 2 1 0 0 0 0 0 0 0 0 0	YSBY 28 7 48 42 0 0 250 425 6 41 31 0 0	V887 as 32 57 5 5 0	VBBY +5 34 56 H II
MC4 210 24 55 3 0 0	NC 4 3 10 7 40 27 1 0	≥\$0 4 98 11 49 23 → 0 MC 4 2 10 11 49 21 → 0	MC 4 2 10 6 37 27 0 0	260 4 26 27 50 2 0 0 MC 4 2 10 25 48 2 0 0	HC4±10 27 37 3 0
68	131	286	131	120 130 2 0 0	Files Falls
19	20	21	22	23	?
HIND SPEED (KNOTS)	WIND SPEED (KNOTS)	HIND BARED (WHOLE)	HIND SPEED (KNOTS)	NIND SPEED (KNOTS)	WIND SPEED IKNOT
LCC - VARY 3 10 21 33 334	LCC - VARY 3 10 21 33 234	LCC - YBBY 3 10 21 33 P34	LCC - YAMY 0- 4- 11- 22- 3 10 21 33 234	LCC - YEAY 3 10 81 33 334	LCC - VSBY 3 10 21 31
41.8 40A 4.5 0 0 0 0 0	41.540R 4.E 0 0 0 0 0	<1.54 nR <.5 0 0 0 + 0	41.84 CR 4.8 U U O O O	41.84 0A 4.5 0 + + 0 0	<1.8 4 DR <.5 0 0 U U
46 4 OR 42 0 0 0 0 0	*6 4 OR *2	45 4 68 47 0 + 2 1 0	46 4 dA 4P 0 0 0 0 0	*6 t 6R *2 G + + + O	46 4 OR 42 0 0 0 U
410 4 5H 42 0 3 3 0 0	*10 4 0R *2 G 1 3 2 0	410 4 08 48 0 2 11 3 0	410 4 OH 42 D D 13 D D	*10 & OR <2 D 1 1 + U	410 4 0R 42 D 4 D D
-20 4 OR -5 0 3 8 0 0	420 LOR 45 0 3 9 3 0	420 4 OR 45 + 5 17 4 0	420 4 0R 45 D 5 72 D D	490 4 DR 48 + 3 4 1 0	*20 4 DR *6 D 22 D D
VBBY 38 6 46 49 0 0	V86Y bB 2 25 67 6 0	vésras 2 35 52 7 0	V667 aft 4 36 53 4 D	V&BT a8 14 43 36 7 0	V88Y 26 13 48 30 9
80 4 18 6 43 37 U O	2 50 4 as 2 22 52 3 0	#80 4 #8 2 30 35 4 D	350 4 35 4 25 29 4 D	#50 4.25 13 39 30 6 0	*80 4 a 5 13 26 30 9
MC 4 D D 6 43 37 0 0	MC 4 > 10 2 22 51 2 0	HC 4 = 10 2 26 33 3 0	HC 4 2 10 4 24 25 4 0	MC 6 2 10 13 38 29 6 0	HC 4 a 10 13 26 30 4
28	29	30	31	32	3
HIND SPEED (KNOTS)	HIND SPEED (HNOTS)	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOT.
LCC - VERY 3 10 21 33 234	LCC - VERY 3 10 21 33 234	LCC - Y88Y 0- 10- 11- EE- 34	LCC - VBEY 9 10 21 33 234	LCC - YEBY 3 10 21 33 834	LCC - VBRY 3 10 21 33 1
41.5408 4.6 D 0 0 0 D	<1.84 00 <.8 U 0 0 0 0	41.54 GA 4.5 D O O O O	41.54 OF 6 U O O O O	-1.84 DR 4.6 D D D 0 0	41-8 4 0E 4-6 0 0 0 0
<8 4 OR <2 0 0 1 0 0	-84 OR -F 0 0 1 D 0	48 4 DR 42 0 0 1 2 0	*B 4 GR 42 1, 0 0 0 0	<84 SR +2 0 0 + 1 +	48 4 GR +2 U
410 A 0R 48 0 2 2 + +	410 4 64 48 0 0 0 0 0 0	VBBY 42 0 0 0 0 0 0	V487 47 0 0 0 0 0	Vaav +2 0 0 0 0 0	V88Y -2 0 0 0 0
420 A 66 48 0 2 2 + +	410 4 0R 48 D 1 19 9 D	*10 4 08 4 0 0 1 14 8 2	*10 4 0R *2 C 2 5 0 2 *20 4 0R *8 3 20 13 5 3	<10 4 DR <2 + 2 1 3 1	*10 & 0R *2
V68Y as 5 40 40 12 1	V887 AS 5 23 53 17 0	V66Y 36 4 27 48 14 4	VEST 15 41 30 18 5	V687 35 4 41 35 16 4	V687 15 2 32 43 17
a 50 4 a 5 5 34 29 9 1	250 4 25 4 18 31 9 G	2 50 4 26 3 24 26 7 2	2 50 4 25 2 10 11 10 2	250 4.25 2 24 23 8 1	280 4 25 1 18 27 10
MC 4 a 10 5 32 27 9 1	MC 4 10 4 19 29 8 U	HC 4 > 10 3 24 23 7 1	NC : 4 10 2 8 11 7 0	HC 4 2 10 2 22 21 B 1	MC 6 a 10 1 17 25 B
37	77	91	61	335	9/
3/	20	20	A C)	A 1	• •
	38 HIND SPEED (KNOTS)	39	40	4 1	4.
	38 HIND SPEED (KNOTS) LCC - V887 0- 4- 11- 29- 34 32 33 334	39	40	4] HIND SPEED (KNOIS) 1.CC VART 0- 4- 11- 22- 9 10 21 33 254	41

INSUFFICIENT

DATA

<u>Graphs</u> represent the objective compilation of available data for specified areas without the <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjust

VERY AS

INSUFFICIENT

DATA

INSUFFICIENT

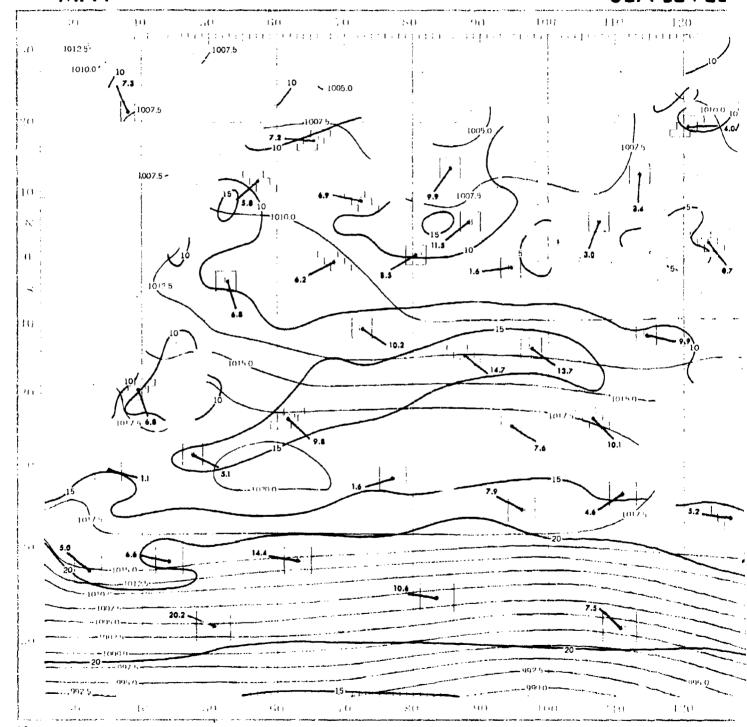
DATA

TY-WIND

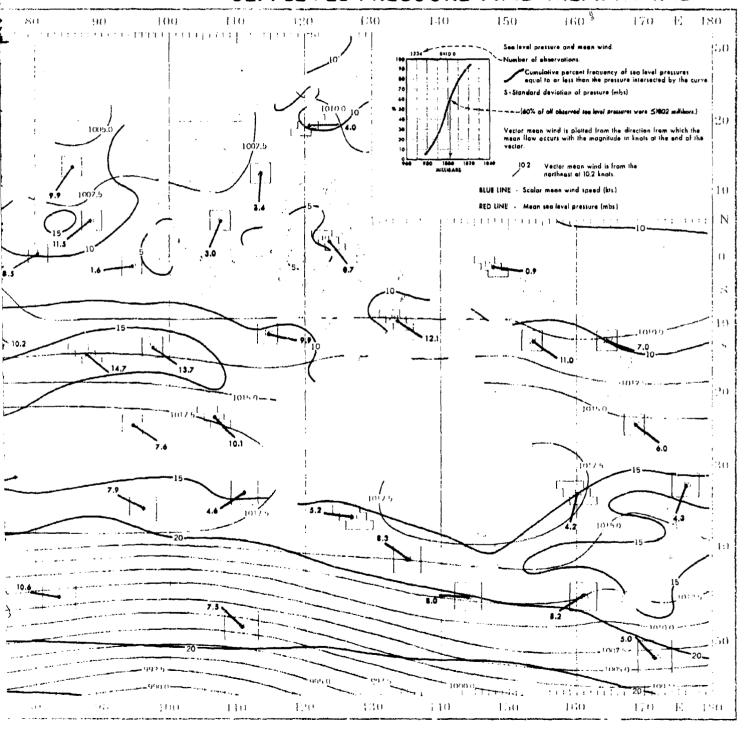
MAY

WIND SPEED (KNOTS)	NIND SPEED (KNOTS)	6 WIND SPEED (KNOTS)	HIND SPEED (KNDTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)
CC - SBE 7	CC - VOBY			CC - V85Y 5 0 0 10 27 33 34 44 15 6 4 08 15 6 10 10 10 10 10 10 10 10 10 10 10 10 10	CC - VBAT 3 10 21 33 334 41.8 4.08 4.8
13	1 4	15	16	17	18
NIND SPEED KNOTS	HIND SPEED (KNOIS) LCC - YeBY	NIND SPEED (KNOIS)	HIND SPEED (KNOTS) LCC - VMBY 3 10 21 33 34 1.5 4 OR < 5 0 0 0 0 0 44 0R < 2 0 0 1 6 450 4 OR < 5 0 0 1 6 400 4 OR < 5 0 0 1 6 400 4 OR < 5 0 0 1 6 400 4 OR < 5 0 0 1 6 400 4 OR < 5 0 0 1 6 400 4 OR < 5 0 0 1 0 400 4 OR < 5 0 0 1 0 400 4 OR < 5 0 0 1 0 400 4 OR < 5 0 0 1 0 400 4 OR < 5 0 0 1 0 400 4 OR < 5 0 0 1 0 400 4 OR < 5 0 0 0 1 0 400 4 OR < 5 0 0 0 0 400 4 OR < 5 0 0 0 400 4 OR < 5 0 0 0 400 4 OR < 5 0 0 0 400 4 OR < 6 0 0 400 4 OR < 7 400	HINU SPEED (KNOTE) LCC - VERY 2 0 0 10 E1 33 844 11-E 4 0R 1-5 0 0 0 0 0 0 0 18 4 0 R 1-7 0 0 0 1 1 1 1 2 420 4 0R 1-7 0 0 1 1 1 1 2 420 4 0R 1-5 0 0 3 15 3 2 VSST 1-6 2 2 11 62 12 2 180 4 10 2 2 17 41 7 0 HC 4 10 2 17 41 7 0	HIND SPEED (KNOTS) LUC - VARY S 0 1 1 33 34 34 4 1 1 1 1 2 1 1 1 2 1 1 1 1 1 1 1 1 1
22 NIND SPEED (KNOTS)	23 RINO SPEED (KNOTS)	24 WIND SPEED (KNOTS)	25 HIND SPEED LKNOTS)	26 HIND SPEED (KNOIS)	27 Hind Speed (Knots)
11 12 13 14 15 15 15 15 15 15 15	CC - VBBY 9 10 21 98 244 41.54 OR 4.5 0 + + D 0 41.54 OR 4.5 0 + + D 0 VBBY 47 0 + 0 0 + D 110 4 OR 47 0 1 1 1 + D 20 4 OR 48 1 3 34 1 0 200 4 0R 48 1 3 38 30 8 0 MC 4 A 10 13 30 29 6 0 006	CLC - VBBT 3 10 21 33 ab4 11.6 4 0R 1.5 0 0 0 0 0 0 15 4 08 12 0 0 0 0 0 0 VBBT 12 0 0 0 0 0 0 0 10 4 0 0 0 0 0 0 0 110 4 0 0 0 0 0 0 0 0 110 4 0 0 0 0 0 0 0 0 120 4 0 0 0 0 0 0 0 120 4 0 0 0 0 0 0 0 120 4 0 0 0 0 0 0 0 120 4 0 0 0 0 0 0 0 120 4 0 0 0 0 0 0 0 0 120 4 0 0 0 0 0 0 0 0 0 120 4 0 0 0 0 0 0 0 0 0 0 120 4 0 0 0 0 0 0 0 0 0 0 0 0 0 120 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	CC - V88Y 3 - 1 1 22 3 344 4 1 1 1 2 1 3 344 4 1 1 1 1 1 1 1 1	LCC - VIBY	CC - V887 0 1 1 1 1 3 144
31 Hind Speed (XNOTS)	32 WIND SPEED (KNOTS)	33 HIND SPEED (KNOTS)	34 WIND SPEED (MNOTS)	HIND BPEED (KNOTS)	36
C(- v58 v	CCC - V66Y	CC VSB1 3 10 22 3 34	CCC - VBBF 3 1 0- 1- 12- 22- 3 3- 3-4 4 1- 5- 4 0R 4.5 0 0 0 4 1 0 0 1 3- 3- 3- 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	CC VBBY 3 0 14 11 27 27 28 24 21 25 40 4 25 20 2 27 7 1 26 24 21 2 25 20 6 1 1 168	INSUFFICIENT DATA
NSUFFICIENT DATA	4 HIND GPEI'D (KND15) LCC - VABY	INSUFFICIENT DATA	HIND SPEED (KNOTS) .CC - Vagy 3 0 4 11-22CC - Vagy 3 0 0 10 21 33 284 -1.8464-8 0 0 0 0 0 0 0 -4848-2 0 0 0 0 0 0 0 -4848-2 0 0 0 0 0 0 0 -4848-2 0 0 0 0 0 0 0 -4848-2 0 0 0 0 0 0 0 -4848-2 0 0 0 0 0 0 0 -4848-2 0 0 0 0 0 0 0 -4848-2 0 0 0 0 0 0 0 -4848-2 0 0 0 0 0 0 0 -4848-2 0 0 0 0 0 0 0 -4888-2 0 0 0 0 0 0 0 -4888-2 0 0 0 0 0 0 0 -4888-2 0 0 0 0 0 0 0 0 -4888-2 0 0 0 0 0 0 0 0 -4888-2 0 0 0 0 0 0 0 0 -4888-2 0 0 0 0 0 0 0 0 0 -4888-2 0 0 0 0 0 0 0 0 0 -4888-2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	INSUFFICIENT DATA	INSUFFICIENT DATA
	#64 + 10 0 13 22 6 1 #64 + 10 0 13 19 4 1		*AU 4 28 4 18 18 8 U NC 4 * 10 4 18 18 8 U		

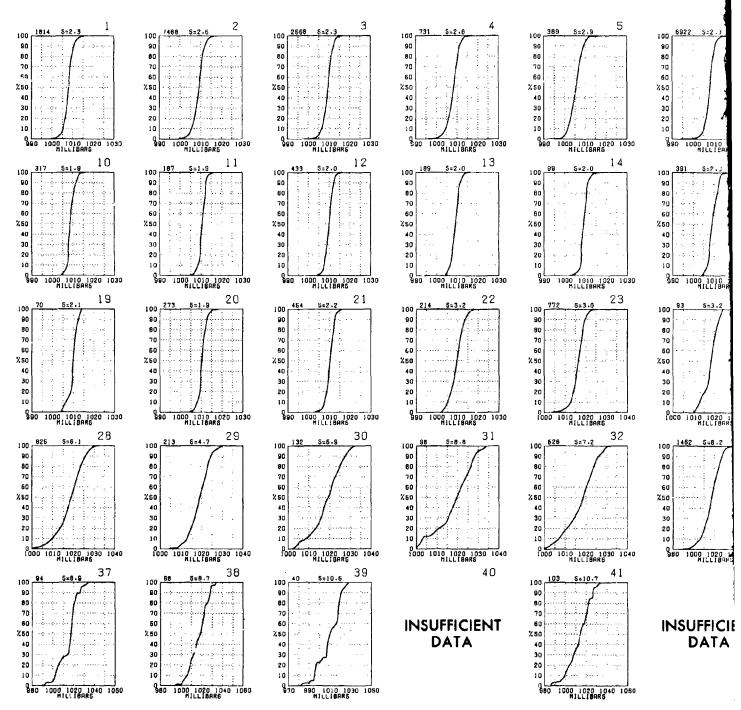
ve compilation of available data for specified areas without regard to suspected blases. Lite page) are based on all available data subjectively adjusted where bias was evident.



SEA LEVEL PRESSURE AND MEAN WIND

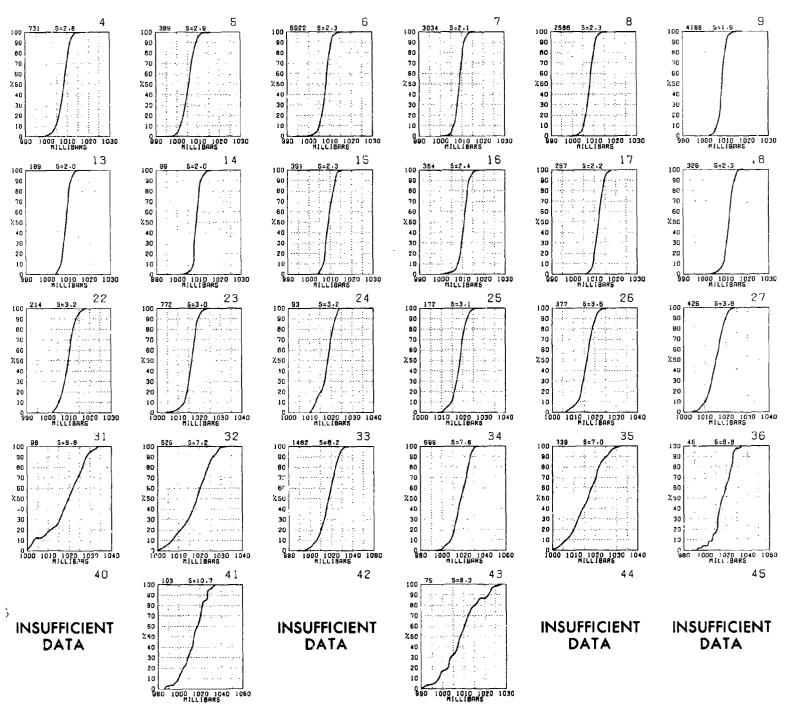


SEA LEVEL PRESSURE

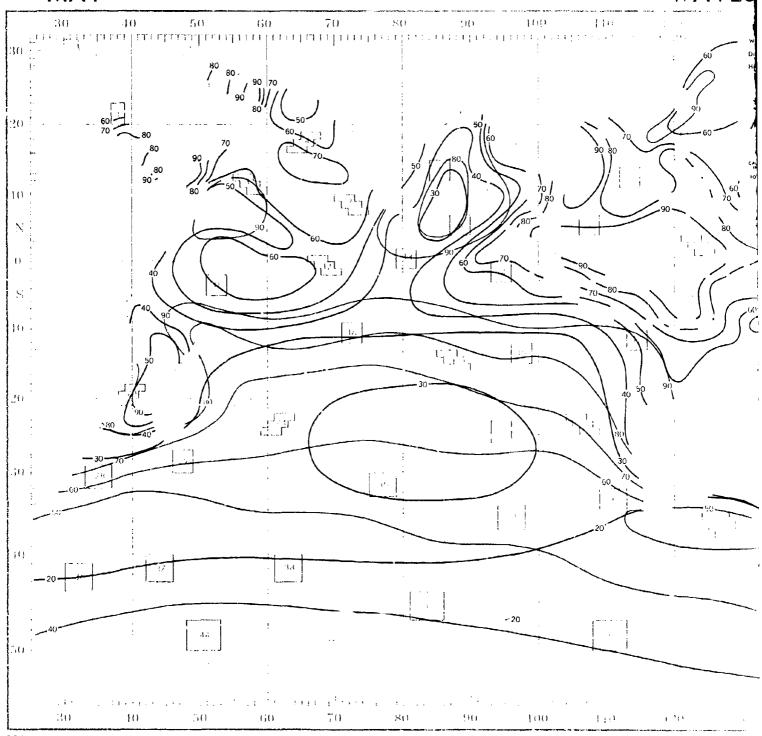


<u>Graphs</u> represent the objective compilation of available data for specified areas with The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively a

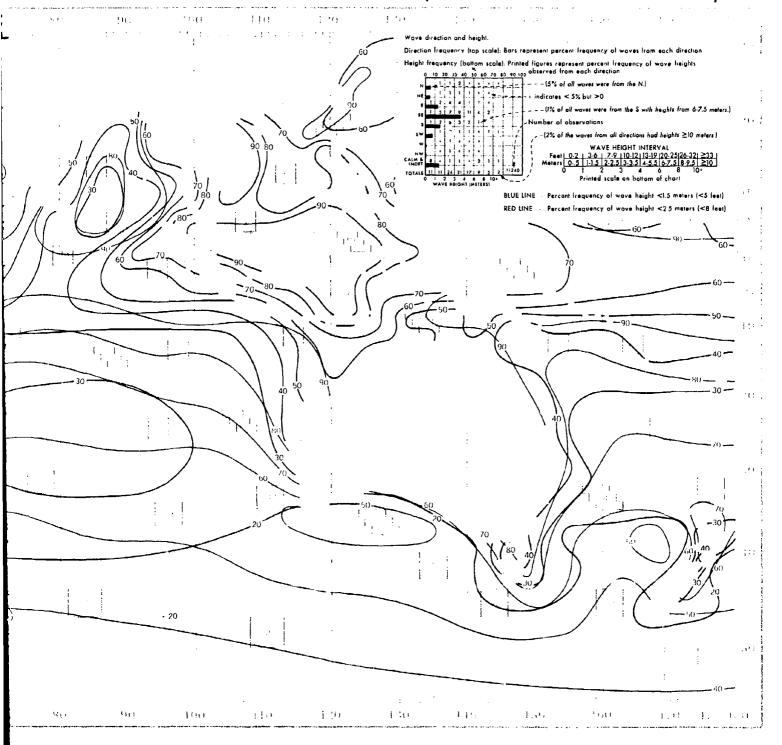
MAY



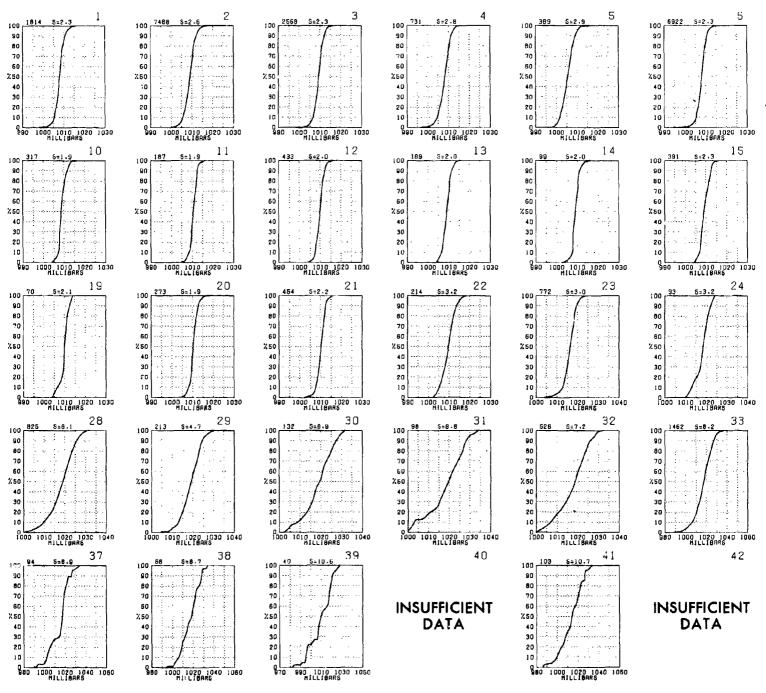
ective compilation of available data for specified areas without regard to suspected biases, posite page) are based on all available data subjectively adjusted where bias was evident.



WAVES (<1.5 AND <2.5 METERS)

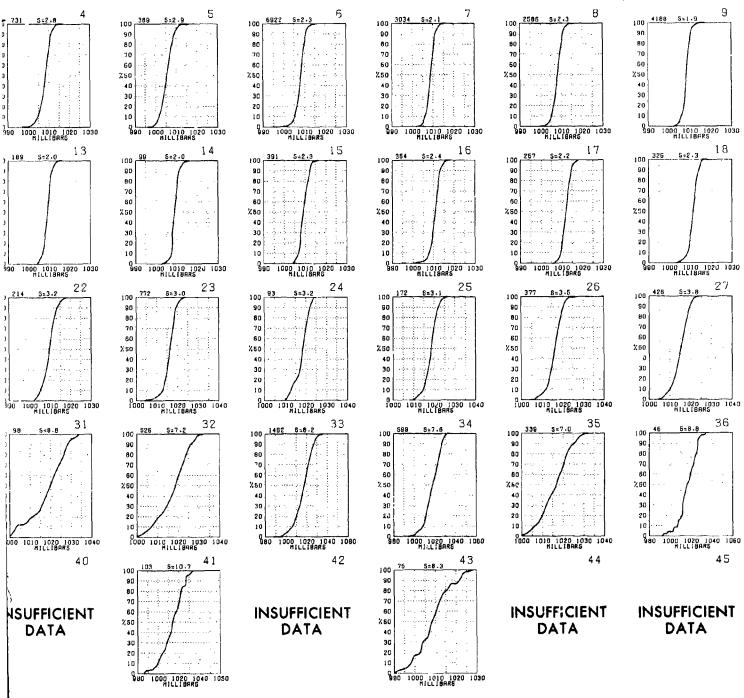


SEA LEVEL PRESSURE

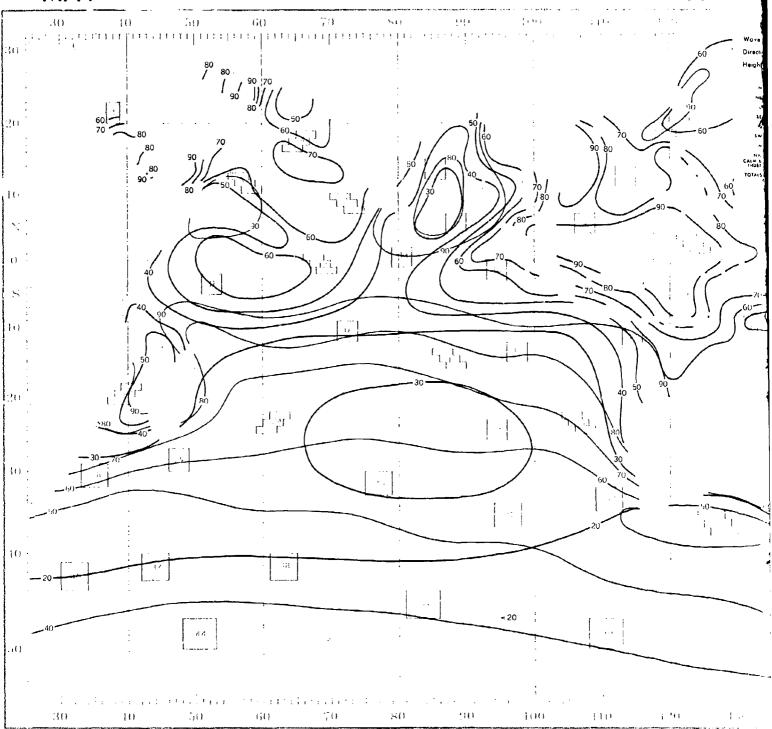


Graphs represent the objective compilation of available data for specified areas without regar. The isopleth analyses (opposite page) are based on all available data subjectively adjusted wi

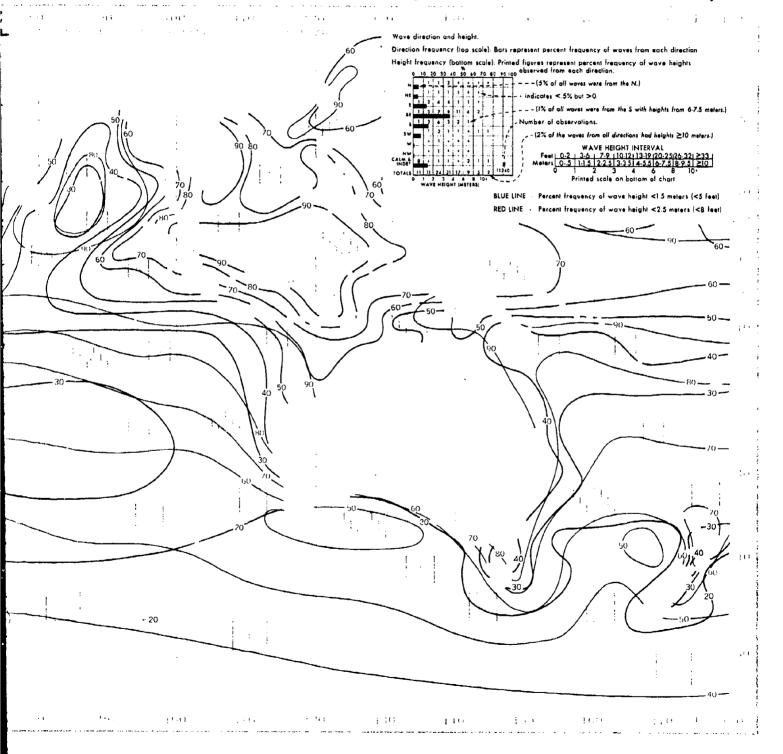
MAY



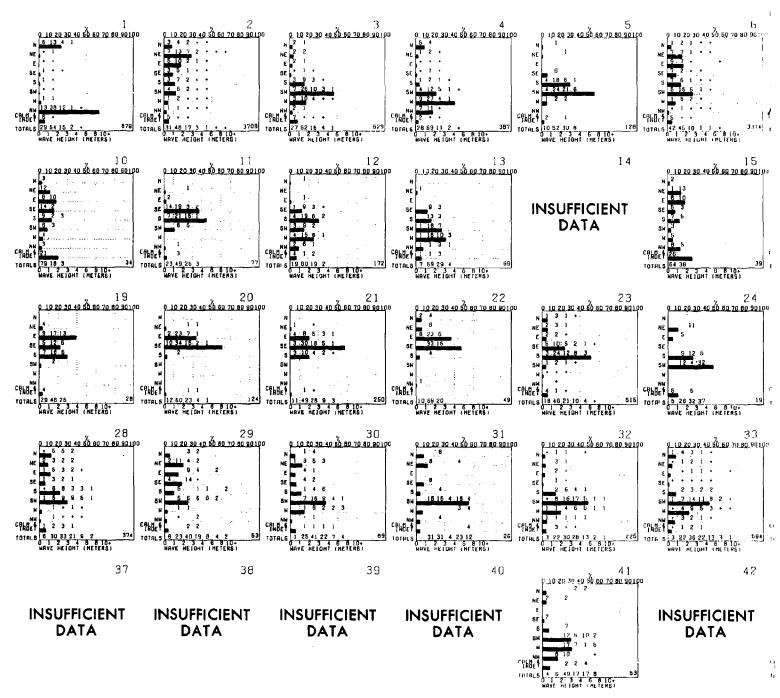
ve compilation of available data for specified areas without regard to suspected biases. ite page) are based on all available data subjectively adjusted where bias was evident.



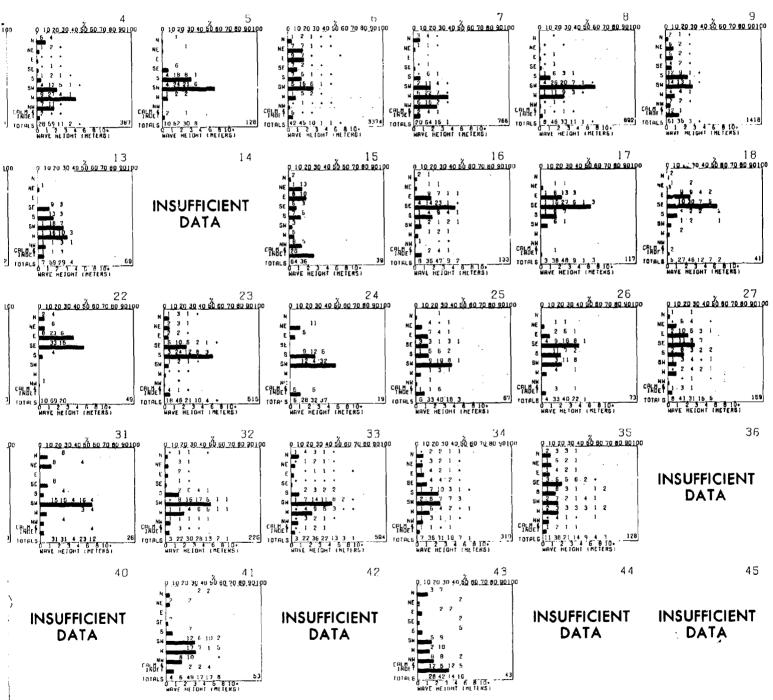
WAVES (<1.5 AND <2.5 METERS)



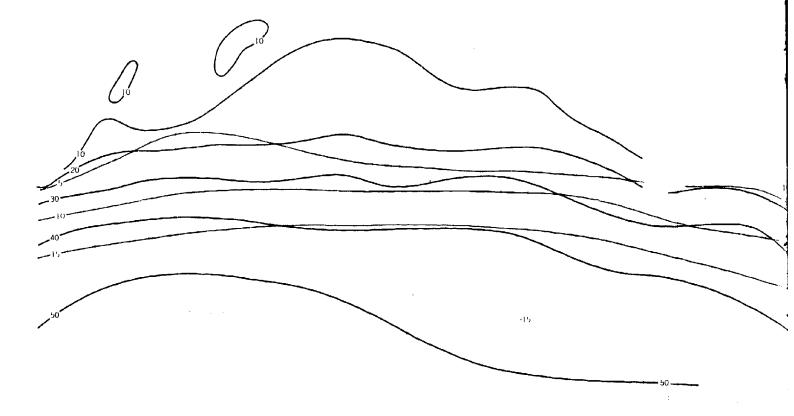
WAVE DIRECTION AND HEIGHT



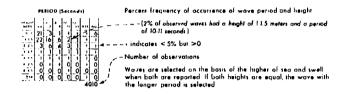
<u>Graphs</u> represent the objective compilation of available data for specified areas without reg The <u>isopleth</u> analyses (apposite page) are based on all available data subjectively adjusted



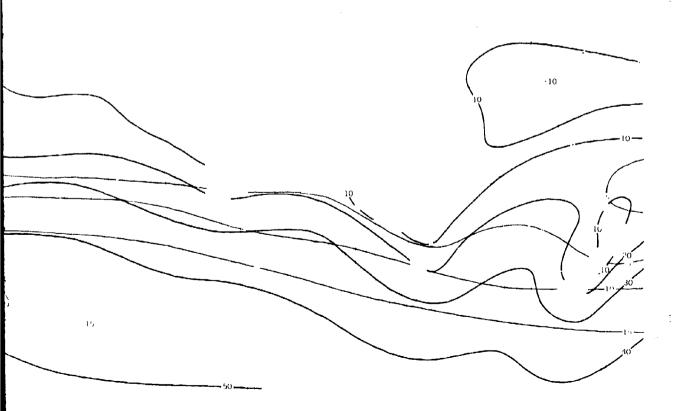
pjective compilation of available data for specified areas without regard to suspected biases. apposite page) are based on all available data subjectively adjusted where bias was evident.



WAVES (≥3.5 AND ≥6 METERS)



BLUE LINE - Percent frequency of wave height ≥3.5 hielers (≥12 feet)
RED LINE - Percent frequency of wave height ≥6 meters (≥20 feet)



WAVE PERIOD AND HEIGHT

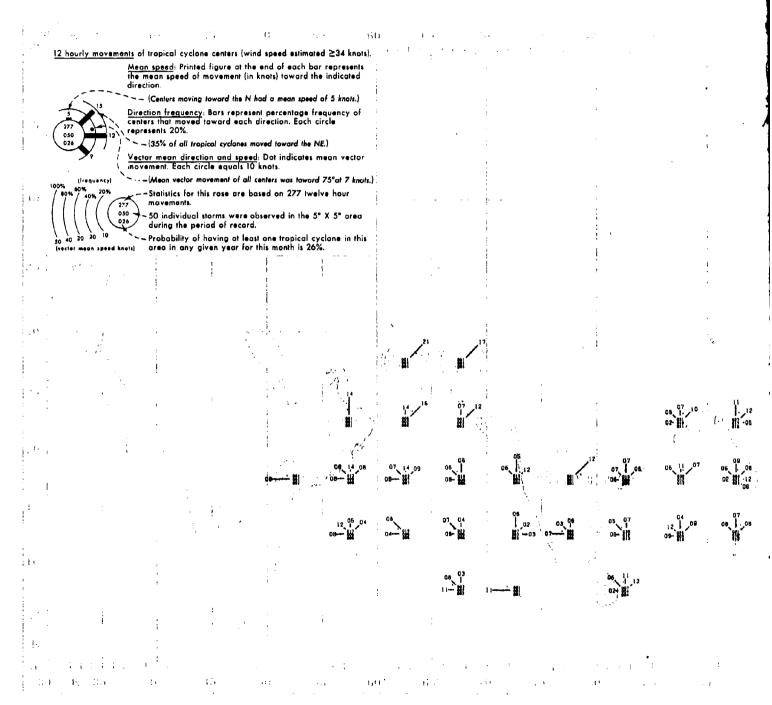
PERIOD I SECONDS: **EIO***I *** 10 - 12 - 12 - 12 12 12 12 12 12	PERIOD (SECONDS) M 1001 1	PERIOD (SECONDS) MC10e1	PERIOD (SECONDS) **(10*1*)	PERIOD I SECONDS 1 [RIFRE] = 4	PER DD (SECONO) (MISS) 46 76 91 12 12 (
PERIOD (SECONDS) **CIBM**	1	12 PERIOD (SECONDS) 12 13 13 14 15 15 15 16 16 17 17 18 18 18 18 18 18	3 PERIOD (SECONDS)	INSUFFICIENT DATA	PERIOD (SECONDS:
PERIOD (SECONDS) HEIDH 6 - 6 - 8 10 12 12 100 0-18 21 4 0 0 0 0 1 1-1-5 25 18 0 0 4 0 0 2-2-5 0 4 18 4 0 0 0 2-3-6 0 0 0 0 0 0 0 3-3-6 0 0 0 0 0 0 0 4-6-7 0 0 0 0 0 0 0 4-7-7 0 0 0 0 0 0 0 4-7-8 0 0 0 0 0 0 0 4-7-9 0 0 0 0 0 4-7-9 0 0 0 0 0 0 0 4-7-9 0 0 0 0 0 0 0 4-7-9 0 0 0 0 0 0 4-7-9 0 0 0 0 0 0 4-7-9 0 0 0 0 0 0 4-7-9 0 0 0 0 0 0 4-7-9 0 0 0 0 0 0 4-7-9 0 0 0 0 0 0 4-7-9 0 0 0 0 0 0 4-7-9 0 0 0 0 0 0 4-7-9 0 0 0 0 0 0 4-7-9 0 0 0 0 0 0 4-7-9 0 0 0 0 0 4-7-9 0 0 0 0 0 4-7-9 0 0 0 0 0 4-7-9 0 0 0	PERIOD (SECONDS) **C1841 6 7 8 11 12 12 100	21 PERIOD (SECONDS) (Albert) 4	PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***********************************	23 PERIOD (SECONDS) PERIOD	INSUFFICIEN' DATA
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<u>Graphs</u> represent the objective compilation of available data for specified areas without The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjus

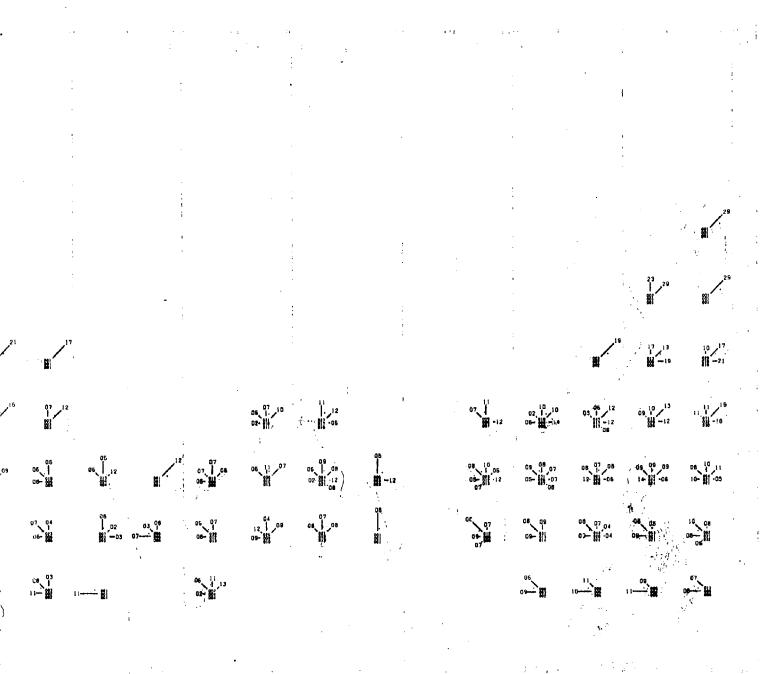
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PERIOD (SECONDS) -(164) - A - 8 - 10 - 12 - 12 - 13 - 14 - 14 - 14 - 14 - 14 - 14 - 14	PERIOD SECONDS	PERIOD (SECONDS) ***I (6-1)	7 PERIOD (SECONDS) (ATES) -4	8 PERIOD SECONDS	SECONDS SECO
13 PERIOD (SECOND) **Iden	INSUFFICIENT DATA	15	1 1 1 1 1 1 1 1 1 1	PERIOD (SECONDS) 1 7 PERIOD (SECONDS) 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1
22	PERIOD (SECONDS) **C(0+1) 6- 0- 13- 17 13- 190 0-1 14 2 + 0 0 6 1-1.8 21 13 7 1 1 0 2 2-7.8 4 8 3 2 2 + 1 3 14 3 2 + 0 0 4 15 15 15 15 15 5 16 17 17 1 1 0 2 2-7.8 4 8 3 2 2 + 1 3 14 3 2 + 0 4-1.1 7 7 7 7 7 4-1.1 7 7 7 4-1.1 7 7 7 4-1.1 7 7 7 4-1.1 7 7 7 4-1.1 7 7 4-1.1 7 7 4-1.1 7 7 5 7 7 5 7 7 5 7 7 5 7 7 5 7 7 5 7 7 5 7 7 5 7 7 5 7 6 7 6 7 6 7 7 7 7 7 7 7 8 7 8 7 8 7 8 7 8 7 9 7	INSUFFICIENT DATA	PER OU (SECONDS No. No. No. No. No. No. No. No. N	26 PERIOD (SECONDS) 1016-1	PERIOD (SECONDS) 6- 0- 19- 11- 11- 11- 11- 11- 11- 11
71 PERIOD (SECONDE) **ION** *	32 Section	HE TRIVET SECURITION SECU	34 PERIOD (SECONDS) (ATES) 46 7 8 10 10 17 18 110 10 10 10 10 10 10 10 10 10 10 10 10	35 FERIOD (SECONDS) ***********************************	INSUFFICIENT DATA
) INSUFFICIENT DATA	PERIOD (SECONDS) ***INTER** 4- 6- 3 6 11 12 13 15 10 ***OA 2 2 0 0 11 0 0 ***I-1-A 4 2 0 0 0 0 0 ***I-1-A 4 17 15 8 4 0 2 ***J-1-B 0 2 6 2 2 2 4 ***I-1-B 0 2 4 0 2 0 0 ***I-1-B 0 0 0 0 0 0 0 ***I-1-B 0 0 0 0 0 0 0 ***J-1-B 0 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-1-B 0 0 0 0 0 0 **J-	INSUFFICIENT DATA	PERIOD (SECONDS) ***CIO*** 4	INSUFFICIENT DATA	INSUFFICIENT DATA

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TROPICAL CYCLONE

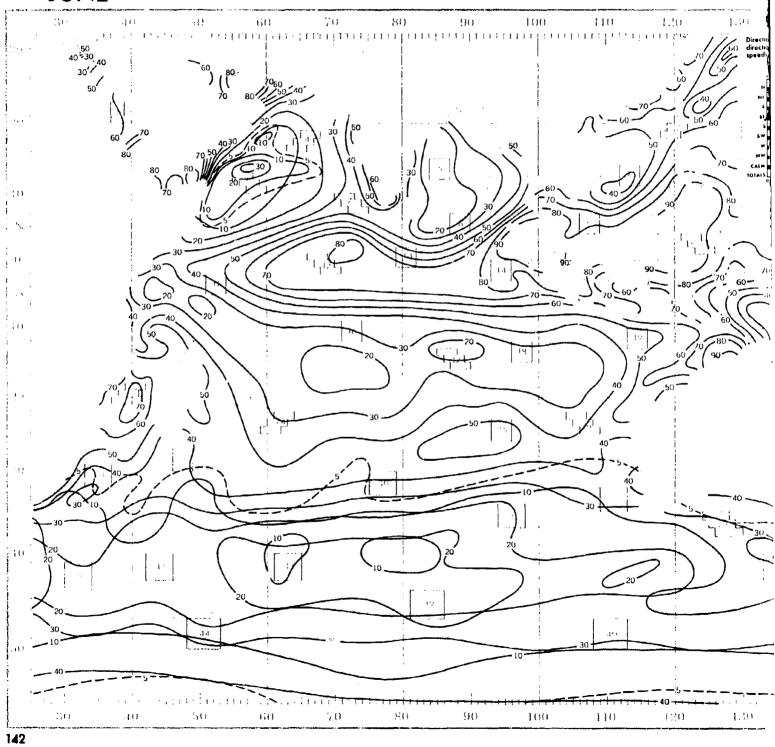


TROPICAL CYCLONE

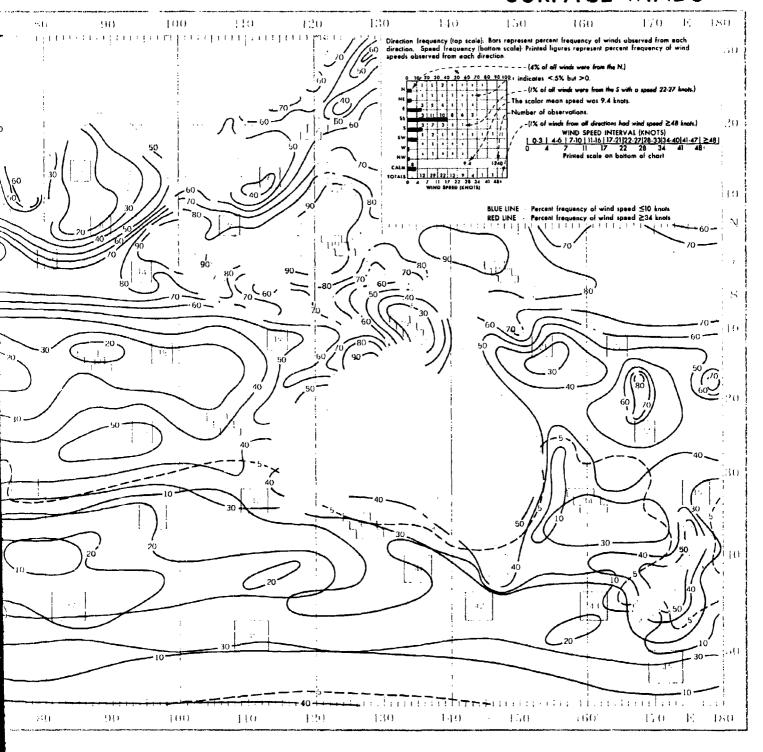
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	:				j	(frequency) (M 100% 40% 20% 5th 100% 40% 20% 5th 100% 40% 20% 5th 100% 40% 20% 5th	ean vector movement of all cent atistics for this rose are based averments. Individual storms were obse ring the period of record.	ers was loward 75°ct 7 knots.) d on 277 twelve hour rved in the 5° X 5° area
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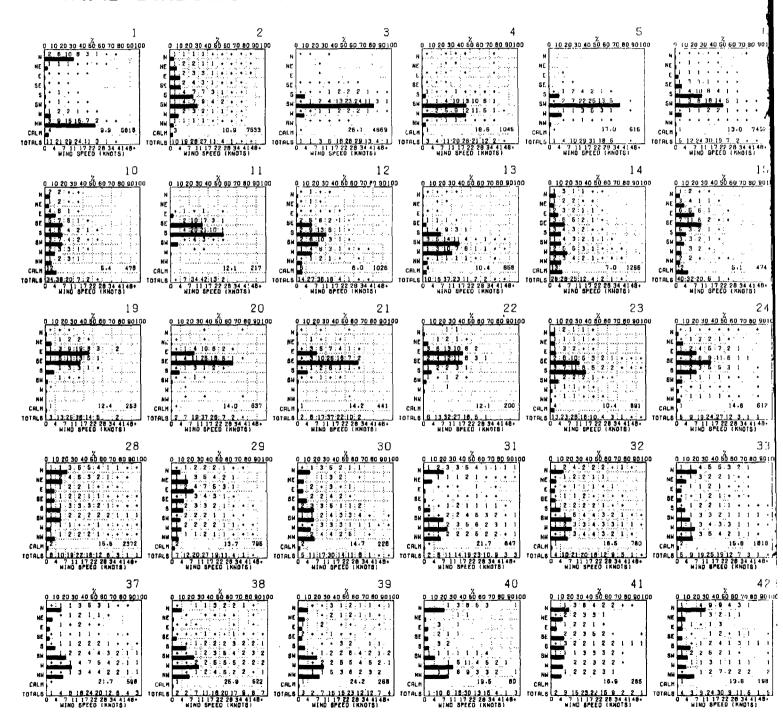
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SURFACE WINDS

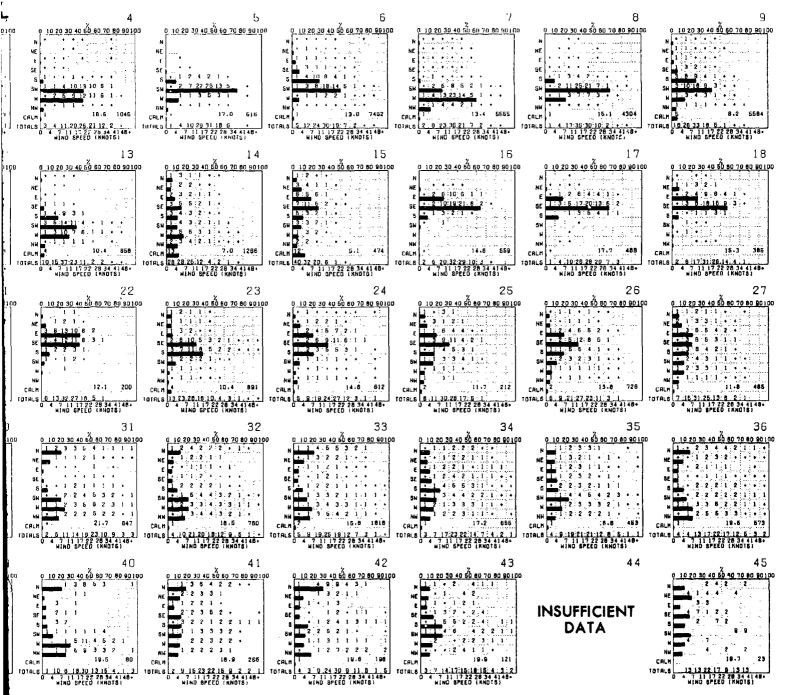


WIND DIRECTION AND SPEED



Graphs represent the objective compilation of available data for specified areas without re The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjuste

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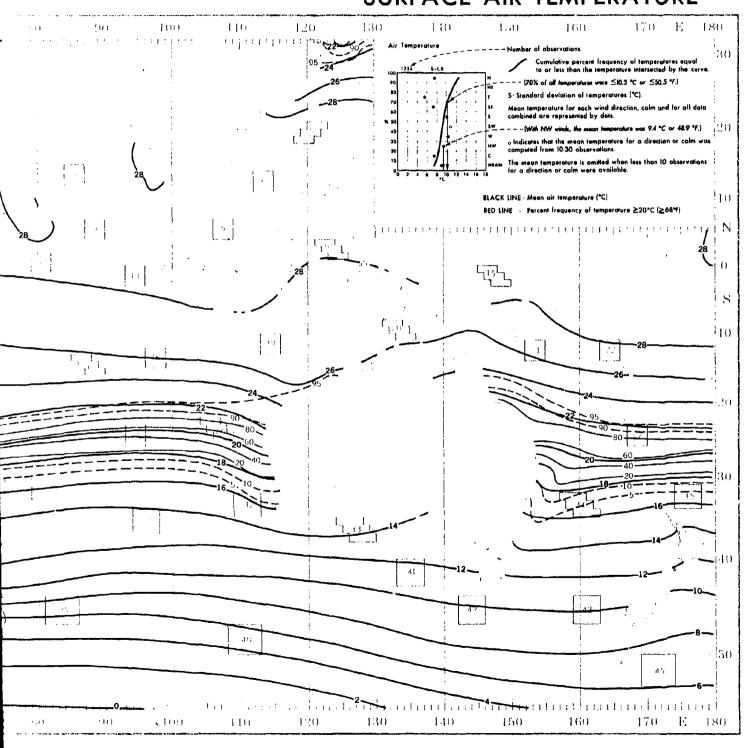


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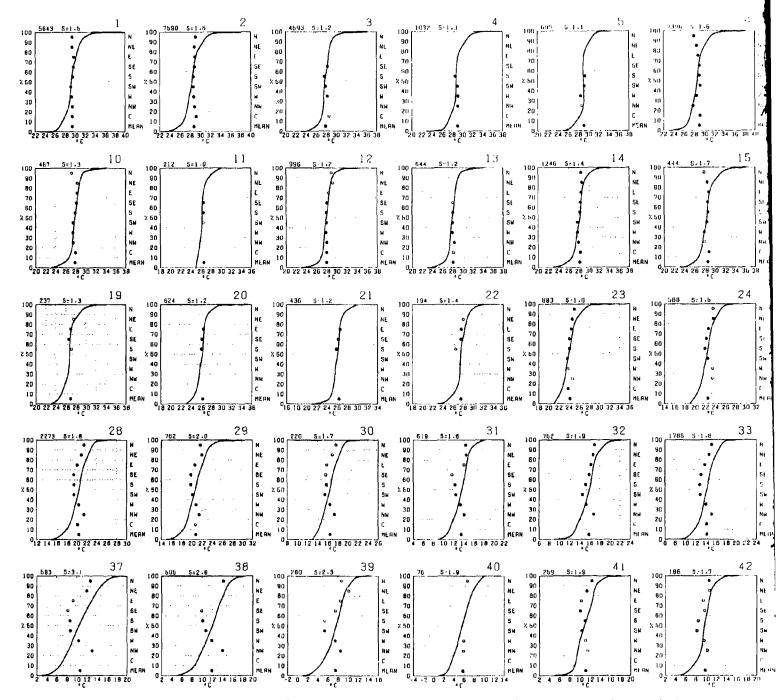
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SURFACE AIR TEMPERATURE

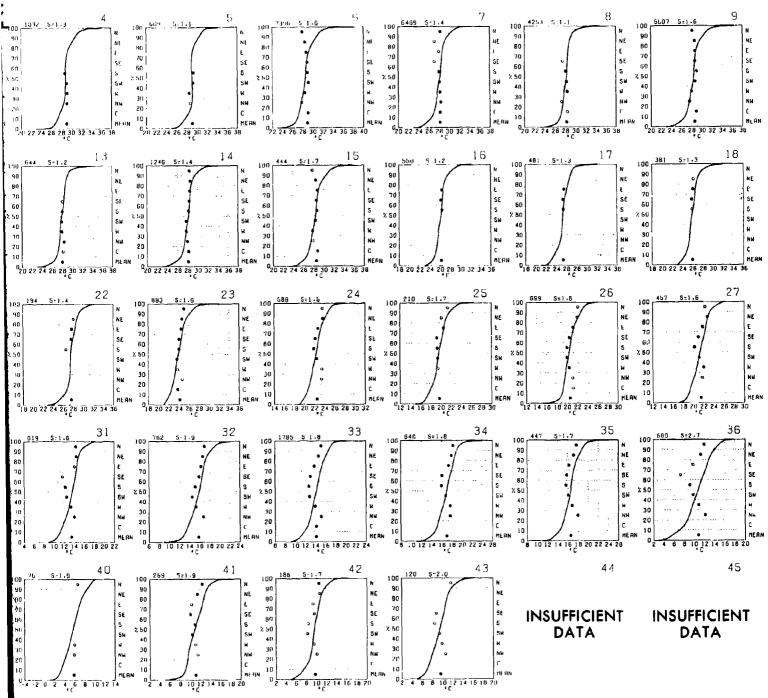


SURFACE AIR TEMPERATURE



Graphs represent the objective compilation of available data for specified areas without re The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjusted

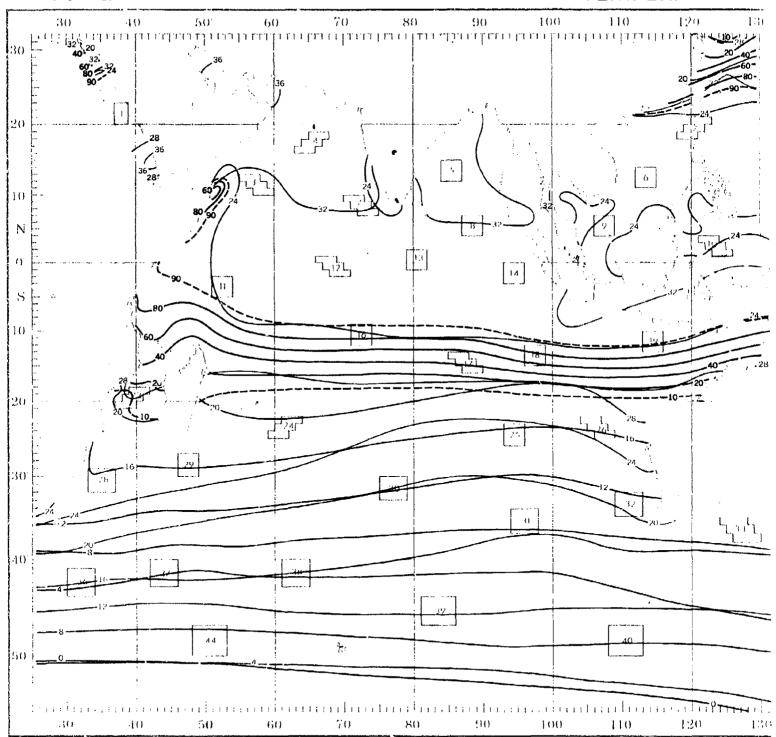
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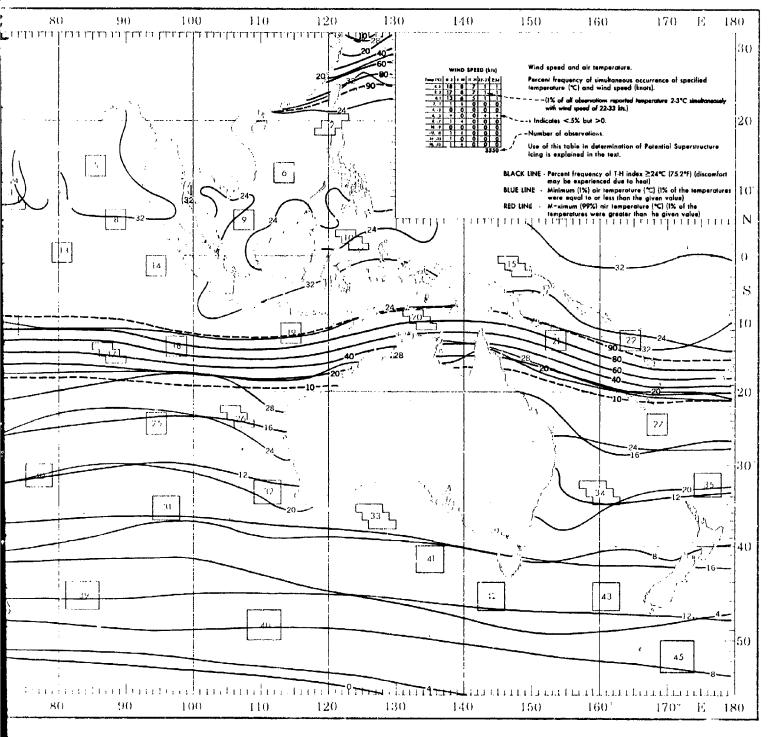
ective compilation of available data for specified areas without regard to suspected biases. posite page) are based on all available data subjectively adjusted where bias was evident.

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TEMPERATURE I



TEMPERATURE EXTREMES AND T-H INDEX



WIND SPEED AND AIR TEMPERATURE

	_	_		_	1
HIND SPEED IKTS)	HIND SPEED (KIS) 2	HIND SPEED (KTS)	WIND SPEED (KTS)	HIND SPEED (KTS) 5	HIND SPEED (KIS)
7EMP (*C1 0-3 4-10 11-21 22-33 a 34	TEMP (*C) 0-3 4-10 11-21 22-33 4 34	34.36 Q + Q Q Q	TEMP (PC) 0-3 4-10 11-21 22-33 a 34	7EHP (*C) 0-3 4-10 11-21 22-33 2 34	36-37 0 + + 0
36,37 + + 0 0	34.35 + + + 0 0 32.33 2 2 + 0	32.33 + + + + 0	37.33 + 1 2 1 0 30.31 1 4 14 7 1	32.33 0 1 2 + 0 30.31 + 4 1(6 +	34.35 + + 1 · 32.33 + 2 3 ·
32.23 1 4 3 · 0 30.31 5 18 13 2 ·	30.31 3 13 9 1 + 20.29 5 24 19 3 +	28.29 + 2 13 32 8 26.27 + 1 6 20 9	28.29 2 8 28 24 2	28.29 + 8 40 17 0 28.27 0 1 3 1 0	30.31 1 9 14 2 20.20 3 20 27 6
28.29 5 23 17 2 + 28.27 1 3 2 + 0	26.27 1 6 7 2 +	22.23 0 0 0 0 0	24.25 0 · 0 · · · · · · · · · · · · · · · ·	24.25 0 0 + 0 0 22.23 0 0 0 0 0	28.27 4 5
24.25 0 · · · 0 22.23 0 · · 0 0	22.23 0	20.21 0 0 0 0 0 0 18.18 0 0 0 0 0	20-21 0 0 0 0 0 18-18 0 0 0 0 0	20.21 0 0 0 0 0	22.23 0 + + 0
20.21 0 0 0 0 0	18-19 0 0 0 0 0 0 18-17 0 0 0 0 0	18.17 0 0 0 0 0 14.18 0 0 0 0 0	16.17 0 0 0 0 0 0 14.16 0 0 0 0 0	18.17 0 0 0 0 0 0 14.18 0 0 0 0 0	18.17 0 0 0 0
5655	7598	4633	1032	609	7
HIND SPEED (KTS)	HIND SPEED (KTS)	WIND SPEED (KTS) 12	HIND SPEED (KTS) 13	WIND SPEED (KTS) 14	HIND SPEED (FTS)
1EHF (°C) 0-3 4-10 11-21 22-39 ± 14 32.33 + 1 + 0 0	76HP (*C) 0-3 4-10 11-21 22-33 2-34 34 30-31 0 1 0 0 0	TEMP (*C) 0-3 4-10 11-21 22-33 34 32.33 + 4 0 0 0	92.33 + 1 + 0 0	52.33 + 1 + 0 0	34.35 + 0 0 0
30.3i 3 2 0 0 0 20.20 23 33 5 • 0	20.29 0 7 10 + 0 24.27 + 28 42 1 0	30.31 1 5 2 0 0 26.29 10 42 12 + C	30.91 1 4 3 + 0 20.20 7 37 23 1 0	30.31 4 7 2 + D 28.29 19 33 8 1 +	32,33 4 1 + 0 . 30,31 8 7 + 0 .
26.27 9 19 3 0 0 24.26 0 2 4 0 0	24.28 0 4 5 + 0 22.23 0 0 0 0 0	26.27 3 15 5 1 + 24.28 4 2 4 + 0	26,27 2 10 8 2 + 24,25 0 1 1 + +	26.27 4 11 4 2 U	28.27 7 11 2 0
20.21 0 0 0 0 0	20.21 D O O O O O	22.23 0 · · 0 0 20.21 0 0 0 0 0	22.23 0 0 0 0 0 0 20.21 0 0 0 0 0	20.21 0 0 0 0 0	22.23 0 0 0 0
18.17 0 0 0 0 0 16.17 0 0 0 0 0	16.17 0 0 0 0 0 14.16 0 0 0 0 0	18,17 0 0 0 0 0 0 18,17 0 0 0 0 0	10.16 U U U U U U U U U U U U U U U U U U U	18.19 0 0 0 0 0 16.17 0 0 0 0 0	20-21 0 0 0 0 18-18 0 0 0 0
14.15 0 0 0 0 0	12.13 0 0 0 0 0 0 10.11 0 0 0 0 0	14.15 0 0 0 0 0 0 12.13 0 0 0 0 0	14.15 0 0 0 0 0 0 12.13 0 0 0 0 0	14.15 0 0 0 0 0 0 12.19 0 0 0 0 0	16.17 0 0 0 0 0 14.18 0 0 0 0 0
470 1 Q	212	1000	647 22	1248	2
NINO SPEED (KTS) 19	MIND SPEED (KIS) 20 TEMP (*C) 0-3 4-10 11-21 22-33 234	HIND SPEED (KIS) 21 TEMP (40) 0-3 4-10 11-21 22-33 234	WIND SPEED (KTS) 22	WIND SPEED (KTS) 23	HIND SPEED (KTS)
32.33 0 + + 0 0	30.91 0 1 1 0 0	30.31 + 0 + + 0	32.33 1 1 1 0 0	30.31 0 + + 0 0	26.28 0 + 0 0
30.31 0 2 2 0 0 20.28 1 9 5 0 0 20.27 2 22 41 3 0	28.29 + 4 6 2 0 26.27 2 18 42 5 + 24.26 + 4 11 2 0	20.29 1 5 10 1 0 26.27 1 16 38 8 0 24.26 0 5 11 2 0	30.31 1 3 3 U 0 28.29 1 22 18 2 0 28.27 2 15 23 4 0	28.27 3 9 5 1 + 24.25 7 23 12 3 +	26.27 • 1 1 0 24.25 1 10 11 2 22.23 2 11 26 8
26.27 2 22 41 3 0 24.25 0 5 1 2 2 22.23 0 0 0 0 0	24.28 + 4 11 2 0 22.23 0 + 3 0 0 20.21 0 0 0 0 0	24.26 D 5 11 2 0 22.23 O 0 1 0 U 20.21 O 0 + O D	28 :27	24.25 7 23 12 3 · 22.23 5 15 8 3 · 20.21 · 1 1 · ·	22.23 2 11 26 8 20.21 1 6 10 6 4
20,21 0 0 0 0 0	18.19 0 0 0 0 0 0 18.17 0 0 0 0 0 0	18.19 0 0 0 0 0 16.17 0 0 0 0 0	20.21 0 0 0 0 0 18.18 0 0 0 0 0	18.19 0 0 0 0 0 18.17 0 0 0 0 0	18.17 0 0 0 0 14.16 0 0 0 0
16.17 0 0 0 0 0 0 14.18 0 0 0 0 0 0	14,15 0 0 0 0 0	14.18 0 0 0 0 0 0 12.13 0 0 0 0 0	18.17 0 0 0 0 0 14.18 0 0 0 0 0	14-15 0 0 0 0 0 0 0 1 12-13 0 0 0 0 0 0	12.13 0 0 0 0
12.19 0 0 0 0 0	12:13 0 0 0 0 0 0 10:11 0 0 0 0 0 0	10.11 0 0 0 0 0	12.13 0 0 0 0	10.11 0 0 0 0 0	6.0 0 0 0
WIND SPEED (KTS) 28	HIND SPEED (HTS) 29	HIND SPEED (KTS)	HIND SPEED (KTS) 31	WIND SPEED (KTS) 32	WIND SPEED (KTS) 31
TEMP (*C1 0-2 4-10 11-21 22-39 + 34	TEMP (*C) 0-3 4-10 11-21 22-33 2 34	TEHP (*C; 0-3 4-10 11-21 22-33 = 34	TEMP (*C) 0-9 1-10 11-21 22-33 2 34		TEHP (*C) 0-3 4-10 11-21 22-33
26.27 + + + 0 0	20.29 0 + 0 0 +	20.21 0 1 1 0	18.19 + 0 + 0 0	22.23 0 + + 0 0	20.21 + 0 + +
22,23 2 8 12 5 1 20,21 3 13 17 7 2	24.25 1 2 3 1 + 22.23 3 9 13 5 +	18,17 4 14 17 7 1 14,16 + 5 14 8 1	14.15 1 5 17 13 6 12.13 1 8 11 12 4	18.19 + 5 6 3 1 16.17 1 12 16 8 2	16.17 1 6 12 5 14.18 2 11 18 7
10.10 2 7 8 3 1 10.17 + 1 2 2 1	20.21 2 13 16 5 · 19.19 1 7 11 2 ·	12.13 0 • 2 0 0	10.11 0 1 2 3 2 8.8 0 0 0 1 1	14.15 1 10 10 7 1 12.13 1 2 4 3 2	12.13 2 8 10 4 10.11 + 2 3 1
14.15 0 + + + +	18-17 + 1 2 1 0 14-18 0 0 0 0 0 +	8.8 0 0 0 0 0 6.7 0 0 0 0 0	8.7 0 0 0 0 0 4.8 0 0 0 0 0	10.11 0 0 + + + 0.9 0 + 0 0 0	9.8 0 0 + + 9.7 0 0 0 0
10.11 0 0 0 0 0 0.8 0 0 0 0 0 0	12.13 0 0 0 0 0	4.5 0 0 0 0 0 2.2 0 0 0 0 0	2.3 0 0 0 0 0 0 0.1 0 0 0 0 0	8.7 0 0 0 0 0 4.5 0 0 0 0 0	4.8 0 0 0 0 0 2.3 0 0 0 0
4.7 0 0 0 0 0 0 2279	8.8 0 0 0 0 0 764	0.1 0 0 0 0 0	-21 0 0 0 0 0 619	7.3 0 0 0 0 0 752	0.1 0 0 0 0
HINO SPEED (KTS) 37	HIND SPEED (KTS) 38	HIND SPEED (KTS) 39	HIND SPEED (KTS) 40	HING SPEED (KTS) 41	NINO SPEED (KTS) 45
TEMP (9C) 0-5 4-10 11-21 22-33 x 34	TEMP (*C) 0-3 4-10 11-21 22-33 a 34	TEMP 14C1 0-3 4-10 11-21 22-33 3 14			
18:17 0 + 3 3 1	18-17 0 1 2 3 2 14-15 0 2 7 9 5	10.11 + + 7 8 6	8.7 1 4 16 11 1	14.16 0 3 5 3 0	14.18 0 0 2 0 12.13 0 1 7 2
14.18 + 2 5 5 1 12.13 0 2 10 5 2	12-13 1 3 8 9 5 19-11 1 2 7 8 8	8.9 1 3 12 9 6 6.7 2 3 7 9 8	4.5 0 4 14 5 5 2.3 0 3 8 3 0	12.13 + 7 17 B 2 10.11 1 9 13 5 2	10.11 2 4 24 10 6.9 1 8 12 6
10.11 1 3 11 6 3 0.0 + 4 8 5 3	8.8 0 1 4 5 4 6.7 0 + 1 3 +	2.3 0 0 2 3 1	-\$:-1 0 0 0 0 0 0.1 0 0 0 0 0	6.7 0 1 0 + 0	6.7 1 0 7 2 4.8 0 0 1 1
8.7 · 1 4 5 2 4.8 · · · 1 1	4.5 0 0 0 0 · · · 2.3 0 0 0 0 0 0	0.1 0 0 0 0 0 0 -11 0 0 0 0 0 0 -43 0 0 0 0 0 0 -66 0 0 0 0 0 0	-43 0 0 0 0 0 0 -66 0 0 0 0 0 0	4.5 0 0 · 0 0 2.3 0 0 0 0 0	2.3 0 0 0 0 0.1 0 0 0 0
2.3 0 0 0 + 0 0.1 0 0 0 0 0 -21 0 0 0 0 0	0.1 0 0 0 0 0 -21 0 0 0 0 0 0 -43 0 0 0 0 0	-13 0 0 0 0 0 0 -55 0 0 0 0 0 0 -57 0 0 0 0 0	-67 0 0 0 0 0 0 -109 0 0 0 0 0 0 -1211 0 0 0 0 0	0.1 0 0 0 0 0 1.1 0 0 0 0 0 0 4.2 0 0 0 0 0	-2,-1 0 0 0 0 0 -4,-9 0 0 0 0 0 -6,-5 0 0 0 0
-21 0 0 0 0 0 0 593	-43 0 0 0 0 0 506	-07 0 0 0 0 0 0 260	-12:-11 0 0 0 0 0 0 76	43 0 0 0 0 0 0 259	-65 0 0 0 0 1

<u>Graphs</u> represent the objective compilation of available data for specified areas without. The <u>isopleth</u> analyses (cpposite page) are based on all available data subjectively adjust

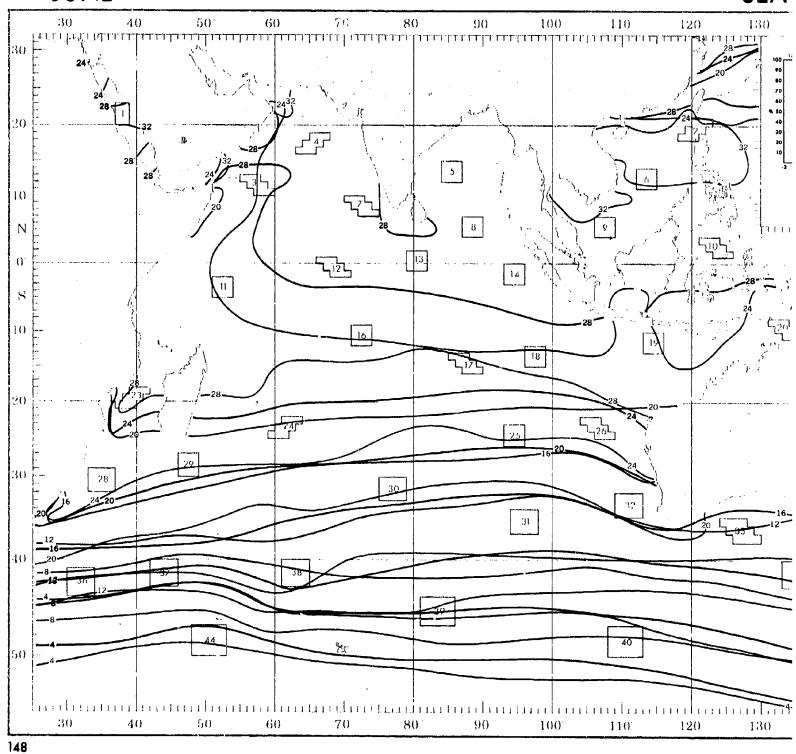
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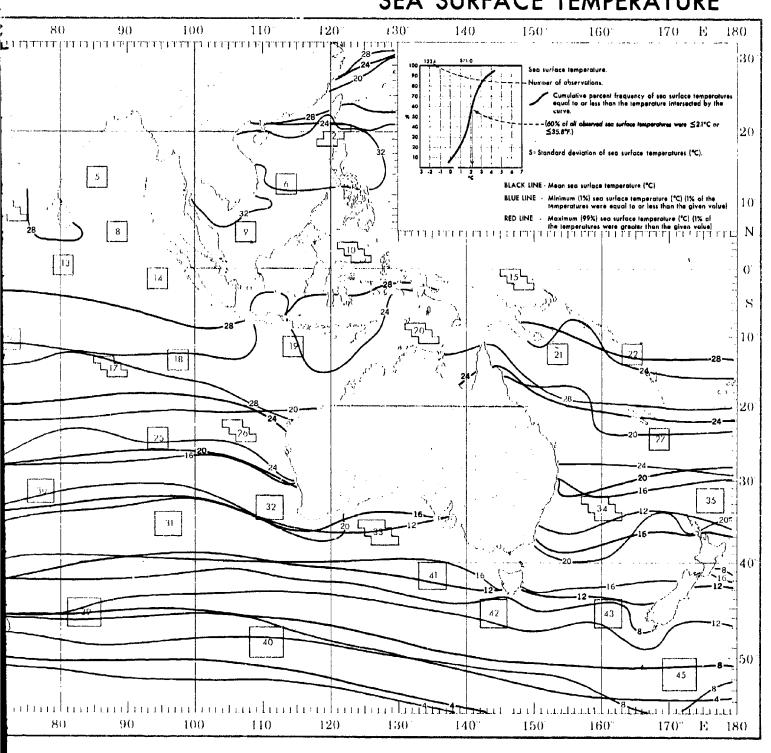
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HIND SPEED (KTS)	WIND SPEED (KTS) 5	HIND SPEED INTS! 6	HIND SPEED (KIS)	WIND SPEED (KIS) 8	WIND SPEED (KTS)
	18MP (*C1 0-3 4-10 11-21 22-33 34	16HF (4C) 0-3 4-10 11-21 22-33 6-24		TEMP (*C) 0-3 4-10 11-21 22-27 2 34	
34.35 0 4 4 0 32.33 4 1 2 1 0	34.35 0 - 0 0 0 32.33 0 1 2 + 0	30,37 0 · · 0 0 34,35 · · 1 · 0	34.35 () + + 0 0 37:33 + 1 1 + 0	34.35 () + + + 0	36.37 + 0 + 0 0
30.31 1 4 14 7 1 28.29 2 8 28 24 2	30.31 • 4 16 6 • 28.29 • 8 40 17 0	32.33 + 2 3 · · · 30.31 1 9 14 2 ·	30.31 + 5 7 1 + 28.29 1 19 34 4 +	30.31 + 2 7 1 0 26.29 1 16 49 8 •	32.33 1 2 1 + 0 30.31 3 11 4 + 0
26.27 0 1 2 2	28.27 0 1 3 1 0	20.20 3 20 27 6 +	26.27 + 6 13 3 •	26,27 + 3 9 2 +	20.20 10 36 12 1 5
24.25 0 + 0 + +	24.25 0 0 + C 0 22.23 0 0 0 0 0	26.27 1 4 5 1 +	24.25 + 1 2 1 + 22.23 0 + + + 0	24.28	26.27 1 9 5 + +
20.21 0 0 0 0 0	20,21 0 0 0 0 0	20.21 0 0 0 0 0	20.51 0 0 0 0 0	20.21 0 0 0 0 0 18.19 0 0 0 0 0	22.23 0 + 0 + 0
16.17 0 0 0 0	18:17 0 0 0 0 0	19.19 0 0 0 0	16.17 0 0 0 0 0	16.17 0 0 0 0 0	18.19 0 0 0 0
14.15 0 0 0 0 0	14.18 0 0 0 0 0	18.17 0 0 0 0 0 0 7398	14:15 D O D 6 C 6470	14.15 0 0 0 0 0 0 4255	18.17 0 0 0 0 0 0 5516
WIND SPEED (KTS) 13	HIND SPEED (KIS) 14	HIND SPEED (KIS) 15	WIND SPEED (KTS) 16	WIND SPEED (KTS) 17	WIND SPEED (HTS) 18
he (*C) 0-3 4-10 11-21 22-33 + 34	1EMP (1C) 0-3 4-10 11-21 22-33 # 34	TEMP (*C1 0-3 4-10 11-21 22-33 234	TEMP (*C) 0-3 4-10 11-21 22-33 2 34	TEHP (*C) 0-3 4-10 11-21 82-33 + 34	TEMP (*C) 0-3 4-10 11-21 22-33 4-4
32.93 . 1 . 0 0	32,33 + 1 + 0 0	34.35 + 0 0 0 0	30.31 0 0 1 0 0	30.31 0 + + 0 0	30.31 0 1 1 0 0
30.31 1 4 3 + 0 20.20 7 37 23 1 0	30.31 4 7 2 + 0 28.29 19 33 8 1 +	32,93 4 1 + 0 0 30,31 B 7 + 0 0	28.29 + 4 6 1 0 26.27 1 16 41 9 0	26.29 0 2 3 1 0 26.27 1 7 22 9 +	28.28 1 1 6 1 D
26.27 2 10 8 2 + 24.25 0 1 1 + +	26.27 4 11 4 2 0 24.25 + 1 1 + +	26.29 21 32 4 + 0 26.27 7 11 2 C 0	24.25 + 6 12 3 +	24.26 + 5 27 15 2 22.23 0 + 2 2 +	24.25 0 5 17 7 1 22.23 0 + 1 0 0
22.23 0 0 0 0 0	22.23 0 + + + 0 20.21 0 0 0 0 0	24.26 1 1 0 0 0 22.23 U 0 0 0 0	20.21 0 0 0 0	20.21 0 0 0 0 0	#G-21 0 0 0 0 0
18.19 0 0 0 0	18-19 0 0 0 0	20.21 0 0 0 0	16-17 0 0 0 0 0	16-17 0 0 D 0 0	18,17 0 0 0 0 0
16.17 0 0 0 0 0 14.15 0 0 0 0 0	16.17 0 0 0 0 0 14.18 0 0 0 0 0	18.19 0 0 0 0 0 0 16.17 0 0 0 0 0	14.15 0 0 0 0 0 12.13 0 0 0 0 0	14.18 0 0 0 0 0 0 12.13 0 0 0 0 0	14.18 0 0 0 0 0 0 12.13 0 0 0 0 0
14.15 0 0 0 0 0 0 12.13 0 0 0 0 0	14-15 0 0 0 0 0 0 12-13 0 0 0 0 0 0	16.17 U 0 0 0 0 0 14.18 0 0 0 0 0 0	10-11 0 0 0 0 0	12.13 0 0 0 0 0 0 10.11 0 0 0 0 0 0	12.13 0 0 0 0 0 0 0 1 10.11 0 0 0 0 0 0 0
22	72	24	25	26	27
HIND SPEED (KTF) 22	WIND SPEED (KIS) 23	WIND SPEED (KTS) 24	WIND SPEED (KTS) 25	MIND SPEED (KTS) 26	WIND SPEED (KIS) 27
P 1°C1	30.31 0 + + 0 0	7EHP '*C1 0-3 4-10 11-21 22-33 2 34	24.25 0 1 + 0 0	TEMP (*C) 0-3 4-10 11-21 22-33 2 34	26.27 + 1 1 0 +
30.31 1 3 3 0 0	28.29 + 1 1 0 C	26.27 + 1 1 0 0	22.23 1 6 5 0 0	22.23 2 9 11 2 0	24.25 + 3 4 0 +
28.29 1 22 18 2 0 26.27 2 16 23 4 0	24.25 7 23 12 3 +	22.23 2 11 25 8 1	16.19 2 15 16 3 0	10-19 + 5 11 4 1	20.21 3 17 16 3 +
24.25 3 1 1 1 0 22.23 0 0 0 0 0	22.23 5 15 8 3 •	20-21 1 6 10 6 +	16.17 + 3 5 0 0 14.15 0 0 0 0 0 0	16.17 0 0 1 + +	10.10 0 7 3 2 U
20.21 0 0 0 0	18.19 (1 0 0 0 0 0 18.17 (1 0 0 0 0 0	18-17 0 0 0 0 0 14-18 0 0 0 0 0	12-13 0 0 0 0	12.13 0 0 0 0 0	14.18 0 0 0 0 0 12.13 0 0 0 0 0
16.17 0 0 0 0	14-16 G G G G G	12.13 0 0 0 0 0	10.11 0 0 0 0 0 0.0 0 0 0 0	6.9 O O O O	10.11 01 01 01 01
14-15 0 0 0 0 0 12-13 0 0 0 0 0	12.13 0 0 0 0 0 0 10.11 0 0 0 0 0	10.11 0 0 0 0 0 •.9 0 0 0 0 0	6.9 0 0 0 0 0 6.7 0 0 0 0 0 4.6 0 0 . 0 0	0.7 0 0 0 0 0 4.8 0 0 0 0 0	9.8 0 0 0 0 0 6.7 0 0 0 0 0
194	904	588	213	699	459
HIND SPEED (KTS) 31	HIND SPEED (KIS) 32	HIND SPEED (HTS) 33	HIND SPEED (KTS) 34	HIND SPEED (HTS) 35	WIND SPEED CATS 36
1°C1 0-3 4-10 11-21 28-33 4 54		TEMP (°C) 0-3 4-10 11-21 22-33 + 34			
18.19 + 0 + 0 0 18.17 + 2 4 4 2	22.23 0 + + 0 0	10.19 + + 1 1 0	22.23 0 0 + 0 0	20.21 + 1 + + 0	18.17 + 0 2 1 0
14-15 1 5 17 13 6 12-13 1 8 11 12 4	18.19 + 5 6 3 1 16.17 1 12 16 8 2	18.17 1 6 12 5 1 14.15 2 11 18 7 1	20.21 + 1 2 1 +	18.17 2 14 19 11 4	14.15 + 2 6 4 2
10.11 0 1 2 3 2	14.15 1 10 10 7 1	12.19 2 8 10 4 2	18-17 10 17 8 3	14-15 + 6 9 3 1	10.11 1 4 10 10 4
8.9 0 0 0 1 1 1 8.7 0 0 0 0 0 0 4.6 0 0 0 0 0	12.13 1 2 4 3 2 10.11 0 0 + + + 1.0 0 + 0 0 0	0.0 0 + + -	12:13 0 + 1 + 1	10.11 0 0 0 0	0.7 1 1 3 2 1
4.6 0 0 0 0 0 2.3 0 0 0 0 0	0.9 0 · 0 0 0 0.7 0 0 0 0 0	#.7 0 0 0 0 0 4.8 0 0 0 0 0	0.9 0 0 0 0 0	0.0 0 0 0 0 0 0.7 0 0 0 0 0 0	4.8 + 1 1 1 1 2.3 0 0 + 0 0
2.3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6.7 0 0 0 0 0 4.5 0 0 0 0 0 2.3 0 0 0 0 0	8.3 0 0 0 0 0 0.1 0 0 0 0 0	6.0 0 0 0 0 0 6.7 0 0 0 0 0 0 4.8 0 0 0 0 0 0	4.5 0 0 0 0 0 2.3 0 0 0 0 0	0.1 0 0 0 0 0 -21 0 0 0 0 0
619	762	1788	647	447	560
WIND SPEED (KTS) 40	HIND SPEED (KTS) 41	WIND SPEED (KTS) 42	WIND SPEED (KTS) 43	4 4	WIND SPEED (KTS) 45
11-01 0-3 4-10 11-21 22-33 2 34		TERP (*C) 0-1 4-10 11-21 28-33 4 4	TEMP (*CT 0-3 4-10 11-21 22-33 4 34		TERP (*C) 0-3 4-10 11-21 22-53 a 54
8.9 0 1 12 11 1 8.7 1 4 16 11 1	16.17 0 0 0 1 0 14.18 0 3 5 3 0	14.15 0 0 2 0 0 12.13 0 1 7 2 1	14-16 0 0 1 1 0 12-13 1 4 6 5 0		10.11 0 0 4 0 0 0.0 0 13 28 4 4
4.5 0 4 14 5 5	12.13 + 7 17 6 2	10.11 2 4 24 10 5	10.11 2 9 16 7 1	INICHEELCIENIT	6.7 0 13 9 13 0
7.3 0 3 8 3 0 0.1 0 0 0 0 0	10.11 1 9 13 5 2 6.9 + 6 B 5 +	0.9 1 8 12 6 4 0.7 1 0 7 2 0	8.9 1 7 10 14 3 8.7 1 1 0 6 5	INSUFFICIENT	2.3 0 0 0 0 4
-21 0 0 L 0 0	6.7 0 1 0 + 0 4.6 0 0 + 0 0	4.8 0 0 1 1 0 2.3 0 0 0 0 0	4.5 0 0 0 0 1 2.3 0 0 0 0 0 0	DATA	0.1 0 0 0 0 4 -2,-1 0 0 0 0 0
66 0 0 0 0 0	2.3 D D D O O	0.1 0 0 0 0 0 -21 0 0 0 0 0	## 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		-43 0 0 0 0 0 -68 0 0 0 0 0
0.4 0 0 0 0	-21 D O D O O	-49 0 0 0 0	-43 0 0 0 0 0		-07 0 0 0 0 0
0 0 0 0	-43 D O O O O	-85 0 0 0 0 0	-05 0 0 0 0 0		-10,-9 0 0 0 0 0

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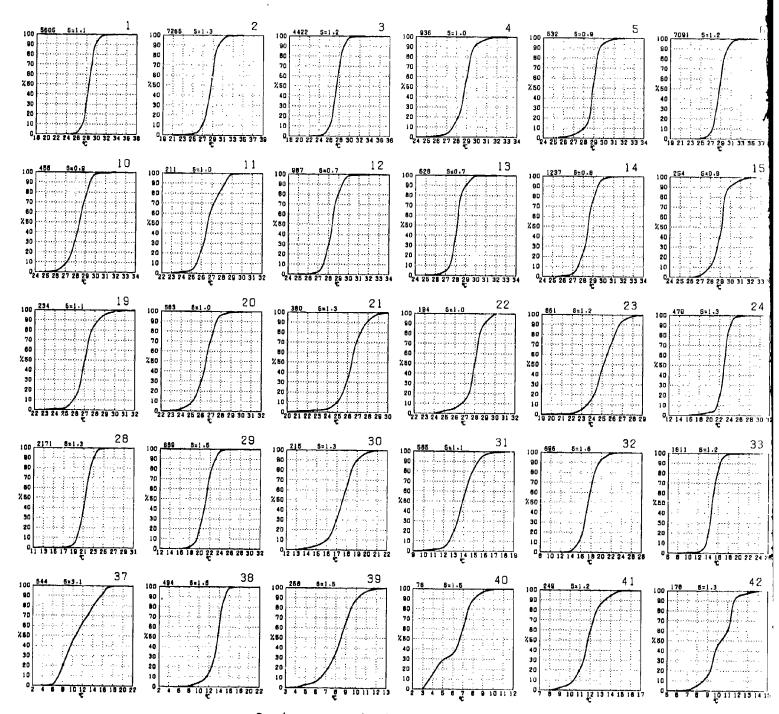
SEA



SEA SURFACE TEMPERATURE

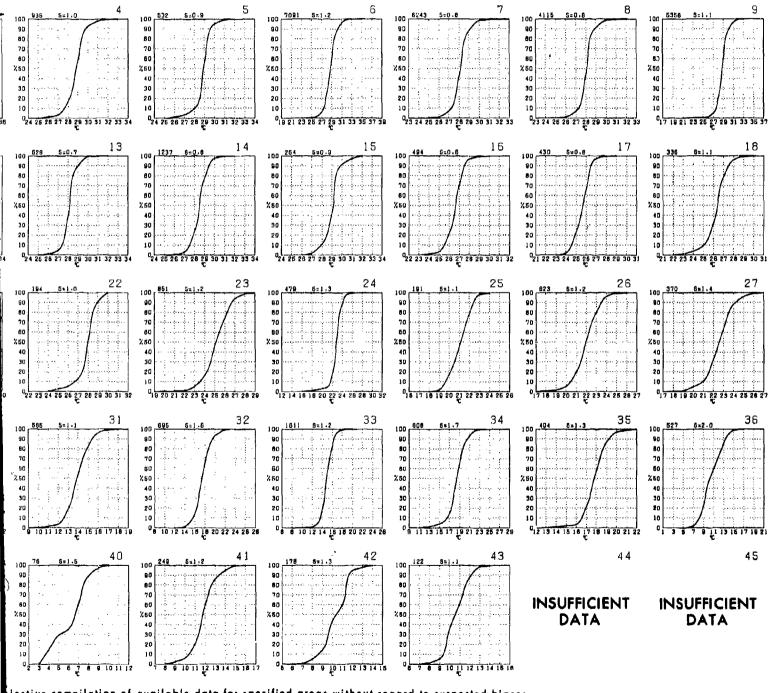


SEA SURFACE TEMPERATURE



<u>Graphs</u> represent the objective compilation of available data for specified areas without re The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjuste

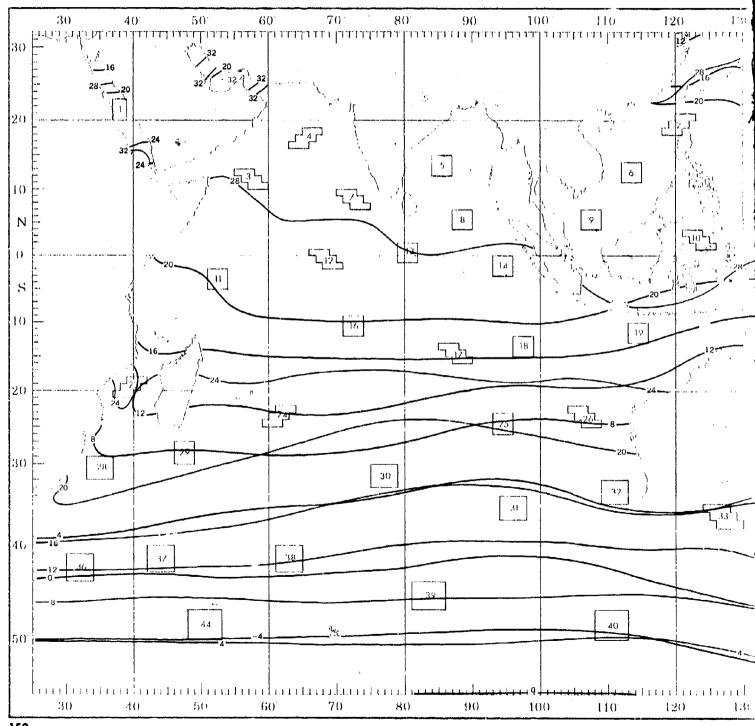




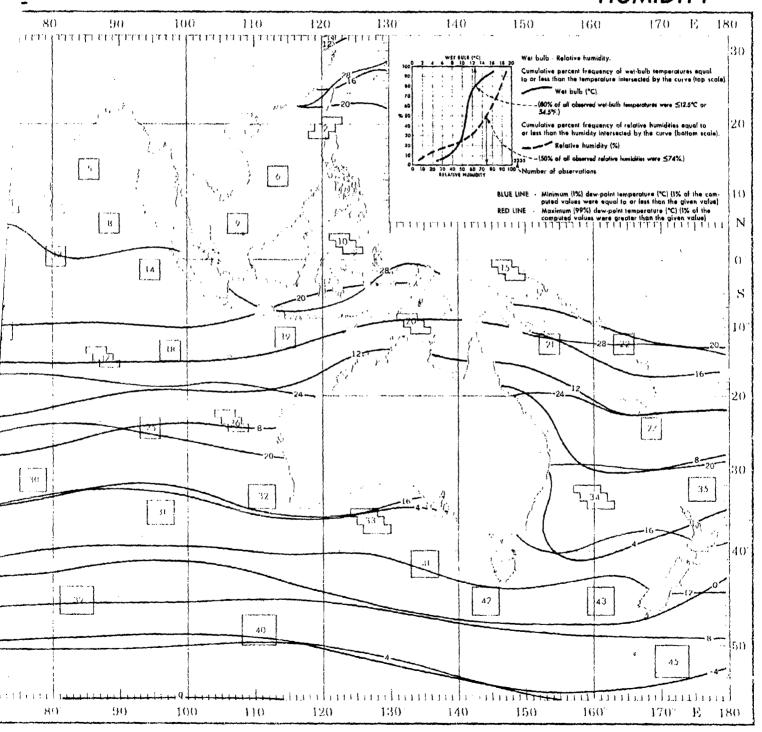
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pposite page) are based on all available data subjectively adjusted where bias was evident.

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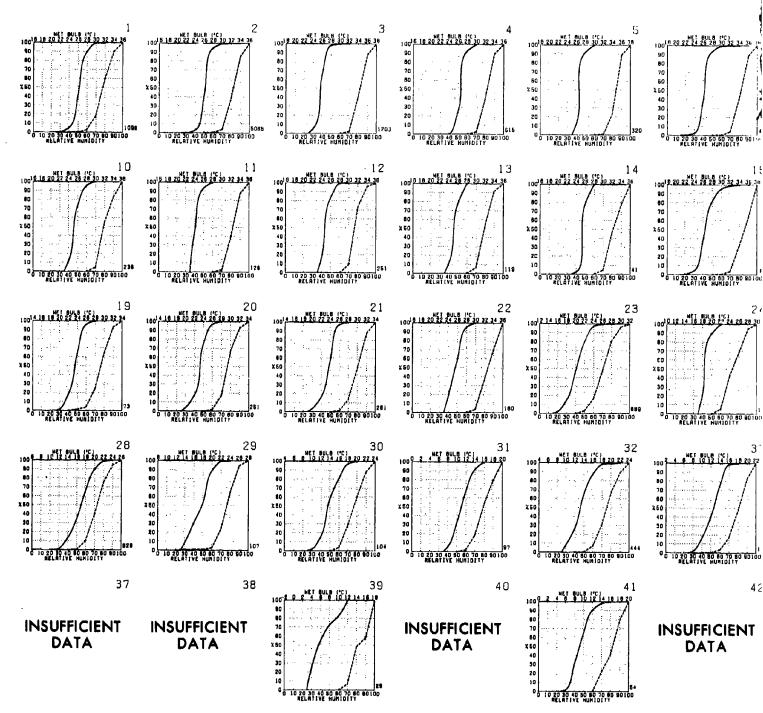
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HUMIDITY



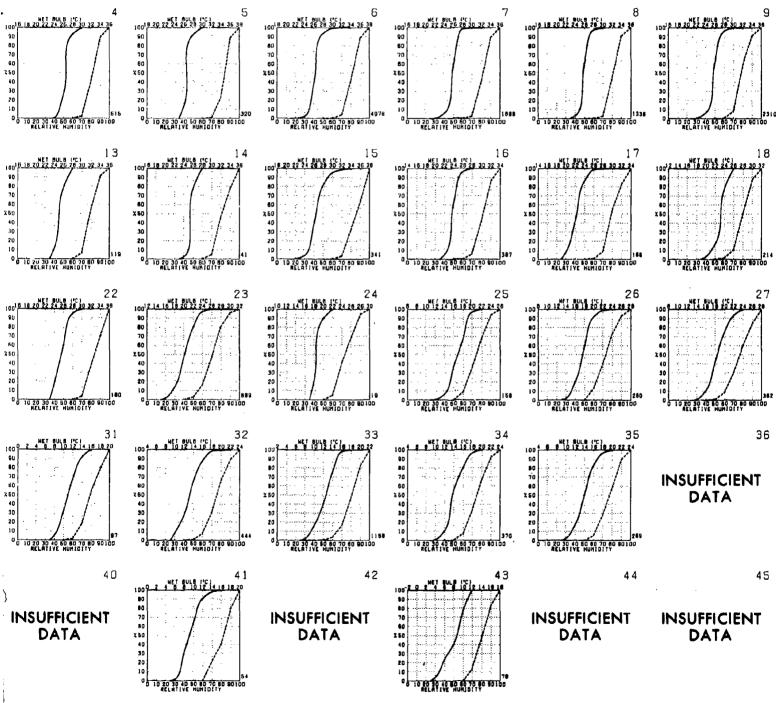
WET BULB AND RELATIVE HUMIDITY



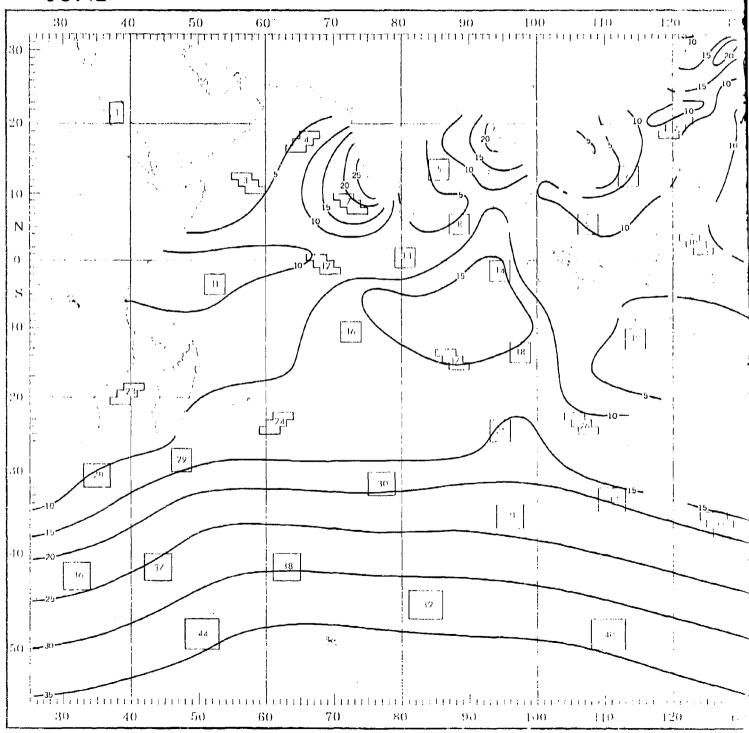
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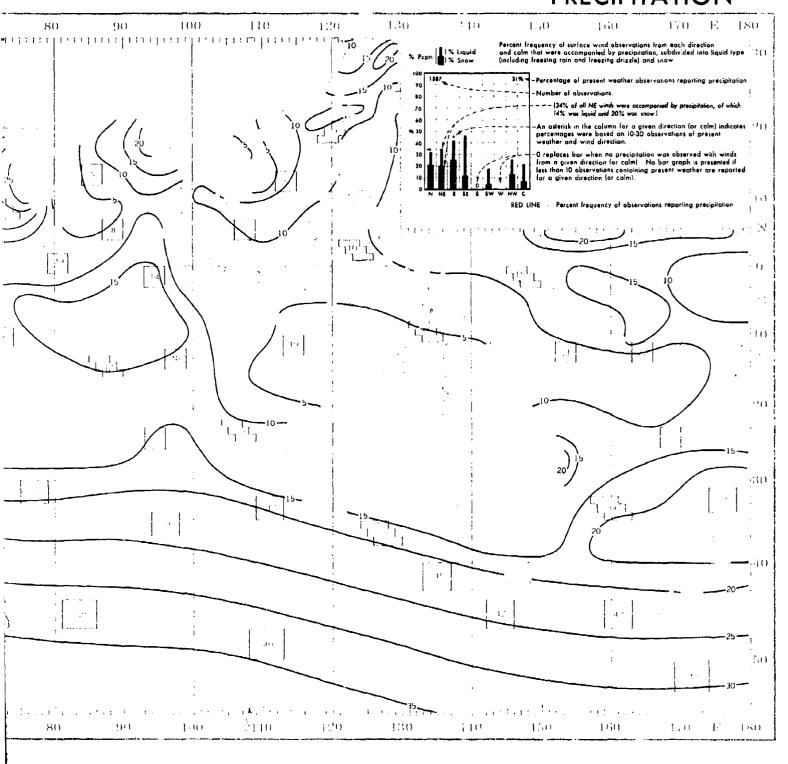
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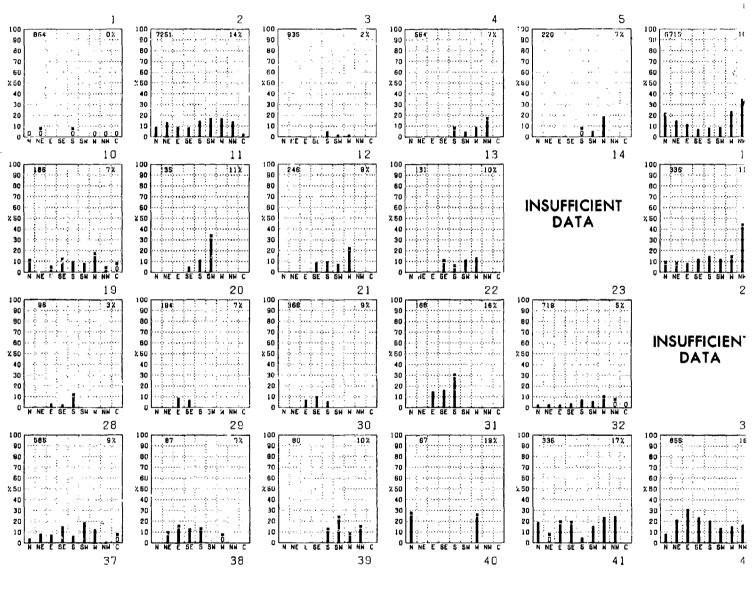
ective compilation of available data for specified areas without regard to suspected biases, posite page) are based on all available data subjectively adjusted where bias was evident.



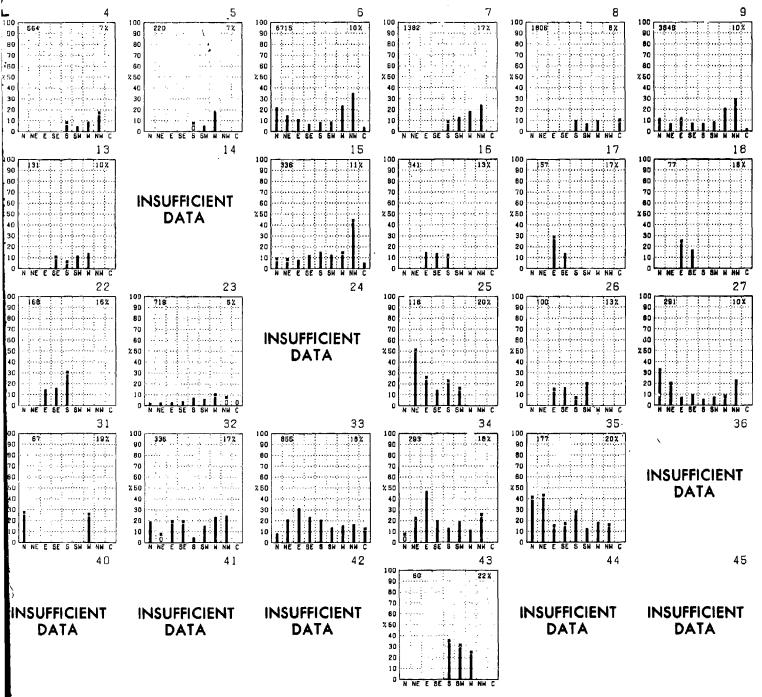
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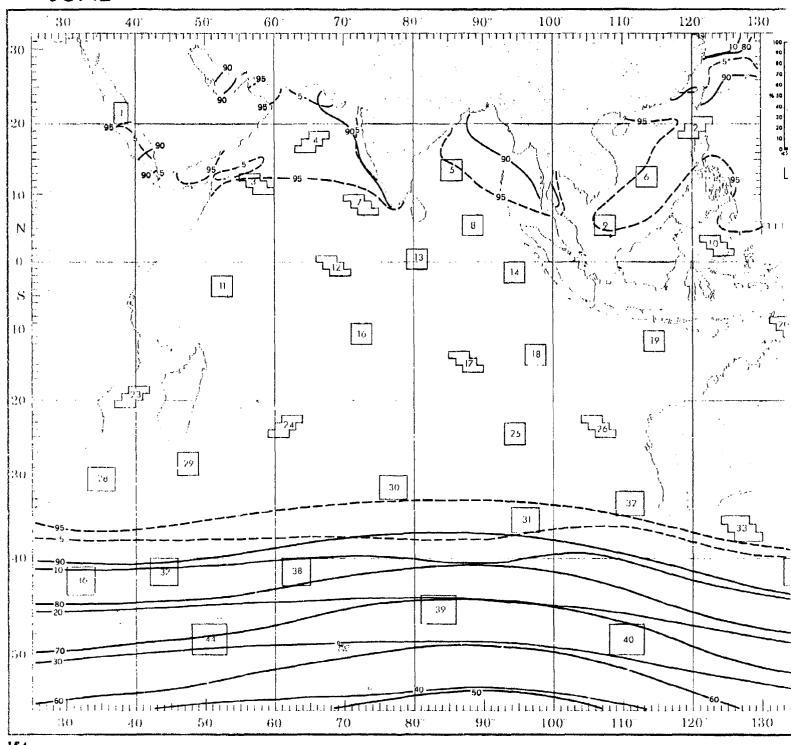
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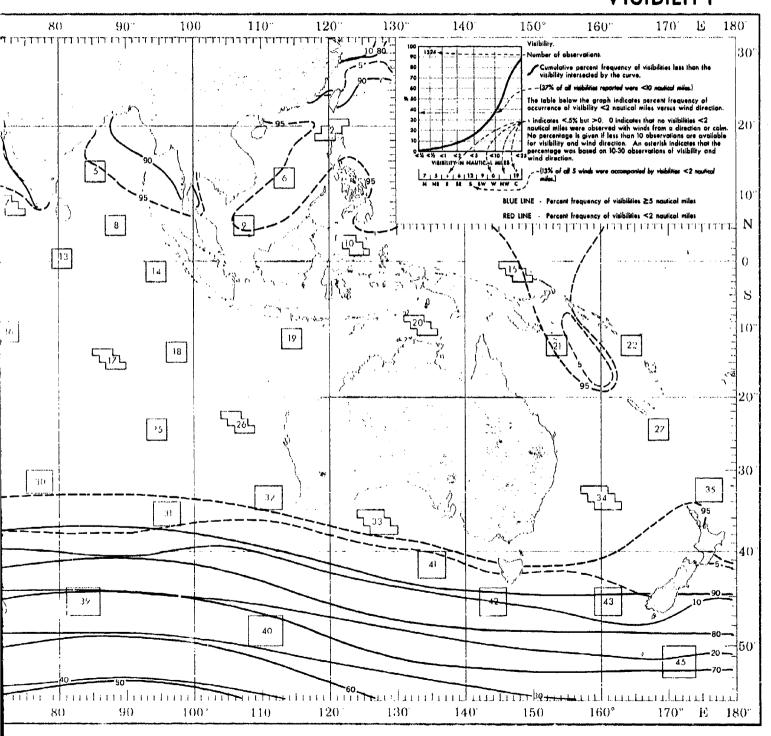
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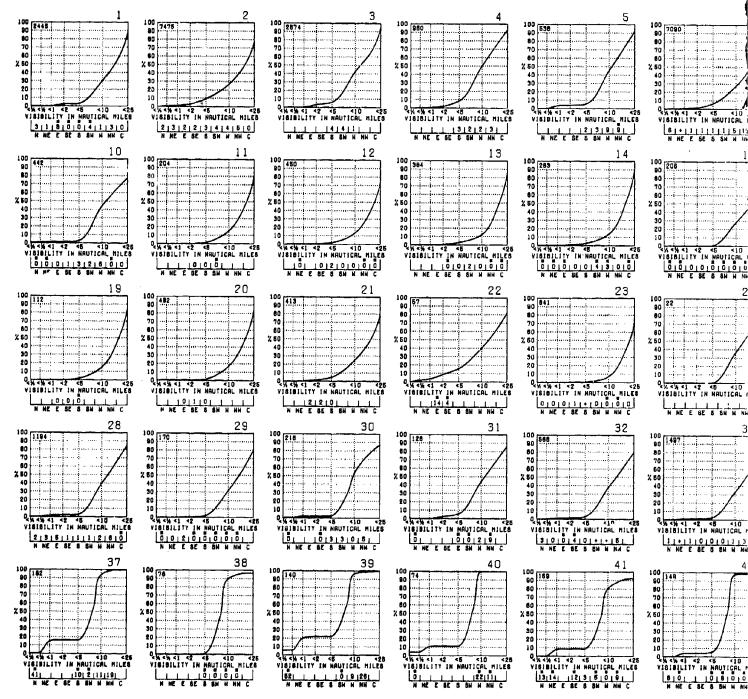
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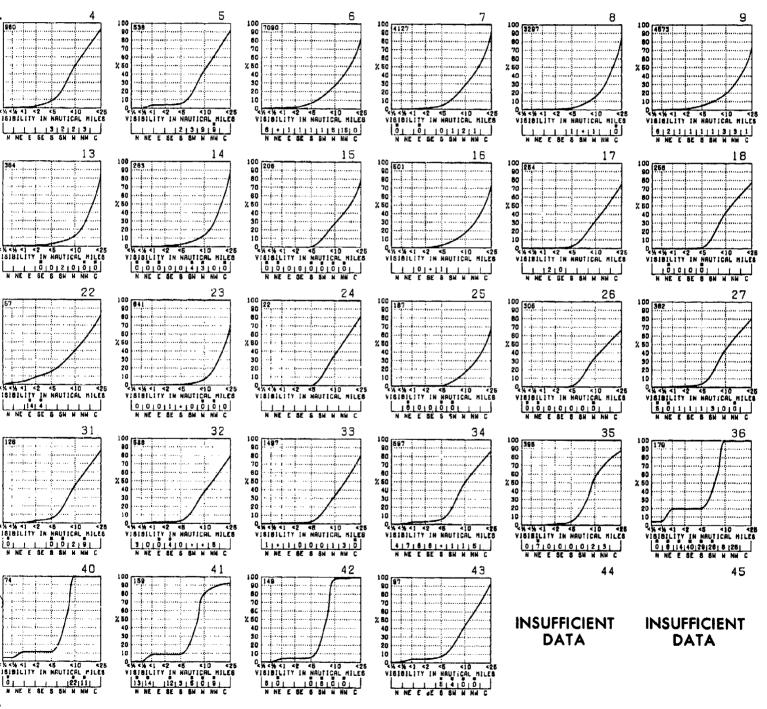
VISIBILITY



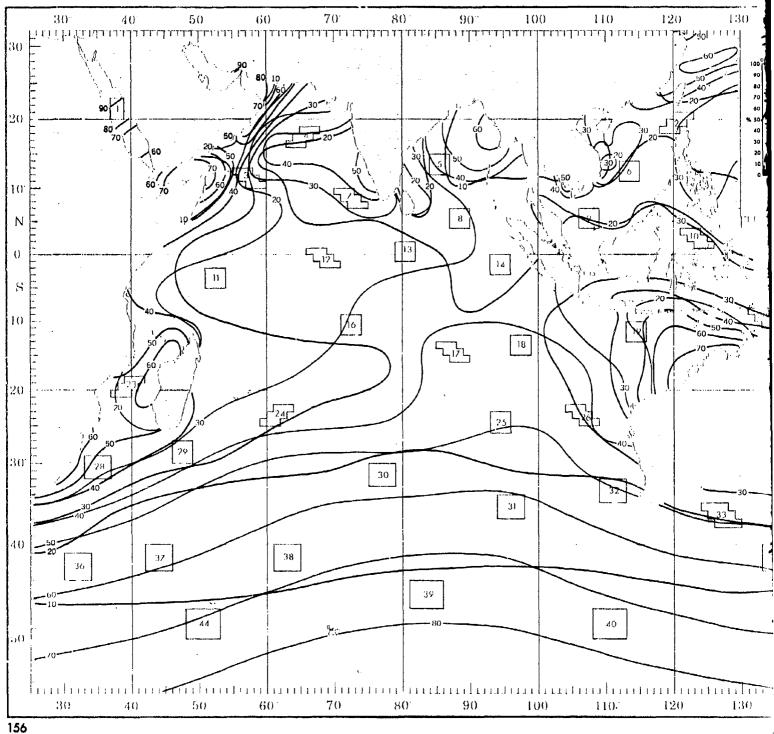
VISIBILITY



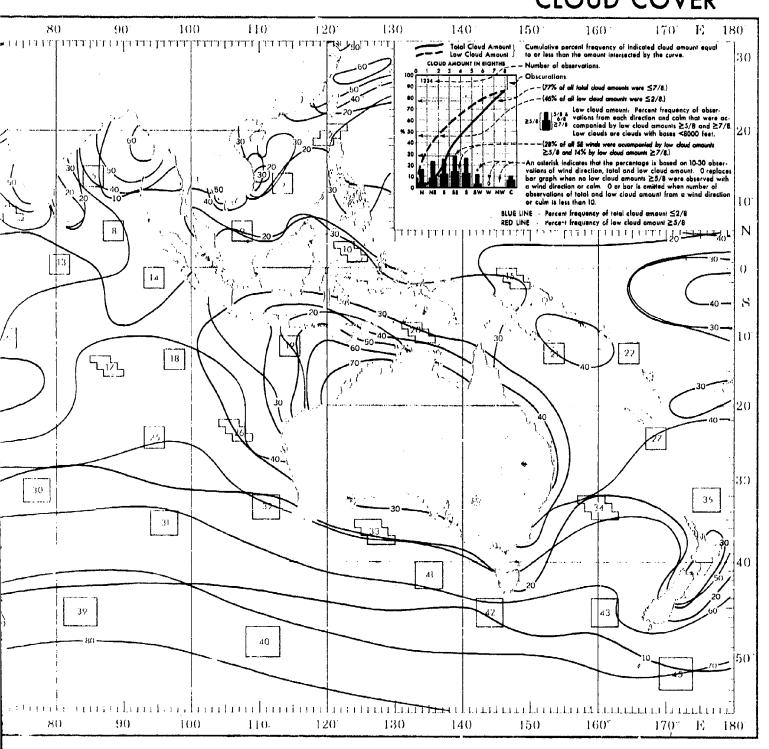
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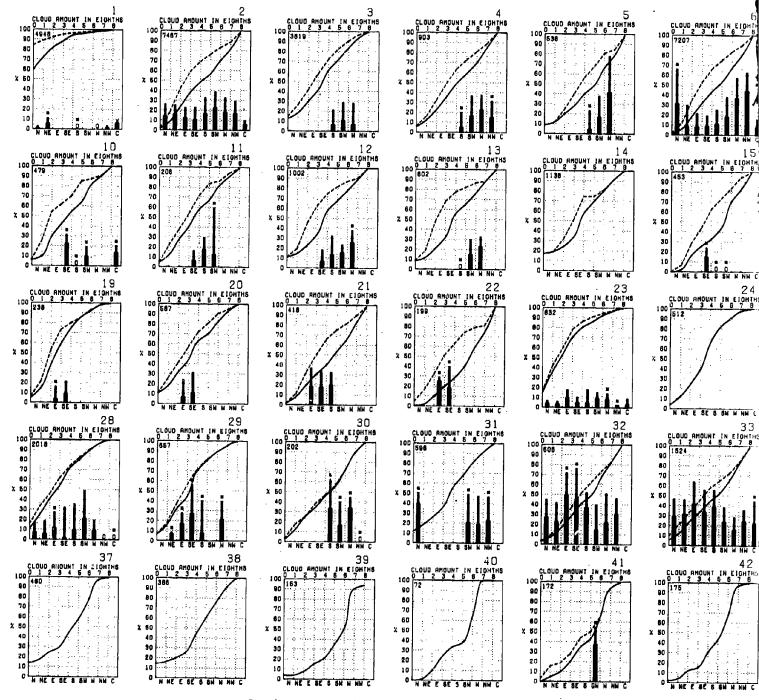
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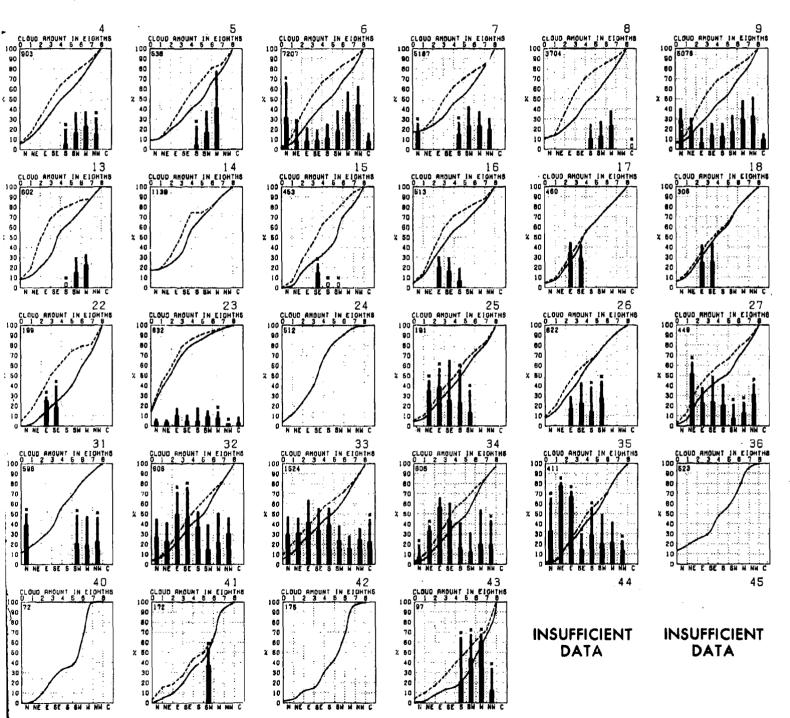
CLOUD COVER



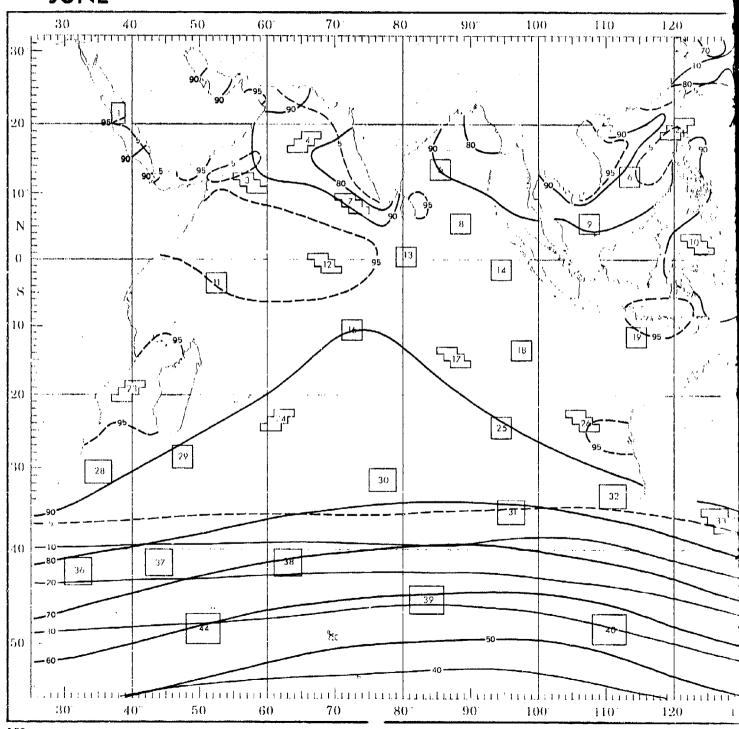
CLOUD COVER



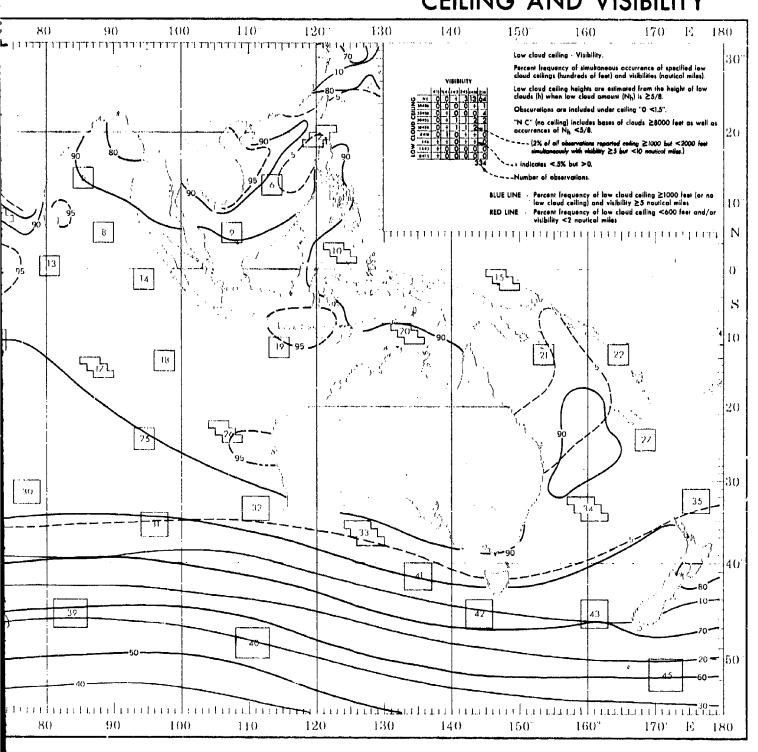
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CEILING AND VISIBILITY



CEILING AND VISIBILITY

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VISIBILITY **** **** **** ***** ***** ***** ***** ***** ***** ***** ***** ***** ***** ***** ***** ***** ******	VIBIBILITY 14 14 14 15 14 14 15 15	VISIBILITY 1/8 1/8 1 1 1 1 1 1 1 1 1	VISIBILITY - 1/2 1/2 1/2 2/4 3/2 1/2 1/2 1/2 1/2 1/2 3/2 3/2 1/2 1/2 1/2 3/2 3/2 1/2 1/2 1/2 3/2 1/2	VIBIBILITY	VISIBILITY 4-1/9 7-4* 1-42 2-6 1-4 NC
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19	VISIBILITY	VISIBILITY 21	VISIBILITY VISIBILITY ACC 0 0 0 0 3 6 56 80 0 0 0 0 0 0 0 0 80 0 0 0 0 0 0 0 0	VISIBILITY 2 3 - 1/4 1/4 1/4 1/4 1/4 1/4 1/4 NC 0 0 0 0 0 1 0 7 SOURCE 0 0 0 0 0 1 67 SOURCE 0 0 0 0 0 0 4 4 SOURCE 0 0 0 0 0 0 4 4 SOURCE 0 0 0 0 0 0 4 3 SOURCE 0 0 0 0 0 0 4 3 SOURCE 0 0 0 0 0 0 0 4 3 SOURCE 0 0 0 0 0 0 0 4 3 SOURCE 0 0 0 0 0 0 0 0 4 SOURCE 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY
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3-6 0 0 0 0 0 0
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VISIBILITY 4	VISIBILITY 5	VIBIBILITY	VISIBILITY 4'/2 1/42 1 42 245 3410 310 8C 0 + + 8C 0 + + 90-80 0 0 0 0 + 10-80 0 0 + + 10-80 0 0 + + 10-80 0 0 + 10-80 0 0 + 10-80 0 0 0 + 10-80 0 0 0 0 10-80 0 0 0 0 0 10-80 0 0 0 0 0 10-80 0 0 0 0 10-80 0 0 0 0 10-80 0 0 0 0 10-80 0 0 0 0 10-80 0 0 0 0 10-80 0 0 0 0 10-80 0 0 0 0 10-80 0 0 0 0 10-80 0 0 0 0 10-80 0 0 0 0 10-80 0 0 0 0 10-80 0 0 0 0 10-80 0 0 0 10-80 0 0 0 10-80 0 0 0 10-80 0 0 0 10-80 0 0 0 10-80 0 0 0 10-80 0 0 0 10-80 0 0 0 10-80 0 0 10-80 0 0 10-80 0 0 10-80 0 0 10-80 0 0 10-80 0 0 10-80 0 0 10-80 0 0 10-80 0 0 10-80 0 0 10-80 0 0 10-80 0 0 10-80 0 0 10-80 0 0 10-80 0 0 10-80 0 10-80 0 0 10-80 0	VISIBILITY c1/g freq c2 g = 6 g = 10 x 1	VISIBILITY
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VISIBILITY 22 ***/*	VISIBILITY	VISIBILITY 24 *1/2 [**1] 1**	VISIBILITY 25 ***\frac{1}{2} \frac{1}{2} \frac^2 \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \frac{1}{2} \f	VISIBILITY 26 ***/********************************	VISIBILITY 27 ***********************************
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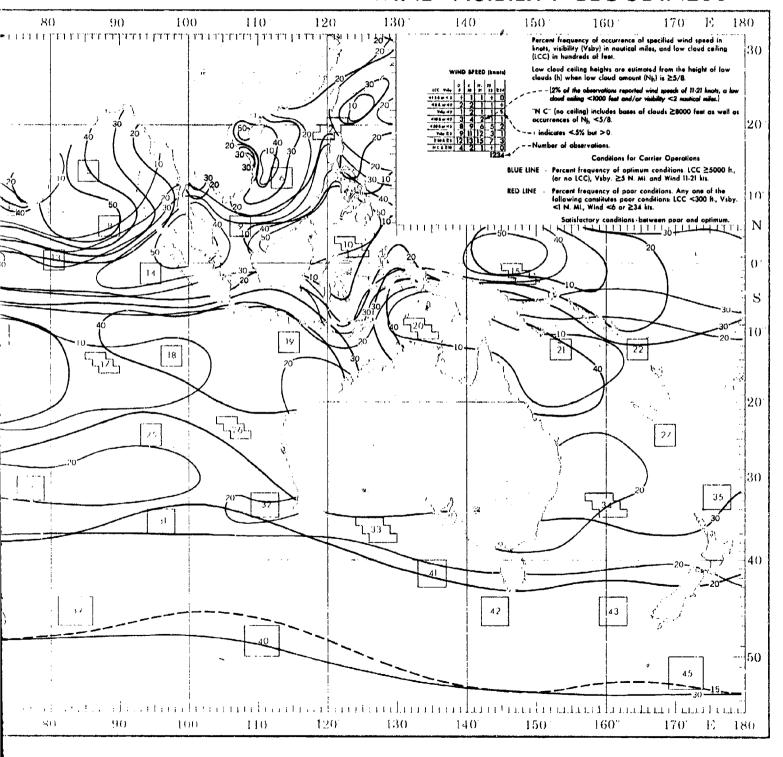
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WIND-VISIBILITY-CLOUDINESS



LOW CLOUD CEILING-VISIBILITY-WIND

1	2	3	4	5	6
HIND SPEED (KNOTS) LCC - VBBY 9 10 21 33 324	HIND SPEED (KNOTS) LCC - 968Y	HIND SPEED (KNOTE) LCC - VBBY 3 0 4 11 22 3 54 41.5 4 08 4 5 0 0 0 0 0 40 4 98 42 0 0 0 0 40 4 08 42 0 0 0 0 40 4 08 42 0 0 1 3 1 410 4 08 45 0 0 4 12 3	HIND SPEED (KNOTE) LCC - vasr 3 10 21 33 354 -1.84 08 -4.8 0 0 + + + -84 08 -2 0 0 1 2 - vasr -2 0 0 + + 0 -10 4 08 -2 0 + 9 8 1 -20 4 08 -6 + 2 10 13 1	HIND SPEED (KNOTS) LCC - V88V	MIND SPEEU (KNOTS) LCC - YABY 3 0- 4- 11-122- 10- 10- 20- 33 3-34 -1.5408-4-5 0 + 4 44840-72 + 1 2 1 +
V887 NS 10 45 41 2 0 a 80 4 a b 10 44 41 2 0 MC 4 * 10 8 38 35 2 0 627	YARY AS 9 44 34 4 • 250 4 as 8 35 23 2 • 1 1 1 1 1 1	V887 35 1 2 23 56 12 a80 4 a5 1 2 17 43 8 MC 4 a 10 1 2 14 31 5 884 1 2	V857 as 3 14 43 28 3 = 50 4 = 6 3 12 32 15 1 = 60 4 = 6 3 12 32 15 1 = 77 1 3 11 21 7 1 1 3	VBBT 36 0 111 63 24 0 380 4 15 0 6 8 40 9 0 40 4 10 0 6 32 7 0 228	v887 a.5
HIND SPEED INNOTS; LCC - VSAY S 0 4- 11-127-127-131-131-131-131-131-131-131-131-131-13	HIND BPEED (XNDTS) CCC - VBBY	#IND SPEED INNO[S] LCC - 468Y	MIND SPEED (KNOTE) LCC - VESAY	MIND SPEED (KNOTS) LCC - Y887	HIND SPEED (KNDIS) LCC - V88Y
MIND SPEED (KNDTS) LCC - V68Y 5	MIND : Er : :un:SI LCC - V887	2 1 MIND SPEED (KNOTS)	## NO SPEED (HNOTE) LCC - YEBY 9 10 11 12 25 394 41 84 98 48 0 0 0 0 0 0 0 0 44 4 98 42 0 6 3 0 0 YEBY 42 0 6 3 0 0 YEBY 42 0 6 3 0 0 YEBY 42 0 6 3 0 0 YEBY 42 0 6 3 0 0 YEBY 43 0 0 15 21 0 0 YEBY 48 0 15 59 8 0 BO 4 98 0 15 54 8 0 HC 4 4 10 0 16 35 6 0	### A SPEED (KNOTE) **CC - VSSY*** **C1.5 A OR <.6*** **O	### A PRESSOR OF THE
28 NJND SPEED (KNOTE) LCC - VBBY	29 HIND SPEED INDUSTS J LCC - VEB: 9- 1- 13- 15- 15- 15- 15- 15- 15- 15- 15- 15- 15	30 MIND SPEED (HNOTS) LCC - V88Y 9 10 21 25 38 384 11.5 4 88 4.6 0 0 0 0 0 0 0 48 4 8 4 2 0 1 0 0 0 0 V88Y 42 0 0 0 0 0 0 410 4 18 4 18 10 10 16 8 0 V88Y 35 8 30 37 22 4 850 4 18 3 16 15 13 3 MC 4 9 10 3 16 13 10 3 79	31 HIND SPEED (KNDTS) LCC - VBBY	32 MIND SPEED (KNDTS) LCC - VSSY	33 HIND SPEED (KNOTS) LCC - VBBY
3,	30	33	70	HIND SPEED (MNOTS) LEC - VERY 9 10 21 33 224	,,

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HIND BPEEG (KNOTS)						
FCC - A68A	0.	4. 10	111	22- 33	234	
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48 4 OR 42	0	0	0	0	0	
VEDY 45	0	0	0	0	0	
<10 4 0R <r< td=""><td>0</td><td>6</td><td>13</td><td>0</td><td>3</td></r<>	0	6	13	0	3	
420 4 08 45	0	13	22	6	3	
V607 26	0	34	41	22	3	
100 4 16	0	18	13	16	n	
MC 4 4 10	70	16	13	18	0	

INSUFFICIENT DATA

Graphs represent the objective compilation of available data for specified areas without regains is a specified areas without regains in the isopleth analyses (opposite page) are based on all available data subjectively adjusted visits.

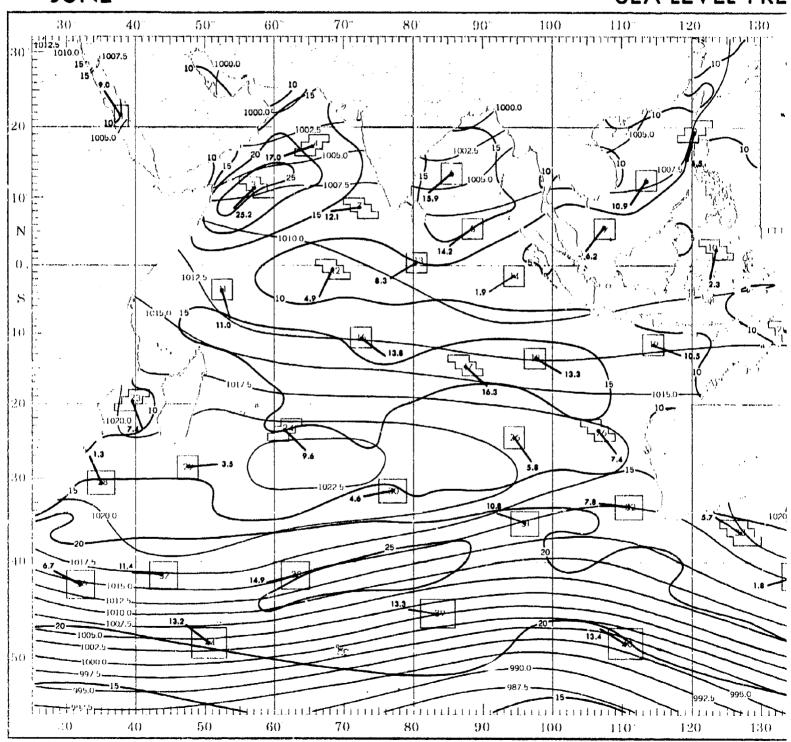
TY-WIND

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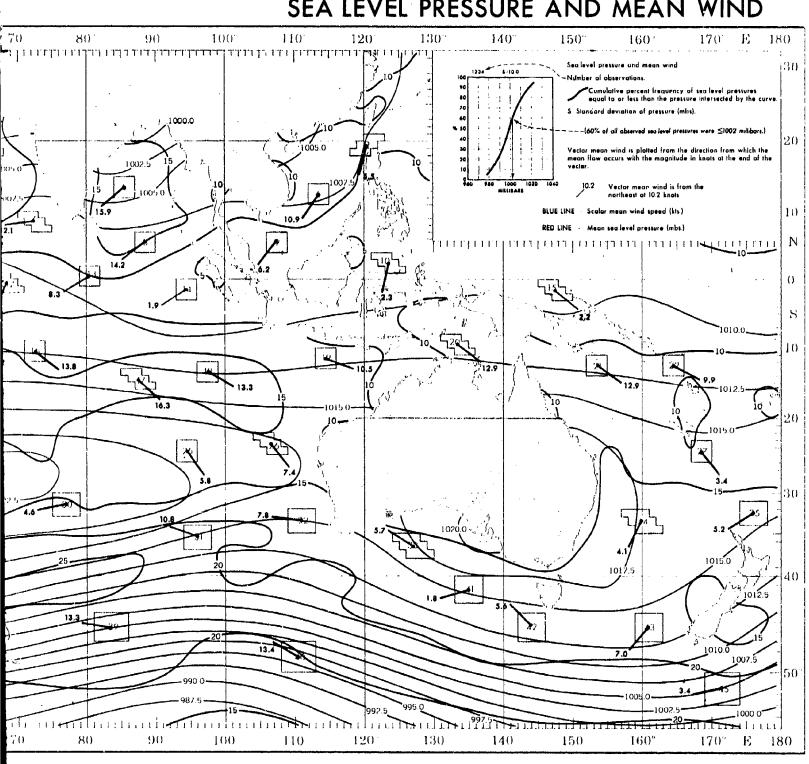
L 4	5	6	7	8	9
HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)
LCC - VSBY 3 10 21 33 234	LCC - VBSY 3 10 21 33 834	LCC - Y88Y 0- 6- 11- 22- 3 234	LCC - Y66Y 3 10 21 33 834	LCC - VESY 3 10 21 33 834	LCC - VARY 3 10 21 39 234
1.54 DR 4.6 0 0 + + +	41.54 OR 4.5 0 0 0 0 0	*1.54 QR *.5 0 + + + +	<1.8 4 0R < .8 () + + / ()	<1.6 & ON <.8 0 0 + + 0	<1.5 4 OR < . 5 + + + + O
*64 OR *2 0 0 1 2 +	46 4 QR 42 0 0 1 1 0	<8 4 OR <2 + 1 2 1 + VSBY <2 + 1 1 + 1	V687 <8	48 4 DR 42	48 4 88 48 + 2 1 + 0
*687 <2 0 0 + + 0	410 4 0A 42 0 0 4 2 0	<10 4 OR <2 + 2 B 3 +	V687 <8	<10 4 DR 42 + 1 6 1 +	410 4 0R 4E 1 5 4 + 0
-20 t OR -5 + 2 10 13 1	420 4 DR 45 0 1 15 10 0	420 4 DR 45 1 6 18 5 +	420 4 08 48 + 4 18 3 +	120 4 DR 46 + 2 14 4 +	-20 404 46 2 11 11 1 0
V687 A5 3 14 43 28 3	VEST 16 0 11 63 24 0	vdev ab 5 33 48 € +	vasy as 1 23 86 7 +	VSSY 25 2 16 69 11 +	Y687 26 13 53 28 1 +
>80 tas 3 12 32 15 1	a 80 4 8	# 50 4 # B 4 27 31 4 +	±50 4 NE 1 17 43 3 +	2 80 4 28 2 12 52 7 +	#60 4 #6 11 40 17 + +
MC 4 * 10 3 11 21 7 1	MC 4 9 10 0 6 32 7 0	HC 4 a 10 3 24 26 3 0	NG 4 = 10 1 15 36 2 +	MC4+10 2 12 47 8 +	MC 4 = 10 10 36 15 + +
13	14	15	16	17	18
HIND SPEED (KNOTS)	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	WIND BPEED (KNOTS)	HIND SPEED (KNOTS)
CC - VBBY 3 10 21 33 254	LCC - VORY 0- 4- 11- 22- 3 10 21 33 234	LCC - VAST 3 10 21 33 A34	LCC - V88Y 9 10 81 39 294	LCC - VBSY 3 10 21 D9 234	LCC - VARY 0- 4- 11- 22- 23 234
-8 4 CM 4.5 0 0 0 0 0	41.84 dR 4.8 0 0 0 0 0	-1.54 OR 5 0 0 0 0 0	41 -8 4 0R 4 -8 D D D B D	* .5 & 08 * .5 D D D D	41.64 08 4.5 0 0 0 1 0
-64 OR <2 0 1 0 0 0	48 4 OF 42 0 0 0 0 0	48 4 08 42 0 3 0 0 0	46 6 OR 42 0 0 1 1 0	<8 4 6R <2 0 0 2 1 D	48 4 98 42 0 0 1 1 0
Y887 47 0 0 0 0 0	vsev et 0 0 0 0 0	V66Y 4Z 0 0 0 0 0	V88Y 4E 0 0 0 0 0	. VABY 42 0 0 1 0 C	V88Y 4R 0 0 0 0 0
10 LOR 42 2 2 3 0 0	410 4 0R 42 0 5 0 0 0 420 4 0R 45 2 12 5 0 0	410 4 0R 42 3 10 0 0 0 420 4 0R 45 3 13 3 0 0	419 4 584 42	<10 4 0R 42 0 1 5 5 2 <20 4 0R 45 1 4 17 14 2	410 t pr 42 0 1 3 2 0
- V8BY BS 9 56 34 0 U	VSAT 35 12 61 27 0 0	VSBY a6 33 57 10 0 0	Y88Y 88 2 25 61 10 0	Veer 35 1 18 49 25 4	veer as 1 21 85 20 1
250 4 85 7 50 21 0 0	280 4 28 10 44 22 0 0	a 50 4 a 5 27 43 7 U O	> E0 4 b8 1 20 43 7 0	280 4 26 0 14 31 9 1	250 4 25 1 14 34 8 1
MC 4 & 10 7 60 20 0 0	NC4 + 10 10 39 20 0 0	MC 4 2 10 27 40 7 0 0	MC 4 2 10 1 20 42 6 0	MC 4 a 10 D 14 27 7 1	MC 4 = 10 1 13 30 P C
117	41	90	367	169	128
22	23	24	25	26 HIND SPEED (KNOTS)	27 HIND BPEED (KNOTS)
HIND SPEED (KNOTE) 0- 4- 11- 22- 00 - 40 21 93 234	HIND SPEED (MNOTS) LCC - VORT 0- 4- 11- 22- 12- 13-	HIND SPEED (KNOTG) CCC - VSBY 0- 4- 11- 22- 22- 23- 24-	HIND SPEED (KNOTS) LCC - V46Y 3 10 21 33 334	0-14-11-122-1	10- 4- 11-122-1
CC - VORY 9 10 21 99 834	41.6 4 DR 4.6 0 0 + 0 D	1.5 6 6R 4.5 0 0 0 0 0	LCC - V46Y 3 10 21 33 334	41.6 4.08 4.6 D D D D D	
*8 4 GR -2 0 6 3 0 0	48 4 84 8 0 + + 0 0	48 4 02 42 0 0 0 0 0	40 4 OR 48 0 0 1 0 0	-8 4 DR -F D 1 1 D O	46 4 6K 4E 1 1 3 0 0
VBBY 42 0 8 3 0 0	V887 -2 D O O O O	VBSY 42 0 0 0 0 0	V48Y 42 0 0 0 0	V887 42 D 0 0 0 0	V88Y -2 0 0 1 0 0
10 t OR 42 0 12 8 0 0	<10 4 OR <2 + 2 1 + D	410 4 DR 42 0 6 0 8 0	410 4 6R 4E 0 1 8 1 0	410 A 0R 48 D 1 2 D 0	410 4 02 42 1 3 7 3 0
20 4 OR 46 0 15 21 0 0 V887 95 0 16 59 6 0	480 4 OF 45 1 3 3 4 0	*20 & OR *5 0 13 0 6 0	480 4 0R 48 1 10 18 2 0 VSSY 28 7 38 48 7 0	V88Y 25 4 35 53 6 1	480 4 06 48 2 9 16 5 0 V687 28 4 43 40 10 1
250 4 25 0 15 41 6 0	a 50 4 25 14 47 24 4 +	2 50 4 25 Q 31 50 O O	280 425 6 21 21 4 0	a 50 4 a 6 3 2 4 3 6 5 0	2 50 4 28 2 31 24 4 1
HC 4 > 10 0 15 35 8 D	NC 4 > 10 14 48 24 3 +	HC 4 + 10 0 31 44 0 0	MC 4 2 10 6 20 20 2 0	HC 4 a 10 2 22 35 4 0	MC 4 8 18 2 30 23 4 1
34	658	16	143	185	197
31	32	33	34	35	36
HIND SPEED (MNOTS) 0- 4- 11- 24- 10 - 11 - 21 - 33 - 34	HIND SPEED (KNOTS) LCC - VSSY 0- 4- 11- 22- 3 3 3 3 4	WIND BPEED (KNOT8) [0- 4- 11- 22-	HIND SPEED (KNOTS)	HINO SPECO (KNOTS) LCC - VP: 3 10 21 25 35 194	
C - VANT 3 10 E1 33 334	41.8 4.08 4.8 D D + D D	LCC - VEST 3 10 21 59 234	1.54 08 4.5 0 0 0 0 4 2	41.8 4 08 4.8 0 0 1 1 0	
64 0A -2 0 0 2 0 1	48 4 SA 48 0 + 1 1 1	-6 4 SR -2 + + + 1 +	44 00 42 0 1 0 1 2	48 4 GR 42 0 1 2 3 0	INICHIEGICIENIT
V887 42 0 0 0 0 1	VSBY -E D - O + O	V881 42 0 + 0 + 0	V\$AY 48 0 + 0 U 1	V88Y 42 0 1 1 1 0	INSUFFICIENT
0 4 0F -2 0 1 7 1 6	410 4 0R 48 + 2 4 4 1	<10 4 0R <2 + 2 4 3 1	416 4 OR 48 1 3 7 5 3	410 4 0H 42 0 4 9 5 3	DATA
10 t 0# 45 0 2 16 7 10	480 4 08 48 + 9 10 9 2	480 4 0R 48 1 5 13 6 3	420 4 0R 46 1 8 14 8 5	420 4 0R 45 0 10 22 7 3	
*50 4 25 0 11 22 13 7	V687 28 2 31 38 21 5	VERY AS 5 24 48 17 4 48 0 7 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4	vsdv as 5 17 50 16 5	v887 28 3 27 43 16 4 250 4 25 3 16 22 9 1	
MC 4 + 10 D 10 20 13 1	MC 4 8 10 1 18 19 9 1	MC 4 a 10 3 15 27 9 1	HC 4 B 10 4 12 28 9 1	HC 4 2 10 3 15 20 8 1	
83	337	916	276	145	
40	4 1	42	43	4 4	45
•	HIND SPEED (KNOTS)		HIND SPEED (KHDTS)		
)	LCC - VBBY 3 10 21 23 234		LCG - Y887 0- 4- 11- 29- 234		
I'	<1.8 4 OR <8 0 0 0 0 0 0		41.54 OR 4.5 0 0 0 0 2 0 5		
NSUFFICIENT	48 4 5F 42 0 0 0 0 0 0	INSUFFICIENT	48 4 58 42 0 0 2 0 5	INSUFFICIENT	INSUFFICIENT
DATA	410 4 0# 42 0 6 13 0 3	DATA	*10 A OR 42 D 2 5 13 10	DATA	DATA
	420 4 68 48 0 13 22 6 3		*20 4 OR *5 2 7 13 15 11		
	V48Y NU 0 34 41 22 3		vder as 7 26 28 28 10		
	MG 4 # IQ 0 16 13 16 0		#C 4 a 10 3 13 11 B 2		
	32		61		

ve compilation of available data for specified areas without regard to suspected blases. ite page) are based on all available data subjectively adjusted where bias was evident.

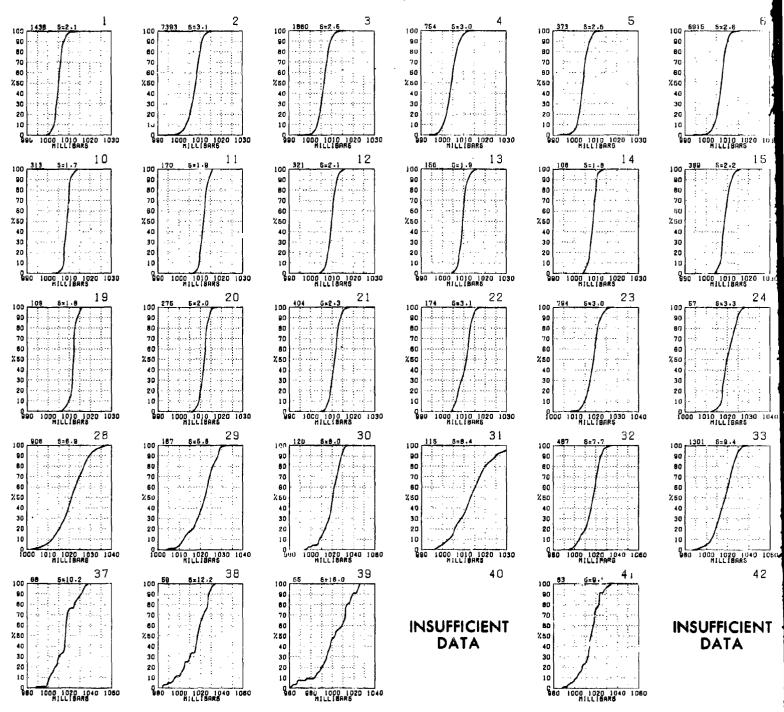
SEA LEVEL PRE



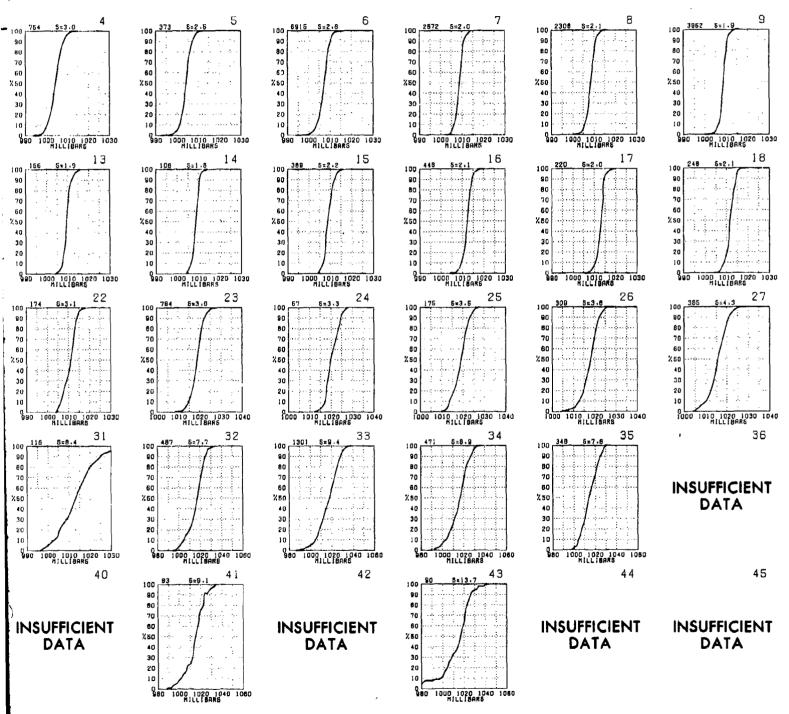
SEA LEVEL PRESSURE AND MEAN WIND



SEA LEVEL PRESSURE



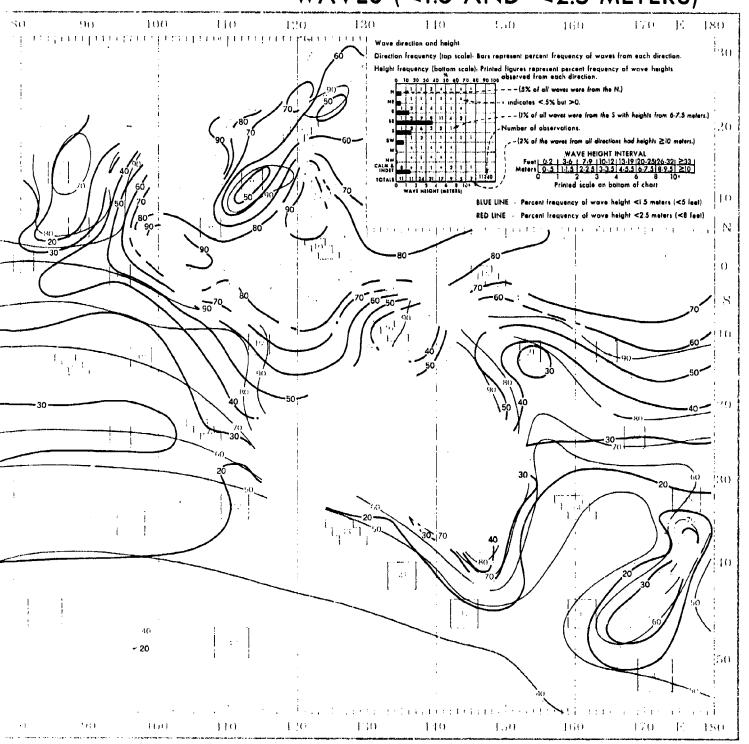
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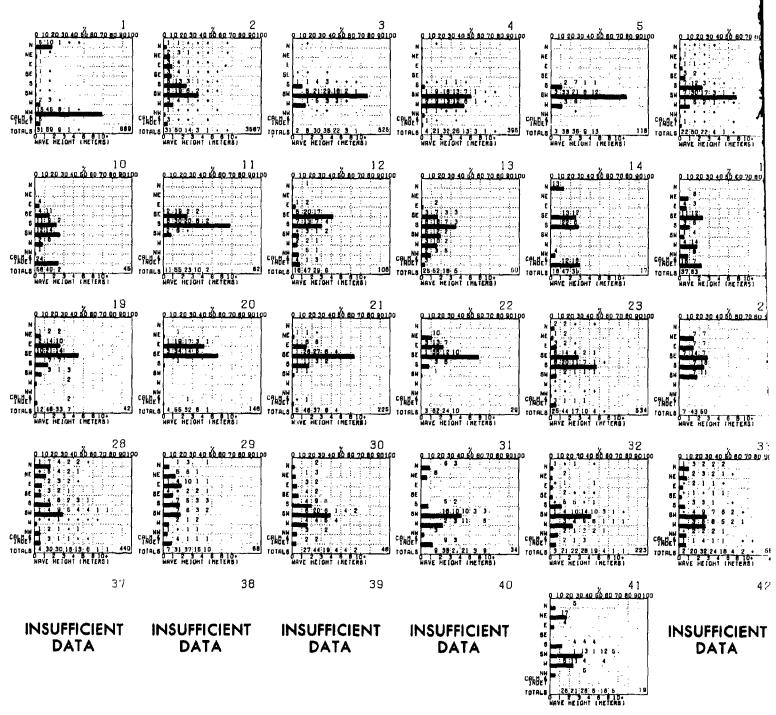
ctive compilation of available data for specified areas without regard to suspected biases. posite page) are based on all available data subjectively adjusted where bias was evident.

JUNE WAVI Particular in the contraction of the state 30 10 .111 $\mathbf{L}(0)$ 120

WAVES (<1.5 AND <2.5 METERS)



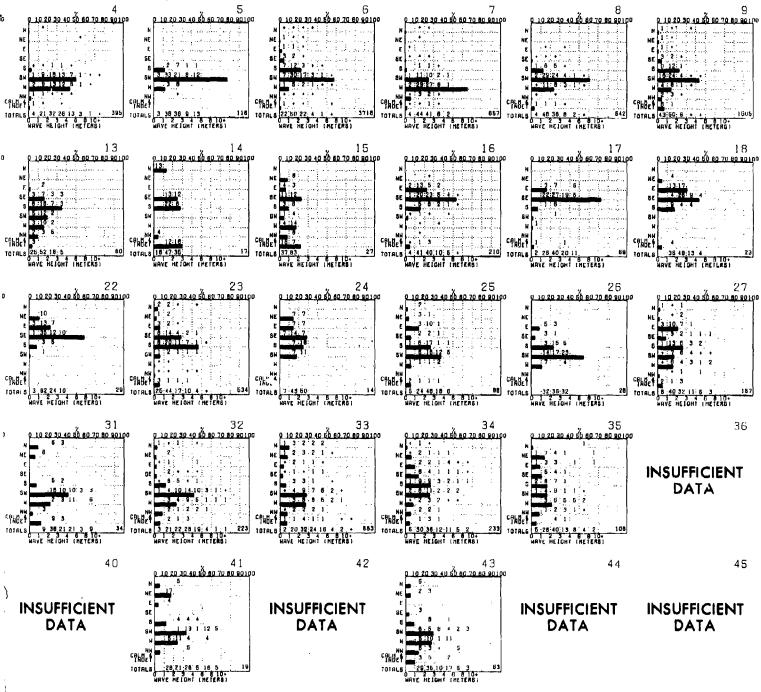
WAVE DIRECTION AND HEIGHT



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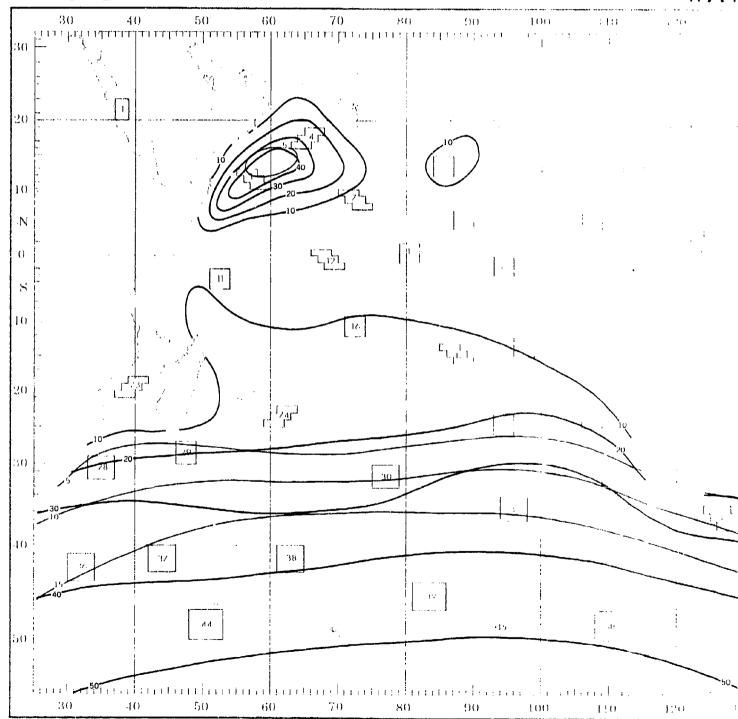
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WAVES (≥3.5 AND ≥6 METERS)

CONTRACTOR OF THE PROPERTY OF	WAVES (ES.S AIND EG METERS)	
	= 110 - 120 - 130 - 149 - 150 - 160 - 17	*(1)
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	11001 1,1	:
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10	Waves are selected on the basis of the higher of sea and swell when both are reported. If both heights are equal, the wave with the longer period is selected.	
· ()		
	âLUE LINE Perceni frequency of wave height ≥3.5 meters (≥12 feet)	1
	RED LINE - Percent frequency of wave height ≥6 meters (≥20 feet)	:
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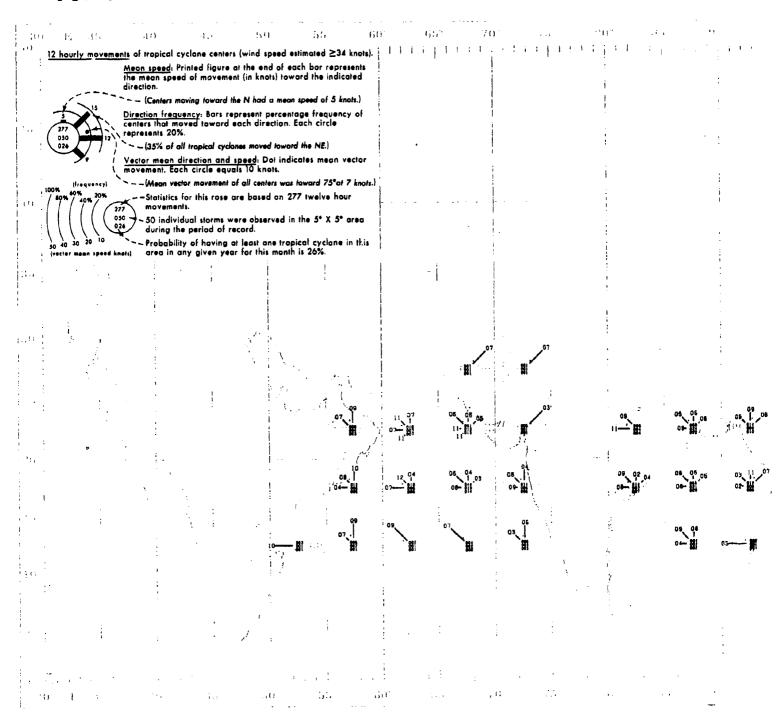
WAVE PERIOD AND HEIGHT

,											
PERIOD (SECONDS) HELOWIT	PERIOD (SECONDS)	PERIOD (SECONDS:	PERIOD ISECONDS) HEIDHT 10 - 17 - 17 - 17 18 19 180 G-6 5 0 + 0 0 0 0 + 1-1-8 7 10 2 0 0 + 1-1-8 5 9 11 3 + 0 2 2-3-5 2 4 7 9 2 + 1-3-5 0 + 1 1 1 1 1-3-5 0 + 1 1 1 1 1-3-6 0 0 0 0 + 0 1-3 0 0 0 0 0 1-3 0 0 0 0 0 0 1-3 0 0 0 0 0 1-3 0 0 0 0 0 1-3 0 0 0 0 0 1-3 0 0 0 0 0 1-3 0 0 0 0 0 1-3 0 0 0	PERIOD (SECONDS) 10 10 10 11 12 12 120	PERIOD (SECONDS) Meton						
PERIOD (SECONDS) **(*1865) 46 6-, 16-, 17-, 17-, 17-, 17-, 17-, 17-, 17-, 17	1 PERIOD (SECONDS) 1	1 1 1 1 1 1 1 1 1 1	1 3	1 1 1 1 1 1 1 1 1 1	PERIOD SECONDS						
1 1 1 1 1 1 1 1 1 1	PERIOD (SECONDS) PERIOD (SECO	PERIOD (SECONDS)	PERIOD (SECONDS) PERIOD (SECO	PERIOD (SECONDS) 10-10-11-11-11-11-11-11-11-11-11-11-11-1	PERIOD (SECONDS) ***TIPE** **TIPE** ***TIPE** **TIPE** ***TIPE** ***TIPE** ***TIPE** ***TIPE** ***TIPE** **TIPE**	PERIOD (SECONDS) ***TERIOD (SECONDS) **TERIOD (SECONDS) ***TERIOD (SECONDS) **TERIOD (SEC	PERIOD (SECONDS) PERIOD (SECONDS) 1	PERIOD (AECONDS) ***RETURN 0 0 10 11 13 18 180 0 -4 0 0 0 0 0 0 0 1-1.8 4 6 2 2 0 4 1-2.8 2 4 2 0 6 0 4 1-3.8 0 0 2 2 0 0 1-1.8 0 0 0 2 2 0 0 1-1.8 0 0 0 0 2 0 0 1-1.8 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0	#EIDO (SECONDE) PERIOD (SECONDE)	FERIOD SECONDS	#ERIOC (SECONDS) ***PERIOC (SECONDS) **PERIOC (SECONDS) ***PERIOC (SE
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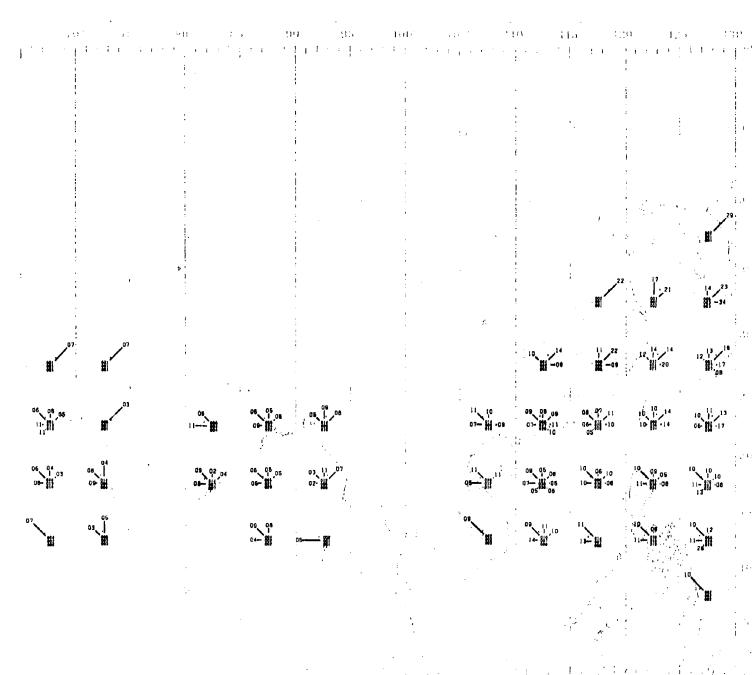
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1 3	1 4	15	Helioni	17 18 18 18 18 18 18 18	No. No.
PERIOD (SECONDS) ***PERIOD (S	PERIOD (SECONDS) PERIOD (SECO	PERIOD (SECONDS) ***********************************	PERIOD (SECONDS) ***********************************	PERIOD (SECONDS) PERIOD (SECONDS) PERIOD (SECONDS) 101001 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0	27 FERIOD [SECOND6] MEION [
S PERIOD (SECONDS)	32 FERIOD (SECONDS) **E1001 8-1 10 15 10 10 11183 44 7 8 11 12 13 10 1-1.8 8 9 5 4 4 3 0 1 1-1.8 1 9 4 4 3 0 1 1-1.8 1 3 5 4 3 2 0 1-1.8 1 3 5 4 3 2 0 1-1.8 0 0 0 0 0 0 0 1-1.8 0 0 0 0 0 1-1.8 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 1-1.8 0 0 0 0 0 0 1-1.8 0 0 0 0 0 1-1.8 0 0 0 0 0 1-1.8 0 0 0 0 1-1.8 0 0 0 0 1-1.8 0 0 0 0 1-1.8 0 0 0 0 1-1.8 0 0 0 0 1-1.8 0 0 0 1-1.8 0 0 0 1-1.8 0 0 0 0 1-1.8 0 0 0 1-1.8 0 0 0 1-1.8 0 0 0 0 1-1.8 0 0 0 1-1.8 0 0 0 1-1.8 0 0 0 1-1.8 0 0 0 1-1.8 0 0 0 1-1.8 0 0 0 1-1.8 0 0 0 1-1.8 0 0 0 1-1.8 0 0 1-1.8 0 0 0 1-1.8 0 0 1-1.8 0 0 0 1-1.8 0 0 1-1.8 0 0 0 1-1.8 0 0 0 1-1.8 0 0 1-1.8 0 0 0 1-1.8 0 0 1-1.8 0 0 0 1-1.8 0 1-1.8 0 0 1-1.8 0 0 1-1.8 0 1-1.8	S S S S S S S S S S	34 **PERIOD (SECONDS)** **Infras 49 6-7 6-8 16-1 18 18 18 18 19 **O	STATE STAT	INSUFFICIENT DATA
INSUFFICIENT DATA	4 1 PERIOD (SECONDS) PERIOD (SECONDS) PERIOD (SECONDS) 0-18 0 0 0 0 0 0 0 0 1-18 0 21 5 0 0 0 0 1-18 0 18 5 0 0 0 0 1-18 0 18 5 0 5 0 0 1-18 0 0 0 0 0 0 0 5 0 0 1-18 0 0 0 0 0 0 5 0 0 1-18 0 0 0 0 0 5 0 0 1-18 0 0 0 0 0 0 0 0 1-18 0 0 0 0 0 0 0 0 1-18 0 0 0 0 0 0 0 0 1-18 0 0 0 0 0 0 0 0	INSUFFICIENT DATA	43 PERIOD (SECONDS) (17563) 46 7 9 10 11 13 11 10 10 10 10 10 10 10 10 10 10 10 10	INSUFFICIENT DATA	INSUFFICIENT DATA

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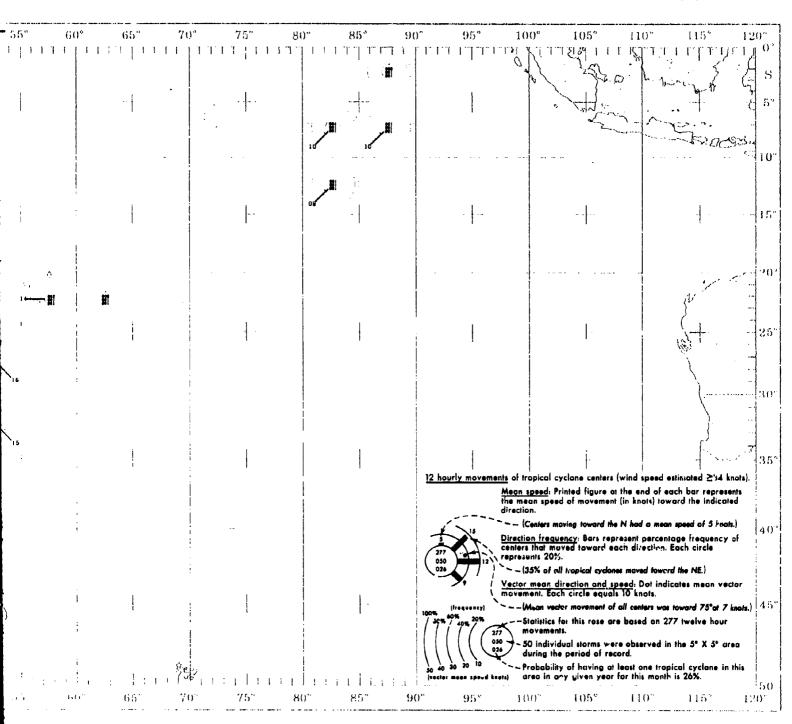
TROPICAL CYCLONE

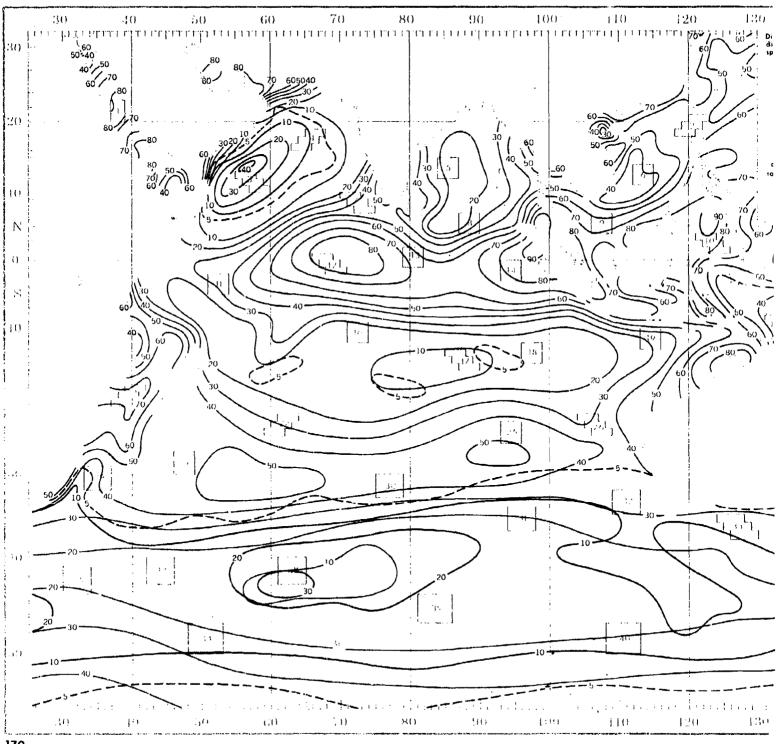


TROPICAL CYCLONE

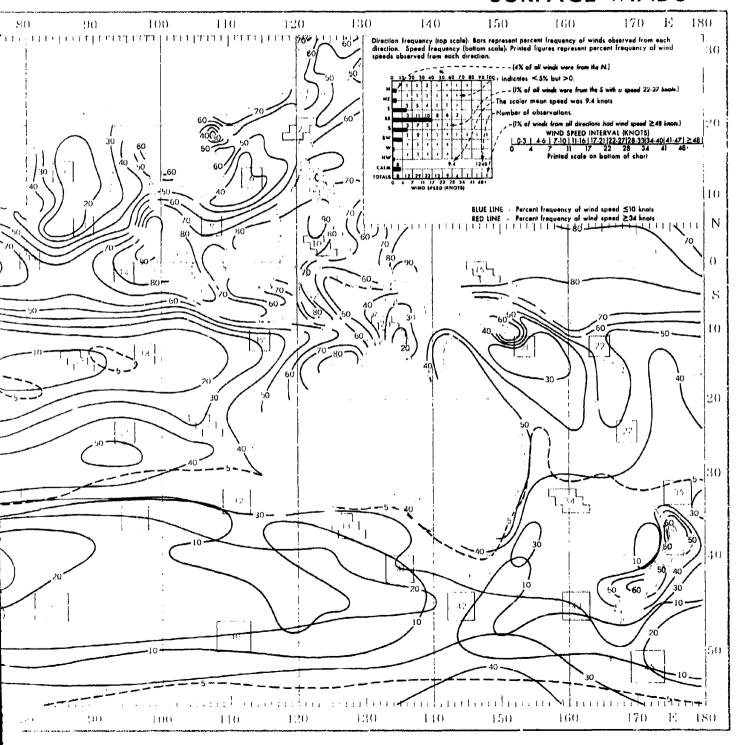
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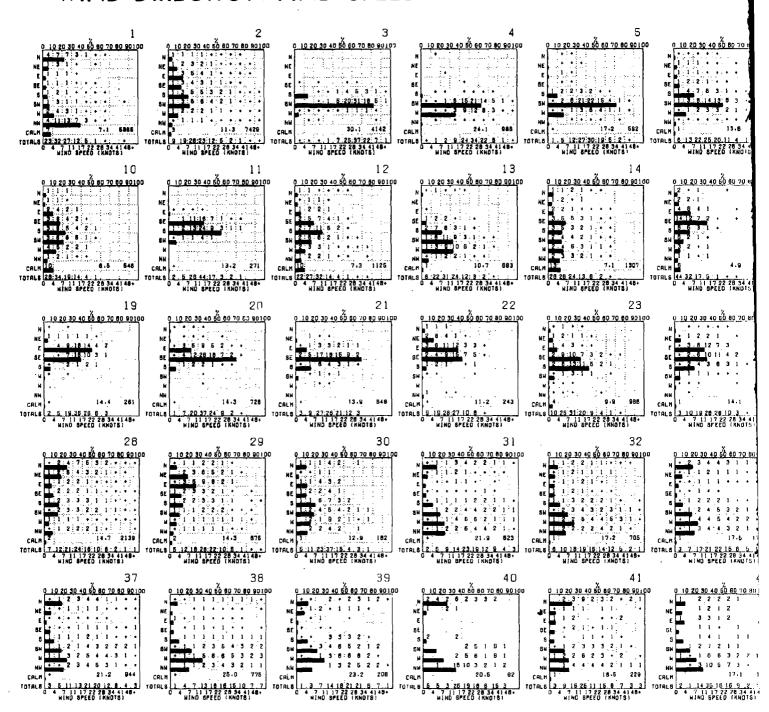




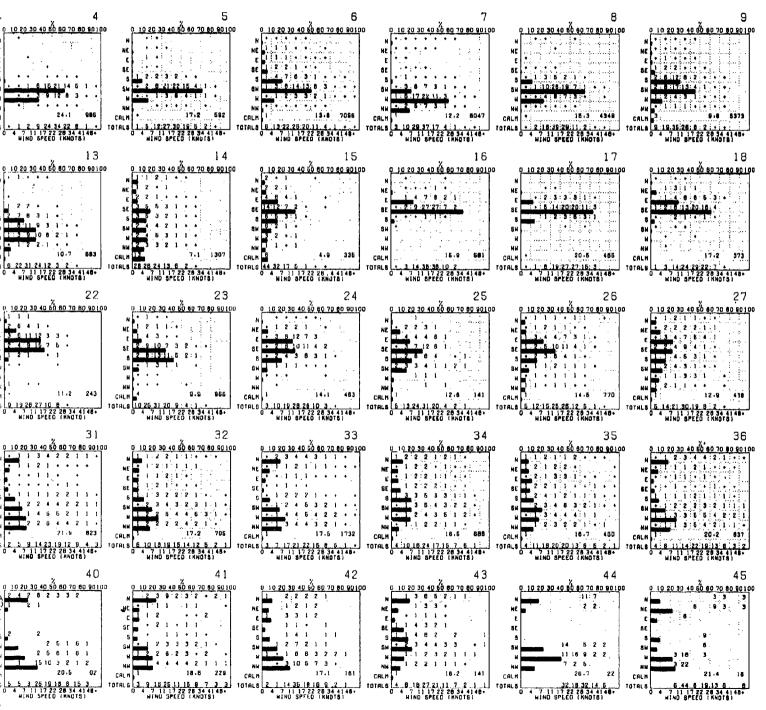
SURFACE WINDS



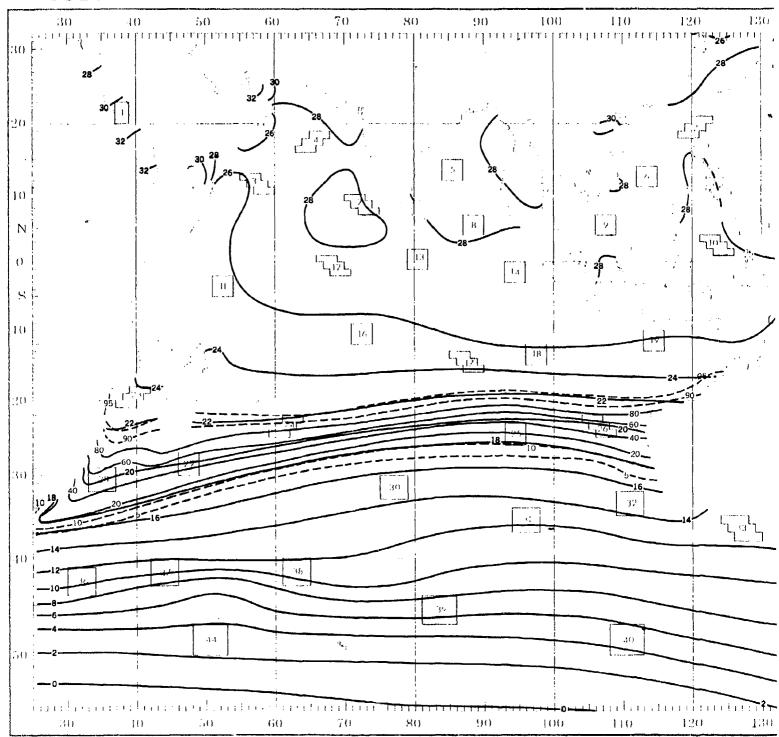
WIND DIRECTION AND SPEED



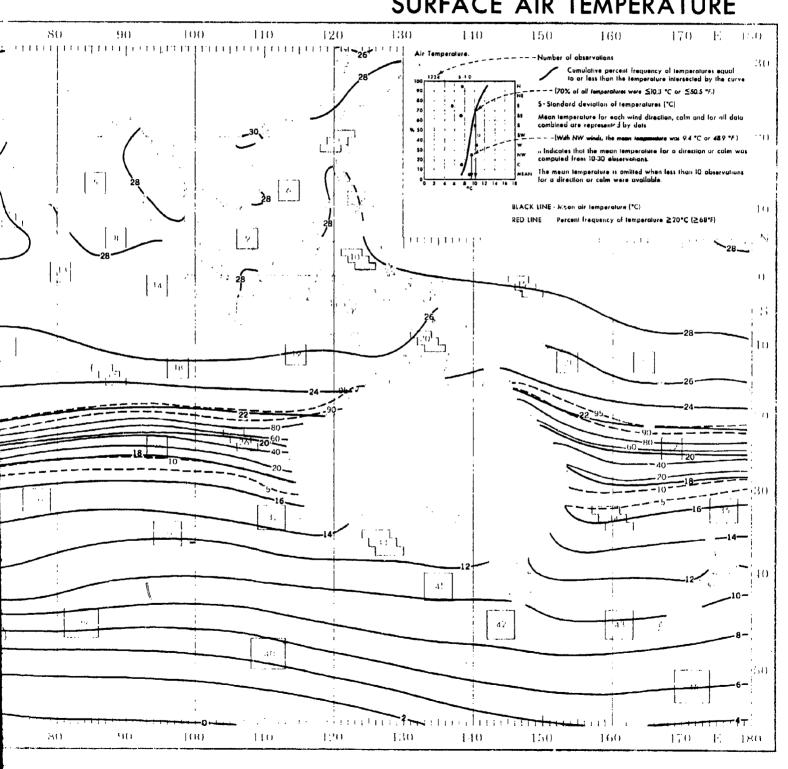
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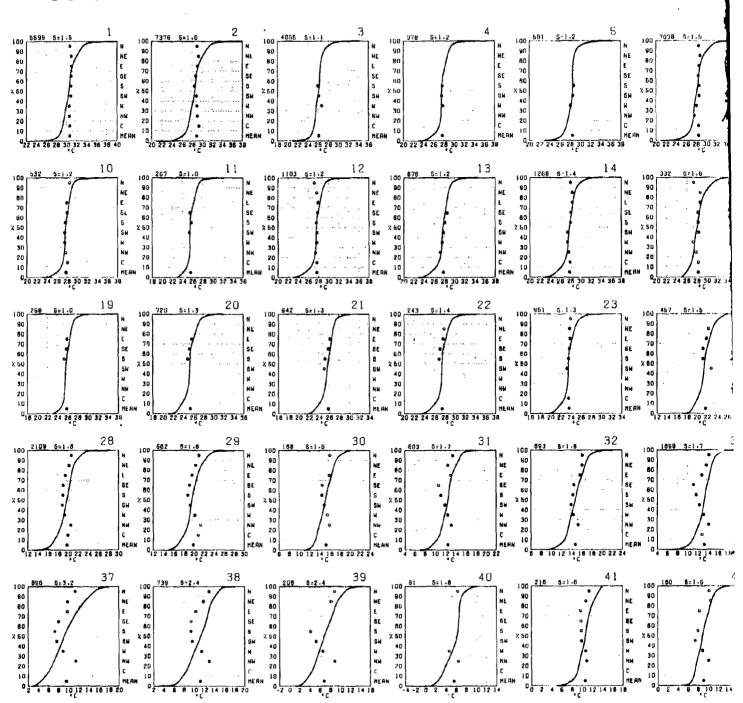
ive compilation of available data for specified areas without regard to suspected biases. (ite page) are based on all available data subjectively adjusted where bias was evident.



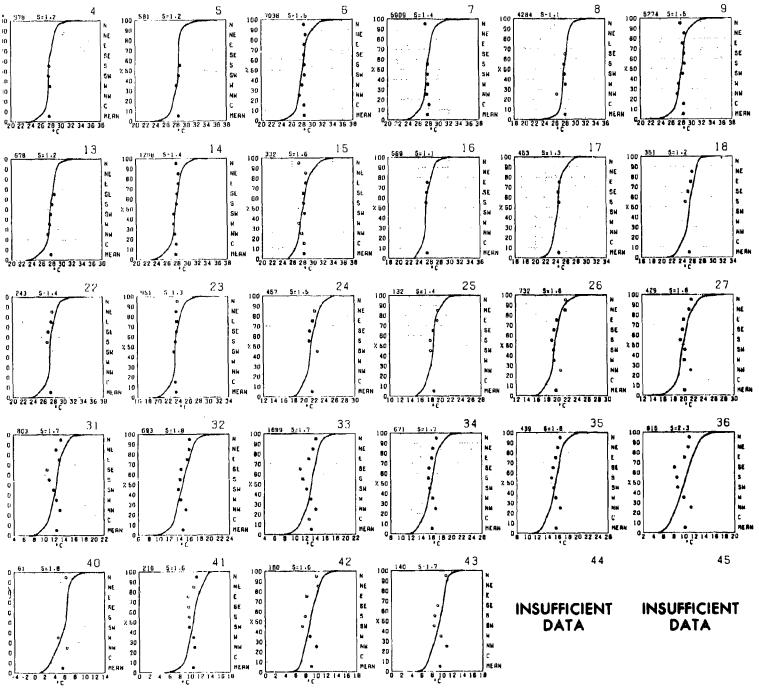
SURFACE AIR TEMPERATURE



SURFACE AIR TEMPERATURE



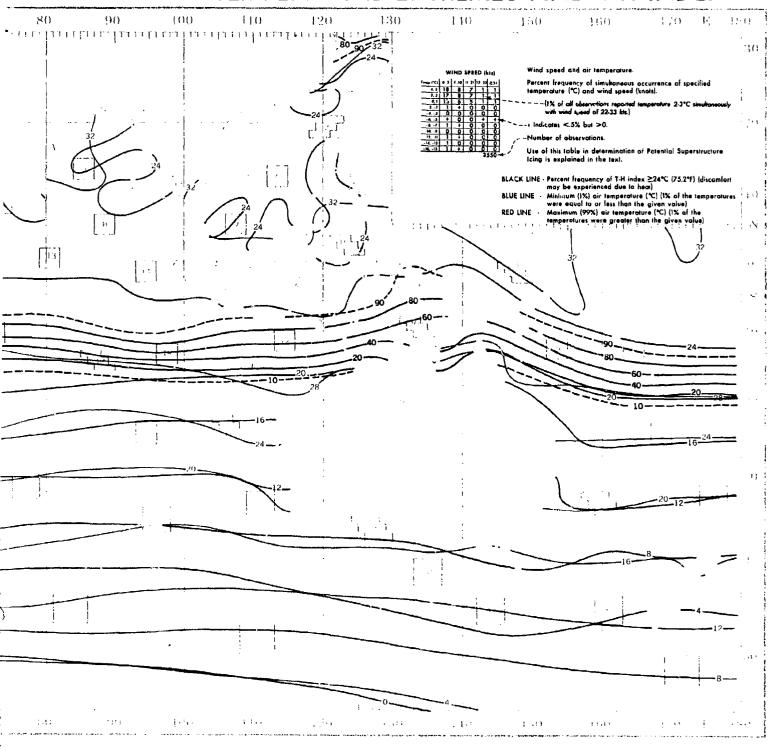
Graphs represent the objective compilation of available data for specified areas with The isopleth analyses (opposite page) are based on all available data subjectively as



ctive compilation of available data for specified areas without regard to suspected biases.

JULY TEMPERATURE E 30

TEMPERATURE EXTREMES AND T-H INDEX



WIND SPEED AND AIR TEMPERATURE

WIND SPEED (KTS)	WIND SPEED (KTS) 2	HIND SPEED (KTS) 3	WIND SPEED (KTS) 4	WIND SPEED (KTS) 5	WIND SPEED (K
TEMP (*C) 0-3 4-10 11-21 22-33 a 34	1. 1 1 1 1		TEMP (*C1 0-3 4-10 11-21 22-33 2 34		
30.37 + + 0 0 30.37 + + + 0 0	36.37 0 + + 0 0 34.38 + + + 0 0	32.33 0 0 + 0 30.31 + 0 + 1 +	32.39 0 + + + 0 30.31 0 + 2 3 0	34.35 0 0 + 0 0 32.33 + + 1 1 0	38.37 0 + + 34.35 0 + +
34.36 1 2 1 + 0 32.33 6 13 5 + 0	32.33 1 3 2 + 0 30.31 3 13 8 1 +	28.27 D + 1 7 2 28.27 D + 5 42 20	20.20 0 1 17 28 4 26.27 + 1 14 24 5	30.31 0 2 B 2 + 28.29 1 12 42 18 +	32.33 + 2 1 30.31 1 6 B
30.31 12 32 8 1 + 20.28 4 12 3 + 0	ta.28 5 25 19 4 + 28.27 1 6 5 2 +	24.25 + + 2 13 6	24.25 0 0 + 1 + 22.23 0 0 0 + 0	26.27 0 2 5 4 1 24.25 0 + 1 1 +	26.29 3 19 27 26.27 1 6 8
26.27 + + + 0 0	24.28 + + 1 + +	20.21 0 0 + + +	20.21 0 0 0 0	22.23 0 0 0 0 0	24.25 + 1 1
22.23 + 0 0 0 0	20.21 0 0 0 0 0	18.17 O O O O O	18.19 O O O O O O	20.21 0 0 D 0 0 16.19 0 0 D 0 0	20.21 0 0 0
20.21 0 0 0 0 0	18-18 0 0 0 0 0 0 18-17 0 0 0 0 C 0	14.16 0 0 0 0 0 12.13 0 0 0 0 0	14.15 D O O O O	16.17 0 0 0 0 0 14.15 0 0 0 0 0	18.19 0 0 D
5619	7392	4065	978	581	
HIND SPEED (KTS)	HIND SPEED (KTS) 11	HIND SPEED (KTS) 12	HIND SPEED (KTS) 13	HIND SPEED (KTS) 14	HIND SPEED (K
TEMP (*C) 0-9 4-10 11-21 22-93 5 34	TEMP (*C) 0-3 4-10 11-21 22-33 2-34	7EHP (*C) 0-3 4-16 11-21 22-33 × 34	7Emp (*C) 0-3 4-10 11-21 22-33 2 34	TEMP (*C) 0-3 4-10 11-21 22-33 2 34 32 32 35 4 4 4 0 0	32,33 2 3 0
30.31 2 2 + 0 0	20.20 0 1 2 1 0	30.31 1 3 1 0 0	30.31 0 3 1 0 0	30.31 3 5 1 0 0	30.31 8 4 0
20.29 19 35 8 + 0 28.27 7 17 6 1 0	28.27 2 17 30 3 + 24.25 + 11 28 2 +	20.29 11 35 9 + 0 26.27 9 20 6 + +	26.27 2 13 12 3 +	28.29 15 30 8 1 0 28.27 8 13 8 1 0	28.29 19 26 3 28.27 14 15 3
24.25 + 1 2 0 0 22.23 0 0 0 0 0	22.23 0 + + 0 0	24.25 1 2 1 + 0	24.25 0 1 1 1 +	24.25 1 2 2 1 0 22.23 0 4 + 0 0	24.26 + 1 0 22.23 0 0 0
20.21 0 0 0 0 0 10.10 0 0 0 0 0	19-19 0 0 0 0 0 16-17 0 0 0 0 0	20.21 0 0 0 0 0	20,21 0 0 0 0 0 10,10 0 0 0 0 0	20.21 0 0 0 0 0 18.19 0 0 0 0 0	20.21 0 0 0
18.17 0 0 0 0 0	14.15 0 0 0 0 0	18.17 D 0 0 0 0	18.17 0 0 0 0 0	16.17 0 0 0 0 0	16.17 0 0 0
14.15 0 0 0 0 0 0 12.13 0 0 0 0 0	12.13 0 0 0 0 0 10.11 0 0 0 0 0	14.15 0 0 0 0 0 0 12.19 0 0 0 0 0	14.18 0 0 0 0 0 18.19 0 0 0 0 0	14.15 0 0 0 0 0 0 12.13 0 0 0 0 0	14.18 0 0 0 12.13 0 0 0
633 1.0	267 20	1107	879	1258	
HIND SPEED (KTS) 19	HIND SPEED (KTS) 20	HIND SPEED (KTS) 21	HIND SPEED (KTS) 22	WIND SPEED (KTS) 23	HINO BPEED (K
TEMP (*C) 0-3 4-10 [1-21 22-33 234	1EHP (°C) 0-3 4-10 11-21 22-33 2 34	TEMP (°C) 0-3 4-10 11-21 22-33 a 34	TEMP (*C) 0-9 4-18 11-21 22-33 2 34	TERP (*C) 0-3 4-10 11-21 22-33 × 34 28.28 + + + 0 0	7EMP (4C) 0-3 4-10 11-21
29.21 1 2 2 0 0	28.28 0 1 3 1 0	20:20 0 3 4 1 0	30.31 2 2 + + 0	28.27 + 4 2 + 0	24.25 1 5 3
24.25 0 8 19 7 0	24.28 1 13 29 6 +	24.28 2 11 13 5 0	26.27 5 22 16 4 0	22.23 5 22 12 3 •	20.21 1 13 22 20.21 1 10 24
20.21 0 0 0 0 0	26.23 0 2 4 1 0 20.21 0 0 + 0 0	22.23 1 1 2 1 0 20.21 0 0 0 0 0	24.25 0 + 3 2 0 28.29 0 0 0 0 0	20.21 + 2 1 1 0 18.19 0 0 0 0 0	18.19 0 1 5 18.17 0 0 0
19.19 0 0 0 0 0 18.17 0 0 0 0 0	18.17 0 0 0 0 0 0	18-19 0 0 0 0 0	20.81 0 0 0 0 0 18.18 0 0 0 0 0	18.17 0 0 0 0 0	14.15 0 0 0
14.16 0 0 0 0 0 0 12.13 0 0 0 0 0	14.15 0 0 0 0 0	14-18 0 0 0 0 0 0 12-13 0 0 0 0 0	18.17 0 0 0 0 0	12.19 0 0 0 0 0 10.11 0 0 0 0 0	10.11 0 0 0 6.9 0 0 0
10.11 0 0 0 0 0	18.13 0 0 0 0 0 18.11 0 0 0 0 0	10.11 0 0 0 0 0	14.15 0 0 0 0 0 0 18.19 0 0 0 0 0 0	•.• o o o o o	8.7 0 0 0
HIND SPEED (KTS) 28	WIND SPEED (KTS) 29	HIND SPEED (KTS) 30	HIND SPEED (KTS) 31	HIND SPEED (KIS) 32	
TEMP (*C) 0-3 4-10 11-21 22-32 2 34	1EHP (*C) 0-0 4-10 11-21 22-33 2 34	MIND SPEED (KTS)	HIND SPEED (KTS) TEMP (PC) [0-3 4-10 11-21 22-33 34	ATHO SIECO (MIST	WIND SPEED (K'
28.27 + + 0 0 0	26.27 0 + + + 0	20.21 0 0 1 0 0	18-18 0 D O + D	20.21 + + + 0 0	18.19 0 + +
24.26 + + 1 + + 22.23 1 5 6 3 +	24.25 0 1 1 + 0	10-10 0 2 4 1 0 16-17 3 11 25 1 0	16:17 + + 1 1 1 14:18 + 4 10 8 4	10.19 + 2 2 1 + 10.17 2 9 10 8 2	18.17 + 2 4 14.18 + B 17
20.21 2 15 18 6 1 10.10 3 11 13 5 2	20.21 2 9 21 5 1 10.10 1 12 16 5 1	14.15 2 15 17 4 0 12.13 0 7 4 2 1	12.13 6 18 14 5 10.11 4 7 8 3	14.15 1 11 14 9 4 12.13 2 4 6 6 2	10.11 + 3 5
18,17 + 3 2 2 1	18-17 + 3 2 1 0 14-18 0 0 + + 0	10.11 0 0 0 0 0	0.8 + 1 1 1 1 6.7 0 0 0 0 0	10:11 0 • 1 2 • 8:8 0 0 0 0 0	8.7 0 0 0
18.13 0 0 0 0	12:13 0 0 0 0	0.7 0 0 0 0 0	4.6 0 0 0 0 0	8.7 0 0 0 0 0	4.6 0 0 0
10.11 0 0 0 0 0 0 1.0 0 0 0 0 0	0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4.6 0 0 0 0 0 0 2.3 0 0 0 0 0	2.3 0 0 0 0 0 0 0.1 0 0 0 0 0 0 -21 0 0 0 0 0	4.5 0 0 0 0 0 0 2.3 0 0 0 0 0	7.3 0 0 0 0.1 0 0 0
9.7 0 0 0 0 0 0 2121	6.7 0 0 0 0 0 662	0.1 0 0 0 0 0 169	-21 0 0 0 0 0 0 803	0-1 0 0 0 0 0 694	-8. · · 0 0 0
HIND SPEED (KTS) 37	WIND SPEED (KTS) 38	WIND SPEED (HIS) 39	HIND SPEED (KTS) 40	HIND SPEED (KTS) 41	WIND SPEED IK:
TERP (*C) 0-8 4-10 11-21 22-38 2 34	1EMP (*C) 0-9 4-10 11-E1 22-33 2 34	TEHP (°C) 0-9 4-10 11-21 22-33 2 34	TEMP (PC) 0-3 4-10 11-21 22-33 2 34	TERP (PC) 0-8 4-10 11-81 22-83 2 34	
10.10 0 0 + + 0	18-17 0 + + + • 14-18 + 1 6 8 5	12.13 0 0 + 0 1 10.11 0 1 2 5 3	0.0 0 2 10 2 2 0.7 3 5 20 15 2	14·18 0 + 1 1 + 12·13 + 6 12 8 5	12.13 0 2 3 10.11 1 3 15
14.15 0 1 3 4 2 12.13 + 1 5 5 1	12.13 + 3 10 8 5	8.9 · 3 5 11 6	4.8 2 2 8 7 8	10.11 1 9 17 9 4	8.8 1 6 26
10.11 1 3 6 7 2	0.0 0 1 5 7 4	4.5 • 3 11 10 1	0.1 0 0 0 0 2	8.7 0 1 1 2 0	4.5 0 0 1
9.9 + 5 7 7 3 9.7 1 4 6 5 2	4.8 0 0 0 0 + +	2.3 0 + 2 2 + 0.1 0 0 0 0 +	-21 0 0 0 0 0 -43 0 0 0 0 0	4.5 0 + 0 0 0 2.3 0 0 0 0 0	9.3 0 0 0 9.1 0 0 0
2.3 + + + + +	#.3 0 0 0 0 +	-91 0 0 0 0 0 0 -4:-3 0 0 0 0 0 0	-06 0 0 0 0 0 -07 0 0 0 0 0	0.1 0 0 0 0 0 -21 0 0 0 0 0	-21 0 0 0 -43 0 0 0
0.1 0 0 0 0 0 -t,-1 0 0 0 0 0	-2:-1 0 0 0 0 0 -4:-3 0 0 0 0 0	-68 0 0 0 0 0 0 -67 0 0 0 0 0	-10:-0 0 0 0 0 0 -12:-11 0 0 0 0 0	-43 0 0 0 0 0 -66 0 0 0 0 0	-85 0 0 0 -87 0 0 0
895	739	206	51 B1	216	

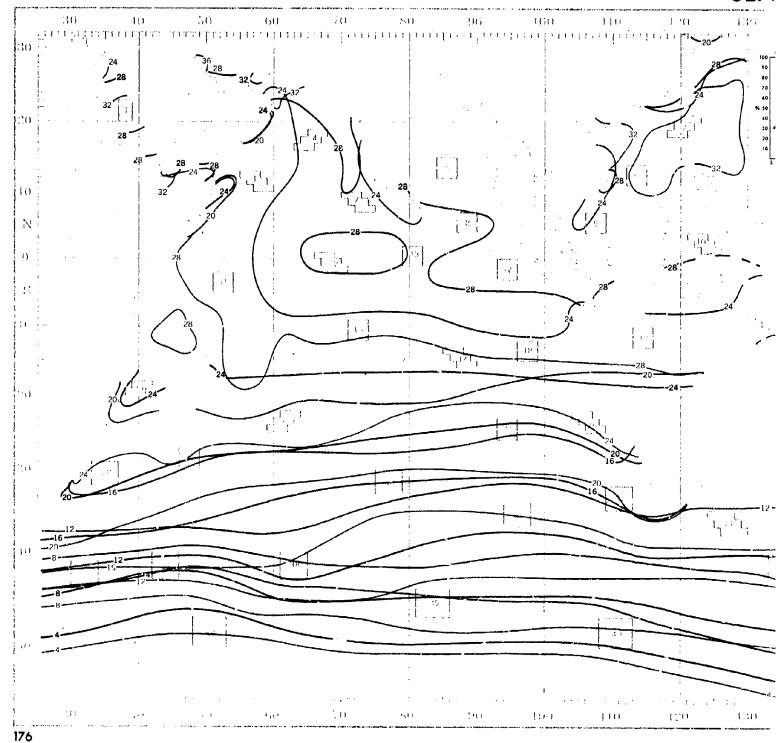
Graphs represent the objective compilation of available data for specified areas with The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively a

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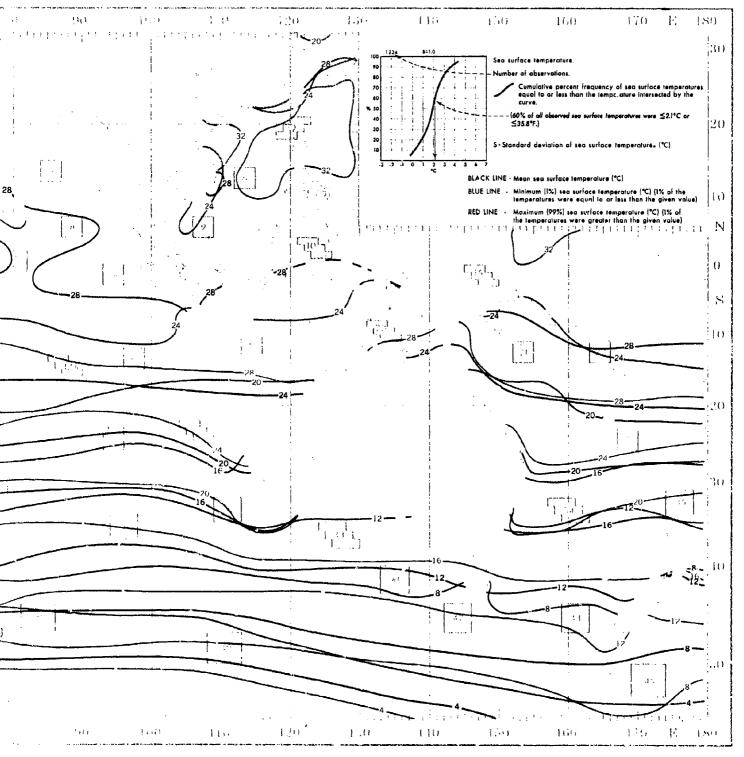
JULY

- WIND SPEED (KTS) 4	HIND SPEED (KTB) 5	WIND SPEED (KTS) 6	WIND SPEED (KTS) 7	HIND SPEED (KTS) 8	HIND SPEED (KTS)
1	TEMP (°C.) 0-3 4-10 11-21 22-39 3-34 34 34 5 0 0 + 0 0 0 32-33 + 1 1 0 0 0 32-33 + 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TEMP (4C) 0-3 (-10 11-2 22-33 24 38 (-37 D ~ + 0 D 0 0 0 0 0 0 0 0	TEMP (*C1 0-3 4-10 11-£1 22-33 à 34 34.35	TEMP (*C1	TEMP (*C) 0-3 (-10 11-2) 22-52 3-34 34 35 + + + 4 0 0 0 32-53 3 + 2 1 + 0 30-53 1 1 d 5 + 0 0 24-52 6 5 34 20 1 + 24-52 7 2 10 7 + 24-55 7 1 1 + 0 22-52 7 0 + + 7 0 22-52 7 0 + + 7 0 22-52 7 0 + + 7 0 0 22-52 7 0 + + 7 0
18.17 0 0 0 0 0 0 14.15 0 0 0 0 0 0 12.13 0 0 0 0 0 0 978	20.21 0 0 0 0 0 18.18 0 0 0 0 0 0 18.17 0 0 0 0 0 14.15 0 0 0 0 0 581	22.23 0 + + 0 0 0 20.21 0 0 0 0 0 0 18.19 0 0 0 0 0 0 18.17 0 0 0 0 0 7043	20.21 0 0 0 0 0 0 0 1 16.19 0 0 0 0 0 0 0 16.17 0 0 0 0 0 0 0 0 14.18 0 0 0 0 0 0 0 5909	16.19 0 0 0 0 0 0 0 0 0 16.17 0 0 0 0 0 0 0 0 14.18 0 0 0 0 0 0 0 0 12.13 0, 0 0 0 0 0 4284	20,21
NINO SPEED (KTS) 13	WIND SPEED (KTS) 14	HIND SPEED (KTS) 15	HIND SPEED (KIS) 16	HIND SPEED (KTS) 17	HIND SPEED (KTS) 18
1°C 0-2 4-10 1-2 22-33 34 12-33 0 4 0 0 0 10-33 0 3 1 0 0 10-33 0 5 5 1 1 0 28-26 5 35 21 1 0 28-27 2 13 12 3 4 4-25 0 1 1 1 4 72-23 0 0 0 0 0 20-21 0 0 0 0 0 16-17 0 0 0 0 0 16-16 0 0 0 0 0 16-17 0 0 0 0 0 16-18 0 0 0 0 0 16-18 0 0 0 0 0 16-18 0 0 0 0 0 16-18 0 0 0 0 0 0 16-18 0 0 0 0 0 0	TEMP (*C)	TEMP (4C1 0-3 4-10 11-21 22-33 3-4	TEMP 1*G)	TERP (*C)	TERF (1-C1 0-3 4-10 11-E1 22-33 3-96
HIND SPEED (KTS) 22	HIND SPEED (KTS) 23	NIND BPEED (KTS) 24	WIND SPEED (KTS) 25	HIND SPEED (KTS) 26	HIND SPEED (KIS) 27
1 1 2 2 2 3 2 4 4 5 2 2 3 2 2 4 5 5 2 2 3 2 2 4 5 5 2 2 3 3 3 4 4 5 3 2 3 2 4 5 5 5 2 3 3 5 4 5 5 5 2 3 5 5 5 5 2 3 5 5 5 5 5 2 3 5 5 5 5 5 5 5 5 5	TEMP (*C1 0-3 4-10 11-21 22-33 > 34 28 29	FERP (*C) 0-3 6-10 11-E 2E-33 > 34 26.27 0 1 + 0 0 0 24.45 1 5 3 + 0 0 22.45 1 10 24 6 0 20.21 10 24 6 0 20.21 10 24 6 0 20.21 10 24 6 0 20.21 10 24 6 20.21 10 2	TEMP (4C) 0-3 4-10 11-21 27-33 3 34 ## 23 0 1 2 0 0 10.21 3 1.4 6 1 0 10.10 2 17 34 2 1 16.17 0 5 6 2 1 14.16 0 2 0 0 0 0 10.11 0 0 0 0 0 0 6.7 0 0 0 0 0 0 4.5 0 0 0 0 0 0 0 4.5 0 0 0 0 0 0 0 4.5 0 0 0 0 0 0 0 4.5 0 0 0 0 0 0 0 4.7 0 0 0 0 0 0 10.11 1 1 1 1 1 1 10.11 1 1 1 1 1 1 10.11 1 1 1 1 1 1 10.11 1 1 1 1 1 10.11 1 1 1 1 1 10.11 1 1 1 1 1 10.11 1 1 1 1 1 10.11 1 1 1 1 1 10.11 1 1 1 1 1 10.11 1 1 1 1 1 10.11 1 1 1 1 1 10.11 1 1 1 1 1 10.11 1 1 1 1 1 10.11 1 1 1 1 1 10.11 1 1 1 1 1 10.11 1 1 1 1 1 10.11 1 1 1 1 1 10.11 1 0 0 0 0 0 0 4.8 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0 4.8 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0 2.3 0 0 0 0 0 0 0	TERF (*C) 0-3 4-10 11-E1 2E-38 3-34 26.E7 0 + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TEMP (%) 0-3 (-10 11-11) (22-38) 34 283-27 0 + 4 0 0 24-26 + 2 + 4 0 25-27 0 1 9 1 0 0 24-26 + 2 + 4 0 25-28 1 1 8 9 1 0 25-28 1 1 8 9 1 0 25-28 1 1 9 9 1 0 25-28 1 1 9 9 1 0 25-28 1 1 9 9 1 0 25-28 1 1 9 9 1 0 25-28 1 1 9 9 1 0 25-28 1 1 9 9 1 0 25-28 1 1 9 9 1 0 25-28 1 1 9 9 1 0 25-28 1 1 9 9 1 0 25-28 1 9 9 1 0 25-28 1 9 9 1 0 25-28 1 9 9 1 0 25-28 1 9 9 1 0 25-28 1 9 9 1 0 25-28 1 9 9 1 9 9 1 25-28 1 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
21 0 0 0 0 0 803 HINO SPEED (KTS) 40	0.1 0 0 0 0 0 0 694 HIND SPEED (KTS) 4]	-2,-1 0 0 0 0 0 0 1701 HIND SPEED (KTG) 42	0.1 1 0 0 0 0 672 HIND SPEED (KTS) 43	2.3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-43 0 0 0 0 0 0 618 45
1°C 0-3 4-10 11-21 22-33 3-34 4.0	TERP (*C) 0-8 4-10 1 2 21-23 3-34 14-15 0 + 1 1 + 1 + 1 12-13 + 6 12 8 5 10-11 1 9 17 9 4 9-8 1 7 6 5 3 3 6-7 0 1 1 2 0 0 0 0 0 0 2-3 0 0 0 0 0 0 0 0 2-3 0 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 0 0 0 0 -1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TEMP (*C)	TERP (9G)	75 (PC) 0-8 4-18 11-21 22-33 h 24 24 25 (PC) 0-9 0 0 0 9 0 0 14 23 9 25 25 25 25 25 25 25 25 25 25 25 25 25	INSUFFICIENT DATA

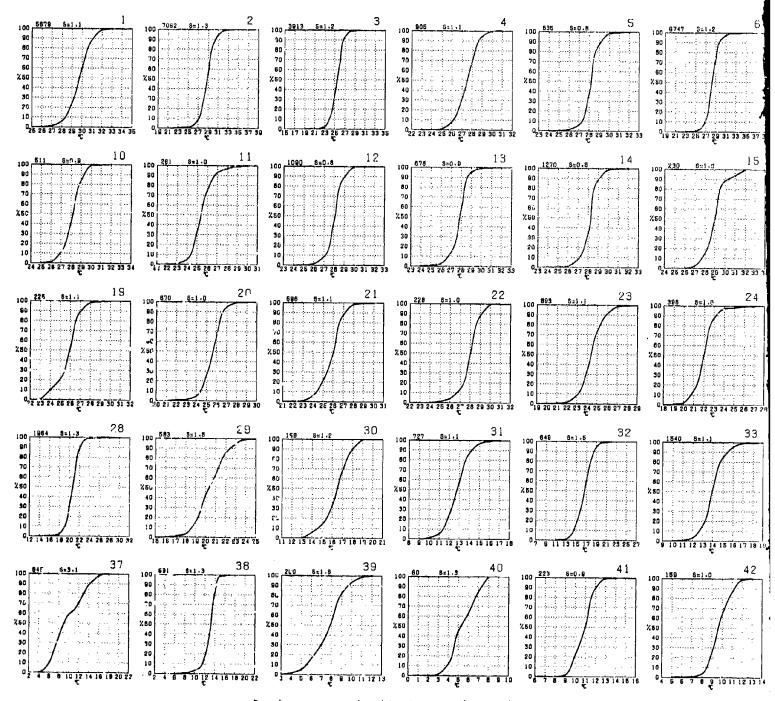
ive compilation of available data for specified areas without regard to suspected biases. site page) are based on all available data subjectively adjusted where bias was evident.



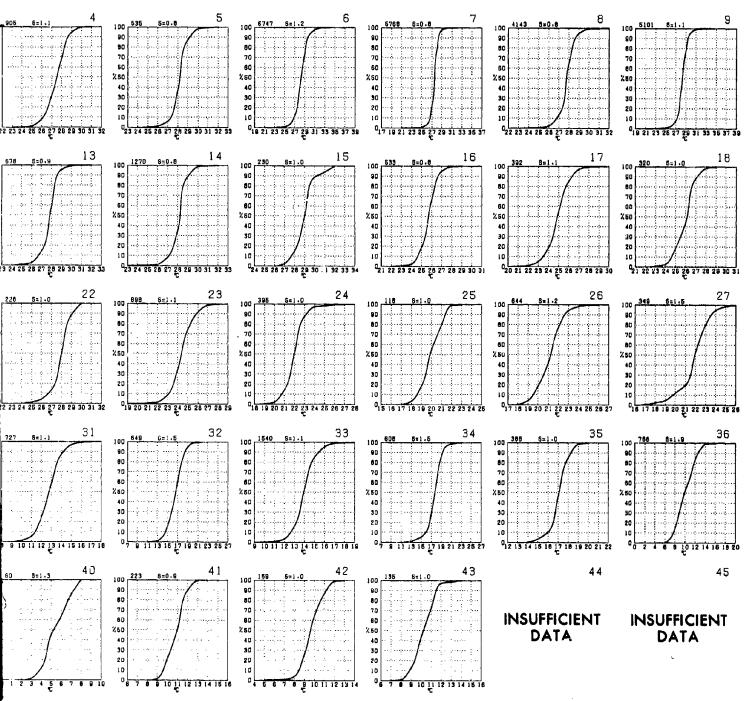
SEA SURFACE TEMPERATURE



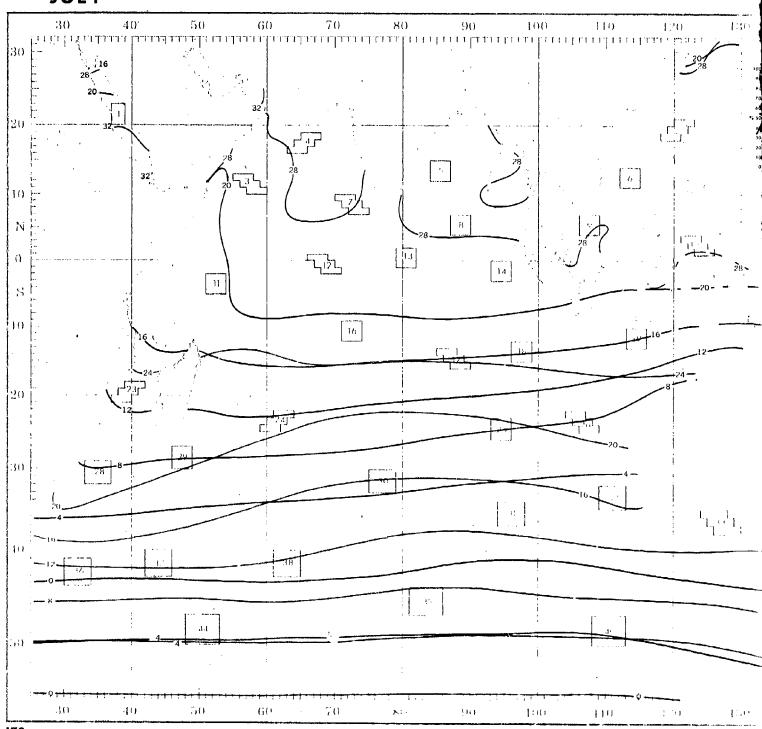
SEA SURFACE TEMPERATURE



Graphs represent the objective compilation of available data for specified areas without re The <u>Isopleth</u> analyses (apposite page) are based on all available data subjectively adjusted

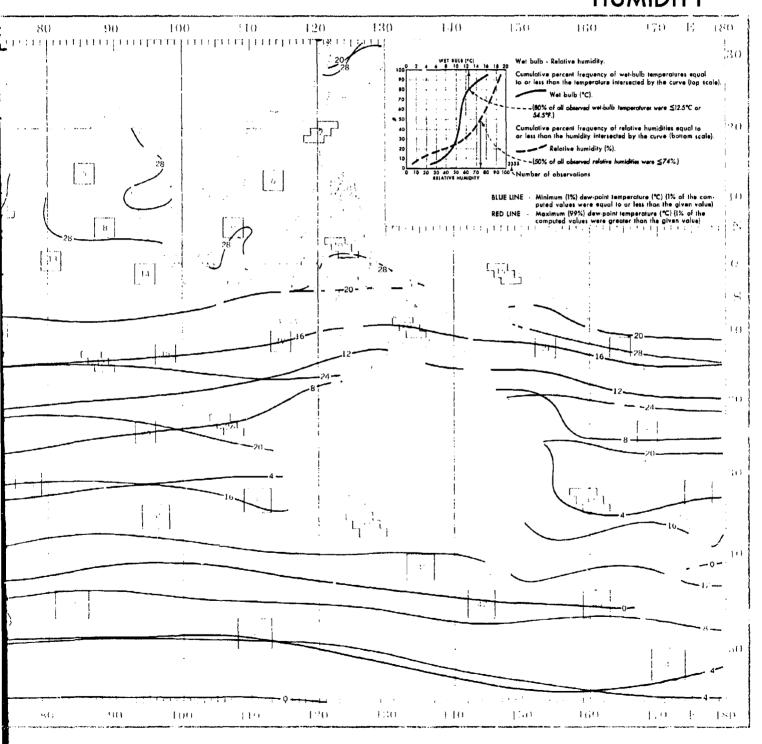


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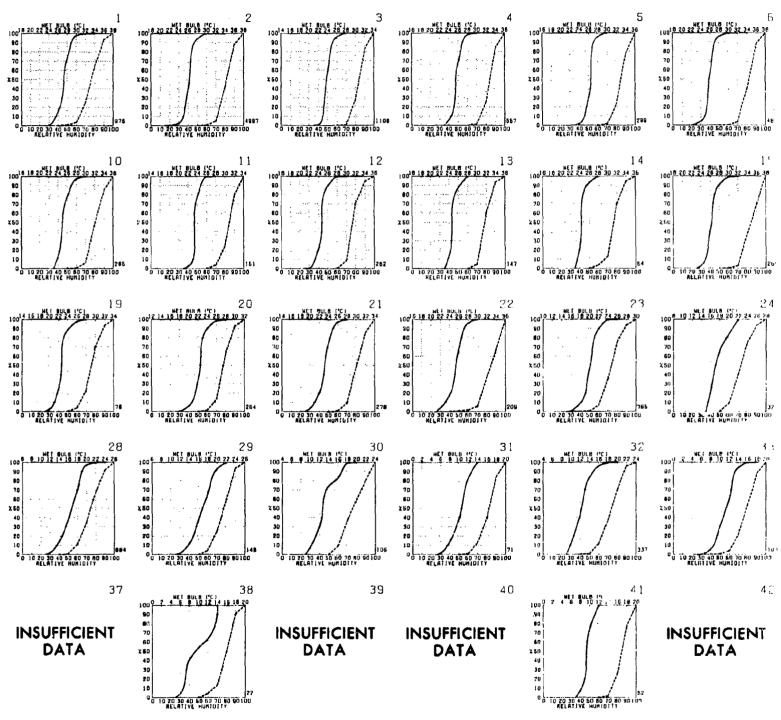


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HUMIDITY

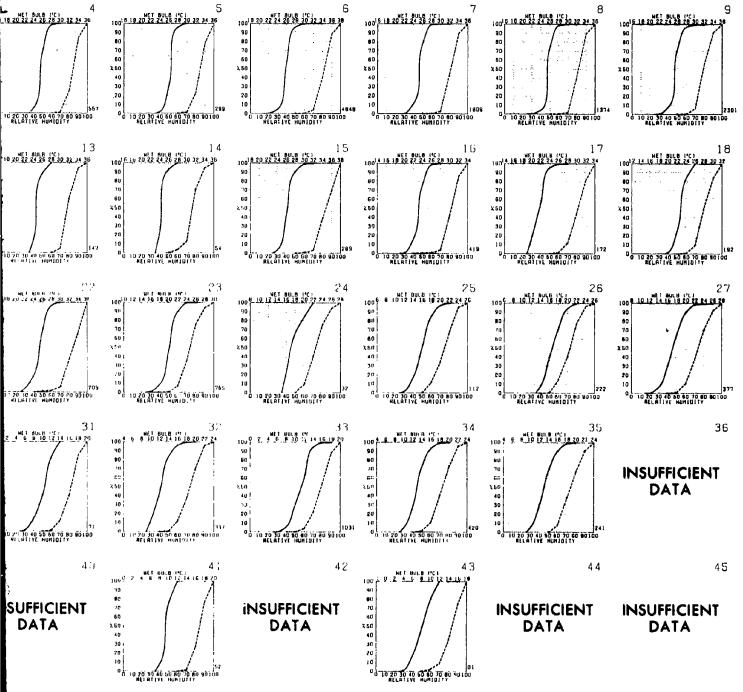


WET BULB AND RELATIVE HUMIDITY

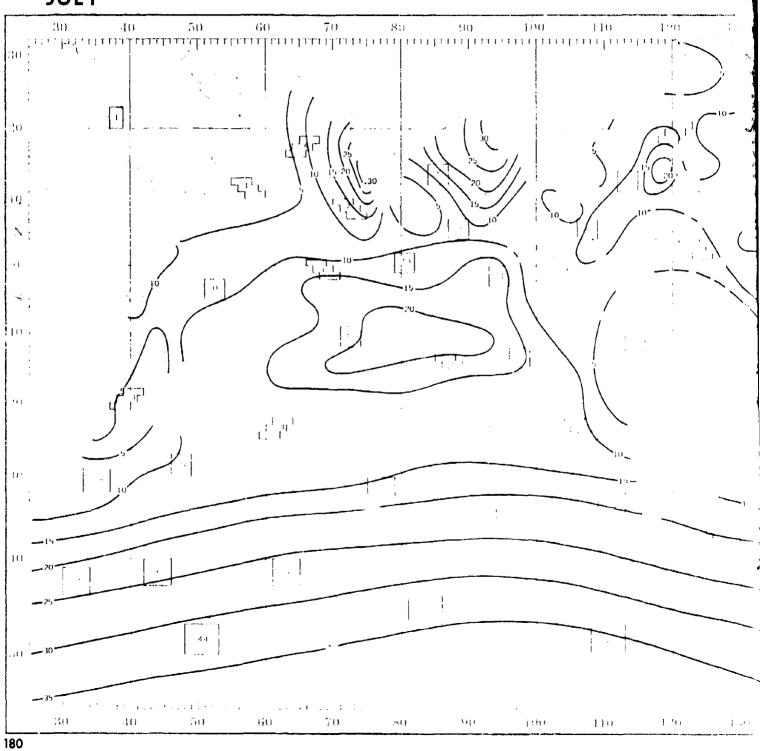


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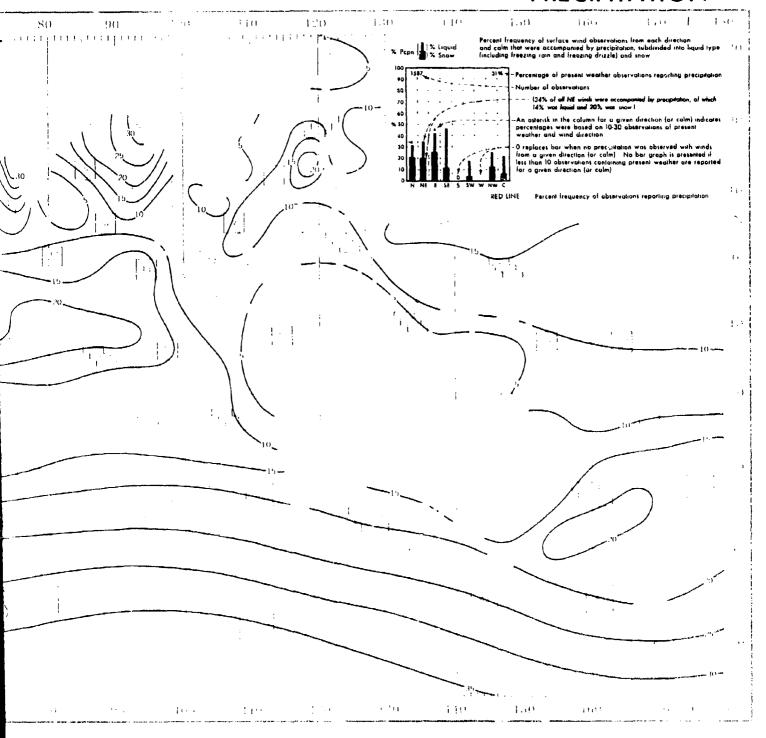
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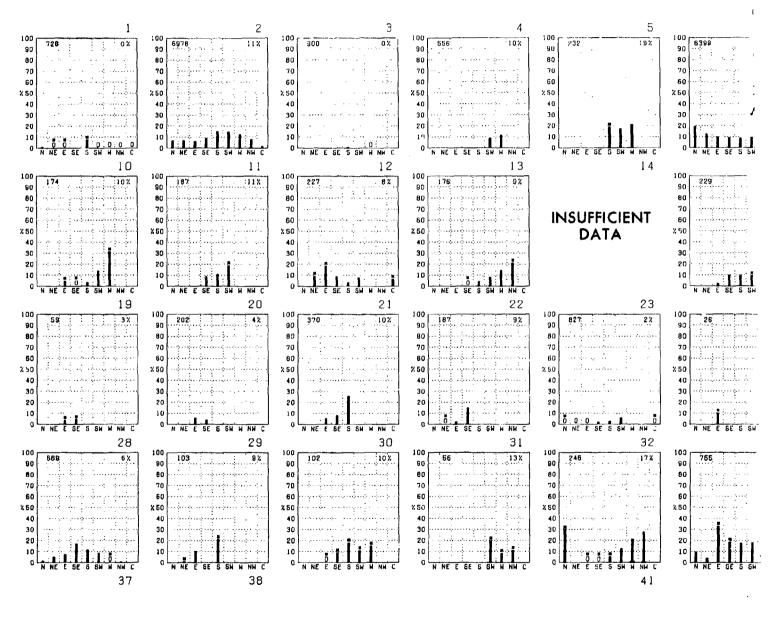
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PRECIPITATION



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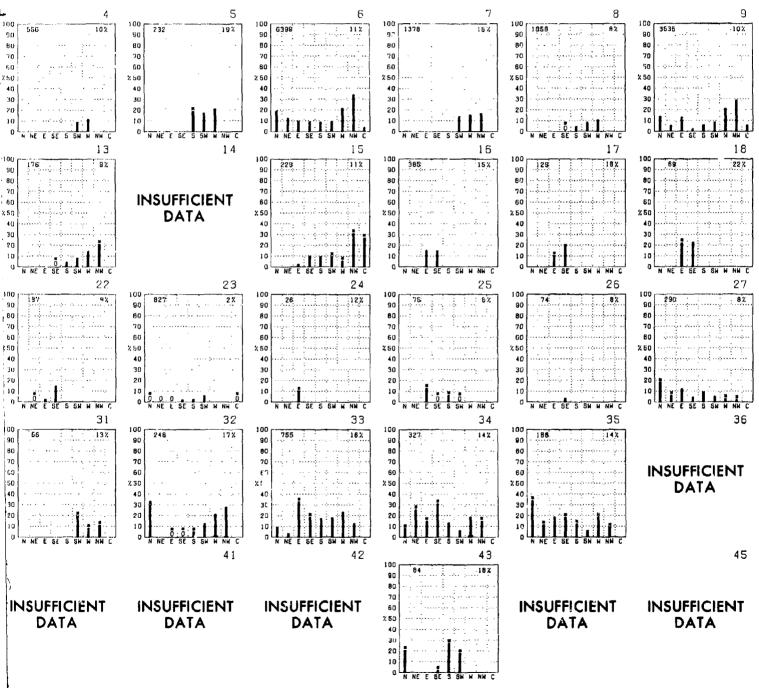
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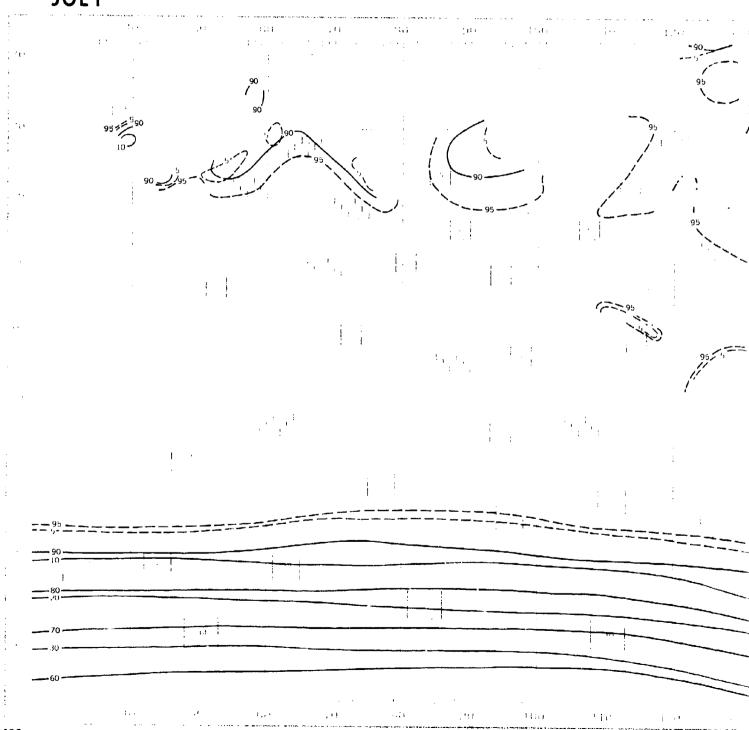
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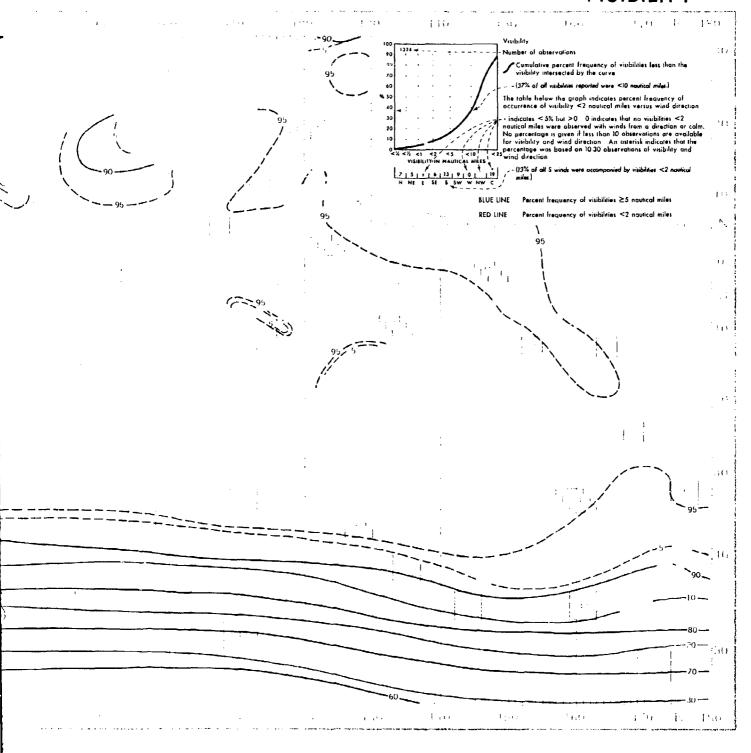
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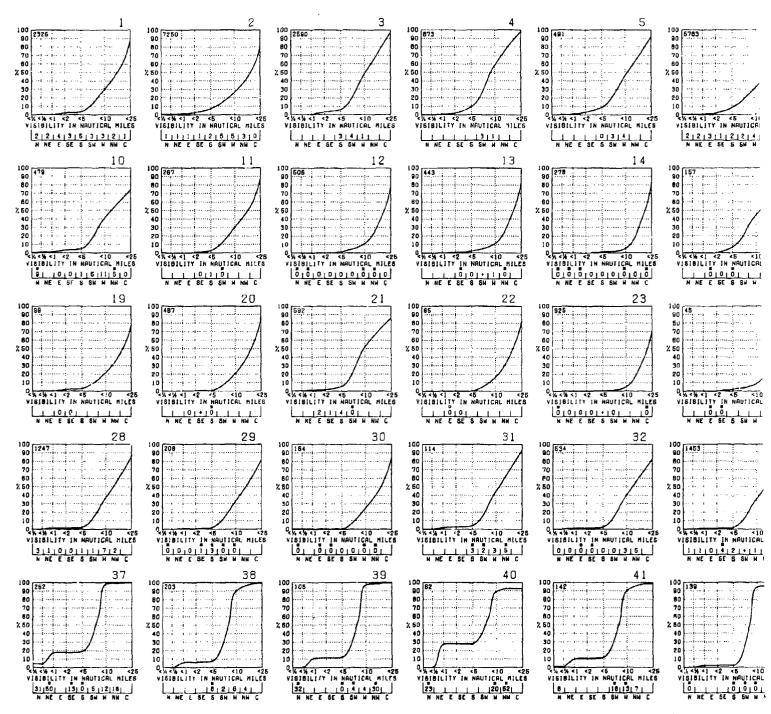
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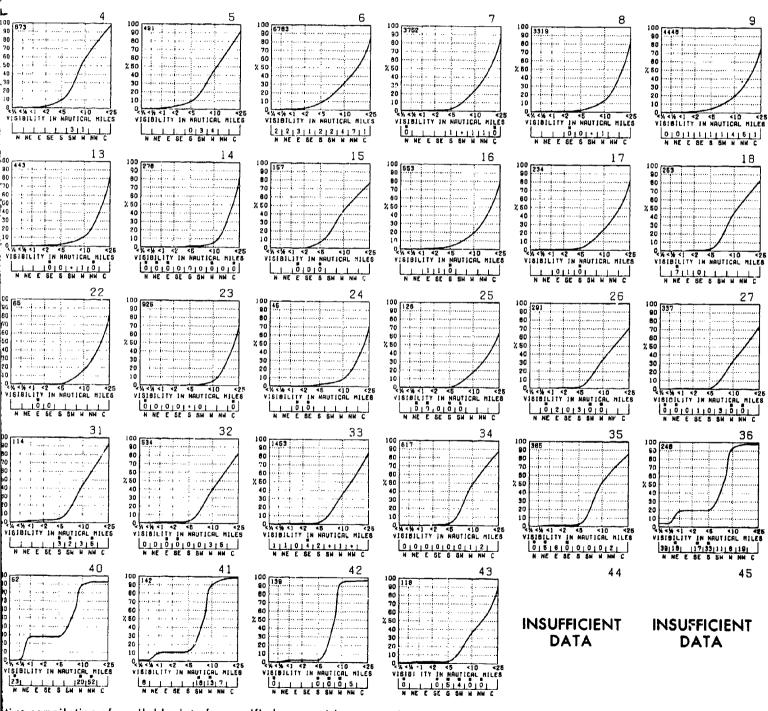
VISIBILITY



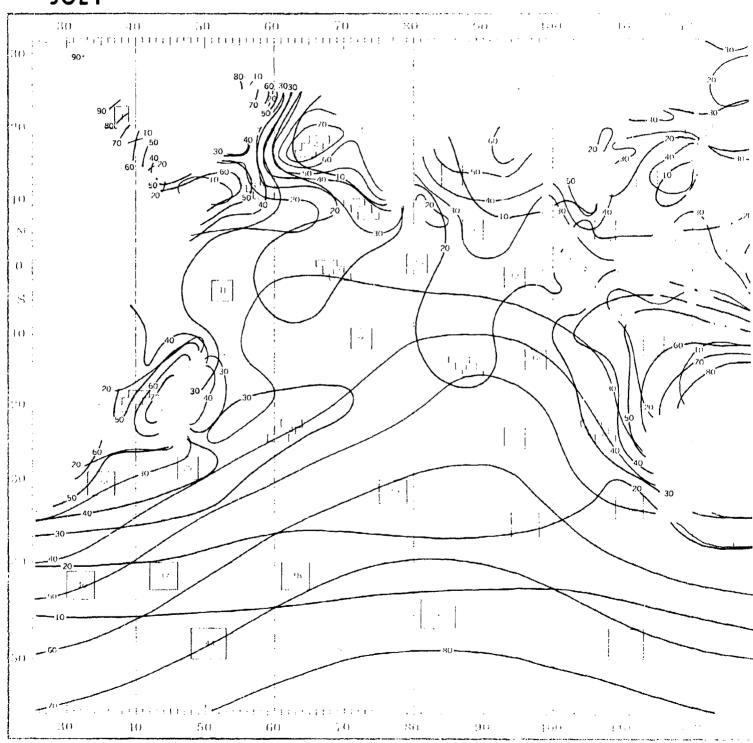
VISIBILITY



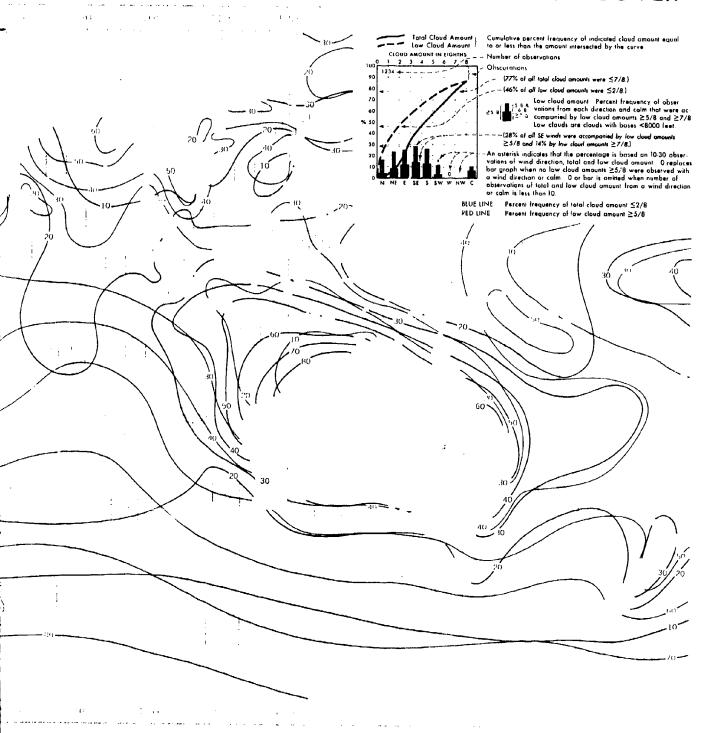
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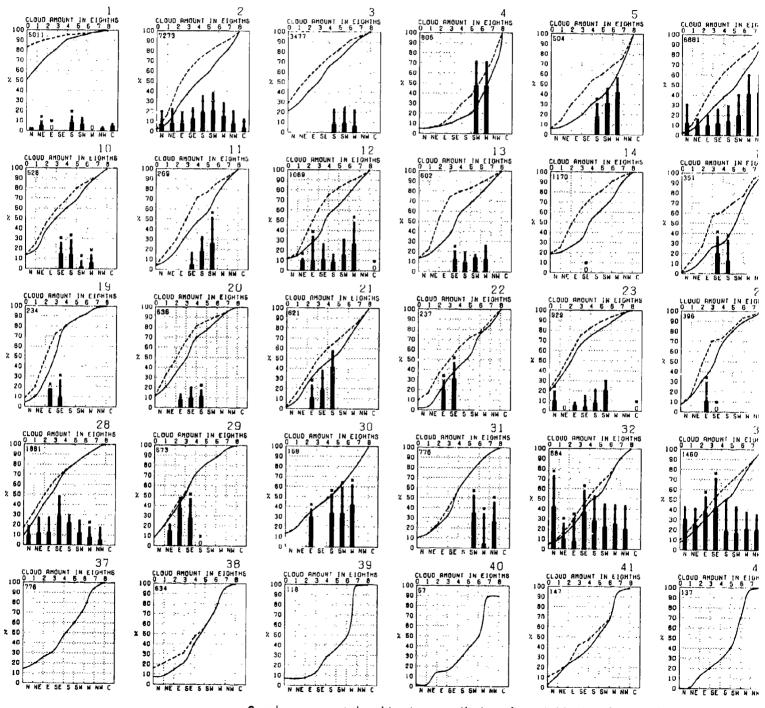
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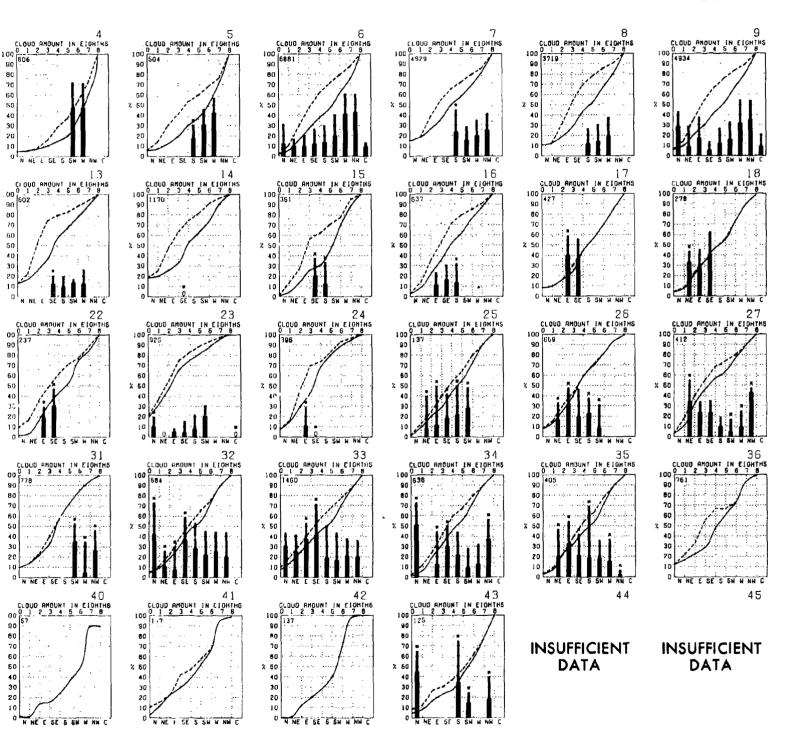
CLOUD COVER



CLOUD COVER

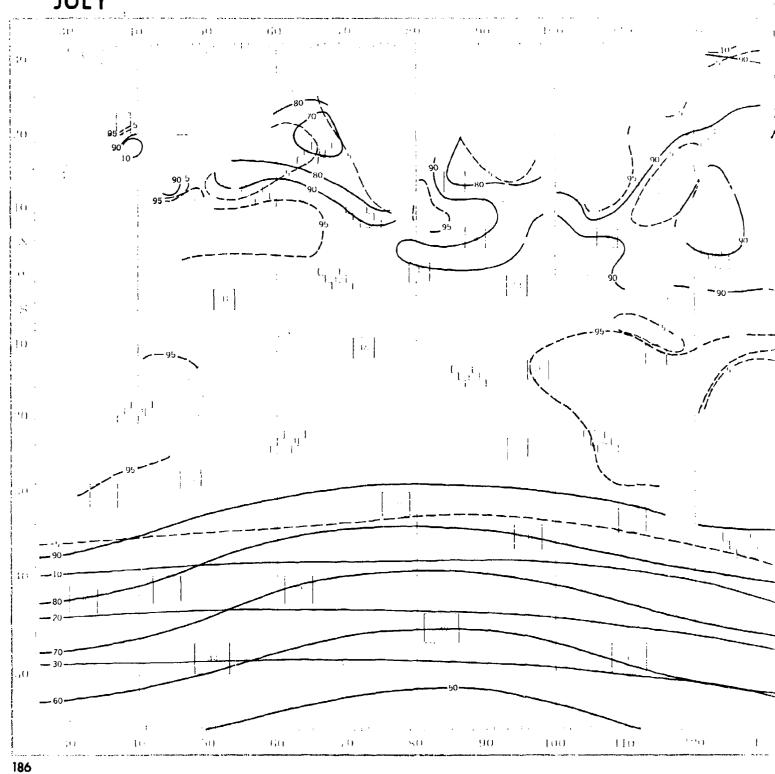


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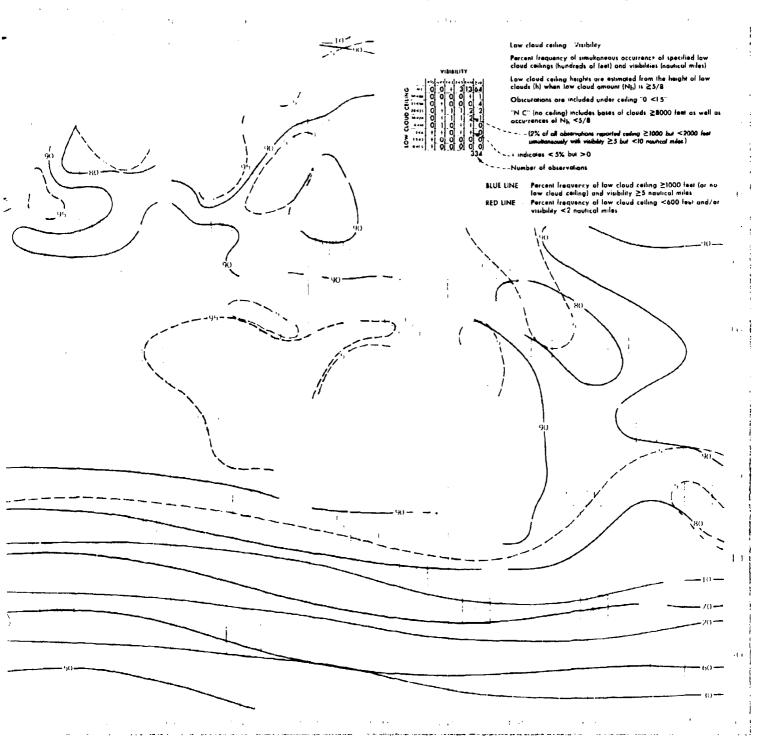


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CEILING AND VISIBILITY



CEILING AND VISIBILITY

VISIBILITY 1	VISIBILITY 4C 0 0 + 1 9 82 60-80 0 0 0 0 + + + 75-80 0 0 0 0 + + + 75-80 0 0 0 0 + + + 75-80 0 0 0 0 0 + + + 75-80 0 0 0 0 0 0 0 0 0 75-80 0 0 0 0 0 0 0 0 75-80 0 0 0 0 0 0 0 0 75-80 0 0 0 0 0 0 0 0 75-80 0 0 0 0 0 0 1 5 75-80 0 0 0 0 0 0 1 5 75-80 0 0 0 0 0 0 1 5 75-80 0 0 0 0 0 0 1 5 75-80 0 0 0 0 0 0 1 5 75-80 0 0 0 0 0 0 1 5 75-80 0 0 0 0 0 0 1 5 75-80 0 0 0 0 0 0 1 5 75-80 0 0 0 0 0 0 0 1 1 75-80 0 0 0 0 0 0 0 1 75-80 0 0 0 0 0 0 0 1 75-80 0 0 0 0 0 0 0 1 75-80 0 0 0 0 0 0 0 1 75-80 0 0 0 0 0 0 0 1 75-80 0 0 0 0 0 0 0 1 75-80 0 0 0 0 0 0 0 1	VISIBILITY 1-1/4 1/4 1-2 2-46 3-10 10 10 10 10 10 10 10	VISIBILITY 4 VISIBILITY ACC 0 0 0 0 2 11 17 SS-4F0 0 0 0 0 1 1 1 1 20-35 0 0 0 0 1 7 7 10-20 0 0 0 0 1 1 7 7 10-20 0 0 0 0 1 1 7 7 10-20 0 0 0 0 1 1 1 6 3-4R 0 0 0 0 2 12 10 3-4R 0 0 0 0 0 1 1 6 3-4R 0 0 0 0 0 1 1 6 3-4R 0 0 0 0 0 0 1 3-5C VISIBILITY 1-14 (7-2-11 1-2 2-2-5 5-2-10-10) NC 0 0 0 0 1 3 80 VISIBILITY 1-14 (7-2-11 1-2 2-2-5 5-2-10-10) NC 0 0 0 0 1 3 80 20-35 0 0 0 0 0 0 1 3-35 0 0 0 0 0 0 1 3-35 0 0 0 0 0 0 1 3-35 0 0 0 0 0 0 1 3-35 0 0 0 0 0 0 1 3-35 0 0 0 0 0 0 1 3-36 0 0 0 0 0 0 1 3-36 0 0 0 0 0 0 0 1 3-36 0 0 0 0 0 0 0 0 0-1.5 0 0 0 0 0 0 0 0	VISIBILITY 1-1/2 7/2 1-2 2-5 3-10 10 10 10 NC	VISIBILITY G
NC U U 0 0 2 75 80-80 0 0 0 0 0 0 4 10-40 0 0 0 0 0 0 14 10-40 0 0 0 0 0 0 14 10-40 0 0 0 0 0 0 0 14 10-41 0 0 0 0 0 0 0 0 0 10-41 0 0 0 0 0 0 0 0 0 10-41 0 0 0 0 0 0 0 0 0	V:SIBILITY -14 PAR-11-1-2 2-6 5-10-10 -10 0 0 0 0 4 78 -10 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 -10 0 0 0 0 0 0 -10 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	223 VISIBILITY -1/4 1/41 1/42 2/4 1/4 1/4 1/4 -1/4 1/41 1/42 2/4 1/4 1/4 1/4 -1/4 1/41 1/42 2/4 1/4 1/4 1/4 -1/4 1/41 1/4 1/4 1/4 1/4 -1/4 1/4 1/4 1/4 1/4 -1/4 1/4 1/4 1/4 -1/4 1/4 1/4 1/4 -1/4 1/4 1/4 1/4 -1/4 1/4 1/4 1/4 -1/4 1/4 -1/4 1/4	VISIBILITY VISIBILITY 1/4 6/4-11 1-2 2-6 8-10 1-10 NC 0 0 C 0 0 81 8-0-80 0 0 0 0 0 0 0 9 35-90 0 0 0 0 0 0 2 10-20 0 0 0 0 0 5 7 6-10 0 0 0 0 0 2 17 2 3-6 0 0 0 0 0 0 0 1-5-3 0 0 0 0 0 0 0 1-1-8 0 0 0 0 0 0 0	VISIBILITY 23 VISIBILITY AC 0 0 0 0 1 82 S0-80 0 0 0 0 0 0 2 3560 0 0 0 0 0 0 0 2 1020 0 0 0 0 0 0 0 40 0 0 0 0 0 0 0 40 0 0 0	*** **** **** **** **** **** **** **** ****
VISIBILITY 28 ***********************************	VISIBILITY -1/1	VISIBILITY 30 *** *	VISIBILITY 31 **I/R [V/41] 1-8 [F-8 3-10] 1:10 **MC	VISIBILITY 32	VISIBILITY 3 3
37	VISIBILITY 38 ***********************************	39	40	41	42

INSUFFICIENT DATA INSUFFICIENT DATA INSUFFICIENT DATA

INSUFFICIENT DATA INSUFFICIENT DATA

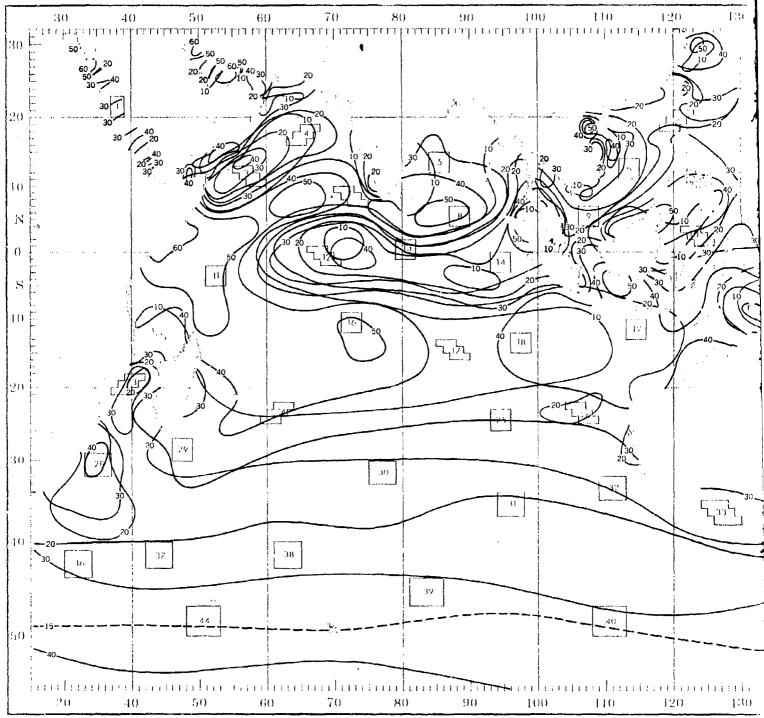
Graphs represent the objective compilation of available data for specified areas without re The isopleth analyses (opposite page) are based on all available data subjectively adjusted

JULY

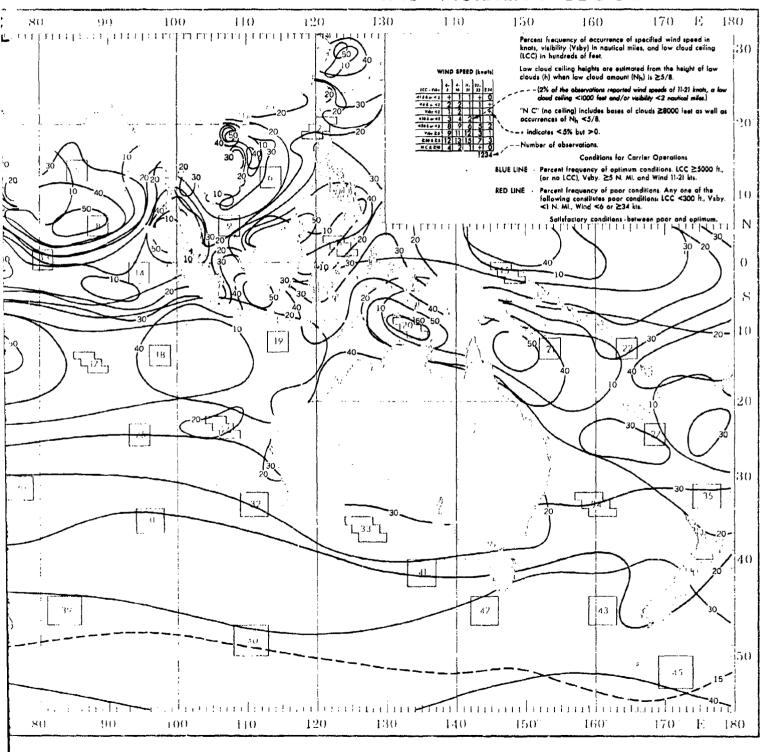
VISIBILITY -1/e	VI518ILITY 5 < ^1/2 ^1/4 1 1 2 2 5 5 10 3 0 MC	VISIBILITY <7/pre> <7/pre> <7/pre> <7/pre> <7/pre> <7/pre> <7/pre> <7/pre> <7/pre> <7/pre> <7/pre> <7/p> <7/p> <7/p> <7/p> <7/p> <7/p> <7/p>	VISIBILITY VISIBI	VISIBILITY c^1/2 f/cc 1 = 2 2 + 6 2 + 10 2 + 10	VISIBILITY VISIBILITY VISIBILITY NC 0 0 0 0 0 0 0 1 1 7 59 50-60 0 0 0 0 0 0 0 1 1 20-38 0 0 0 0 0 0 0 1 1 10-20 0 0 0 0 1 4 0 4-10 0 0 0 0 0 0 0 0 0 1 3-410 0 0 0 0 0 0 1 1 3-410 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
1 3 3 3 3 3 3 3 3 3	VISIBILITY	VISIBILITY VISIBILITY 15 NC 0 0 0 2 8 56 5040 0 0 0 0 0 0 0 38-60 0 0 0 0 0 0 0 39-60 0 0 0 0 0 0 39-60 0 0 0 0 0 6 4 39-60 0 0 0 0 0 6 2 10 45-60 0 0 0 0 0 0 6 45-60 0 0 0 0 0 0 0 45-60 0 0 0 0 0 0 0 45-60 0 0 0 0 0 0 0 45-60 0 0 0 0 0 0 0 45-60 0 0 0 0 0 0 0 45-60 0 0 0 0 0 0 0 45-60 0 0 0 0 0 0 0	VISIBILITY NC 0 0 0 1 4 68 Sec 0 0 0 0 0 1 4 68 Sec 0 0 0 0 0 0 1 4 Sec 0 0 0 0 0 1 4 Sec 0 0 0 0 0 0 1 4 Sec 0 0 0 0 0 0 1 4 Sec 0 0 0 0 0 0 0 1 4 Sec 0 0 0 0 0 0 0 1 5 Sec 0 0 0 0 0 0 0 1 5 Sec 0 0 0 0 0 0 1 5 6 Sec 0 0 0 0 0 0 0 0 0 0 Sec 0 0 0 0 0 0 0 0 0 Sec 0 0 0 0 0 0 0 0 0 0 Sec 0 0 0 0 0 0 0 0 0 0 0 Sec 0 0 0 0 0 0 0 0 0 0 0 Sec 0 0 0 0 0 0 0 0 0 0 0 Sec 0 0 0 0 0 0 0 0 0 0 0 Sec 0 0 0 0 0 0 0 0 0 0 0 0 Sec 0 0 0 0 0 0 0 0 0 0 0 0 Sec 0 0 0 0 0 0 0 0 0 0 0 0 0 Sec 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 Sec 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 Sec 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBIL IT 1 7 1 7 1 7 1 7 1 1	No. No.
VISIBILITY 22 1-1/2 1/2 1/2 1/2 2/5 5/10 1/0 NC 0 0 0 0 0 0 0 0 1 50-60 0 0 0 0 0 0 0 2 20-55 0 0 0 0 0 0 0 2 10-20 0 0 0 0 0 0 2 17 1 3-6 0 0 0 0 0 0 0 0 1 5-7 0 0 0 0 0 0 0 0 1 5-7 0 0 0 0 0 0 0 0 1 5-7 0 0 0 0 0 0 0 0 1 5-7 0 0 0 0 0 0 0 0 1 5-7 0 0 0 0 0 0 0 0 0 1 5-7 0 0 0 0 0 0 0 0 0 1 5-7 0 0 0 0 0 0 0 0 0 1 5-7 0 0 0 0 0 0 0 0 0	VISIBILITY 23	VISIBILITY 24 **C 0 0 0 0 0 0 73 **Sc-40 0 0 0 0 0 0 3 **Sp-40 0 0 0 0 0 0 3 **Desc 0 0 0 0 0 0 0 3 **Desc 0 0 0 0 0 0 0 3 **Desc 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 **Desc 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY 25	VISIBILITY 26 NC 0 0 0 0 0 1 58 5000 0 0 0 0 1 1 13 2035 0 0 0 0 1 1 13 2035 0 0 0 0 0 0 2 2 4 3-6 0 0 0 0 0 0 0 0 1.5-3 0 0 0 0 0 0 0 21.5-3 0 0 0 0 0 0 0 0 21.5-3 0 0 0 0 0 0 0 0	VISIBILITY 27
VISIBILITY 31	VISIBILITY 32	VISIBILITY 33	VISIBILITY 3 4 *** *** *** *** *** *** ***	VISICILITY 35	INSUFFICIENT DATA
INSUFFICIENT DATA	INSUFFICIENT DATA	INSUFFICIENT DATA	VISIBILITY 4 3	INSUFFICIENT DATA	INSUFFICIENT DATA

ctive compilation of available data for specified areas without regard to suspected biases.

sosite page) are based on all available data subjectively adjusted where bias was evident.



WIND-VISIBILITY-CLOUDINESS



LOW CLOUD CEILING-VISIBILITY-WIND

(1)

1	2	3	4 HIND SPEED (KNOTS)	5 WIND SPEED (KNOTS)	WIND SP
WIND SPEED (FNOTS) 0- 4- 11- 22-	HIND SPEED (KNOTS) LCC - YARY 3 10 21 33 834	WIND SPEED (KNOTS) LCC - V887 0- 4- 11- 22-	LCC - V887 5 10 21 33 +34	LCC V3RT 1 10 21 33 234	LCC - YSBY 3 0-
<1.5408<-5 0 0 D O O	<1.84 DR <.8 + + + + +	c).640x c.6 0 0 + 0 +	41.5 4 OR 4.5 0 0 + 0	<1.5 4 dR <.5 0 0 1 0 0	*1.5 4 DH *.E
<€ € 0R <2 0 + 0 0 0	<6 t OR <2 + 1 2 1 +	-8 4 OR <2 G D + 0 1	46 4 OH 47 G D 1 2 1	-B 4 OR -? O + 2 2 +	464 Ox +2 +
Y88Y <2 0 + 0 0 0 0	Y88Y *2 + 1 , 1 + + + + + + + + + + + + + + + +	YSBY 42 0 0 0 0 →	VSBY -2 0 0 0 + 0	V687 <2 () + 1 1 +	V68Y *?
<20 & OR <5 + 1 + 0 0	<20 4 GR <5 1 8 10 4 1	<20 4 OR 45 0 0 1 9 4	120 4 UR 15 0 1 17 27 5	420 4 DR 4	*20 4 OR *5
89 48 15 53 29 1 0	v68Y a6 9 47 32 5 + a 50 4 a6 8 38 22 3 +	- v66x +5 0 + 11 63 23 - a50 4 a5 0 + 9 51 18	v581 a5 0 3 33 47 9 a50 4 a6 U 2 12 14 2	V68T a5 + 11 54 22 2	V587 45 G
HC 4 > 10 13 48 24 1 0	NC 4 # 10 7 34 18 2 +	HC 4 > 10 0 + 8 32 10	NC 4 2 10 0 1 9 7 1	NC 4 a 10 + 8 27 5 1	HC 4 > 10 4
698	6042	876	528	236	
10 HIND SPEED (KNOTS)	l l HIND SPEED (KNDTS)	12 Wind Speed (Kndts)	13 NINO BPEED (KNOTS)	1 4.	HIND SPI
CCC - VANY 3 10 21 33 894	LCC - YEST 0- 4- 11- 22- 35 234	UCC - YBBY 3 10 21 33 434	LCC - VARY 9 10 21 30 354	LCC - V88Y 3 10 21 33 334	LCC - YERY 3
-1.84 DR 8 0 0 0 0 0	<1.8 4 GR <18 0 0 1 0 0	<1.84 OR <.8 0 0 0 0 0	41.5 4 OR 4.5 D D D D D	41.5 L OR 4.5 0 0 0 0 0	<1.5 4 OR5 0
484 08 42 2 3 2 0 D	48 4 0R 42 0 0 3 0 0	48 4 OR 42 0 + 0 0 0	*8 L OR *2 0 0 0 0 0	48 4 0R 42 0 0 0 0 0	<8 4 DA <7 U
*10 4 OR *E 2 8 2 0 D	4887 42 0 0 1 0 0	Y887 42 0 0 0 0 0 0 0	*48Y *2 0 0 0 0 0 0 0 410 4 0R *2 0 0 1 0 0	VABY <2 0 0 0 0 0 0	V88Y <2 ()
420 4 DR 48 3 11 5 0 D	<20 4 OR <5 1 2 14 2 0	<20 4 OR <8 1 8 4 0 0	-20 4 OR -5 7 5 0 0	420 4 OR 45 0 10 4 2 0	<20 4 OR <5 10
V49Y 95 16 61 22 0 D	V68Y 26 2 25 68 3 0	V48Y aB 18 63 18 0 0	V88Y AU 7 51 30 0 0	VSSY 36 25 54 19 0 0	V8BY ≥5 17 ≥50 4 ≥ 5 10
HC 4 a 10 11 47 17 0 0	NC 4 + 10 2 17 39 2 0	HC 4 = 10 16 46 13 0 0	MC 4 a 10 5 52 22 0 0	MC 4 2 10 25 35 15 0 0	NC 4 = 10 8
54	159	219	149	48	
19 WIND SPEED (KNOTS)	20 Nino speed (Hnots)	21 HIND SPEED (KNOTS)	22 WIND SPEED (KNOTS)	23 HIND SPEED (KNOTS)	HIND SPE
LCC - VSSY 3 10 21 33 334	LCC - V88Y 0- 4- 11- 28- 3 10 23 33 234	LCC - VSBY 0- 4- 11- 22- 354	LCC - YANY 9 10 21 39 294	LCC - YERY 0- 4- 11- 22- 33 234	LCC - V887 0-
<1.54 0R <.s 0 0 0 0 0	<1.1 4 0H < .E 0 0 0 0 D	<1-84 OR <-B D D D + D	41.54 GR 4.5 0 0 0 0 0	41.84 OF 4.5 0 0 0 0 0	<1.54 DR <.5 0
484 OR 42 D D D D D D D D D	*8 4 0R <2 0 0 + 0 0	48 4 DR 42 0 0 2 2 0	464 DR 42 0 0 0 0 0 0 0 V8BY 42 0 0 0 0 0 0	*6 4 OR *2	46 4 0F <2 0
410 4 0R 42 D O 2 O O	<10 t 08 45 0 0 8 + 0	410 4 DR 42 0 0 8 6 D	<10 A OR <2 0 0 B 10 0	<10 4 0R <2 0 1 3 · 0	<10 4 OR <2 0
420 4 OR 45 U 8 10 0 0 VSST 25 D 35 63 2 0	420 4 0R 45 0 0 15 1 0 VSSY 35 0 16 77 7 0	480 4 0R 4B 0 2 23 8 0	420 4 GR 45 0 0 18 13 0 VERY 25 5 33 44 18 0	420 4 0R 46 1 4 5 1 0	420 4 OR 45 D
250 4 25 0 29 47 0 0	380 4 a6 0 15 60 6 0	280 428 + 8 39 12 0	280 428 5 33 21 5 0	2 50 4 26 11 48 20 4 +	3 \$0 4 3 6 D
MC 4 = 10 0 29 45 0 0	MC 4 3 10 0 15 58 5 0	MC4210 + 9 32 8 0	MC 4 ± 10 5 33 21 E 0	MC 4 2 10 11 4B 20 4 +	MC 4 a 10 D
28	29	30	31	32	
HIND SPEED [KNOTS]	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPE
LCC - Y88Y 3 10 21 23 434	LCC - VARY 3 10 21 33 254	LCC - Y88Y 0- 4- 11- 22- 3 10 21 33 454	LCC - VSBY 3 10 21 33 834	LCC - YERY 5 10 21 33 a51	LCC - V68Y 3
41.84 98 4.8 0 0 0 0 0 0	41.8 4.08 4.8 0 0 0 0 0 0	4).6 4 DR 4.8 D D D D D	<1.5 LOR <.8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	<1.840R <.5 0 0 0 0 0 0 <	<) -B 4 GR < -B D
Y88Y 42 0 0 0 0 0	Y887 42 0 0 0 0 0	V887 42 0 0 0 0 0	V667 45 0 0 0 0 0	V687 <2 0 + 0 + +	v487 -2 0
410 4 0R 42 + 1 3 1 + 420 4 0R 46 1 4 D 3 +	410 4 0R 42 0 3 10 2 0	410 4 98 48 0 8 22 1 0	<10 4 0R =2 0 0 2 5 0	<10 s OR <2 1 3 1 4 2 	410 & GR 42 .
420 4 0R 46 1 4 B 3 + Y80Y 26 4 32 48 14 1	420 4 0R 48 0 7 14 2 0	420 4 0R 48 0 8 22 1 0	-20 4 SR -8 0 3 16 10 2 	*20 & OR *5 2 7 8 8 5 *287 *5 3 28 31 27 7	<20 4 GR 45 1 YEST 25 2 2
a 50 4 a 5 3 25 37 10 1	1 19 39 10 0	250 425 3 29 19 2 0	-50 4 25 0 13 27 19 0	250 485 1 15 19 17 3	260 & a5]]
#C 4 ≥ 10 3 23 35 9 1 837	MC & a 10 1 18 37 10 0	MC 4 a 10 2 27 18 2 0	MC 6 2 10 0 13 27 18 U	#C4+10 1 13 17 15 3	HC 4 2 10 1 1
37	38	39	40	4 1	
	MIND SPEED (KNOTS)			WIND SPEED (KNOTS)	
	CCC - Y48Y 9 10 21 33 234			1.5 LOR 4.8 0 0 0 0 0	
INSUFFICIENT	46 4 DR 42 D D D D E	INSUFFICIENT	INSUFFICIENT	-8 4 6# =2 0 0 0 0 0	INSUFFIC
DATA	VSDT 42 0 0 0 0 0	DATA	DATA	V88Y <2 0 0 0 0 0	DAT
PAIA	<10 4 0R <2 0 0 D B 12 <20 4 0R <8 0 0 B 24 12	DAIA	PAIA	<20 4 08 48 0 7 29 7 0	UAI
	V48Y AS 0 6 24 53 6			VBBY as 0 21 36 29 0	
	850 6 8			280 4 25 0 14 14 21 0 MC 4 2 10 0 14 14 21 0	

<u>Graphs</u> represent the objective compilation of available data for specified areas wi The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively

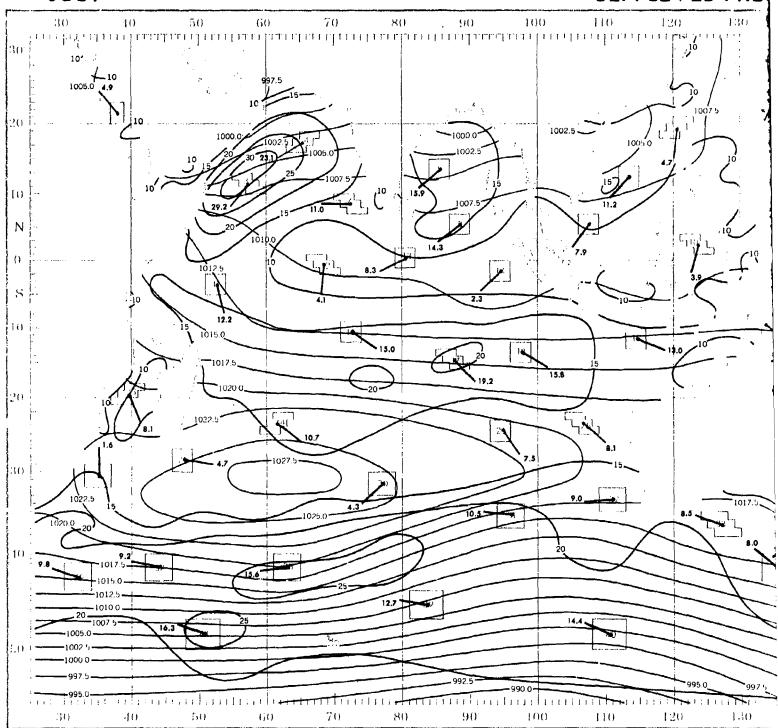
TY-WIND

JULY

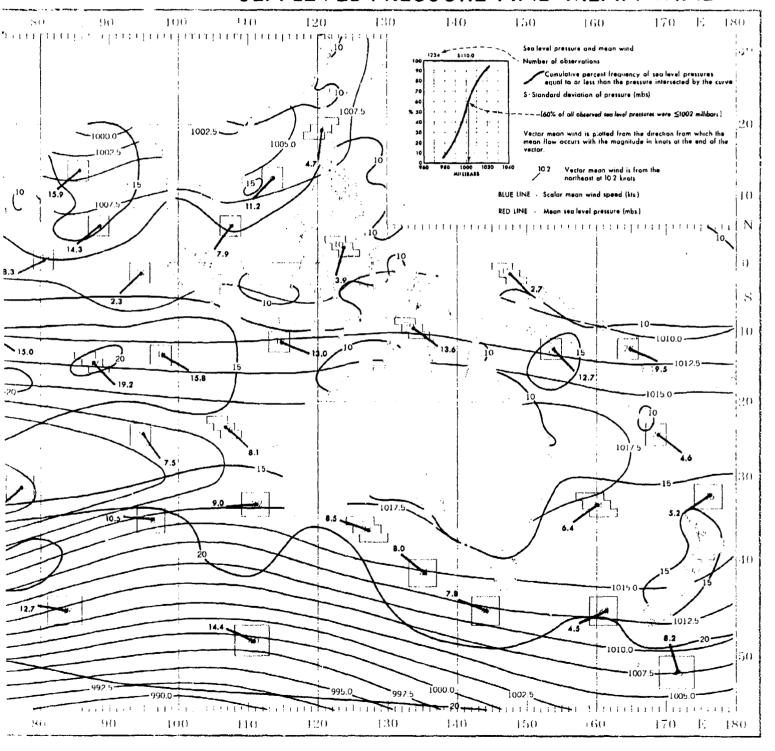
<u>_</u>	4	5	6	7	8	9
,	WIND SPEED (KNOTS)	HINO SPEED (KNOTS)	WIND SPEED IXNOTES	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	WIND RPEED (KNOTS)
166 - V88	7 3 10 25 33 234	LCC - VSBY 0- 7- 11- 22- 33 234	LCC - Y88Y 0- 4- 15- 22+ 3 10 21 33 234	LCC - VSOY 3 10 21 33 434	LCC - VSBY 3 10 21 33 234	LCC - VBSY 9 10 21 39 134
11-5 4 OR 4 .1		*1.540X *.6 U 0 1 U 0	<1.54 UR <.5 + + 1 + 4	41-54084.5 U U + 0	<1.5 4 OR 4.6 D D + + D	-1.54 OR <.5 0 + + + 0
'6 4 OF 4	2 0 0 1 2 1	48 £ 98 47 0 + 2 2 +	464 DR +2 + 1 3 1 +	48 4 OK 42 0 + 1 + 0	<8 4 OR <2 0 + 1 1 0	48 4 00 42 + 1 2 + 0
VS81 43	2 G O O + O	ARBA -5 () + 1 1 +	Y887 *7	Y88Y 42 U + + O	V58Y -2 D + + + D	YBBY <2 + + 1 + 0
* - 10 L OR +	7 0 1 8 12 3	<10 4 0R <2 0 1 8 3 1	<10 4 OR <2 + 4 8 3 +	<10 4 dR 42 0 1 6 1 +	10 4 0# 12 D 1 6 1 0	<10 4 0R <2 + 4 6 1 0
*70 & OR *1		*20 t 0# -5 0 4 16 15 2	-20 & OR -5 1 9 17 7 +	420 4 GR 45 + 3 15 3 +	420 4 0R 45 D 3 15 3 +	<20 4 98 56 1 11 12 1 +
vSit v at		¥887 ≥6 + 11 54 22 2	V887 25 6 33 41 11 +	Y88Y 25 31 60 5 +	v681 ≥5 + 19 70 9 •	VAAY 25 9 49 36 2 0
3 50 4 a		450 4 ab + 9 34 8 2	250 426 5 25 25 5 +	a50 4 a5 25 38 2 +	250 4 28 + 15 49 5 +	250 4 25 8 35 23 1 0
HC 4 > 10	0 0 1 9 7 1	NC 4 + 10 + 8 27 6 1 236	NC 4 ≯ 10 4 22 20 3 + 5552	HC 6 2 10 1 23 35 2 +	HC4210 + 14 46 5 0	NC4 & 10 7 32 20 1 0
	13	14	15	11)	17	18 WIND SPEED (KNOTS)
	NIND SPEED (KNOTS)	WIND SPEED (MNOTS)	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	
TEC - 489		LCC - VBBY 3 10 21 33 294	LCC - VERT 3 10 21 33 a34	LEC - V88Y 3 10 21 55 R34	LCC - V68Y 9 10 21 99 a34	LCC - Y88Y 3 10 21 33 834
1.5 4 0# •		41.5 4 DR 4.5 D D O O D	<1.5 L OR = .5 0 0 0 0 0	*1.540R <.6 0 0 0 0 0	«1.5 A OR «.6 O O O 1 O	<1.5 4 OR <.5 0 0 0 0 0
-6 & OF 4		-84 DR -2 G G O O D	-8 4 OR -2 0 0 0 0 0	<6 4 OR <2 0 0 + 1 0	48 4 OR 42 0 1 3 1 0	48 4 00 4 Z O O O O O
V687 -		*10 4 0K *7 0 2 2 2 0	VBBY 42 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VBBY <2 0 0 + 1 0	VABY 42 0 0 0 1 0	V6BY <2
470 4 OR 4		480 4 8R 46 0 10 4 2 0	-20 4 DR -5 10 10 6 0 D	<20 4 OR <5 0 1 14 5 0	420 4 0R 45 D 4 20 14 D	-20 4 0R -5 1 2 10 10 0
V881 at		VARY 25 25 54 19 0 0	V887 35 17 58 17 0 0	V48Y a5 + 16 67 13 0	VSBY 26 0 13 58 28 1	VSSY 35 3 22 50 25 1
A 50 4 2		» 50 4 » 5 25 30 15 0 0	450 415 10 44 8 0 0	2 50 6 25 + 14 49 9 0	ESO 4.8 0 8 30 8 1	a Str 4 a S 1 16 25 5 1
NE & & 1		MC4 # 10 25 35 15 0 0	NC 4 2 10 8 40 8 0 0	NC 4 > 10 + 13 47 8 0	HC 4 2 10 0 B 2B 5 1	MC 4 a 10 1 15 24 4 1
	149	48	48	383	156	105
	22	23	24	25	26	27
. 1	HIND SPEED (KNOTS)	KIND SPEED (KNOTS)	WIND SPEED (KNOTS)	WIND GPEED (KNOTS)	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)
LCC - V88	Y 3 10 21 33 a34	LCC - V88Y 0- 4- 11- 22-	LCC - YERY 3 10 21 33 234	LCC - Y887 3 10 21 33 334	LCC - YSSY 3 10 21 39 234	LCC - VARY 3 10 81 33 384
1.5 4 OR «.		*1.540R *.5 0 0 0 0 0	41.6 4 DR < . 6 0 0 0 0 0	*1.5 4 OR *.5 0 0 0 0 0	41.6 6 OF 4.8 O O O O O	41.84 08 4.8 0 1 0 0 0
48 6 0A 4	2 0 0 0 0	46 4 GM 42 D + + O O	48 4 0R 42 D O O O O	<84 OF <2 0 0 1 0 0	0 0 0 0 9 NO 1 P>	48 £ 0R 48 0 2 1 1 0
Y68Y 4		Y88Y -Z 0 + 0 0 0	VBBY 42 0 0 0 0 0	V687 <2 G O O O O	ABBA 45 0 0 0 0 0	V88V 4Z 0 0 0 0 0
<10 4 OF 4		<10 4 0F <2 0 1 3 + 0	<10 4 OR -2 0 0 3 3 0	<10 & DR <2 0 3 5 0 1	<10 4 dR <2 1 D 1 C 0	410 4 08 48 1 3 4 2 0
420 4 0# 4 V581 a		<20 4 08 <8 1 4 5 1 0	420 4 9R 46 0 7 10 3 0	<20 4 DR <6 1 9 14 1 1 1 1 1 20 4 20 4 20 4 20 4 20 4 2	420 4 0R 45 1 3 5 1 0 ¥887 ≥5 4 43 49 4 0	420 4 08 46 2 7 9 4 0
4 50 4 a		>50 4 >8 1 48 20 4 +	280 425 0 17 60 20 0	v887 a5 3 40 49 5 2 a50 4 a5 2 22 30 1 1	veev as 4 43 49 4 0 a 50 4 a 5 3 32 24 1 0	vsev as 5 25 58 11 1 as0 4 as 3 15 43 7 1
NE 4 4 1		MC 4 2 10 11 4B 20 4 ·	MC 4 2 10 0 10 50 13 0	HC 4 & 10 2 22 30 0 0	MC 4 2 10 3 30 24 1 0	MC 4 = 10 3 14 43 7 0
	38	772	30	67	148	197
li	31	32 ·	33	34	35	36
	WIND BPEED (KNOTS)	WIND SPEED LKNOTSJ	WIND SPEED (KNOTS)	NIND SPEED (KNOTS)	WIND SPEED (KNOTS)	
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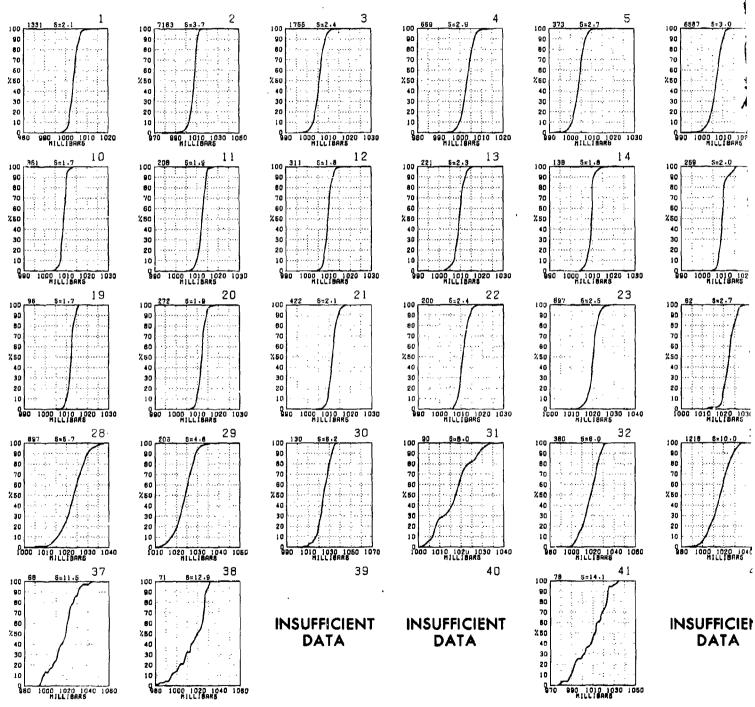
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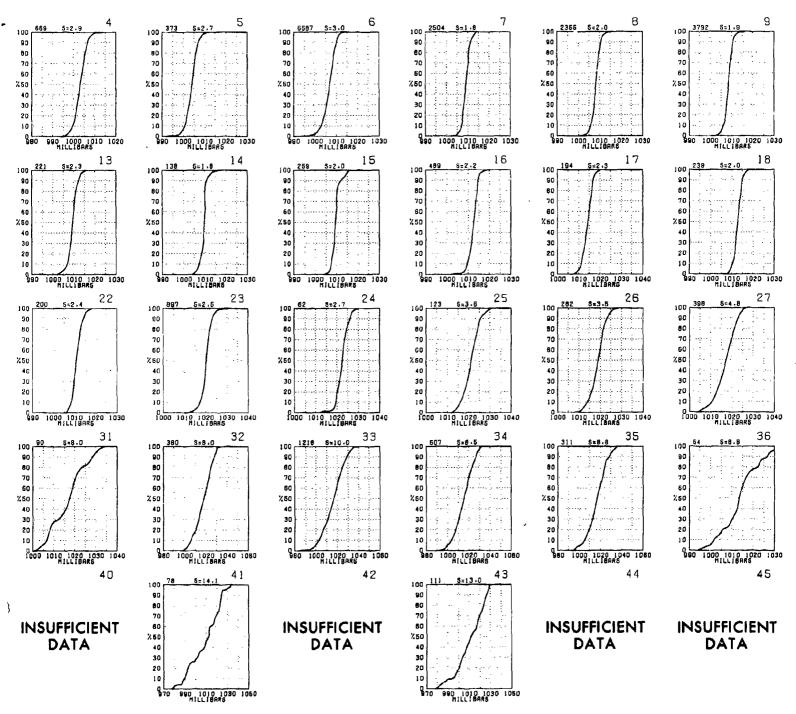


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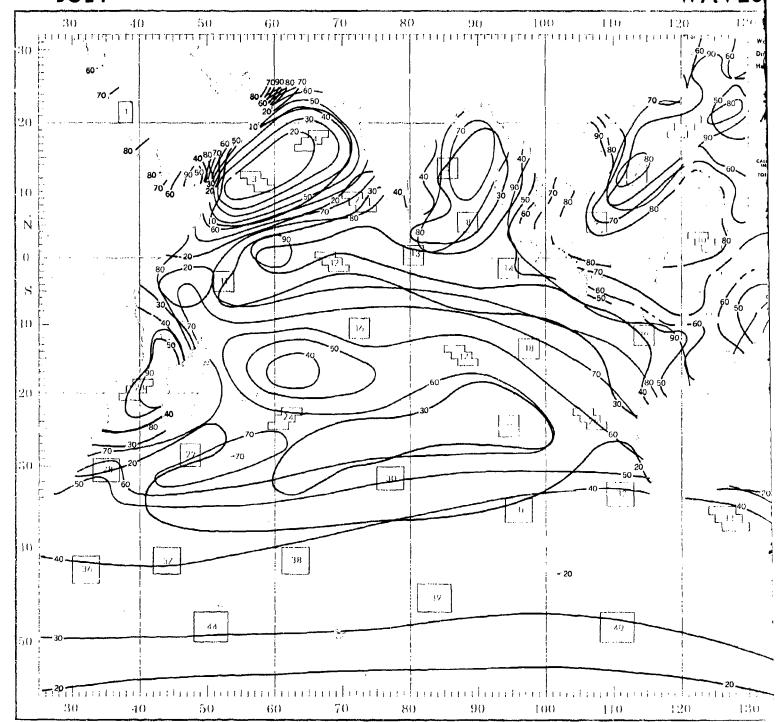
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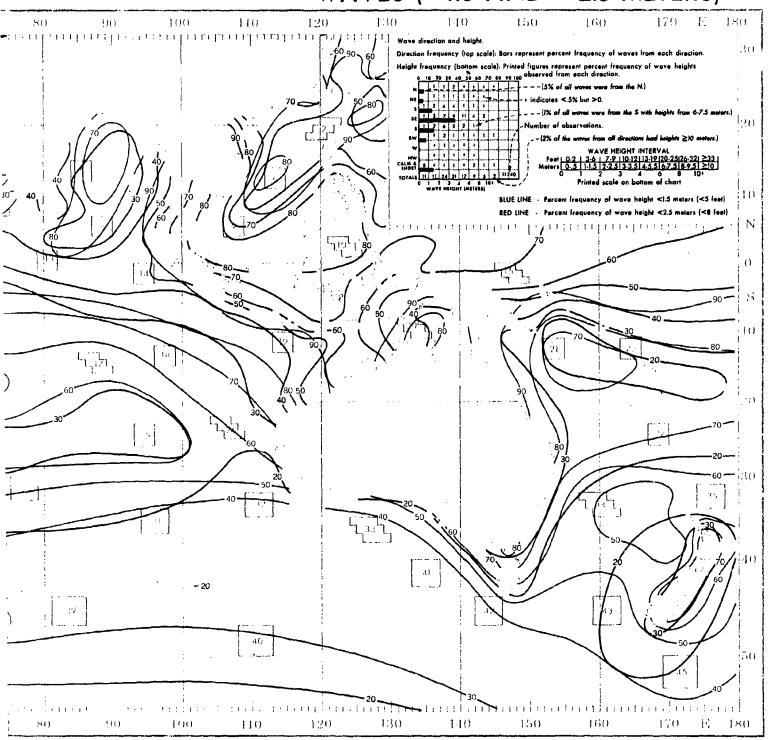


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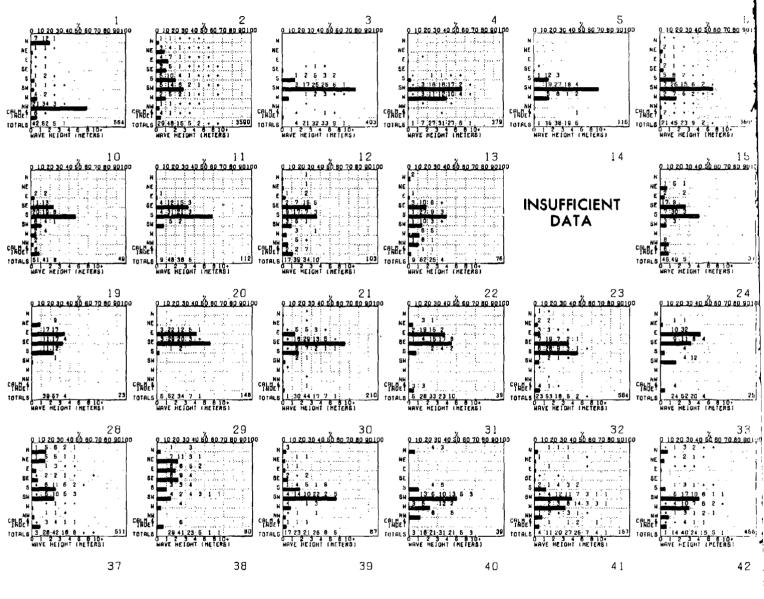
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WAVES (<1.5 AND <2.5 METERS)



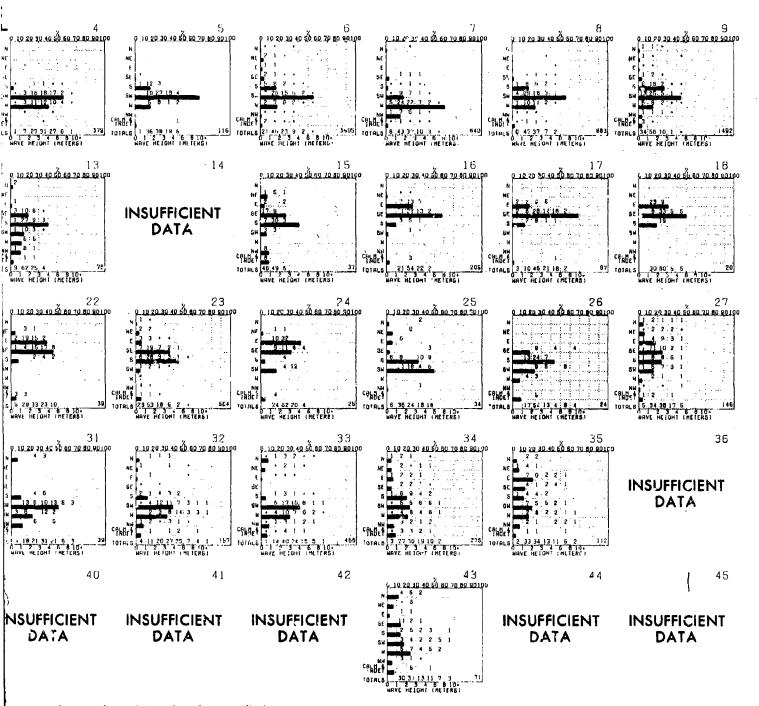
WAVE DIRECTION AND HEIGHT



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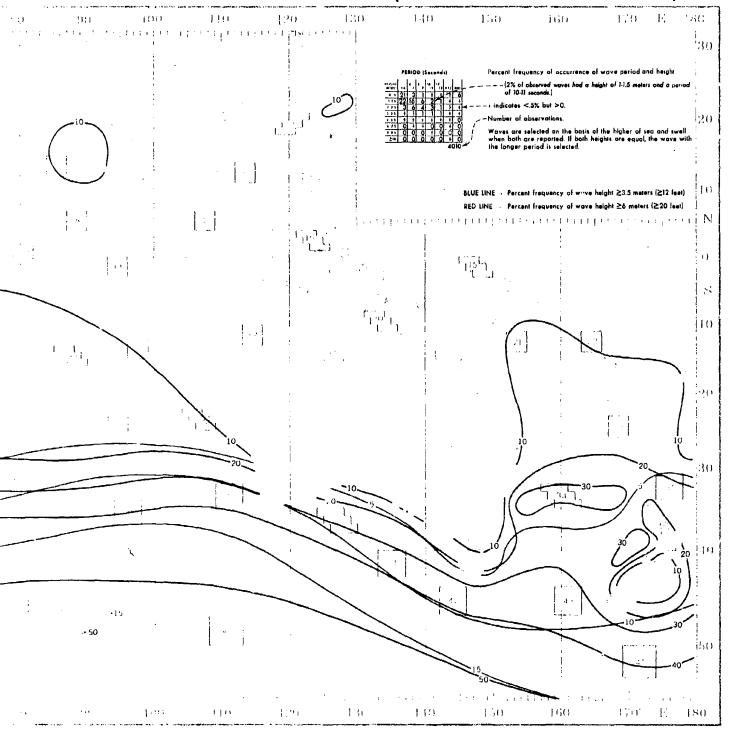
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WAVES (≥3.5 AND ≥6 METERS)



WAVE PERIOD AND HEIGHT

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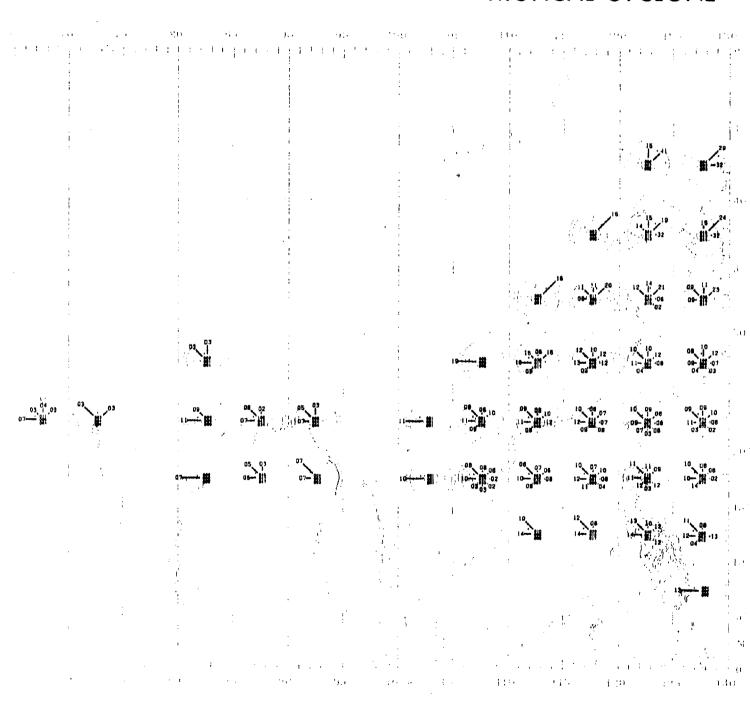
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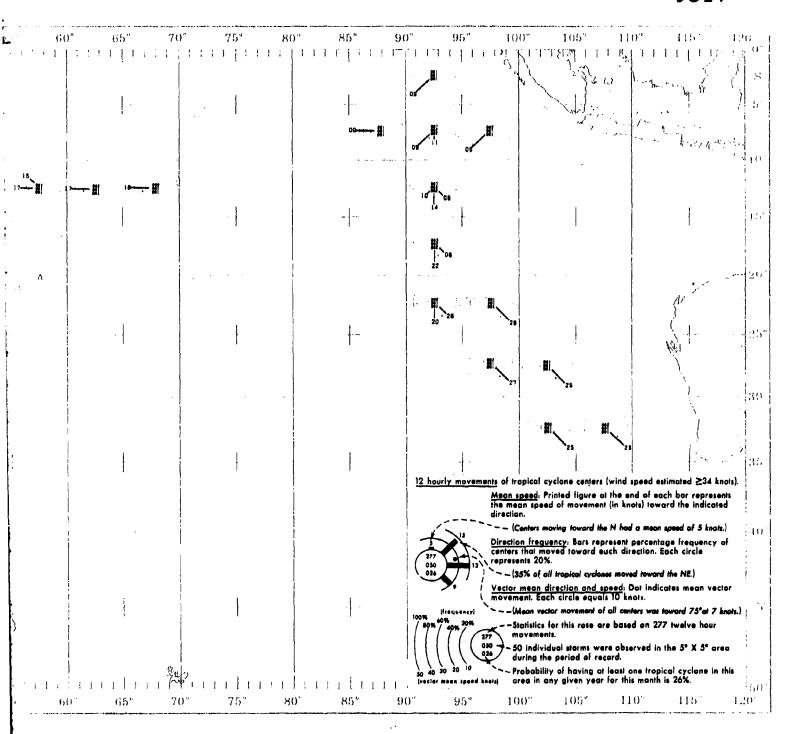
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TROPICAL CYCLONE

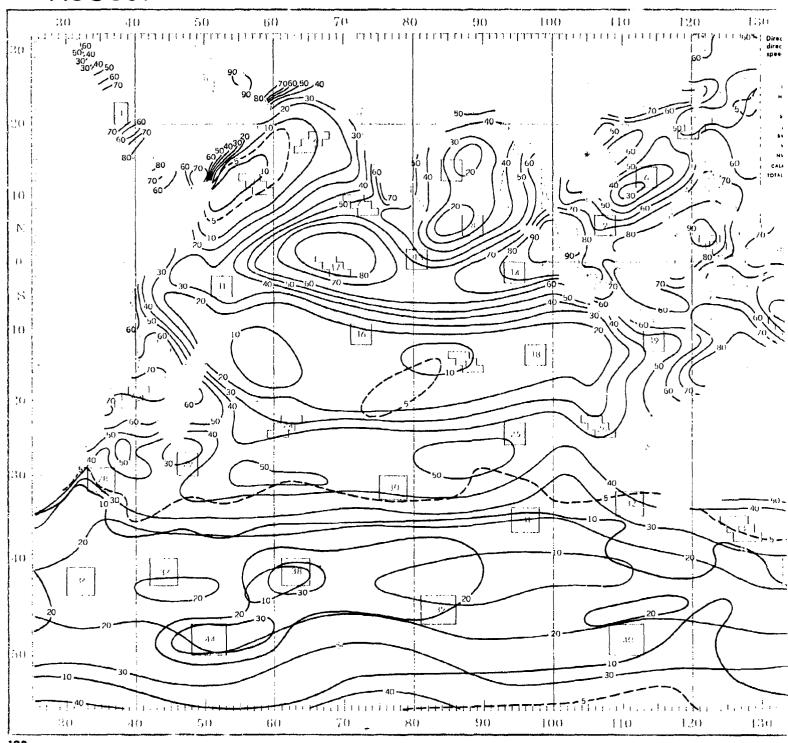


TROPICAL CYCLONE

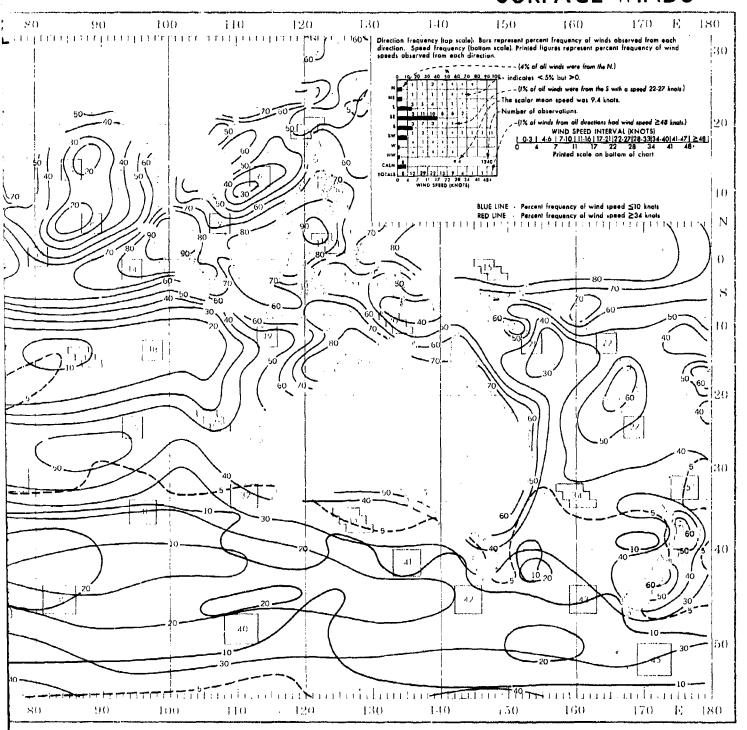
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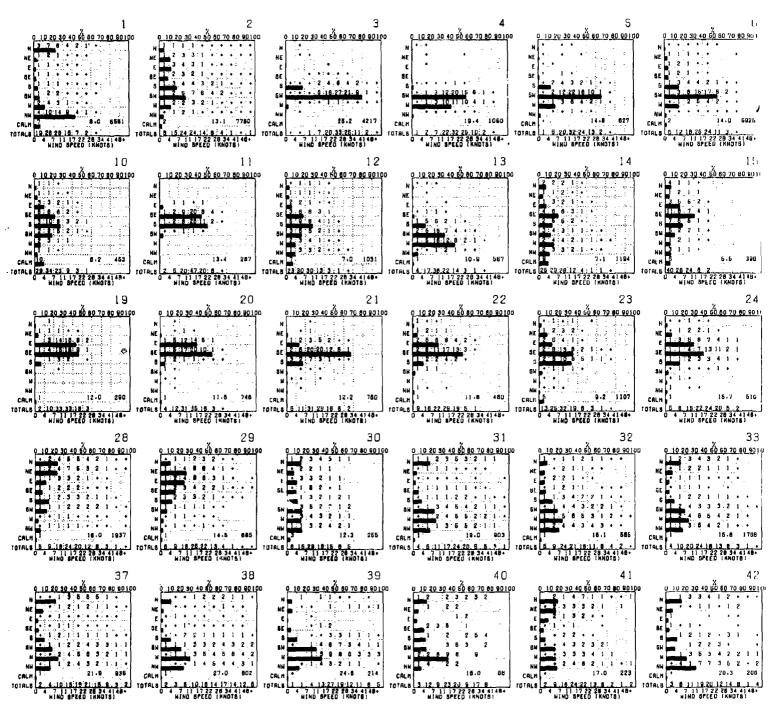
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SURFACE WINDS

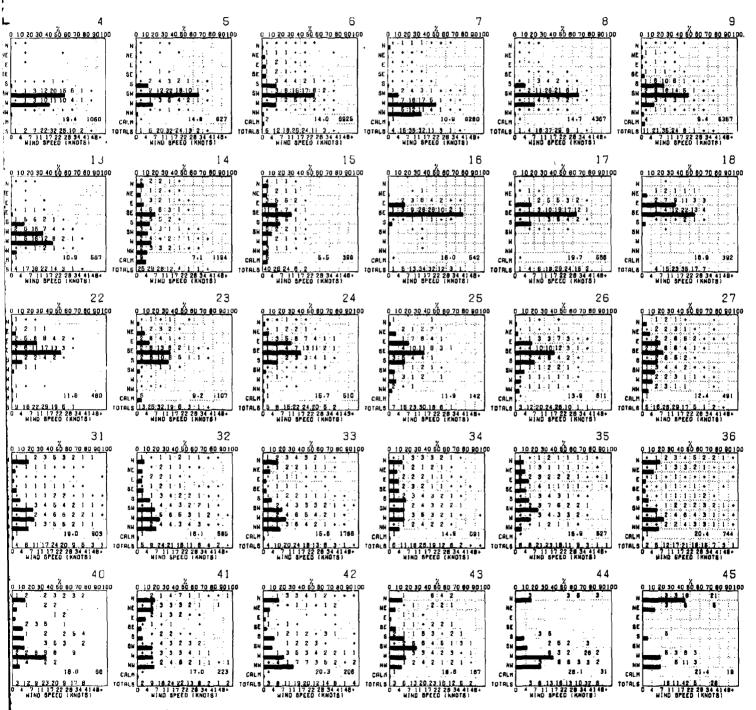


WIND DIRECTION AND SPEED



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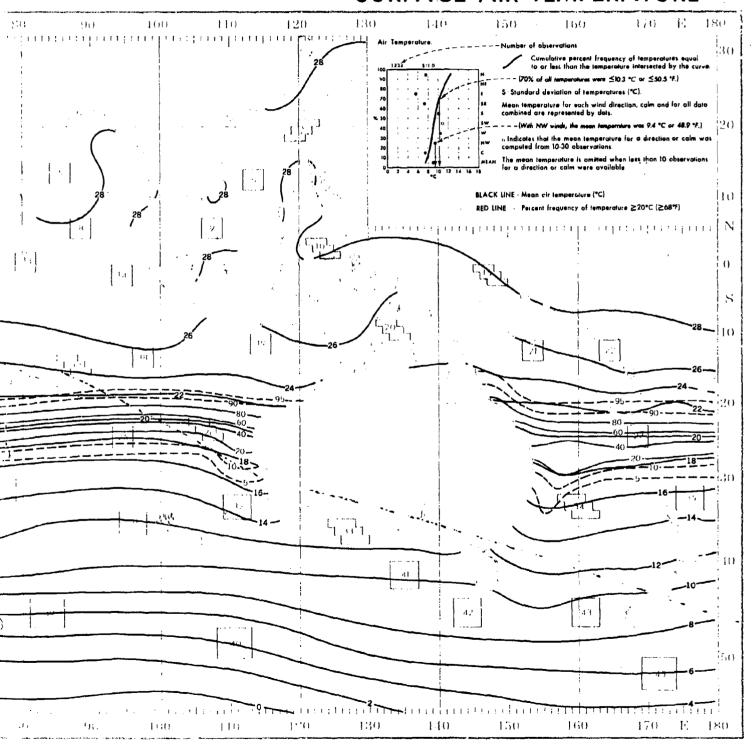


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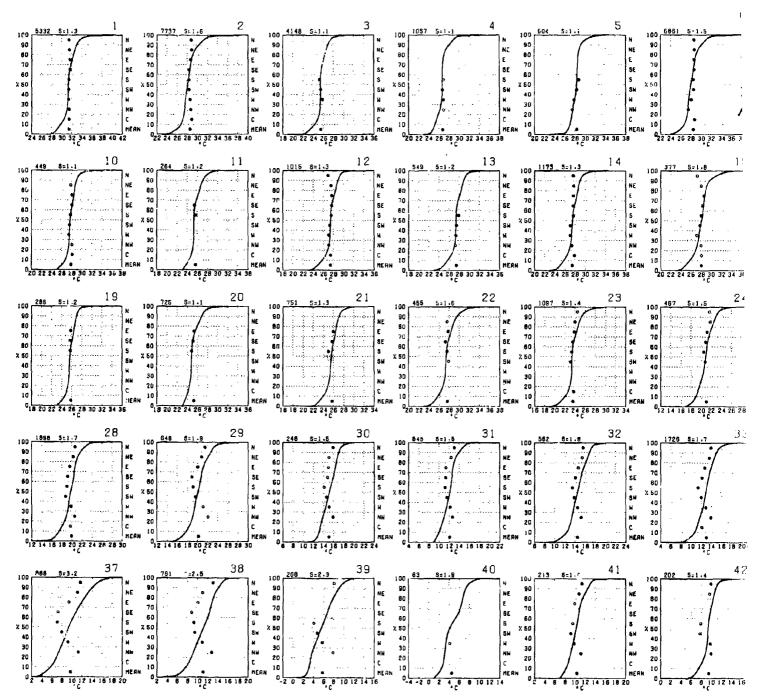
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SURFACE AIR TEMPERATURE

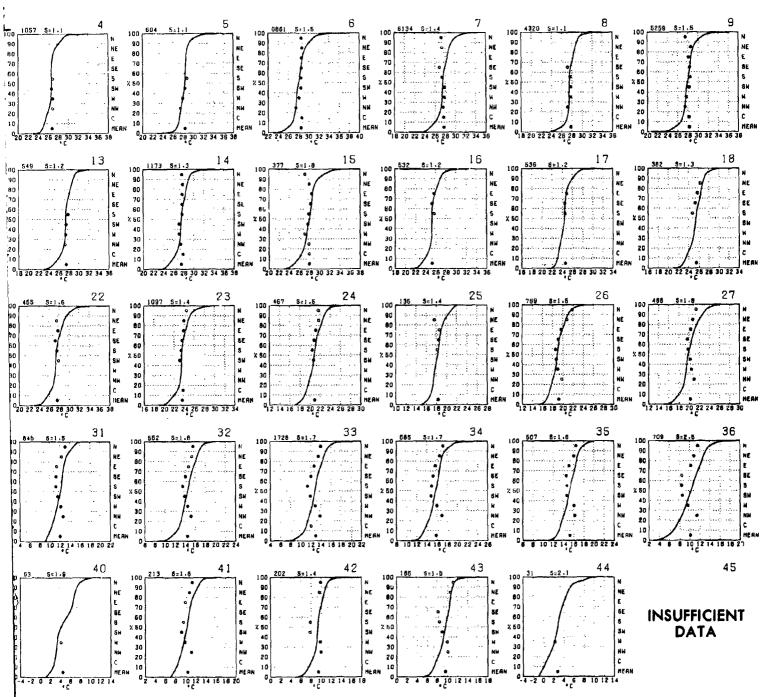


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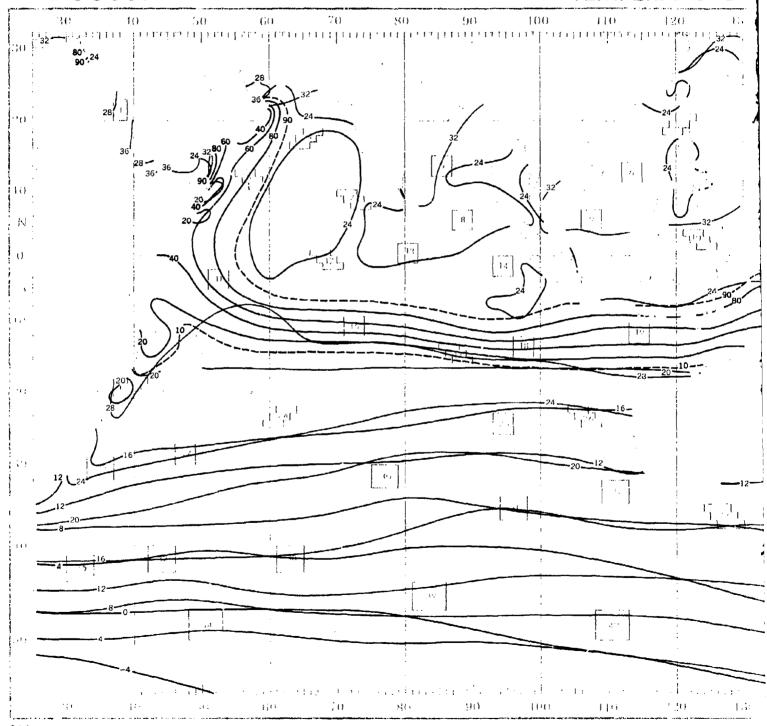


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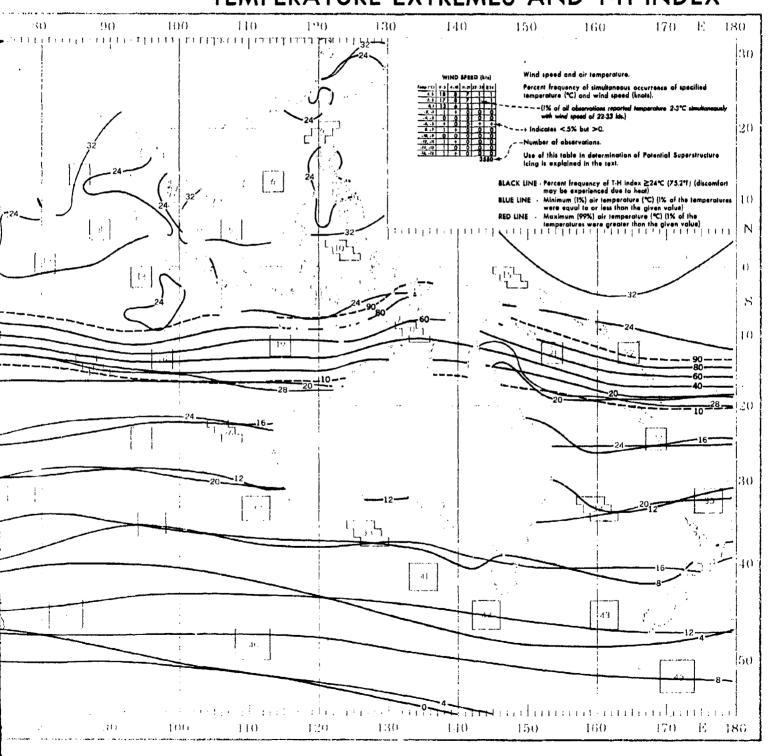
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TEMPERATURE EXTREMES AND T-H INDEX



WIND SPEED AND AIR TEMPERATURE

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HIND SPEED (KTS) 19	MIND SPEED (KTS) 20 TEMP (*C) 0-0 4-10 11-21 22-33 24	HIND SPEED (KTS) 21	HING SPEED (KTS) 22		HIND SPEED (KT
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80.23 0 + 1 0 0 80.21 0 0 0 0 0	24.26 2 24 29 2 0 22.23 0 1 2 + 0	24,28 3 16 15 3 C 22,23 + 2 1 + 0	26.27 2 16 27 4 0 24.28 + 1 2 1 0	88.88 6 22 11 2 4	18.19 0 2 7 .
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<u>Graphs</u> represent the objective compilation of available data for specified areas withon The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively ad

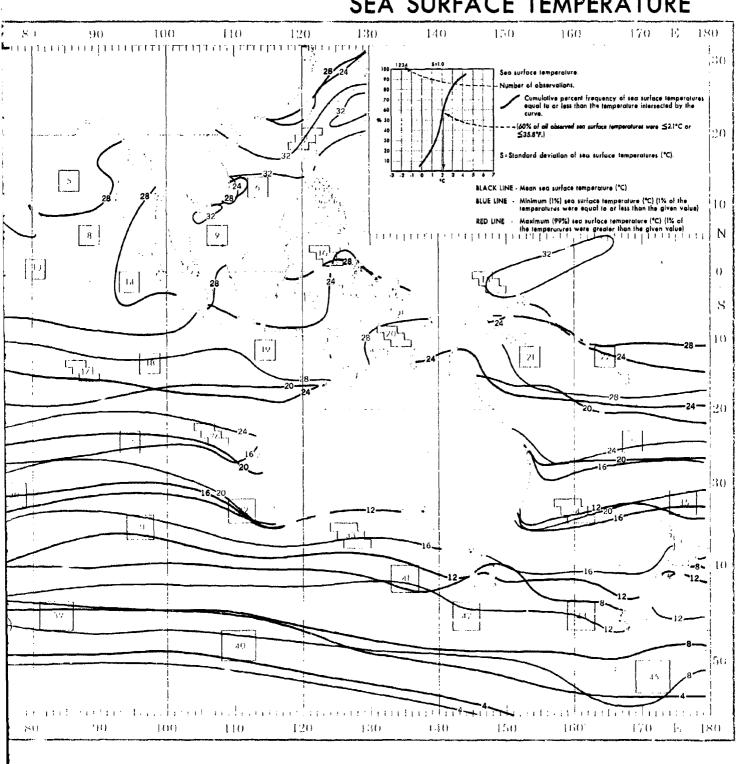
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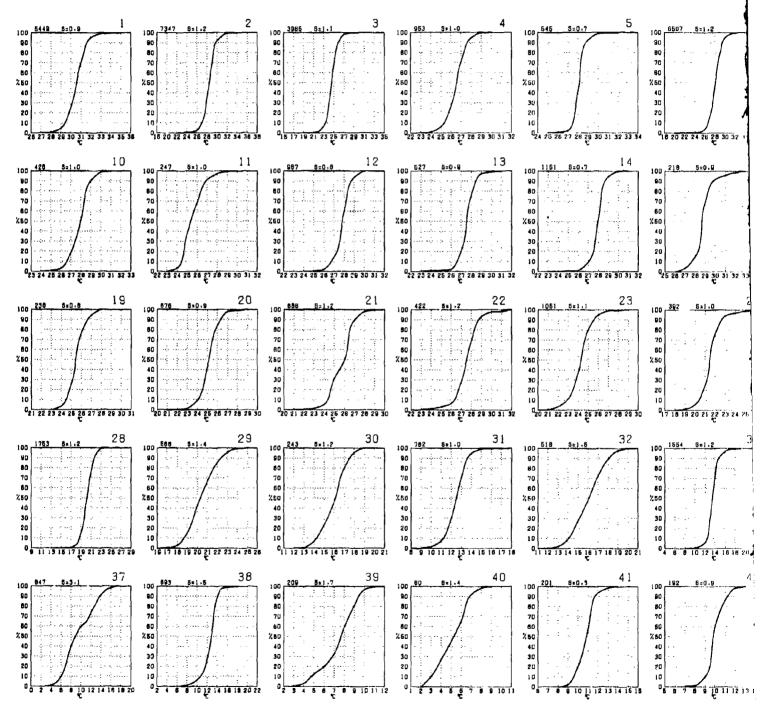
L HIND SPEED (KTS) 4	HIND SPEED (KTS) 5	WIND SPEED (KTS) 6	HIND SPEED (KTS)	WIND SPEED (HTS) 8	HIND SPEED (KTS)
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ENP (°C) 0-9 4-10 11-21 22-23 3-6 30.51 0 3 1 0 0 22-23 3-6 30.51 0 3 1 0 0 22-23 3-6 3 0 0 22-23 3 0 0 0 0 0 0 0 0	TEMP (*C)	TEMP (PC)	TEMP 1ºC1 0-3 4-10 11-21 22-30 34 30 31 0 0 0 0 0 0 0 0 0	TEMP (4C1	TEMP 1°C1 0-3 4-10 1-21 EE-88 134
HIND SPEED (KTS) 22	HIND SPEED (KTS) 23	HIND SPEED (KTB) 24	HIND SPEED (KTS) 25	WIND SPEED (KTB) 26	WIND SPEED (KTS) 27
PMP (C)	TEMP 19C1	TEMP (PC)	TEMP (*C)	TEMP (PC)	TEMP 1°C) C-8 4-10 1-21 21-29 24 25 17 0 0 0 0 0 0 0 0 0
HIND SPEED (KTS) 40	HIND SPEED (KTS) 41	HIND SPEED (HTB) 42	HIND BPEED (KTS) 43	HIND SPEED (KTS) 44	45
P 1°C1 0-9 4-10 11-81 22-39 34 34 4-10 11-81 22-39 34 34 34 35 35 35 35 35	TEMP (*C) 0-3 4-10 11-21 25-23 3 24 14.16 0 0 + 1 0 15:13 0 5 16 4 1 10:11 1 11 19 8 1 6:0 + 8 12 7 0 6:7 0 3 1 1 0 4:8 0 0 0 0 0 0 5:8 0 0 0 0 0 0 6:1 0 0 0 0 0 -5:1 0 0 0 0 0 0 -5:1 0 0 0 0 0 0 -4:3 0 0 0 0 0 0 -5:1 0 0 0 0 0 0 -6:5 0 0 0 0 0 0 -1:0 0 0 0 0 0 0 -1:0 0 0 0 0 0 0 -1:0 0 0 0 0 0 0 -1:0 0 0 0 0 0 0 -1:0 0 0 0 0 0 0	TEMP (FC) 0-9 4-10 11-21 22-50 a 24 12:10 1 1 3 3 1 0 10:11 1 8 19 11 7 6.6 1 7 0 3 3 3 3 1 4.6 0 0 1 0 0 2:5 0 0 0 0 0 0 -2:-1 0 0 0 0 0 0 -4:-5 0 0 0 0 0 0 -5:-5 0 0 0 0 0 0 -6:-5 0 0 0 0 0 0 -6:-5 0 0 0 0 0 0	TEMP (*C) 0-9 4-10 11-E1 EE-58 8 24 16+16 1 0 0 0 0 0 0 15:18+18 0 1 3 2 0 0 1 3 2 0 0 15:18+18 0 1 1 3 2 0 0 15:18 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	TEMP 19C1 0-3 4-10 11-21 29-38 3 24 4 6-6 0 0 0 3 0 0 0 6-7 0 0 0 0 0 3 16 16 16 16 16 16 16 16 16 16 16 16 16	INSUFFICIENT DATA

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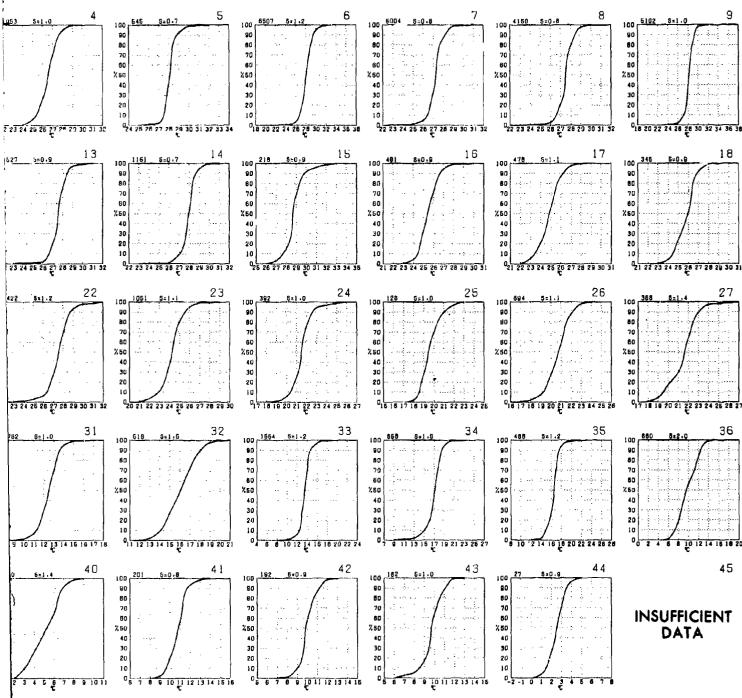
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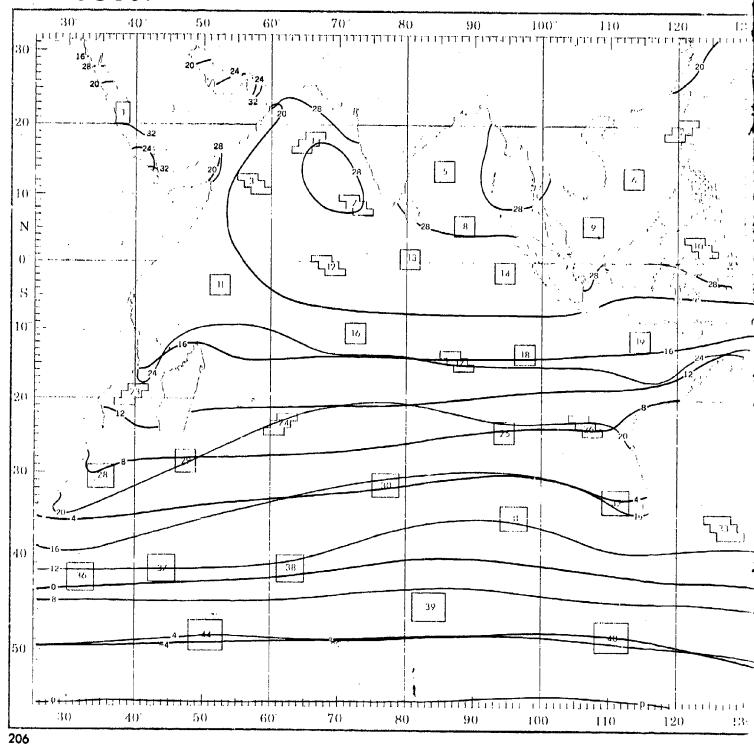
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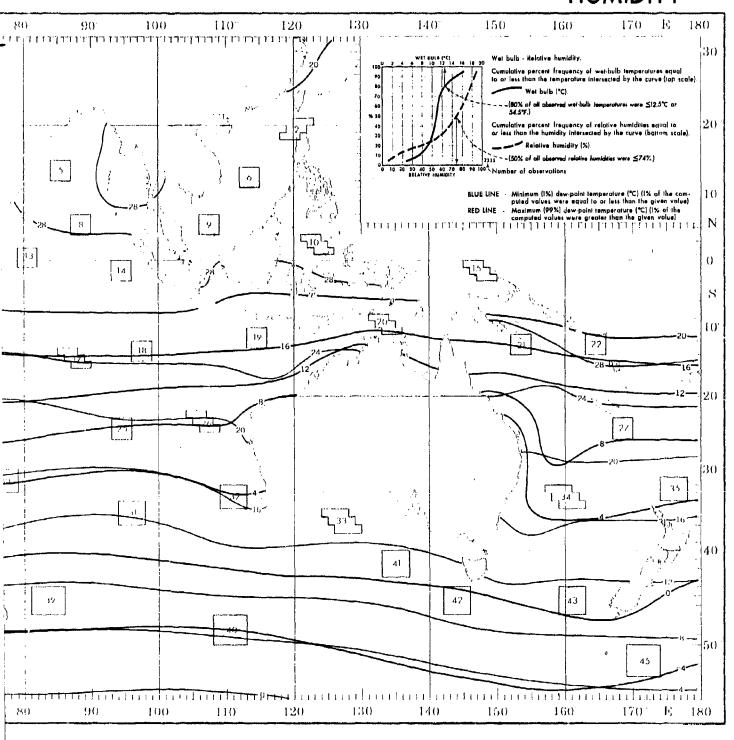
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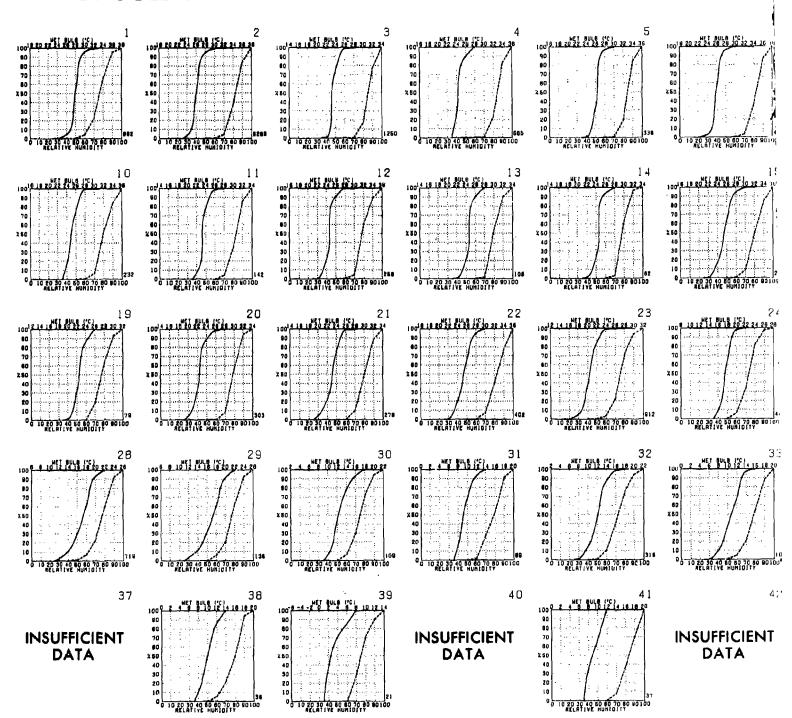
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HUMIDITY



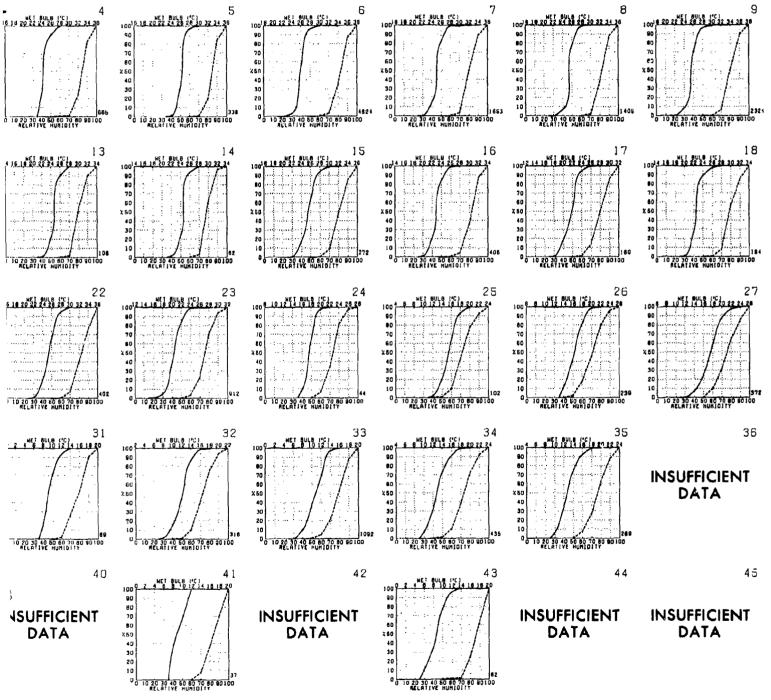
WET BULB AND RELATIVE HUMIDITY



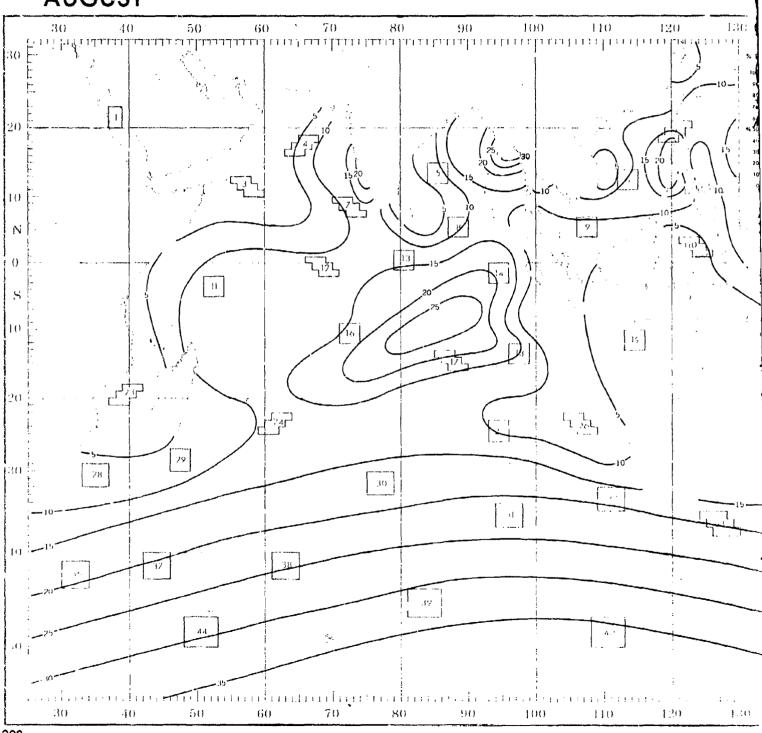
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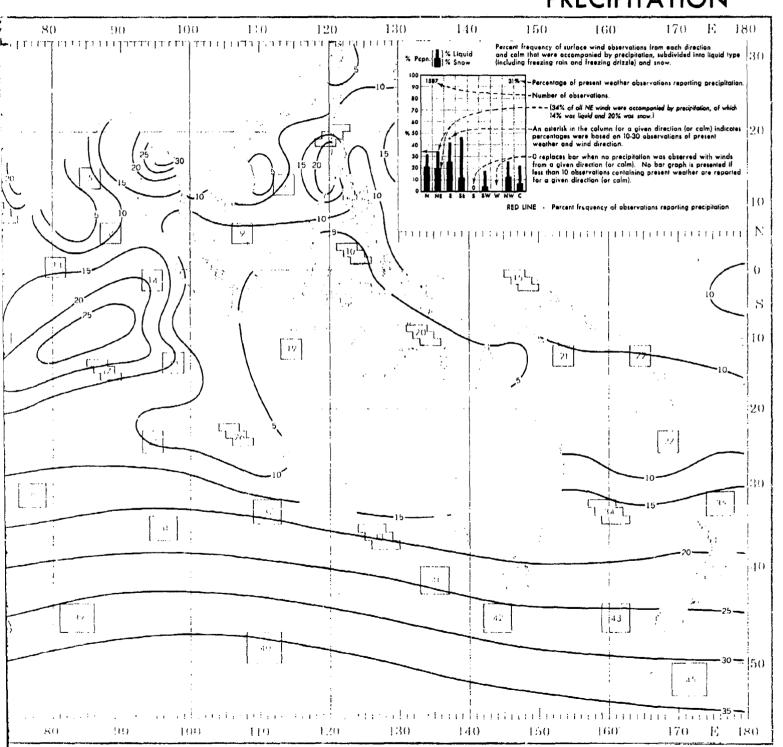
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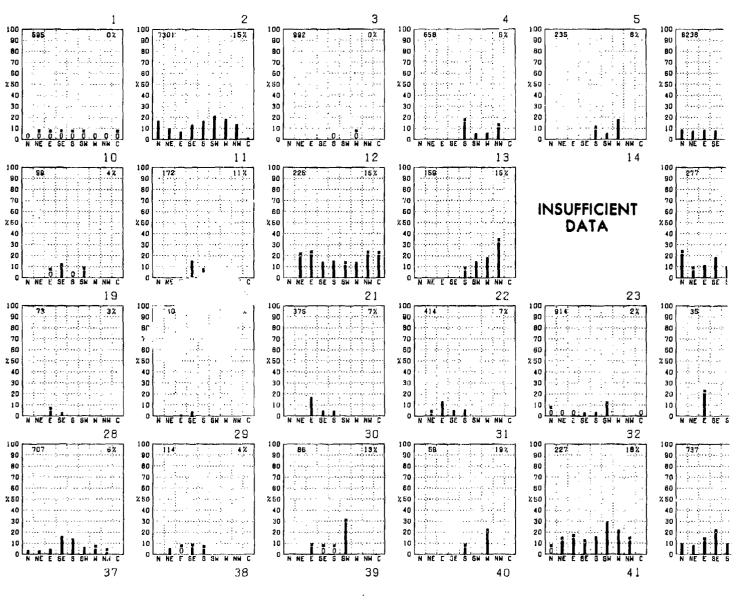
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PRECIPITATION



PRECIPITATION

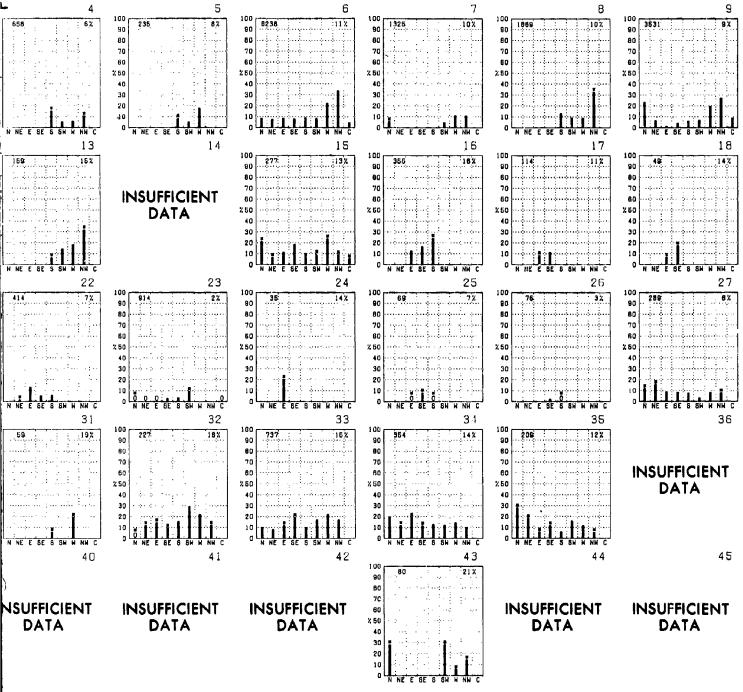


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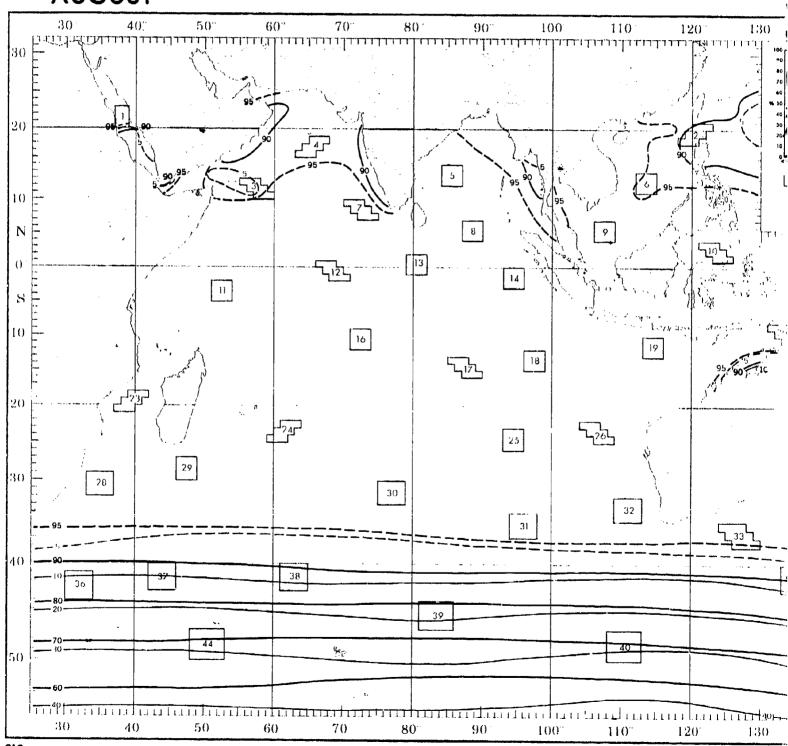
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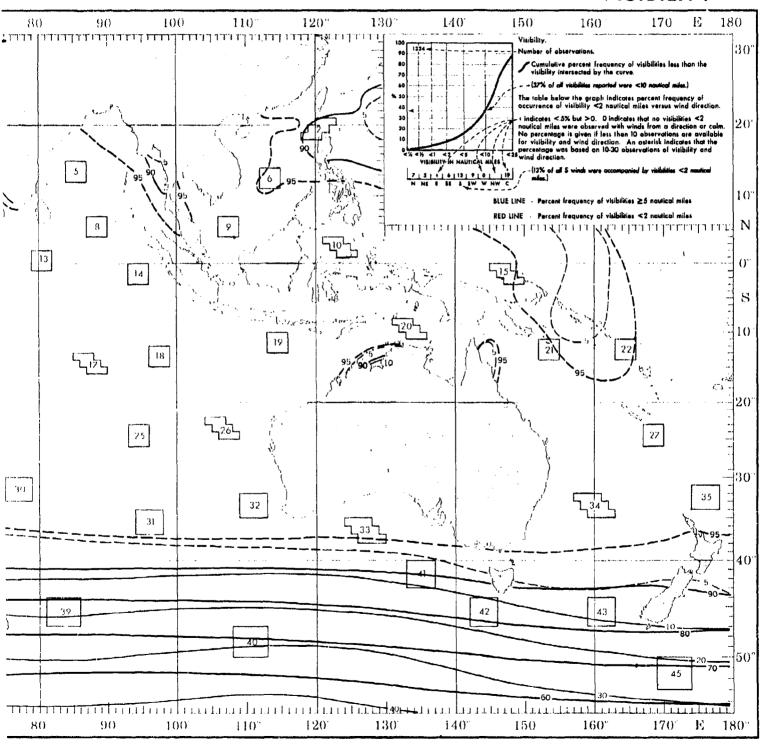
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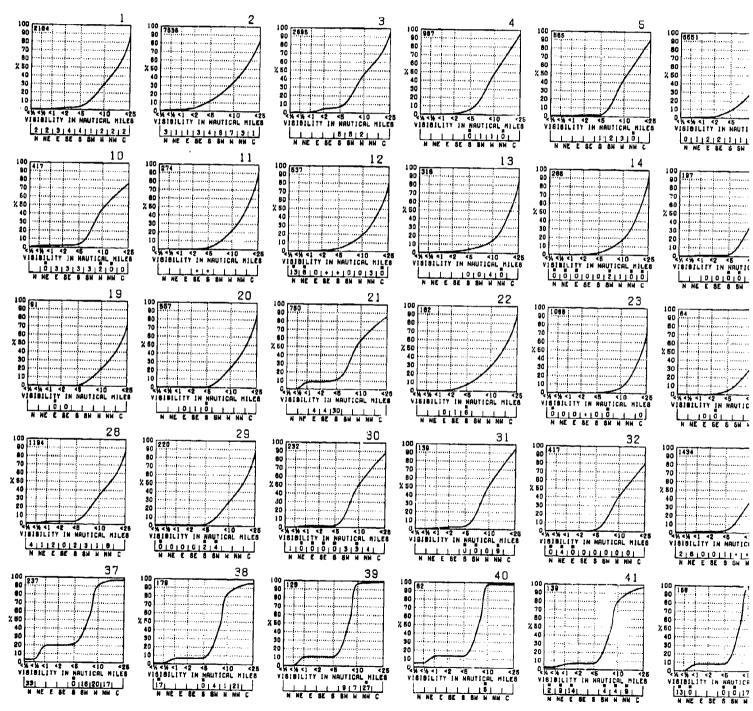
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VISIBILITY

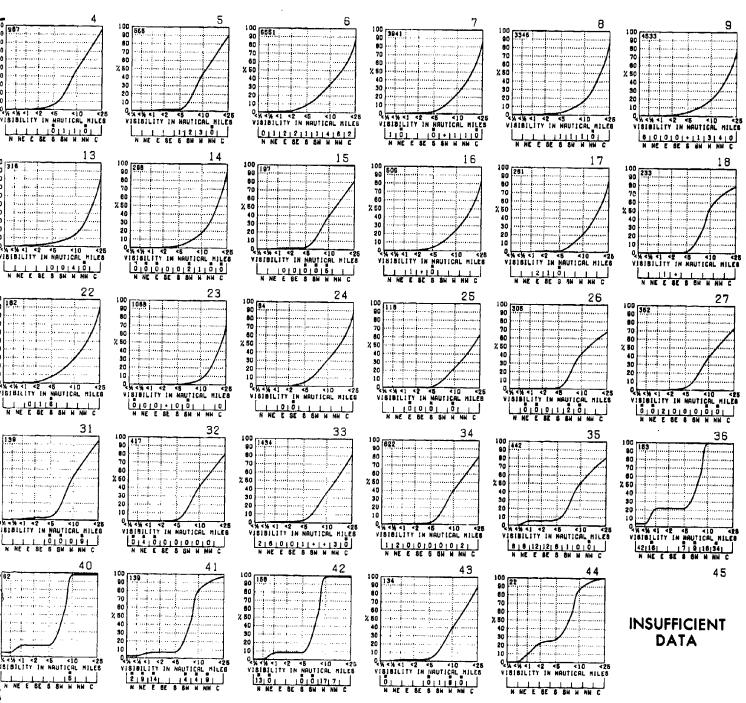


VISIBILITY

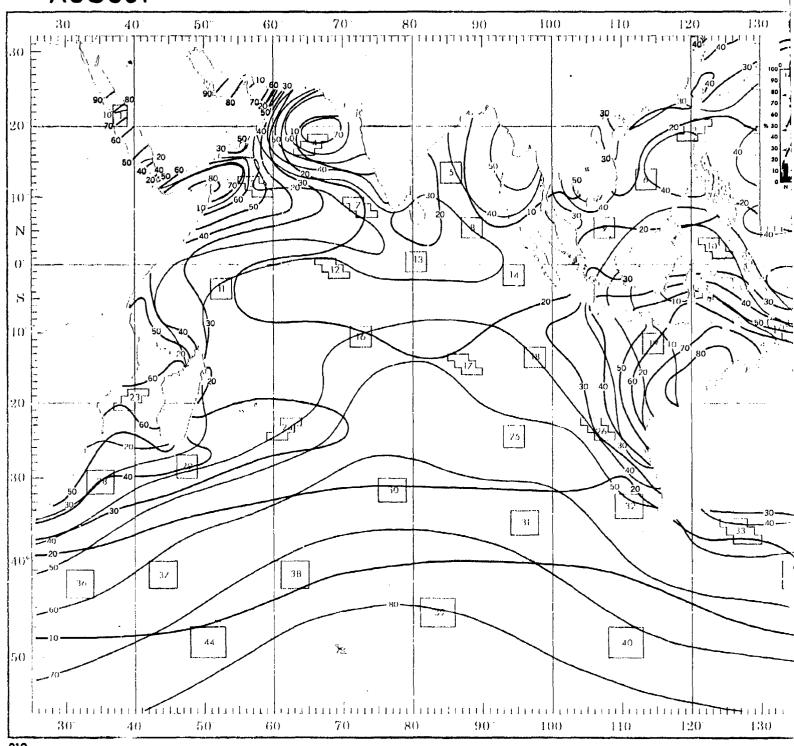


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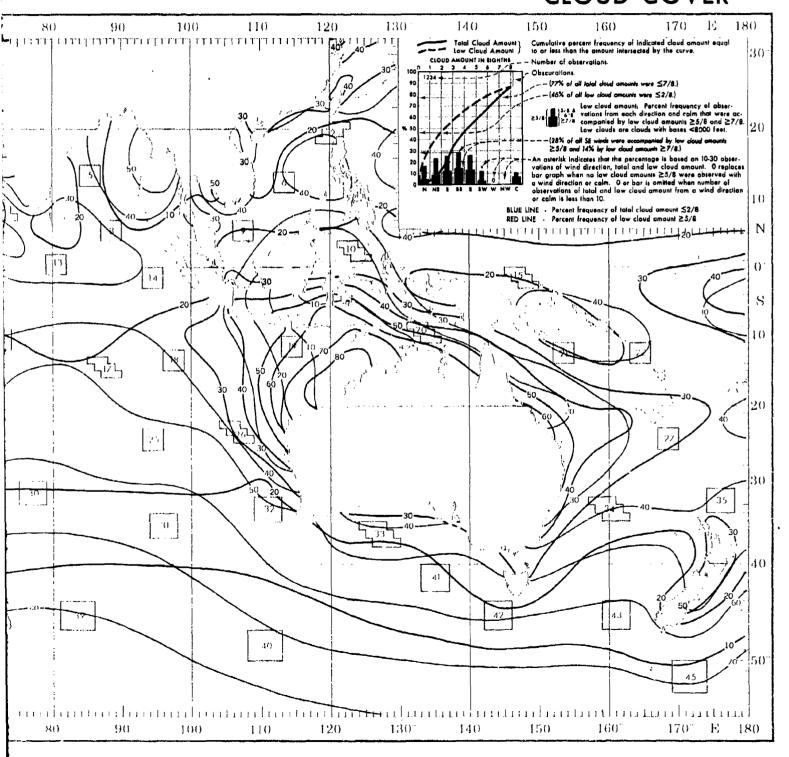


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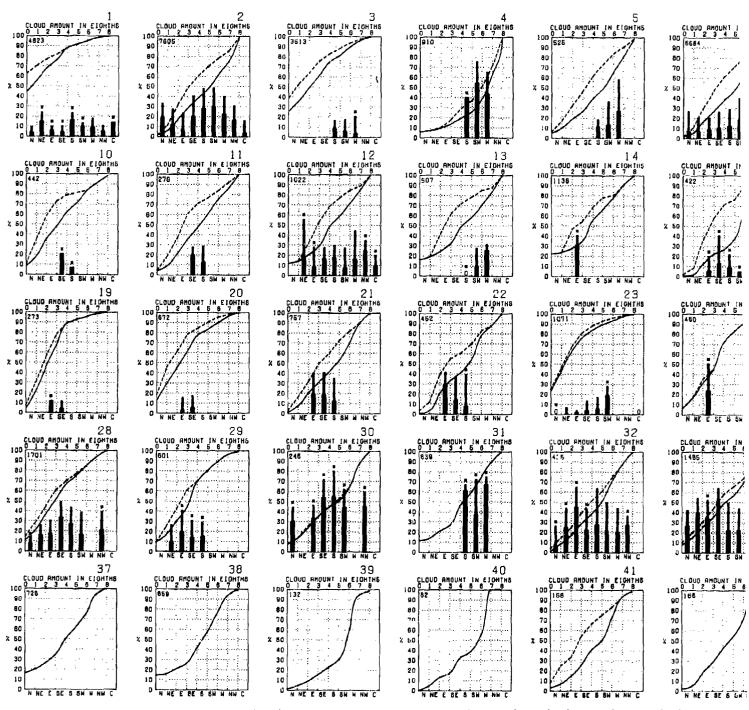


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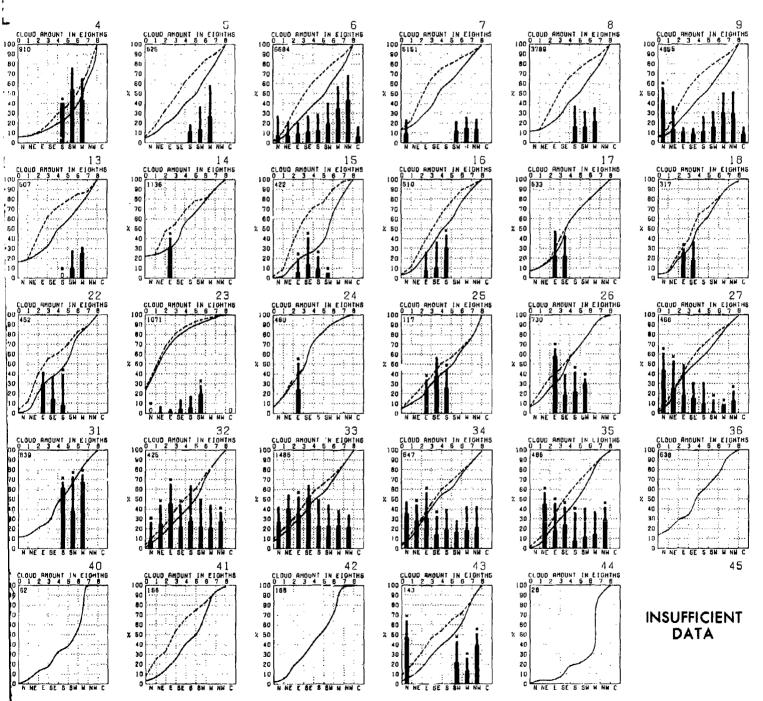
CLOUD COVER



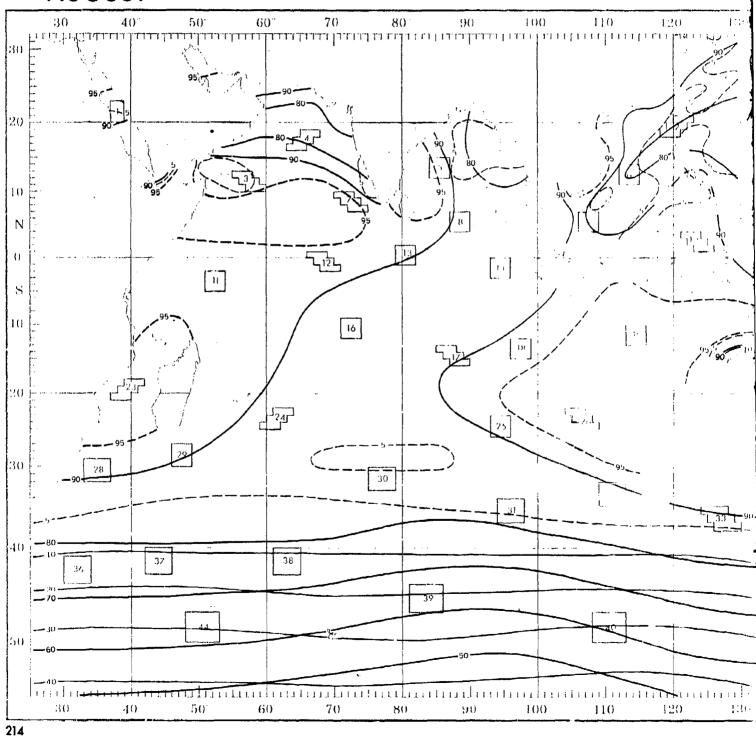
CLOUD COVER



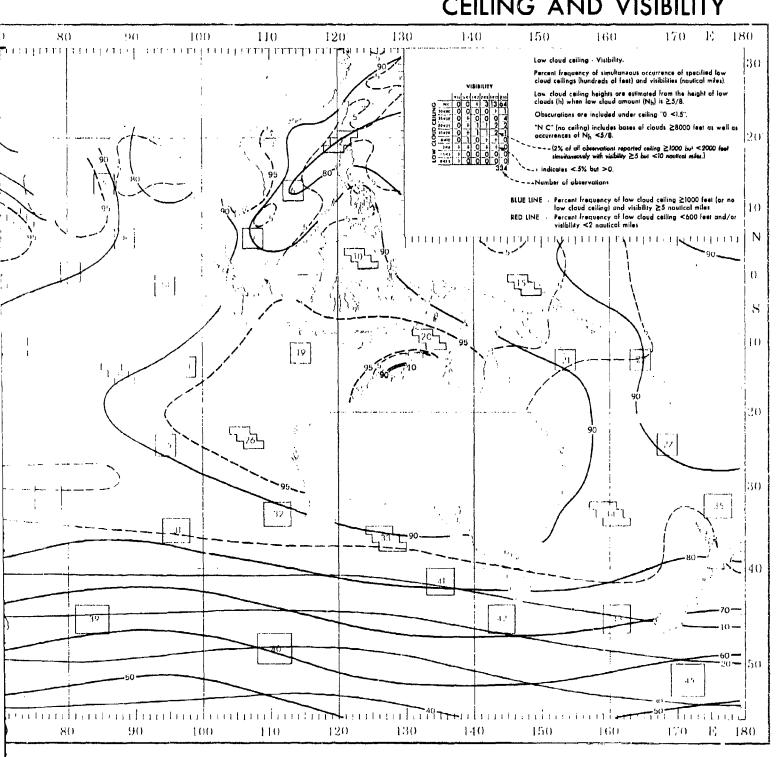
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ive compilation of available data for specified areas without regard to suspected biases. site page) are based on all available data subjectively adjusted where bias was evident.



CEILING AND VISIBILITY



CEILING AND VISIBILITY

VISIBILITY	VI6181LITY 2 VI	VISIBILITY AC 0 0 + 2 24 58 S0-80 0 0 0 + 2 1 20-36 0 0 0 0 + 2 1 20-36 0 0 0 0 + 2 3 End 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY + 1/2 74 + 1 + 2 2 + 5 8 + 10 + 10 + 1/2 74 + 1 + 2 2 + 5 8 + 10 + 10 + 1/2 74 + 1 + 2 2 + 5 8 + 10 + 10 + 1/2 74 + 1 + 2 2 + 5 8 + 10 + 10 + 1/2 5 6 0 0 0 0 0 0 + 1/2 5 6 0 0 0 0 0 + 1/2 5 74 0 0 0 0 0 + 1/2 1 1 1 1 + 1/2 1 1 1 1 + 1/2 1 1 1 1 + 1/2 1 1 1 + 1/2 1 1 1 + 1/2 1 1 1 + 1/2 1 1 1 + 1/2 1 1 + 1/2 1 1 + 1/2 1 1 + 1/2 1 1 + 1/2 1 1 + 1/2 1 1 + 1/2 1 1 + 1/2 1 1 + 1/2	VISIBILITY c'/s f'sci c'2 2 c'5 B c 10 5 10	VISIBILITY 40 2 049 0 0 0 23443 0 0 0 0 . 27948 0 0 29948 0 0 3440 3440 3440 3440 3440 3440 3440 3440 3440
VISIBILITY 10 10 10 10 10 10 10 10 10 1	VISIBILITY	VISIBILITY 12 1-17 1-	VISIBILITY	VISIBILITY -1/n [7/4] 1-8 24 5 4 10 310 -80 0 0 0 2 0 01	VISIBILITY
VISIBILITY ***********************************	VISIBILITY 14	VISIBILITY -1/2 1/2 1/2 1/2 1	VISIBILITY	VISIBILITY 23	VIBIBILITY
VISIBILITY	VISIBILITY 1/4 F/4-1 1 = 2 2 +	VISIBILITY	VIBIBILITY 4/A A-4 48 44 4-10 410	VISIBILITY	VISIBILITY

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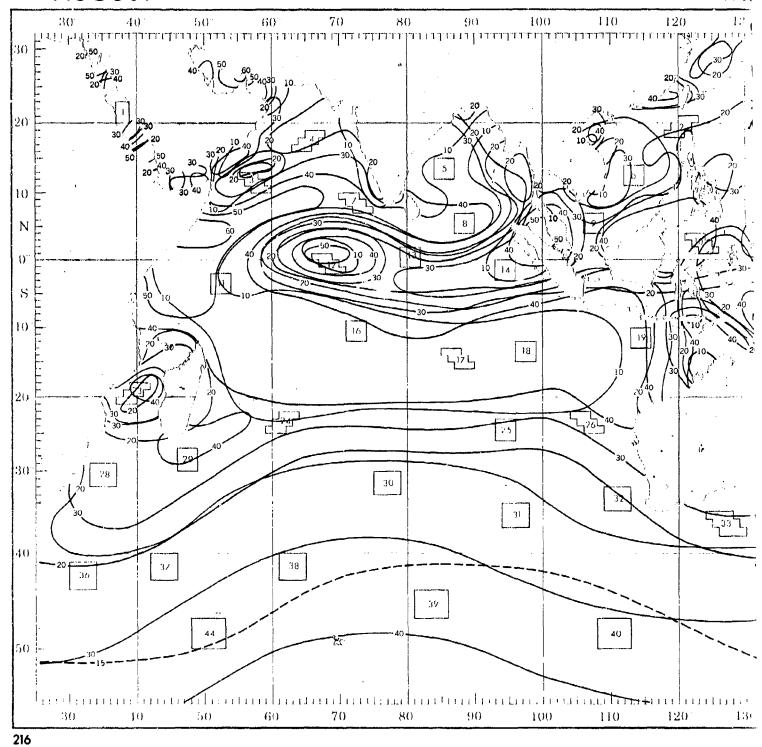
INSUFFICIEN DATA

INSUFFICIENT DATA	INSUFFICIENT DATA	INSUFFICIENT DATA	**************************************	INSUFFICIENT DATA	INSUFFICIENT DATA
VISIBILITY 31 **/***Presipres** 2 2*** Restributo** **C	VIBIBILITY 32 *1/8 *74 148 246 84 0 10 MC	VISIBILITY 33	VISIBILITY 34	VISIBILITY 35	INSUFFICIENT DATA
VISIBILITY 22	VISIBILITY 23 ***********************************	VISIBILITY 24 *** *	VISIBILITY 25 *** ** ** ** ** ** ** ** ** ** ** ** *	VISIBILITY 26 ***********************************	VISIBILITY 27 ***********************************
VISIBILITY 13 *** *	VISIBILITY 1 4 **********************************	VIBIBILITY 1 5 47/2 7/4 1 1 2 2 5 5 10 10 MC	VISIBILITY	VISIBILITY e1/2 P/42	VISIBILITY
VISIBILITY 4	VISIBILITY -1/2 1/2 + 1/2 2 + 1/2 2 + 1/2 3 + 1/2 3 + 1/2 4 + 1	VISIBILITY 1/21 1/22 2/45 5/10 3/10	VISIBILITY **/** */**	VISIBILITY	VISIBILITY */*/ */

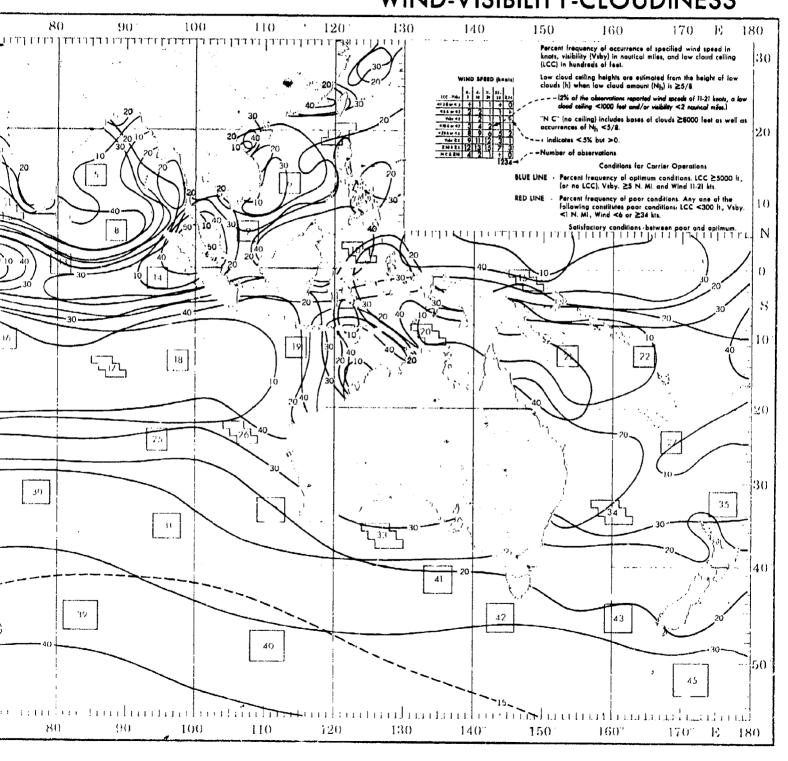
tive compilation of available data for specified areas without regard to suspected biases.

osite page) are based on all available data subjectively adjusted where bias was evident.

WII



WIND-VISIBILITY-CLOUDINESS



LOW CLOUD CEILING-VISIBILITY-WIND

			•		
1	2	3	Δ	5	
NIND SPEED (KNOTS)	WIND BPEED (KNOTS)	WIND BREED (KNOTS)	HIND BPEED (KNOT6)	HIND SPEED (KNOTS)	HIND SPEED (KND
[0- 4- 11- 22-	10-14-111-128-1	10-14-1114991 1	LCC - VERY 3 10 21 33 494	LCC - V887 0 4- 11- 27-	LCC - VORY 0- 4- 11- 28-
		LCC - VBBY 3 10 21 39 434	41-8 4 0R 4-8 0 0 + + 0	41.6 4 OR 4.8 0 0 1 0 0	41.6 6 QR < .6 + + 1 +
<1.8 & DR < .6	41.5 à DR 4.5 + 1 1 +	*6 4 DR *2	10 4 OR 12 0 0 1 1 +	49 4 GR 42 0 + 3 0 0	48 4 OR 42 + 1 3 1
V887 42 4 4 0 0 0	VB07 -2 + + 1 1 1	V881 42 0 0 0 + 0	VEST 42 0 0 0 0 0	Y887 4 0 0 1 0 0	V887 *2 • • 1 ·
410 4 0H 42 1 1 0 0 0	410 4 0R 42 1 4 7 4 1	410 4 0H 42 0 0 1 3 1	410 4 0R 42 0 1 9 8 +	410 4 0A 48 0 2 5 3 0	<10 4 DA <2 0 4 9 3
-20 4 08 -5 2 3 2 1 0	480 4 PR 46 1 8 15 7 2		420 4 OR 46 + 3 24 18 1	-20 4 OR -5 0 5 11 4 0	<20 4 0R <6 1 7 19 6
VEST 26 14 50 28 2 0	V887 AS 8 37 34 9 1	V&BT a5 0 1 32 52 13	VERY 35 + 8 54 30 2	VAST 15 + 31 53 14 1	VBBY 35 6 28 45 12
≥50 4 ±8 14 47 28 Z O	360 4 a5 6 26 22 4 +	a 80 4 a 8 0 1 28 44 10	480 6 45 + 5 20 8 +	a 50 4 a 6 + 21 32 7 +	ad0 4 a8 5 21 27 7
MC 4 3 10 11 39 23 2 0	MC 4 2 10 G 24 17 3 +	MC4+10 0 + 22 29 6	MC 4 » 10 + 4 15 9 0	NC 4 a 10 (1 21 28 5 0	MC 4 # 10 4 18 21 5
533	6335				1
10	11	12 NIND SPEED (MNOTS)	13	14 WIND SPEED (KNOTS)	HIND SPEED (KNO:
WIND SPEED (KNOTS)	WIND SPEED (KNOTS)	ا امعوام المام المام المام المام المام المام المام المام المام المام المام المام المام المام المام المام المام	[0-14-113-128-1		
LCC - V68Y 9 10 21 38 a34	LCC - VSBY 3 10 21 32 +34				
4) B 4 6R 4 B 0 0 0 0 0	<1.6408 <-6 0 0 1 0 0	49 & OR 48 D 4 + D D	41.64 OR 4:6 0 0 0 0 0	41-5 4 OR 4-8 0 0 0 0 0 0 0 0 0 0 0	41 4 48 48 0 0 0 0 0
48 4 OR 42 0 2 0 0 0 0 V68Y 48 0 0 0 0 0 0	46 4 dR 42 0 0 1 0 0	48 4 OR 48 D 4 + D 0	V20V 42 0 1 0 0 0	V887 42 0 0 0 0 0	48 4 OR 42 0 0 0 0 0
410 4 6R 4E 2 12 5 0 0	410 4 08 48 0 2 3 0 0	10 4 08 48 2 8 2 0 0	410 : 04 =2 1 4 2 1 D	*10 4 OR *2 0 10 3 0 0	410 4 DR 42 U 3 D O
420 4 0R 46 2 14 7 D O	480 4 08 48 0 7 9 0 0	-20 4 OR -16 5 14 4 0 0	480 4 0R 46 1 14 4 1 D	420 4 OR 45 3 20 5 0 0	420 4 0R 45 2 8 2 0
YSBT 25 12 63 19 0 0	Y88Y AS 4 28 84 4 0	VEST 18 88 8 0 0	· V897 NE 8 60 29 2 0	V867 = 13 85 18 0 0	\48Y 25 25 55 17 C
2 50 4 28 9 49 16 O C	3 18 53 2 0	280 6 28 14 5D 7 0 D	180 4 16 4 45 22 0 0	#80 4 #5 13 43 5 D O	250 4 35 18 45 14 0
MC 4 2 10 9 49 16 0 0	HC 4 4 10 2 18 50 2 0	HC 4 a 10 13 48 6 0 0	MC4 = 10 4 44 16 0 0	HC4 + 10 13 43 5 0 0	HG 4 > 10 18 42 14 0
43	138	238	112	40	
19	20	21	22	23	, 2
MIND SPEED (KNOTS)	HIND SPEED (KNOTS)	WIND SPEED (KNOTS)	WIND SPEED (\$1078)	HIND SPEED (KNOTS)	WIND 8FEED (KNOT 0- 4- 11- 22-
LCC - YARY 3 10 21 33 234	LCC - VERY 3 10 21 35 A34	LCC - VABY 3 10 21 33 234	LCC - VARY 2 17 21 35 834	LCC - VBCY 3 10 23 33 244	LCC - VABY 3 10 21 33
<1.54 68 <.5 0 0 0 0 0	41.8 4 00 4.8 0 0 0 0 0	4) .5 4 DR < .8 0 0 0 0 0	<1.84 98 < .8 0 0 0 0 0	<1.8408<.8 0 0 0 0 0	41.8 4 OR 4.6 0 0 0 0
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	48 4 58 4 5 0 0 0 0 0 0 0	48 4 68 48 0 1 1 A 0	48 4 OR 42 0 0 1 0 0	48 4 0R 42 2 4 4 0 0 4 0 0 0 VBBY 48 0 0 0 0 0 0 0	VBBY 42 0 0 0 0
-10 4 50 42 0 0 0 D	*10 L 0R <2 0 + 2 0 0	410 8 GR 4E D 3 1U 3 D	410 4 0R 48 0 2 3 3 0	-:D 4 Sh 42 O 1 1 4 O	<10 t OR <5 O C C
420 4 BR 45 Q 5 2 0 0	*** 4 DR ** 0 1 6 0 0	-10 4 OK -E U 8 21 5 0	420 4 GR 45 0 4 14 C 0	420 A OR 46 + 3 4 + 0	120 4 04 10 0 7 10 3
V887 AS 5 48 45 2 0	VERY NS 6 37 57 1 0	VEST 35 1 24 62 9 0	Y68Y 25 1 15 85 10 0	V68Y 46 15 H7 25 3 0	VBSY 25 7 27 47 17
250 425 5 41 44 2 0	>60 4 hB 6 33 48 1 0	# 50 4 as 1 17 36 5 0	>80 4 28 1 10 37 2 0	280 4 28 15 52 21 2 0	a50 4 a5 3 20 30 17
MC 4 2 10 5 39 42 2 0	MC 4 2 10 5 32 45 1 0	MC 4 a 10 1 18 32 6 0	MC 4 = 10 1 9 35 1 0	NC 4 7 10 14 51 20 2 0	MC 4 > 10 3 20 27 17
68	235	258	101	398	0.4
28	- 29	30	31	32	3:
MIND 8PEED [KNGT8] 0- 4- (11- 22-	HIND SPEED (KNCTS)	41ND SPEED (KNOTS) 10- 4- 111- 22-	HIND SPEED (KNOTS) 0- 4- 15- C2- 10 21 33 234	HIND BREED (KNOTS)	X1ND SPEED (KNOT: 0- 4- 11- 22-
LCL - VIAY 3 10 21 23 134	UCC - VERY 3 10 21 33 234	LCC - VSAY 3 10 21 93 294		LCC - VERY 3 10 21 33 254	LCC - VSEY 3 10 21 35
<1.5 4 OR +.8	48 4 0R 42 D O O D	<1.8 & OR <.8 0 0 0 0 0	*1.84 0R *.6 0 0 0 0 0	*1.6 4 0R *.6 0 + 0 0 0	41.6 ± 0R 4.6 0 + 0 +
*8 4 OR (2 0 0 0 0 0 0	7507 ·2 0 0 0 0 0	VSB? <\$ 1 0 0 0 0	VB97 =2 0 0 0 1 0	40'4 0R 42 0 2 1 0 4 VBBY 42 0 0 0 0 0	VBBY 48 0 + + +
410 4 68 48 0 2 4 2 1	*10 4 06 *2 1 4 4 3 0	*16 L OP -2 2 E 5 9 U	/10 4 08 /2 0 4 9 4 O	<10 4 04 <2 0 6 5 3 1	410 4 08 42 + 3 4 2
-20 4 OR -8 + 6 10 6 2	-20 4 DR -6 1 4 8 8 0	420 4 0R 46 4 20 11 4 ()	420 4 08 4E 1 10 19 17 1	*10 & OR <5 + 14 1 5 1	420 × 0R 48 1 7 10 5
Y697 35 2 23 48 22 4	rser +8 4 20 54 19 1	VSBY 48 12 43 28 13 0	VS87 25 1 32 46 16 1	VABY 25 4 40 36 16 2	vder a6 5 31 42 16
#80 4 e8 2 16 36 15 2	a 80 4 28 4 16 42 10 0	and 4 and 7 18 13 7 0	380 4 8 D 13 13 B D	280 425 3 21 21 9 2	■ 60 A EB 3 19 27 10
MC 4 a 10 2 15 33 13 1	MC 4 to 0 4 18 39 9 0	MC 4 # 10 7 10 9 7 3	NC 4 a 10 0 7 12 4 0	HC 4 + 10 2 20 19 8 +	HC 4 = 10 2 18 25 8
062	113	•••		245	ğ
37	. 38	, 39	40	4 1 HIND SPEED (MNOTB)	. 40
				for Landounteer L	
				LCC - VBBY 3 10 21 33 a54	

INSUFFICIENT DATA

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INSUFFICIENT DATA

NIND SPLED (KNOTS)						
LCC - VSSY	9-	10	11 21	33	224	
-1.6 4 DR - 8	0	0	0	0	٥	
484 04 47	0	0	0	0	D	
F\$87 42	D	٠	0	٥	0	
<10 4 DR <2	О	0	0	0	0	
420 4 GR 45	0	10	0	٥	0	
V857 16	6	52	24	: 9	0	
+80 4 + \$	0	33	19	14	0	
N2 6 8 10	0	13	18	10	0	

INSUFFICIENT DATA

Graphs represent the objective compilation of available data for specified areas without The isopleth analyses (opposite page) are based on all available data subjectively adjus

LITY-WIND

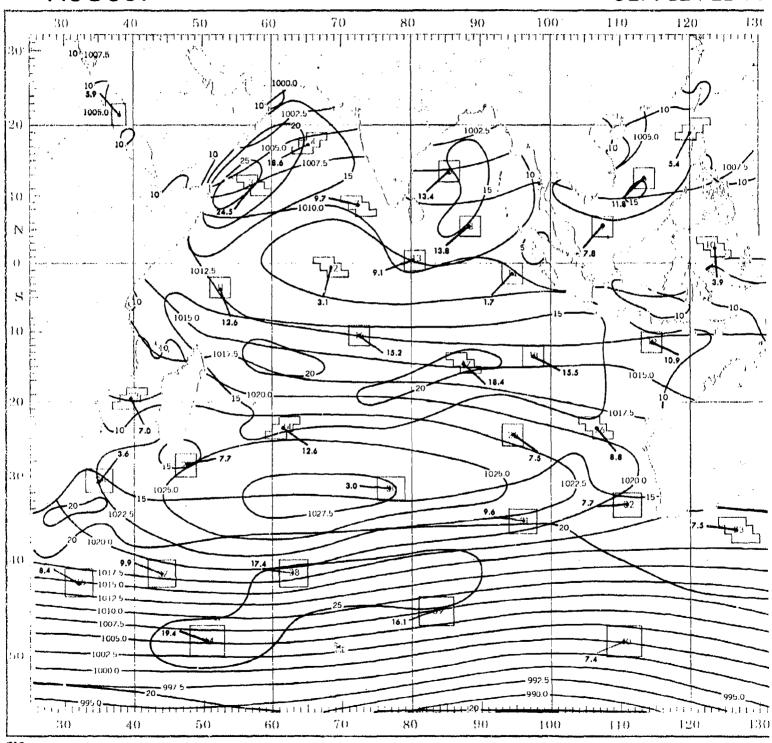
AUGUST

4	5	6	7	8	9
NIND SPEED (KNDTS) LCC - VSST	MIND SPEED (KNOTS) LCC - VBBV	HIND SPEED (KHOTE) LCC - VABY 0 - 4 - 11 - 22 - 23 - 24 11 - 12 - 22 - 23 - 24 11 - 12 - 22 - 23 - 24 13 - 12 - 23 - 24 14 - 12 - 23 - 24 15 - 24 - 25 - 25 - 25 - 25 16 - 25 - 25 - 25 - 25 17 - 26 - 27 - 27 - 27 18 - 27 - 27 - 27 19 - 27 - 27 - 27 10 - 27 - 27 - 27 10 - 27 - 27 - 27 10 - 27 - 27 - 27 10 - 27 - 27 10 - 27 - 27 10 - 27 - 27 10 - 27 - 27 10 - 27 - 27 10 - 27 - 27 10 - 27 - 27 10 - 27 1	HIND SPEED (KNOTS) LCC - VBBY 0- 4- 11- 27- 27- 27- 27- 27- 27- 27- 27- 27- 27	MIND SPEED LKNOTS: LCC - Year 0 - 4 - 11 - 22 - 33 b34 41.8408 - 8 0 + 1 0 -48.408 - 2 0 + 2 0 Year - 2 0 + 4 + 0 -10.404 - 2 7 1 4	MIND SPEED (KNOTS) LCC - V88Y 0
**************************************	**PO 4.08 *5 0 5 11 4 0 **VBBY N5 + 31 53 14 1 **NO 4.38 + 21 32 7 . **MC 4.210 0 21 28 5 0 **239	*20 4 08 48 1 7 19 8 + **Y89" AS 8 28 45 12 + **S0 4 AS 5 21 27 7 + **MC A A 10 4 18 21 5 + **E462	*20 4 08 46	*20 4 0R *5	420 4 OR 46 1 11 11 1
13	1 4	15	16	17	19
HIND SPEED (KNOTG) CCC - V66T 3 6 6 11 27 37 38 11.64.08 - 18 0 0 0 0 0 48.4.08 - 18 0 0 0 0 0 48.4.08 - 18 0 0 0 0 0 48.4.08 - 18 0 0 0 0 0 48.4.08 - 18 0 1 0 0 48.4.08 - 18 1 4 1 0 48.4.08 - 18 1 14 4 1 0 48.4.08 - 18 1 14 4 1 0 48.4.08 - 18 1 14 1 0 48.4.08 - 18 1 14 1 0 48.4.08 - 18 1 14 1 0 48.4.08 - 18 1 14 1 0 48.4.08 - 18 1 1 1 1 48.4.08 - 18 1 1 1 1 48.4.08 - 18 1 1 1 48.4.08 - 18 1 1 1 48.4.08 - 18 1 1 1 48.4.08 - 18 1 1 1 48.4.08 - 18 1 1 1 48.4.08 - 18 1 1 1 48.4.08 - 18 1 1 48.4.08 - 18 1 1 48.4.08 - 18 1 1 48.4.08 - 18 1 1 48.4.08 - 18 1 1 48.4.08 - 18 1 1 48.4.08 - 18 1 1 48.4.08 - 18 1 48.4.08 - 18 1 48.4.08 - 18 1 48.4.08 - 18 1 48.4.08 - 18 1 48.4.08 - 18 1 48.4.08 - 18 1 48.4.08 - 18 1 48.4.08 - 18 1 48.4.08 - 18 1 48.4.08 - 18 1 48.4.08 - 18 1 48.4.08 - 18 1 48.4.08 - 18 1 48.4.08 - 18 1 48.4.08 - 18 1 48.4.08 - 18	HIND SPEED (XNDIS) LCC - V86Y	HIND SPEED (KNOTE) LCC - VABY 3 10 11 12 25 94 94 14 15 15 16 15 16 16 16 16 16 16 16 16 16 16 16 16 16	MIND SPEED (KNDTS) LCC - V88Y	HIND SPEED (KNOTE) LCC - VBBY	HINO 8PEC (KNOTS) LCC - Y68Y
22	23	. 24	25	26	27
HIND SPEED (RNOTS) CCC - Year 3	HIND SPEED (KNOTS) LCC - V88Y 3 10 21 27 27 354 41.84 OR 45 0 0 0 0 0 48 4 OR 42 0 4 4 0 V88Y 42 0 0 4 4 0 V88Y 55 15 57 25 3 0 X80 4 35 15 52 2 2 0 MC 4 4 10 14 51 20 2 0	MIND SPEED (KNOTS) LCC - V&BY 0 4 11 22 32 32 1 - 1 - 1 - 1 22 22 32 32 1 - 1 - 1 - 1 22 22 32 32 1 - 1 - 1 - 1 22 22 32 32 1 - 1 - 1 - 1 22 22 22 22 1 - 1 - 1 - 1 22 22 22 22 1 - 1 - 1 - 1 22 22 22 22 1 - 1 - 1 - 1 22 22 22 22 1 - 1 - 1 22 22 22 22 22 1 - 1 - 1 22 22 22 23 23 1 - 1 - 1 22 23 24 24 1 - 1 - 1 24 24 24 1 - 1 - 1 24 24 24 1 - 1 - 1 24 24 1 - 1 - 1 24 1 - 1 - 1 24 1 - 1 - 1 24 1 - 1 - 1 24 1 - 1 - 1 24 1 - 1 - 1 24 1 - 1 - 1 24 1 - 1 24 1 - 1 24 1 - 1 24 1 - 1 24 1 - 1 24 1 - 1 24 1 - 1 24 1 - 1 24 1 - 1 24 1 - 1 24 1 - 1 24 1 - 1 24 1 - 1 24 1 - 1 24 2 - 1 2 - 1 24 2 - 1 2 - 1 2 - 1 2 - 1 2 - 1 3 - 1 4 - 1 3 - 1 4 - 1 4 - 1 5 - 1 5 - 1 5 - 1 6 - 1 6 - 1 6 - 1 6 - 1 7 - 1 7 - 1 8 - 1 8 - 1 9 -	HIND SPEEU (KNOTE) LCC - VARY 0 10 10 10 10 10 10 10	HIND SPEED (XNOTS) LCC - VSSY	HIND SPEED (KNDTS) LCC - Y8BY
31	32	33	34	35	36
MIND SPEED (KNOTS) 1-1 V6AT	MIND SPEED (XNOTS) LGC - VESY 2 10 21 53 bas 1.5 4 08 - 5 0 0 0 0 0 -8 4 08 - 2 0 2 1 0 4 VESY - 2 0 + 0 0 0 -10 4 08 - 9 0 6 6 3 1 -20 4 08 4	NIND SPEED (KNOTS) LCC - VSST	HIND SPEED (KNOTS) LCC - V68Y	- MIND SPEED (KNOTS)	INSUFFICIENT DATA
40	4 1	42	43	4 4	45
INSUFFICIENT DATA	HIND SPECU (MOTS) 1.0 2 3 33 34 1.5 4 08 - 6 0 0 0 0 0 0 1.5 4 08 - 7 0 0 0 0 0 1.5 4 08 - 7 0 0 0 0 0 1.5 4 08 - 7 0 0 0 0 0 1.5 4 08 - 7 0 0 0 0 0 1.5 4 08 - 7 0 0 0 0 0 0 1.5 4 08 - 8 0 0 0 0 0 0 0 1.5 4 08 - 8 0 0 0 0 0 0 0 0 1.5 4 08 - 8 0 0 0 0 0 0 0 0 1.5 4 08 - 8 0 0 0 0 0 0 0 0 0 1.5 4 08 - 8 0 0 0 0 0 0 0 0 0 1.5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	INSUFFICIENT DATA	MIND SPEED (MOIS) 1.CC - YEAT 9 10 21 33 834 1.84 08 4.6 0 0 0 0 0 0 48 4 08 42 0 0 0 0 0 YEBY 42 0 0 0 0 0 10 4 08 47 0 0 0 6 0 0 48 0 08 48 0 0 0 0 0 0 48 0 8 48 0 0 0 0 0 0 0 48 0 8 48 0 0 0 0 0 0 0 0 48 0 8 48 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	INSUFFICIENT DATA	INSUFFICIENT DATA

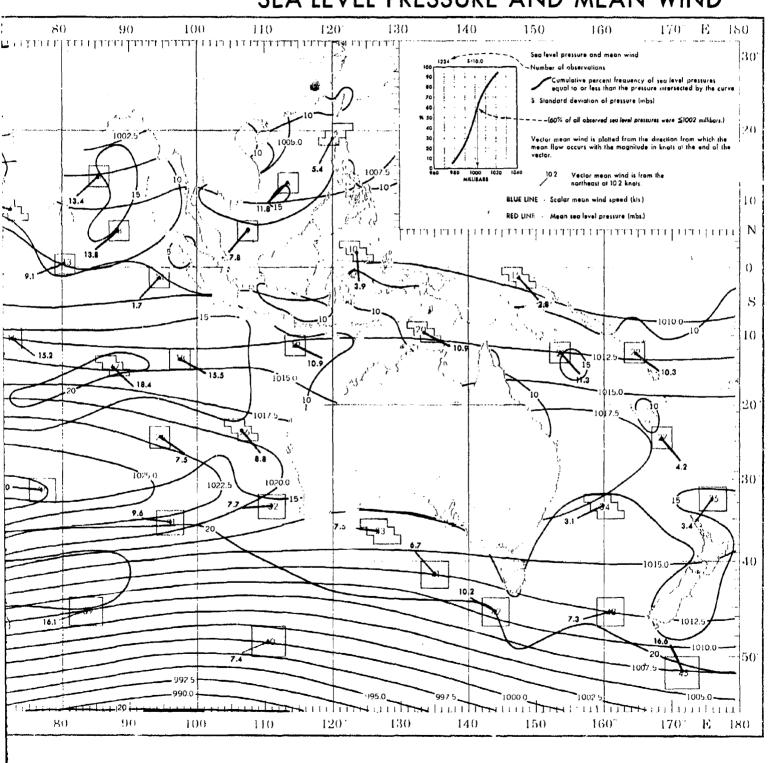
ctive compilation of available data for specified areas without regard to suspected biases.

posite page) are based on all available data subjectively adjusted where bias was evident.

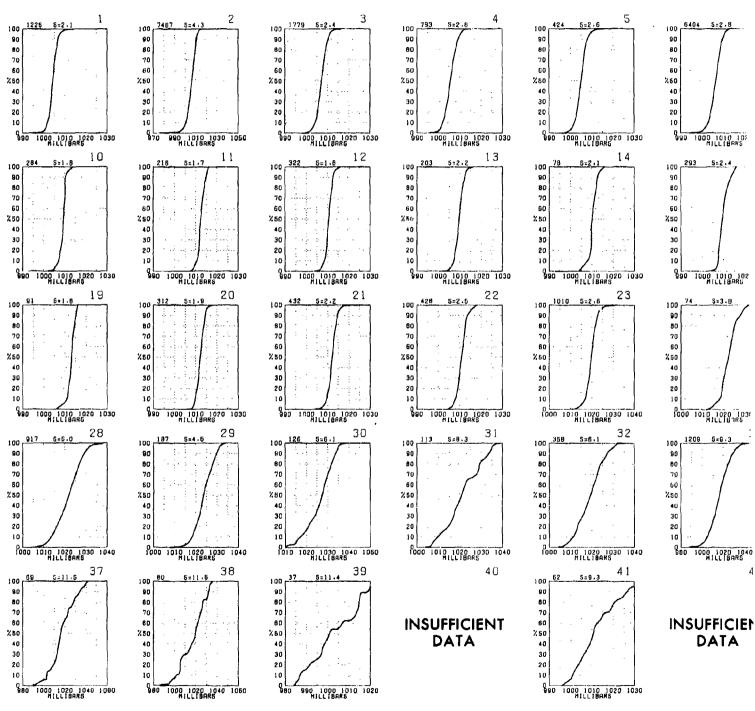
SEA LEVEL PF



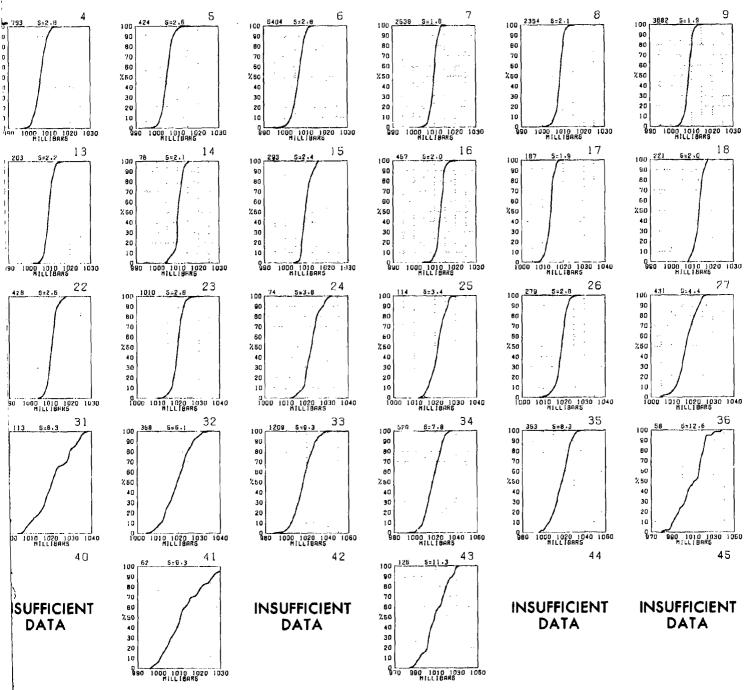
SEA LEVEL PRESSURE AND MEAN WIND



SEA LEVEL PRESSURE

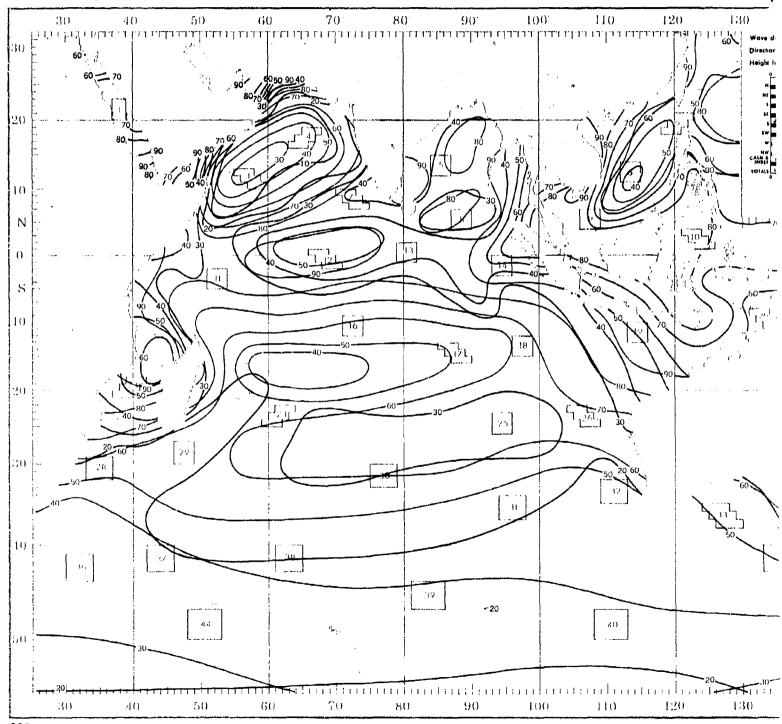


<u>Graphs</u> represent the objective compilation of available data for specified areas witho The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adj

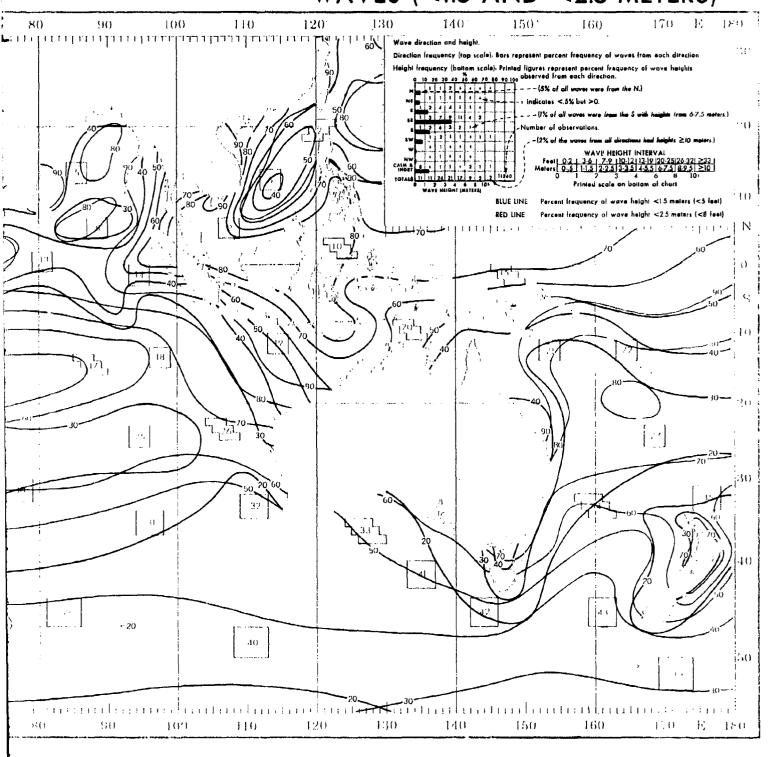


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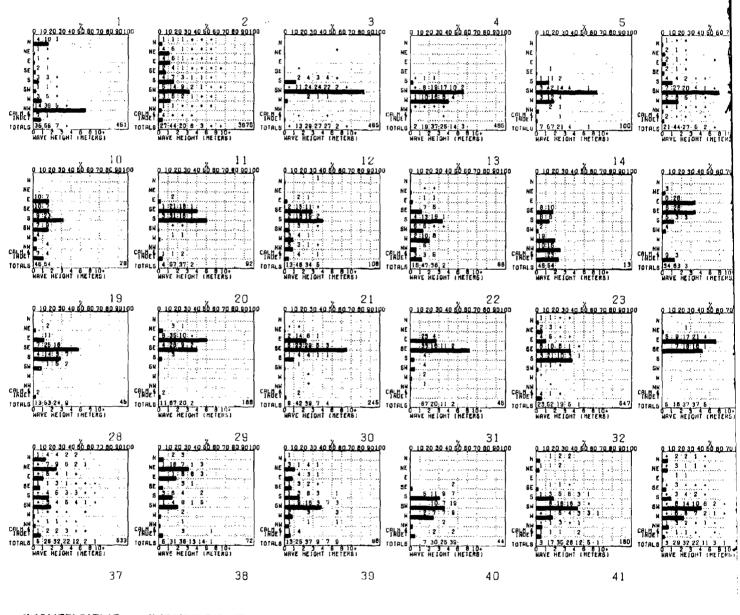
WAVES (



WAVES (<1.5 AND <2.5 METERS)



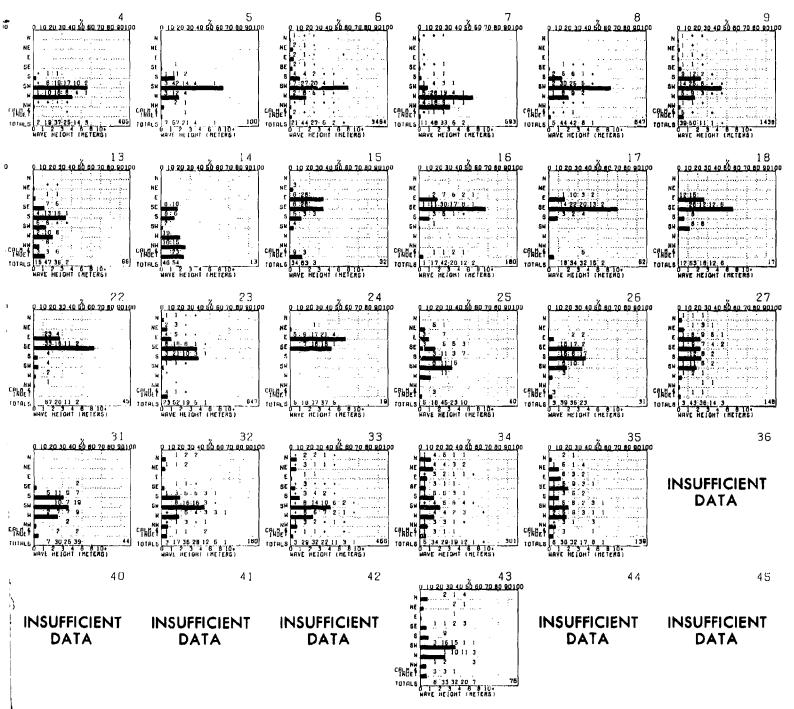
WAVE DIRECTION AND HEIGHT



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ective compilation of available data for specified areas without regard to suspected biases. posite page) are based on all available data subjectively adjusted where bias was evident.

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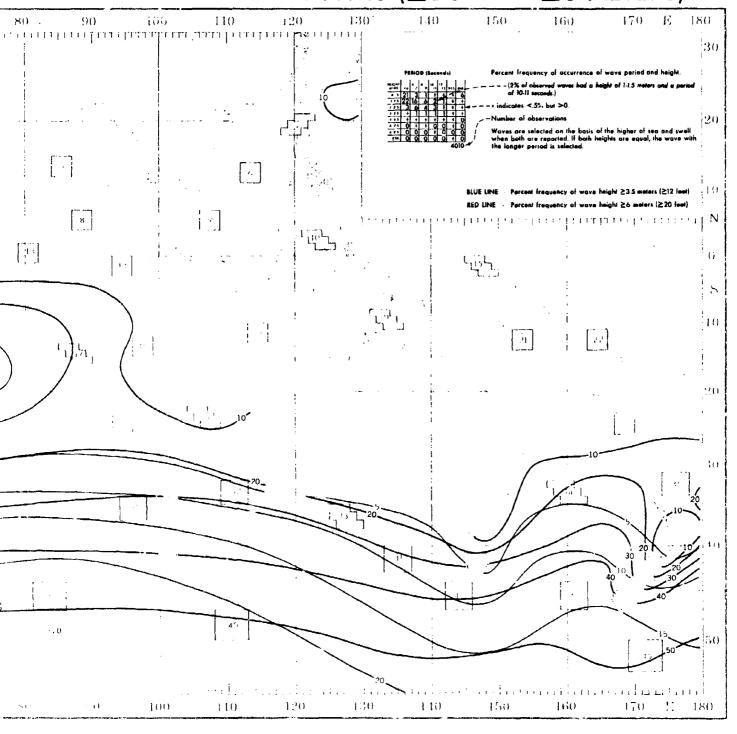
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WAVES (≥3.5 AND ≥6 METERS)



WAVE PERIOD AND HEIGHT

PERIOD (SECONDS) ***Clord** 4-8	PERIOD (SECONDS)	PER 100 I SECONDS: ***ELEM** 18	PERIOD (SECONDS) will low 6- 6- 15- 15- 15- 15- (#IRES 48 7 8 11 13 135 160 6- 1 0 0 0 0 0 0 1-1-1-8 6 7 2 1 1 0 2 7-7-1-8 3 12 13 4 2 1 1 1-3-1-8 1 4 6 8 3 2 1 1-3-1-8 0 0 1 1 0 0 1 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-3-1-8 0 0 0 0 0 0 1-	PERIOD (SECONDS)	PERIOD I SELUND 14 14 15 15 15 14 15 15 15 15 15 15 15 15
Company Comp	1	PERIND (SECONDS) PERIND (SECO	1 3	INSUFFICIENT DATA	PERIOD (SECOND)
19 FERTIOD ISECONDS1 1888 1889 188	PERIOD (SECONDS) albay a 7 9 10 11 12 10 10 11 11 11 11 11 11 11 11 11 11 11	21 **Elbert** **Initial** **	PERIOD (SECONDS) ***Tobal 14	#ERIDO (SECONDS) MEISSAN 10 10 10 10 10 10 10 1	FERIOD (SECONDS) (ATOM) 48 7 8 11 13 13 12 6-6 5 0 0 0 0 0 0 1-1-8 5 5 5 0 0 0 1-1-8 5 5 5 5 0 0 1-1-8 5 5 5 5 0 0 1-1-8 5 0 0 5 5 26 0 1-1-8 0 0 0 0 5 0 1-1-8 0 0 0 0 0 0 0 1-1-8 0 0 0 0 0 0 0 1-1-8 0 0 0 0 0 0 0 0 1-1-8 0 0 0 0 0 0 0 0 1-1-8 0 0 0 0 0 0 0 0 1-1-8 0 0 0 0 0 0 0 0
28 PERIOD (SECONDS) ***(1964)** **(1974)**(19	PERIOD ISECONDSI **IDM**	30 PERIOD (SECONDS) ***I (104)** 1	31 PERIOD (SECONDS) *** *** *** *** *** *** ** ** ** ** **	32 PERIOD (SECONDS) ***Closs** 4	PERIOD (SECONDS (1988) 48 7 8 110 137 137 137 137 137 137 137 137 137 137

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<u>Graphs</u> represent the objective compilation of available data for specified areas without The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjust

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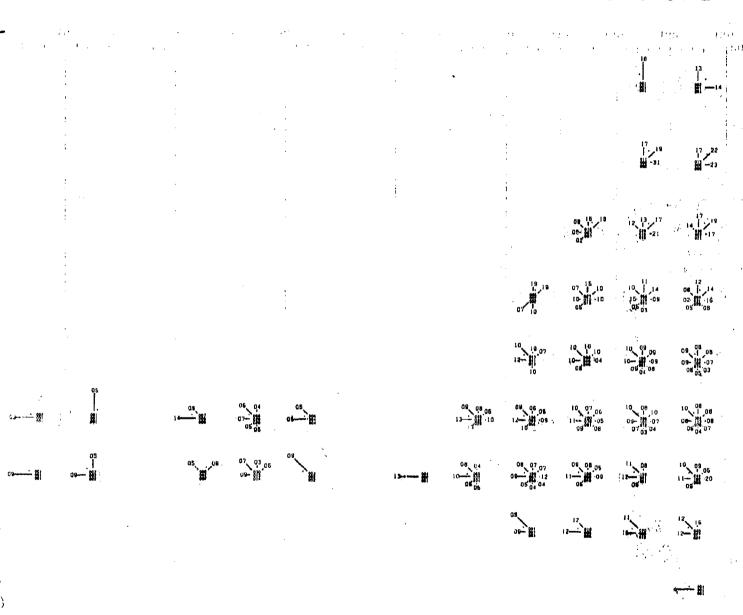
FERIOD (SECONDE) MI 100 7 9 10 12 12 13 100	FERIOD (SECONUS) PERIOD (SECONUS) 10183 46 7 8 111 13 13 130 0-6 7 0 0 0 0 0 0 0 0 1-1-6 29 27 9 2 0 0 0 0 2-6-5 1 15 3 1 0 0 1 1 3-3-6 0 1 1 1 2 0 0 0 0 4-6-6 0 0 0 0 0 0 0 0 0-7-8 0 1 0 0 0 0 0 0 0-7-8 0 1 0 0 0 0 0 0 0 0-7-8 0 0 0 0 0 0 0 0 0 0-7-8 0 0 0 0 0 0 0 0 0	PERIOD (SECONDS) HALDON 1 10 - 12 - 12 - 12 14 15 15 16 O-8 21 1 + + + + + + + + + + + + S-1.5 4 10 9 3 1 + + + + S-2.5 + 2 2 1 4 + + + S-3.5 + 2 2 1 4 + + S-3.5 + 2 2 1 4 + + S-3.5 + 2 2 1 4 + S-3.5 + 2 2 1 4 + S-3.5 0 0 0 0 0 0 S-3.5 0 0 0 0 0 S-3.5 0 0 0 0 0 S-3.5 0 0 0 0 0 S-3.5 0 0 0 0 0 S-3.5 0 0 0 0 0 S-3.5 0 0 0 0 0 S-3.5 0 0 0 0 0 S-3.5 0 0 0 0 0 S-3.5 0 0 0 0 0 S-3.5 0 0 0 0 S-3.5 0 0 0 0 S-3.5 0 0 0 0 S-3.5 0 0 0 0 S-3.5 0 0 0 0 S-3.5 0 0 0 0 S-3.5 0 0 0 0 S-3.5 0 0 0 0 S-3.5 0 0 0 S-3.5 0 0 0 S-3.5 0 0 0 S-3.5 0 0 0 S-3.5 0 0 S-3.5 0 0 S-3.5 0 0 S-3.5 0 0 S-3.5 0 0 S-3.5 S-3.5 0 S-3.5 S-3.5 0 S-3.5 S-3.5 0 PERIOD (SECONDS) **Clost 6- 6- 10- 18- 13- 140 **Chart 6- 6- 10- 18- 13- 140 **Chart 6- 6- 10- 18- 13- 140 **Chart 6- 6- 7- 6- 11- 13- 13- 140 **Chart 7- 8- 11- 13- 13- 140 **Chart 7- 11- 13- 13- 140 **Chart 7- 11- 13- 13- 140 **Chart 7- 13- 13- 13- 140 **Chart 7- 13- 13- 13- 13- **Chart 7- **Cha	PERIOD SECONDS	PERIOD (SECONDS) 10	
PERIOD (SECONDS)	INSUFFICIENT DATA	PERIOD ISECONOS1	FERIOD (SECONDS) FERIOD (SECONDS) FERIOD (SECO	PERIOD (SECONDS) ***PERIOD (SECONDS) **PERIOD (SECONDS) ***PERIOD (SE	INSUFFICIENT DATA
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NSUFFICIENT DATA	INSUFFICIENT DATA	INSUFFICIENT DATA	43 PERIOU (SECONOS: INTER: 40	INSUFFICIENT DATA	INSUFFICIENT DATA

tive compilation of available data for specified areas without regard to suspected biases. site page) are based on all available data subjectively adjusted where bias was evident.

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12 hourly movements of tropical cyclone centers (wind speed estimated ≥34 knots). Mean speed Printed liquie of the end of each bar represents the mean speed of movement (in knots) toward the indicated direction. ~~ (Centers moving toward the N had a mean speed of 5 knots.) Direction frequency: Bars represent percentage frequency of centers that moved toward each direction. Each circle represents 20%. ~ - (35% of all tropical cyclones moved toward the NE.) Vector mean direction and speed. Dot indicates mean vector movement. Each circle equals 10 knots. --- (Mean vector movement of all centers was toward 75° # 7 knots.) -Statistics for this rose are based on 277 twelve liber 50 individual storms were observed in the 5° X 5° area during the period of record. Probability of having at least one tropical cyclone in this area in any given year for this month is 26%.

TROPICAL CYCLONE

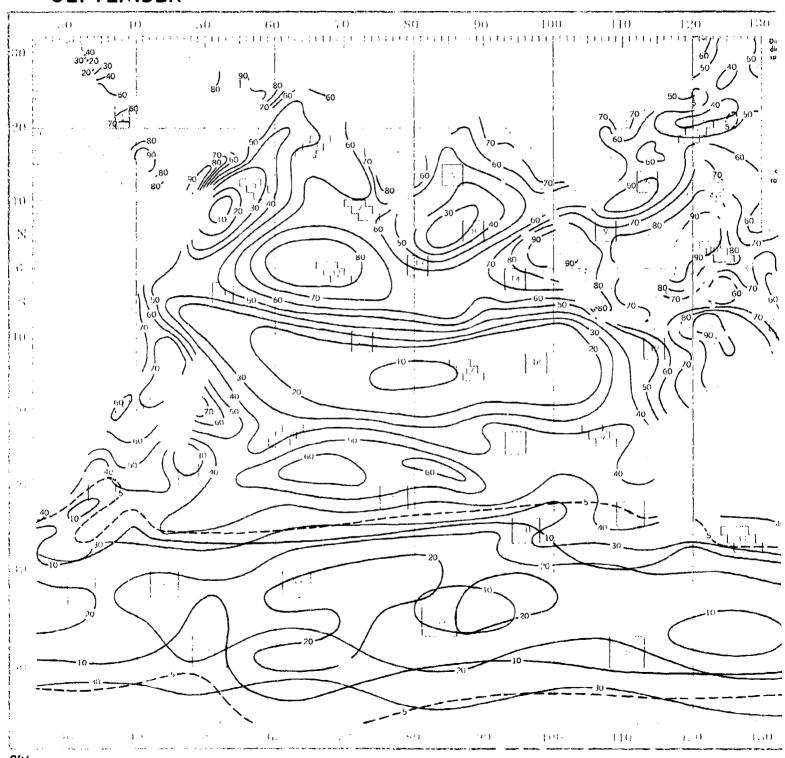


TROPICAL CYCLONE

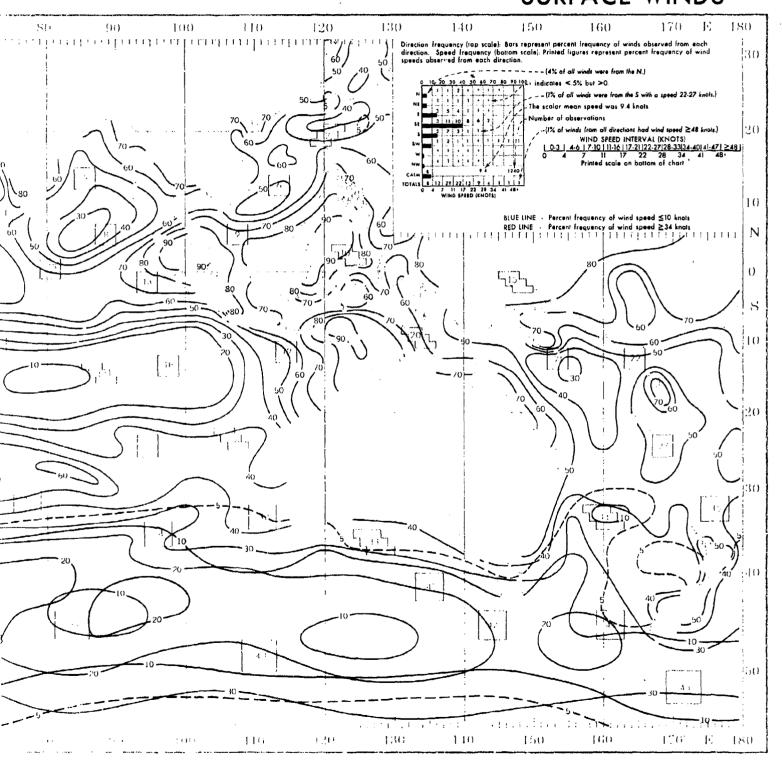
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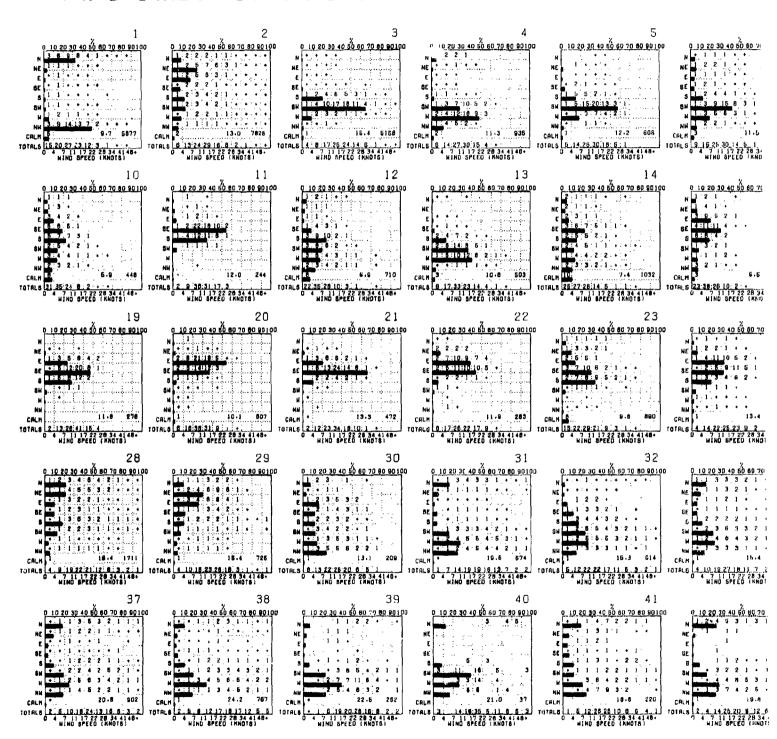
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	:		:						Direction fro centers that represents 2	equency: Bars repr moved toward ea	esent percen ch direction.	tage frequency Each circle	of !
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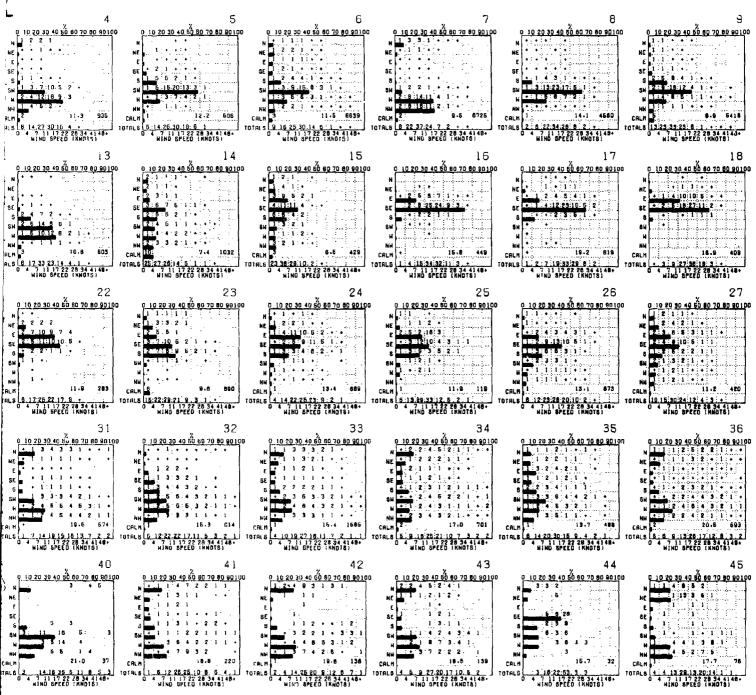
SURFACE WINDS



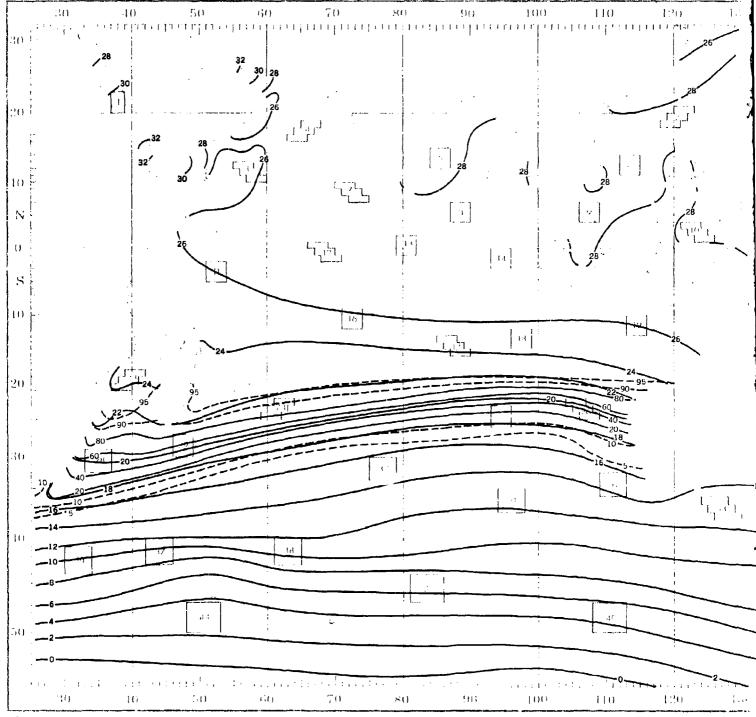
WIND DIRECTION AND SPEED



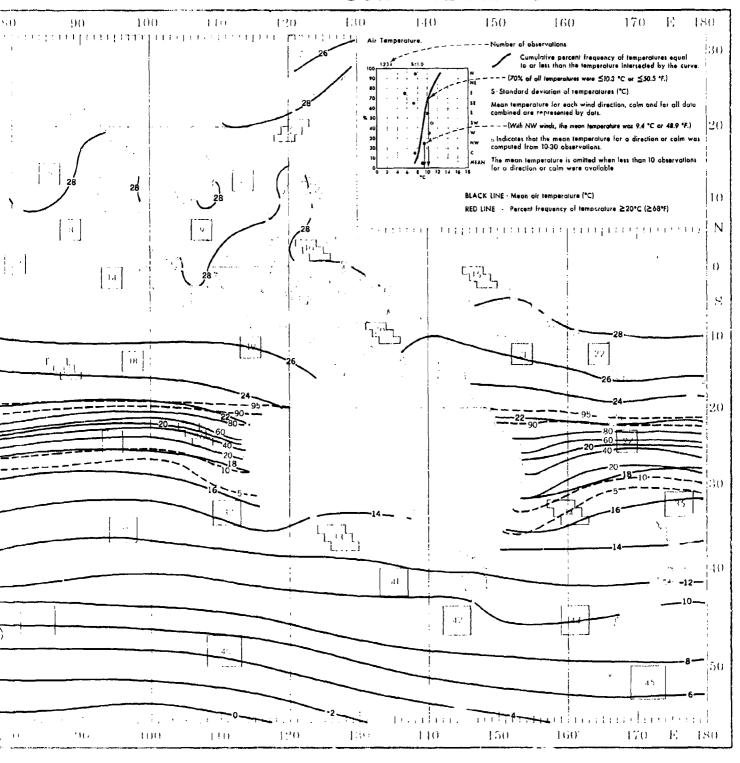
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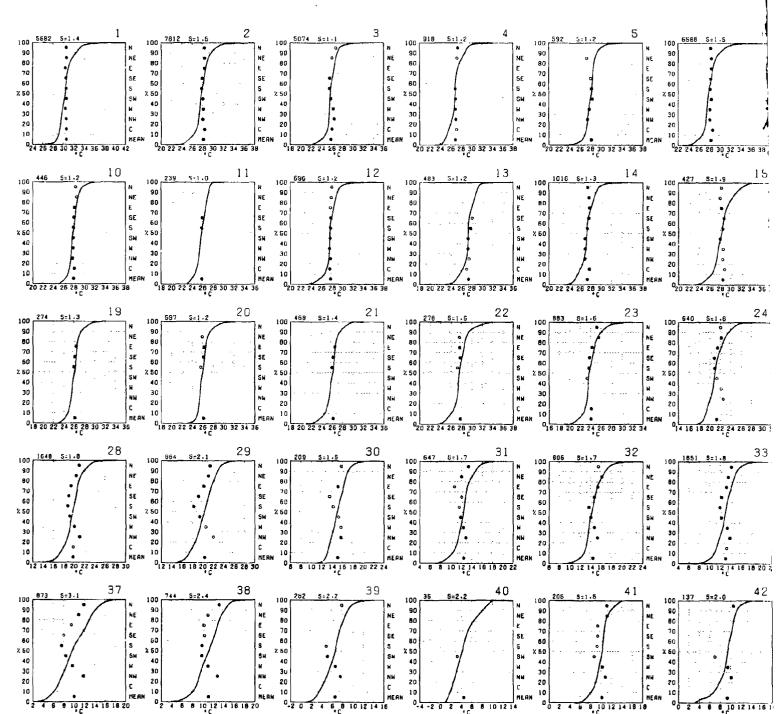
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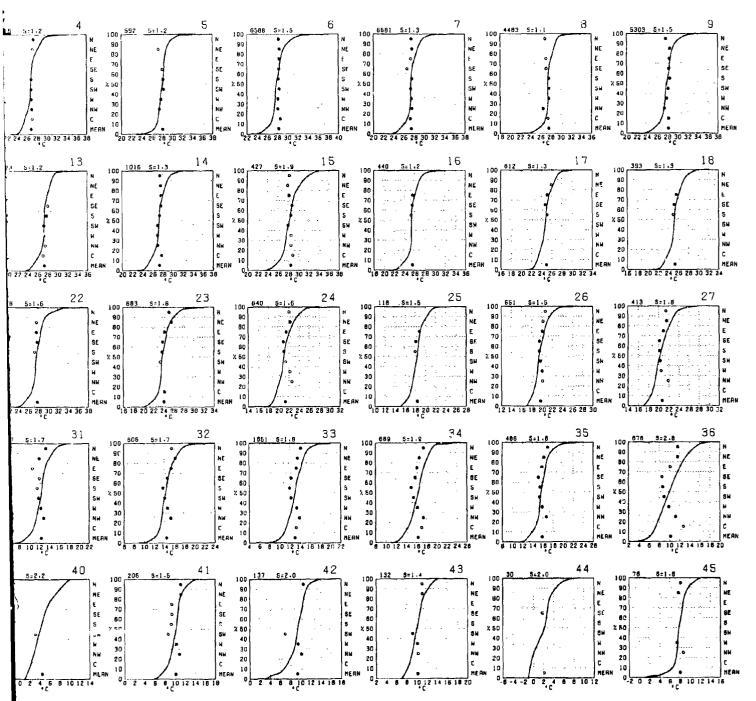
SURFACE AIR TEMPERATURE



SURFACE AIR TEMPERATURE



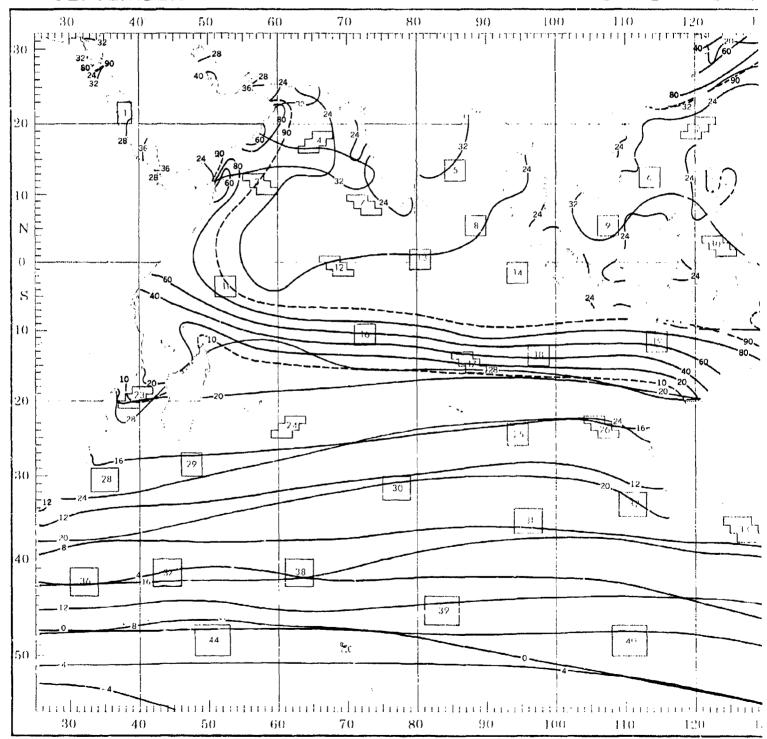
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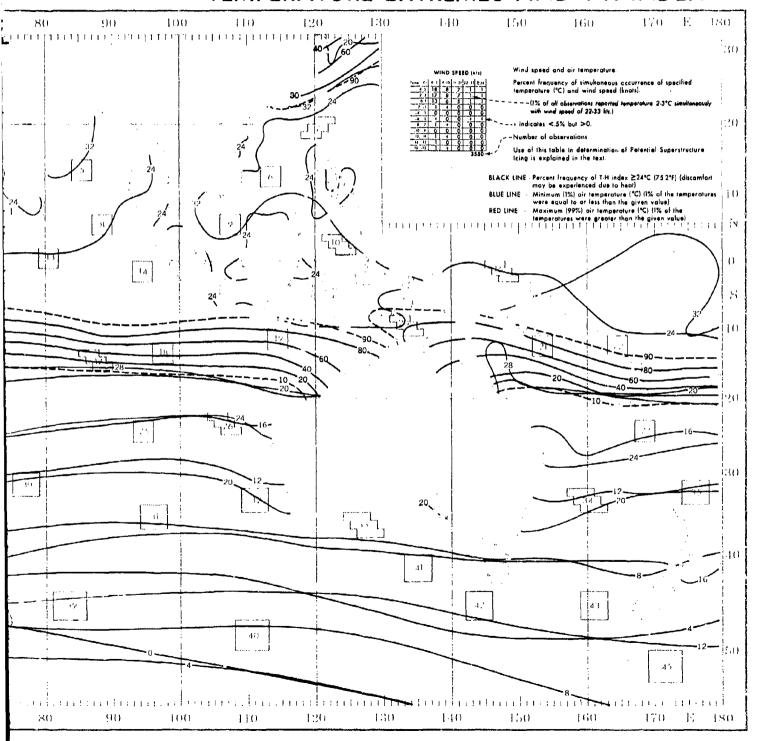
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e page) are based on all available data subjectively adjusted where bias was evident.

TEMPERATURE



TEMPERATURE EXTREMES AND T-H INDEX



WIND SPEED AND AIR TEMPERATURE

1	2	3	4	5	
HIND SPEED (KTS)	HIND SPEED (HTS) 2		WIND SPEED (KTS) 4	WIND SPEED (KTS) 5	WIND SPEED (KTS:
40,41 + + 0 0 0	30.37 + + + 0 0 34.35 + + + + D	32,33 + + + 0 0	37.33 0 + + 0 0 30.31 + 1 2 0 0	32,33 0 + 1 0 0 30,31 1 3 3 + 0	36.37 + + +
36.37 + + 0 0	32.33 + 1 1 + 0	20.29 1 2 3 1 +	20.29 1 10 11 + 0	29.29 4 29 34 4 0	32.33 + 1 1 .
32.53 3 8 7 1 +	29.29 3 21 25 6 1	24.25 1 7 13 9 1	24.25 1 3 2 + 0	24.25 0 • 1 • 0	20.20 5 23 24 3
30.31 8 27 19 2 + 20.20 3 9 7 1 +	26.27 _1 10 12 3 + 24.25 + 1 1 + +	20.21 0 0 0 0 0	22.23 0 0 0 0 0 0 20.21 0 0 0 0 0	22,23 0 0 0 0 0 0 20,21 0 0 0 0 0	26.27 2 10 11 7 24.25 4 1 1
24.28 0 4 0 0 0	20.21 0 + 0 0 0	18.19 O O O O O 18.17 O O O O O	18.19 0 0 0 0 0 0 18.17 0 0 0 0 0	18.19 G O O O O O O O O	22.23 0 0 + 4 20.21 0 0 0 0
20.21 0 0 0 0 0	10.19 0 0 0 0 0 0 10.17 0 0 0 0 0	14.18 0 0 0 0 0 0 12.13 0 0 0 0 0	14.15 0 0 0 0 0 0 12.13 0 0 0 0 0	14.15 0 0 0 0 0 12.13 0 0 0 0 0	10.10 0 0 0 0 10.17 0 0 0 0
5697	7818	5079	921	597 1.4	
HIND SPEED (KTS)	WIND SPEED (KTS) 11	HIND SPEED (KTS) 12	HIND SPEED (KIS) 13	HIND SPEED (KTS)	WIND SPEED (KIS)
TEMP (*C1 0-3 4-10 11-2122-39 2 34)	28.28 0 3 + + 0	TEMP (*C) 0-3 4-10 11-21 22-33 a 34	30.31 1 3 1 0 0	TEMP (*C)	34.35 + 1 0 0
30.31 3 6 0 0 0 20.20 22 35 5 + 0	28.27 2 31 36 2 0 24.26 0 13 11 1 0	30.31 1 4 + 0 0 20.28 13 32 4 1 0	28.29 5 23 16 2 0 24.27 3 22 16 2 +	30.31 2 3 1 0 0 20.28 13 22 8 + 0	32.33 3 4 + 0 30.31 5 10 1 0
20.27 6 16 5 + 0 24.25 + 1 + 0 0	22,23 0 + 1 0 0	26.27 7 25 7 1 + 24.25 + 2 1 + 0	24.25 1 1 4 1 0 27.23 0 0 0 0 + 0	26.27 9 24 8 1 0	28.29 10 28 7 0 26.27 4 20 3 +
22.23 0 0 0 0 0 0	10,10 0 0 0 0 0	22.23 0 0 0 0 0 20.21 0 0 0 0 0	20.21 0 0 0 0 0 18.19 0 0 0 0 0	22.23 0 + 0 0 0 20.21 0 0 0 0 0	24.25 + 2 1 + 22.23 + 0 0 0
18.19 0 0 0 0 0 0	14:16 0 0 0 0 0	10.19 0 0 0 0 0 15.17 0 0 0 0 0	18.17 0 0 0 0 0 14.18 0 0 0 0 0	18.19 D O O O O O O O	22.23 + 0 0 0 20.21 0 0 0 0 18.19 0 0 0 0
14-18 0 0 0 0 0 0 18-13 0 0 0 0 0 0	12:13 0 0 0 0 0 0 10:11 0 0 0 0 0 0 0:6 0 0 0 0 0	14.15 0 0 0 0 0 0 12.13 0 0 0 0 0	12.19 D O O O O O	14.15 0 0 0 0 0 12.13 0 0 0 0 0	18.17 0 0 0 0 14.15 0 0 0 0
461	240	599	486	1016	
HIND SPEED (KTS) 19	HIND SPEED (KTS) 20	HIND SPEED (KTS) 21	HIND SPEED (KTS) 22	HIND SPEED (KTS) 23	WIND SPEED (KIS)
7EMF (*C) 0-3 4-10 11-21 22-33 a 24	1EMP (*C) D-3 4-10 11-21 22-33 2-34	TEMP (4C1 0-3 4-10 11-21 22-33 ≥ 34 30.31 0 + 1 0 0	TEMP (*C) 0-3 4-10 11-21 22-33 × 30 32-33 1 2 0 0 0	TEMP (*C) 0-3 4-10 11-21 22-33 2 34	TEMP (°C) 0-3 4-10 11-21 22-33
28.29 1 B 6 0 0 28.27 + 23 35 3 0	30,31 + 1 1 0 0 28,28 1 6 5 + 0	28.29 + 5 8 1 + 26.27 1 23 30 5 0	30.31 1 4 2 + 0 26.29 5 19 16 2 0	30.91 · · 1 0 0 28.29 · 1 1 0 0	20.27 + 1 + 0
24,25 + 7 14 1 0 22,23 0 1 + 0 0	20.27 2 34 24 1 0	24.25 7 6 11 4 0 22.23 + 1 2 + 0	24.27 1 16 20 6 0	26.27 2 6 4 + D 24.25 8 25 14 1 0	22.23 3 13 13 2 20.21 1 17 22 8
20.21 0 0 0 0 0	24.26 2 12 11 0 0 22.69 0 + 0 0 0 20.21 0 0 0 0 0	20.21 0 0 0 0 0	24.25 + 2 1 + 0 22.23 0 0 0 0 0 0 20.21 0 0 0 0 0	22.23 6 17 9 3 0 20.21 + 1 1 + +	18.19 0 2 7 1 16.17 0 + 0 0
18.17 0 0 0 0 0 14.18 0 0 0 0 0 0	18.18 O O O O O O	10.17 0 0 0 0 0	18.18 0 0 0 0 0 18.17 0 0 0 0 0	18.19 0 0 0 0 0 18.17 0 0 0 0 0	14.15 0 0 0 0 12.13 0 0 0 0
18:13 0 0 0 0 0 10:11 0 0 0 0 0	14.15 O O O O O O O O	12.13 0 0 0 0 0 10.11 0 0 0 0 0	14.15 0 0 0 0 0 0 12.13 0 0 0 0 0 0	14.15 0 0 0 0 0 0 0 12.13 0 G U 0 0	10.11 0 0 0 0 0
274	597	469	279	901	
HIND SPEED (KTS) 28	HIND SPEED (KTS) 29	HIND SPEED (KTS) 30	HIND SPEED (KTS) 31		HIND BPEED (KTS)
TEMP (*C) 0-3 4-10 (1-2) 22-33 ± 34 28-27 0 + + + 0		TEMP (*C) 0-3 4-10 11-2122-33 * 34	TEMP (*C) 0-3 4-10 11-21 22-33 = 34	TEMP (+C) 0-3 4-10 11-2122-33 2 34 20 20 21 + + + + 0	1EMP (*C1 0-3 4-10 1)-21 22-33
22.29 1 4 7 4 1	24.25 + 1 3 1 + 22.23 1 4 12 7 0	10.19 0 1 2 2 +	10:17 0 1 3 1 0	18.10 + 2 2 0 +	10.10 + 1 + +
20.21 2 13 18 8 1	10.21 2 10 20 6 +	14.15 4 12 19 4 0	12.13 1 9 20 12 6	14.15 2 15 18 8 3	14.15 2 9 15 5
18.19 1 9 13 6 1 16.17 • 3 3 1 1	18.17 + 2 3 1 1	12.19 + 6 9 1 + 10.11 0 0 0 0 0	10.11 1 5 6 7 2 0.8 + 1 + 2 +	12.13 1 7 10 4 1	10.11 1 5 5 3
14:15 0 + + + + 12:19 0 0 0 0 0 0	14.15 0 + + + 0 12.15 0 0 0 0 0	0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6.7 0 0 0 + 0 4.8 0 0 0 0 0	e.7 0 0 0 0 0	8.9 + + 1 1 8.7 0 0 0 0
10·11 0 0 0 0 0 0 ••• 0 0 0 0 0 0		4.5 0 0 0 0 0 0 2.3 0 0 0 0 0	t.3 0 0 0 0 0 0.1 0 0 0 0 0	4.5 0 0 0 0 0 2.3 0 0 0 0 0	4.8 0 0 0 0 2.3 0 0 0 0
6.7 0 0 0 0 0 0 1857	6.7 0 0 0 0 0 665	0.1 0 0 0 0 0	-t1 0 0 0 0 0 548	0.1 0 0 0 0 0 608	0,1 0 0 0
MIND SPEED (HIS) 37		HIND SPEED (KTS) 39			WIND SPEED (KTS) 4
TEMP (*C1 0-3 4-10 11-21 22-39 > 34	TEMP (*C) 0-3 4-10 11-21 22-39 # 34 10-17 + 1 1 1 -	TEMP (*C) 0-3 4-10 11-21 22-33 2 34	TEMP (*C) 0-3 4-10 11-21 22-33 a 34	TEMP (4C) 0-3 4-10 11-21 22-33 2 34	TEMP (*C) 0-3 4-10 11-21 22-33 1
18.17 + + 2 2 +	14.15 + 1 3 7 3	10-11 0 0 5 4 0	6.7 0 0 6 6 9	12.19 0 4 13 2 1	10.11 1 8 20 7
14.15 + 1 4 3 2 12.15 + 2 10 5 2	10.11 1 5 6 9 5	6.7 + 2 16 17 6	4.5 3 9 11 3 3 2.3 0 3 29 6 0	10.11 1 12 26 9 6 0.0 + 3 12 3 2	6.7 0 1 3 1
10.11 + 4 7 5 3 0.1 + 3 8 8 3	0.0	1.5 0 2 8 5 2 2.3 0 2 3 4 1	0.1 0 0 0 0 0 -21 0 0 0 0 0	4.7 0 0 1 2 1 4.8 0 0 0 0 0	4.8 0 0 1 0 2.3 0 1 1 0
6,7 + 3 6 5 1 4.8 + 1 2 2 +	2.3 0 0 0 + 0	0,1 0 0 0 + 0 -1,-1 0 0 0 0 0	-49 0 0 0 0 0 -48 0 0 0 0 0	2.3 0 0 0 0 0 0.1 0 0 0 0 0	0.1 0 0 0 0 -21 0 0 0 0
0.1 0 0 0 0 0		-43 0 0 0 0 0 0 -64 0 0 0 0 0 0 -01 0 0 0 0 0	-07 0 0 0 0 0 0 -109 0 0 0 0 0	-21 0 0 0 0 0 -43 0 0 0 0 0	-4,-9 0 0 0 0 0 -6,-8 0 0 0 0
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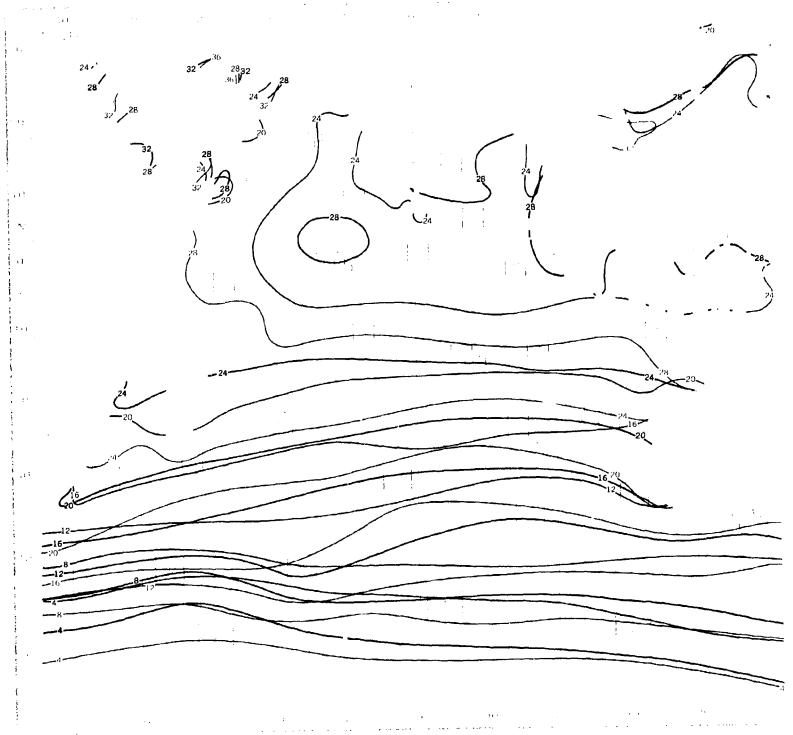
Graphs represent the objective compilation of available data for specified areas without. The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjust

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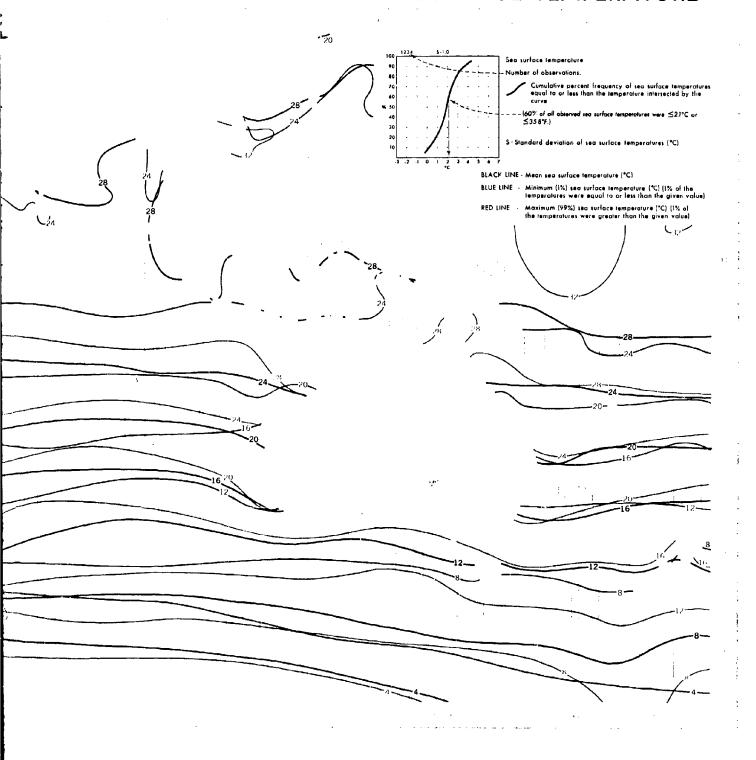
SEPTEMBER

► HINO SPEED (KTS) 4	WIND SPEED (KTS) 5	WIND SPEED (KTS)	WIND SPEED IKTS) 7	WIND SPEED (KTS)	HIND SPEED (KTS)
		TENP (*C) 0-3 4-10 11-21 22-33 2 34			
37.33 0 + 0 0 30.31 + 1 2 0 0	32.33 0 + 1 0 0 30.31 1 3 3 + 0	38.37 + + 0 0 0 34.36 + + 0 0	34.35 0 + 0 0 0 32.33 + 1 + 0 0	32.33 0 + + + 0 30.31 + 1 3 + 0	30.37 0 + + 0 0 34.35 + + + 0 0
28.29 1 10 11 + 0 26.27 6 27 30 4 0	26.29 4 29 34 4 0 26.27 1 8 9 2 0	37.33 + 1 1 + 0 30.31 2 6 6 1 +	30.31 + 4 2 + 0 26.29 3 25 12 + 0	28.29 1 15 32 4 + 28.27 1 11 23 4 +	32.33 + 1 1 + 0 30.31 1 7 3 + 0
24.25 1 3 2 + 0 22.23 0 0 0 0 0	24.25 0 + 1 + 0 22.23 0 0 0 0 0	28.29 5 23 24 3 + 26.27 2 10 11 2 +	26.27 4 27 15 1 +	24.25 0 1 1 + + 22.23 0 + + 0 0	20.27 9 35 17 1 0 26.27 2 12 7 1 +
20.21 0 0 0 0 0 19.18 0 0 0 0 0	20.21 0 0 0 0 0 18.19 0 0 0 0 0	24.25 + 1 1 + + 28.23 0 0 + + 0	22.23 0 + + + 0 20.21 0 0 0 0 0	20.21 O O O O O	24.28 + 1 1 + + 22.23 + + + 0 0
16.17 0 0 0 0 0 0 14.16 0 0 0 0 0	16.17 0 0 0 0 0 0 14.16 0 0 0 0 0	20.21 0 0 0 0 0 18.19 0 0 0 0 0	10.19 0 0 0 0 0 0 16.17 0 0 0 0 0	18.17 0 0 0 0 0 14.16 0 0 0 0 0	19.10 0 0 0 0 0
12.13 0 0 0 0 0 921	12.13 0 0 0 0 0 597	16.17 0 0 0 0 0 0 6601	14-15 0 0 0 0 0 0 6584	12.13 0 0 0 0 0 0 4483	18.17 0 0 0 0 0
WIND SPEED (KTS) 13	WIND SPEED (KTS) 14	HIND SPEED (KTS) 15	HIND SPEED (KTS) 16	HIND SPEED (KIS) 17	HIND SPEED (KTS) 18
MP (*C) 0-3 4-10 11-2122-33 234	7EHP (4C) 0-3 4-10 11-21 22-33 2 34	TEMP (*C) 0-3 4-10 11-2122-33 2 34	TERP (*C) 0-3 4-10 11-21 22-33 2 34	TEMP (*C) 0-3 4-10 11-2122-33 2 34	TERF (*C) 0-3 4-10 11-2122-33 234
30.31 1 3 1 0 0 7 20.28 5 23 16 2 0	32.33 + 0 0 0 0 30.31 2 3 1 0 0	34,35 · 1 0 0 0 32,33 3 4 · 0 0	30.31 0 · · · 0 0 28.29 0 1 3 · 0	30.31 0 0 + 0 0 20.29 0 1 1 1 0	30,31
25.27 3 22 16 2 + 24.25 1 1 4 1 0	28.27 9 24 6 1 0	30,31 5 10 1 0 0 28,29 10 28 7 0 0	26.27 1 8 33 6 4 24.26 0 9 28 7 +	28.27 + 3 17 9 + 24.25 1 4 28 23 1	28.27 + 5 29 8 + 24.25 + 5 32 10 +
22.23 0 0 0 0 + 0 20.21 0 0 0 0 0	24.25 + 4 2 + + 22.23 0 + 0 0 D	28,27 4 20 3 + 0 24,25 + 2 1 + 0	22.23 0 1 1 + 0 20.21 0 0 0 0 0	22.23 0 + 5 4 + 20.21 0 0 0 + 0	22.23 0 1 1 2 0 20.21 0 0 0 0 0
18-19 O O O O O O	#0.21 0 0 0 0 0 10.19 0 0 0 0 0	22.23 + 0 0 0 0 20.21 0 0 0 0 0	10.19 0 0 0 0 0 16.17 0 0 0 0 0	18.17 0 0 0 0 0 0	19.10 0 0 0 0 0 18.17 0 0 0 0 0
14-15 0 0 0 0 0	18.17 0 0 0 0 0	16,19 0 0 0 0 0 16,17 0 0 0 0 0	14.16 0 0 0 0 0	14-15 0 0 0 0 0	14.18 0 0 0 0 0 0 12.13 0 0 0 0 0
12.13 0 0 0 0 0 0 10.11 0 0 0 0 0 0 486	14.18 0 0 0 0 0 12.13 0 0 0 0 0 1016	18-17 0 0 0 0 0 0 14-15 0 0 0 0 0 0 430	12-13 0 0 0 0 0 0 10-11 0 0 0 0 0 0 440	12.13 0 0 0 0 0 0 10.11 0 0 0 0 0 0 612	10.11 C O O O O O
HIND SPEED (KTS) 22	WIND SPEED (KTS) 23	WIND SPEED (KTS) 24	WIND SPEED (KTS) 25	HIND SPEED (KTS) 26	WIND SPEED (KTS) 27
P 190 0-3 4-10 11-2122-39 2 34	TEMP (*C) 0-3 4-10 11-21 22-39 a 34	TEMF (*C) 0-3 4-10 11-21 22-33 2 34	TEMP (*C1 0-3 4-10 1:-21 22-33 a 34	TEMP (40) 0-3 4-10 11-21 22-33 = 34	TEHP (*C) 0-3 4-10 11-21 22-33 2 34
32.33 1 2 0 0 D	32.33 0 + 0 0 0 30.31 + + 1 0 0	28.29 0 + 0 0 0 28.27 + 1 + 0 0	22,23 0 3 0 0 0 20,21 1 9 7 1 0	24.25 0 + + 0 0 22.23 1 5 5 1 +	29,27 1 1 1 0 0
28.28 5 19 15 2 0 28.27 1 16 20 6 0	28.29 + 1 1 0 0	24.26 + 4 3 + 0 22.23 3 13 13 2 1	18.19 5 22 28 2 0 16.17 1 8 8 4 1	20.21 2 15 17 5 0 18.10 3 14 21 5 +	22.23 4 12 5 + 0 20.21 3 19 17 3 0
24.25 + 2 1 + 0 22.83 0 0 0 0 0	24.25 B 25 14 1 0 22.23 6 17 9 3 0	20,21 1 17 22 8 1 18,19 0 2 7 1 +	14.16 0 0 1 0 0 12.13 0 0 0 0 0	16-17 0 1 4 1 0 14-15 0 0 0 0 0	18.18 1 11 12 4 + 16.17 0 0 1 + 0
20.21 0 0 0 0 0	20·21 · 1 1 · · · 1 10·10 0 0 0 0 0	18-17 0 + 0 0 0 14-16 0 0 0 0 0	10.11 0 0 0 0 0 0 •.9 0 0 0 0 0	12.13 0 0 0 0 0 10.11 0 0 0 0 0	14,15 0 0 0 0 0
18-17 0 0 0 0 0 0 14-15 0 0 0 0 0 0	18-17 0 0 0 0 0 0 14-15 0 0 0 0 0	12,15 0 0 0 0 0 10,11 0 0 0 0 0	0.7 0 0 0 0 0 4.5 0 0 0 0 0	6.9 0 0 0 0 0 6.7 0 0 0 0 0	10.11 0 0 0 0 0 0.0 0 0 0 0 0
12.13 0 0 0 0 0	12.13 0 0 0 0 0	0.0 0 0 0 0	2.3 0 0 0 0 0	4.8 0 0 0 0 0	8.7 0 0 0 0 0
HIND SPEED (KTS) 31	WIND SPEED (KTS) 32	HIND SPEED (KTS) 33	HIND SPEED (KTS) 34	HIND SPEED (KTS) 35	HIND SPEED (KTS) 36
P 1*C1 0-3 4-10 11-21 22-33 × 34	TEHP (*C) 0-3 4-10 11-21 22-33 a 34	TEHP (%) 0-3 4-10 11-21 22-33 2 34	1EMP (*C) 0-3 4-10 11-21 22-39 & 34	1EMP (*C) 0-3 4-10 11-81 28-33 = 34	
18.19 0 + 0 0 0 18.17 0 1 3 1 0	20.21 + + + + 0	20.21 0 0 + 0 0	22.23 + + + 0 0	22.23 0 + + 0 0 20.21 1 0 1 + 0	16.19 D O + O O
14.15 0 5 10 6 3 12.13 1 9 20 12 6	16-17 1 9 9 3 1 14-15 2 15 18 8 3	18.17 + 3 4 1 + 14.15 2 9 15 5 1	18.18 1 6 13 4 1 16.17 1 11 18 7 2	18.18 1 3 7 1 + 16.17 3 18 21 4 1	14:15 1 2 3 3 1 12:13 1 3 9 5 1
10.11 1 6 6 7 2 8.8 + 1 + 2 +	.2.13 1 7 10 4 1 10.11 0 + + 1 1	17,13 1 12 19 7 2 10,11 1 5 5 3 1	14:15 2 7 1G 4 2 12:13 + + 3 2 2	14,15 1 13 14 6 1 12,13 + + 1 1 +	10.11 + 4 12 6 3
6.7 0 0 0 + 0 4.5 0 0 0 C 0	6.9 0 0 0 0 0 6.7 0 0 0 0 0	8.7 0 0 0 0 0	10.11 0 0 0 0 0 0.0 0 0 0 0	10.11 0 0 0 0 0 ••• 0 0 0 0 0	6.7 + 2 6 4 2 4.8 0 + 1 + 1
2.3 0 0 0 0 0	4.5 0 0 0 0 0	4.8 0 0 0 0 0	6.7 0 0 0 0 0	6.7 0 0 0 0 0	2.3 0 0 0 0 +
0.1 0 0 0 0 0 -21 0 0 0 0 0	2.3 0 0 0 0 0 0 0.1 0 0 0 0 0 0	2.3 0 0 0 0 0 0 0.1 0 0 0 0 0 0 1655	4.5 0 0 0 0 0 0 2.3 0 0 0 0 0 0	4.6 0 0 0 0 0 0 2.3 0 0 0 0 0 0	0.1 0 0 0 0 0 -11 0 0 0 0 0
HIND SPEED (KTS) 40	HIND SPEED (KTS) 41	HIND SPEED (KTS) 42	HIND SPEED (KTS) 43	HIND SPEED (KTS) 44	HIND SPEED (KTS) 45
F (*C) 0-3 4-10 11-2122-33 a 14	TEHP (40) 0-3 4-10 11-21 22-33 2 34	TEMP (%) 0-3 4-10 11-8188-93 4 94	TERF (40) 0-5 4-10 11-21 22-33 4 34	TERP 1901 0-3 4-10 11-21 22-33 + 34	TERP (*C) 0-3 4-10 11-21 22-33 4 84
8.8 0 0 6 3 6 36.7 0 0 6 6 9	14.15 0 0 0 0 0 0 12.13 0 4 13 2 1	12.19 0 3 5 4 2 10.11 1 6 20 7 0	12.13 2 2 7 6 1 10.11 1 7 29 14 4	6.7 0 3 0 0 0 4.8 0 7 7 3 0	12.19 0 0 1 0 0 10.11 1 0 4 7 0
4.5 3 9 11 3 3 2.1 0 3 29 5 0	10.11 1 12 26 9 6 8.9 + 3 12 3 2	6.9 1 9 15 9 3 6.7 D 1 3 1 3	8.8 2 4 11 8 1 8.7 0 0 2 1 2	2.3 0 3 37 3 0 0.1 0 3 17 0 0	6.8 1 7 20 20 0 6.7 0 11 16 7 3
0.1 0 0 0 0 0	6.7 O O I 2 I 4.8 O O O O O	4.5 0 0 1 0 4 E.3 0 1 1 0 1	4.5 0 0 0 0 0 2.9 0 0 0 0 0	-21 0 0 17 0 0 -43 0 0 0 0 0	4.8 1 0 0 1 0 2.3 0 0 1 0 0
-43 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2.3 0 0 0 0 0 0.1 0 0 0 0 0	0.1 0 0 0 0 0	0.1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-66 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.1 0 0 0 0 0 -21 0 0 0 0 0
-07 0 0 0 0 0 0 109 0 0 0 0 0	-2,-1 0 0 0 0 0 0 -4,-3 0 0 0 0 0	-43 0 0 0 0 0	-43 0 0 0 0 0	-10 0 0 0 0	-43 0 0 0 0 0
211 0 0 0 0 0	-21 D O O O O O O O O O O O O O O O O O O	-67 0 0 0 0 0 0 -67 0 0 0 0 0 0	-88 0 0 0 0 0 0 -87 0 0 0 0 0 0	-1211 0 0 0 0 0 0 -1413 0 0 0 0 0	-07 0 0 0 0 0 0 -07 0 0 0 0 0 0
35	205	137	133	30	76

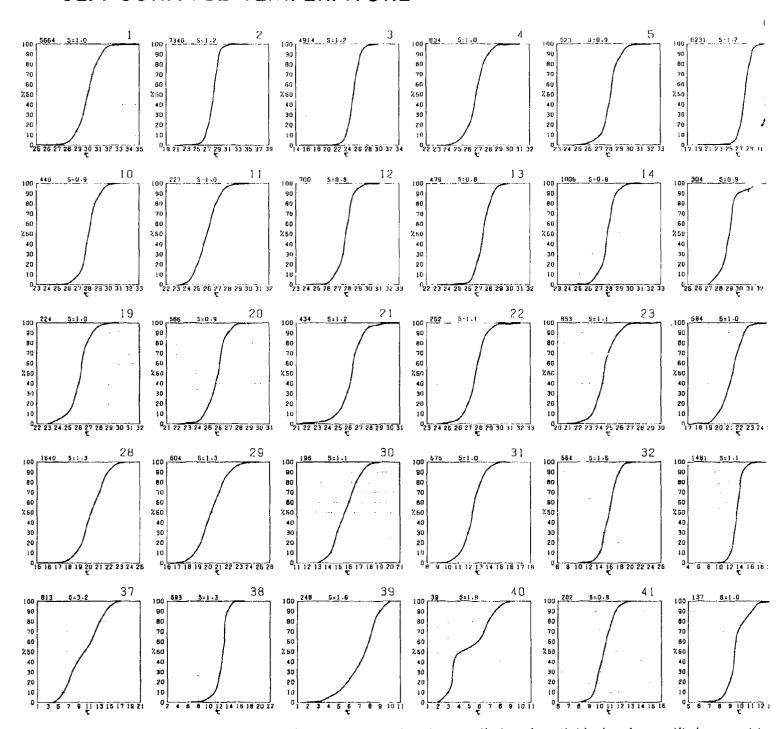
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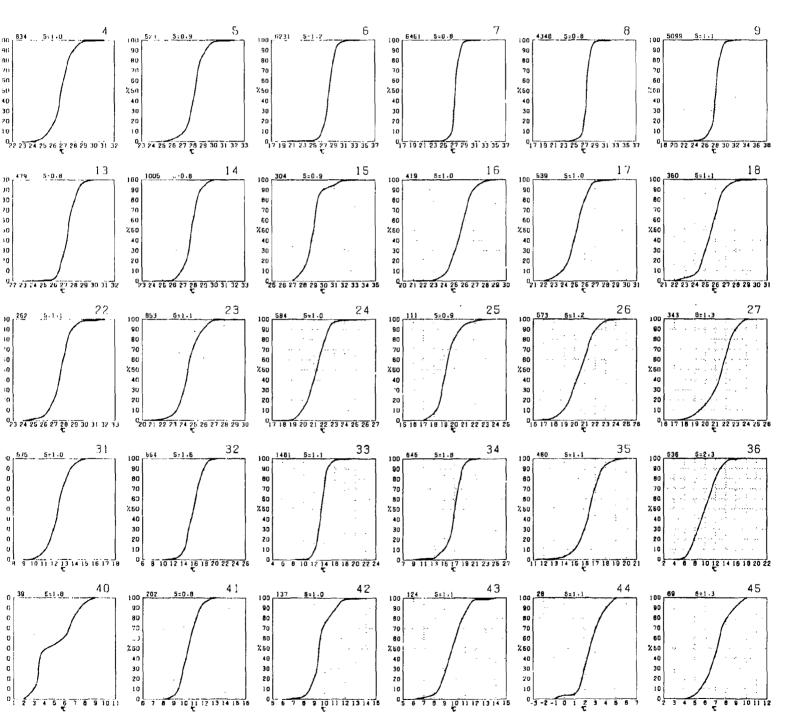
SEA SURFACE TEMPERATURE



SEA SURFACE TEMPERATURE

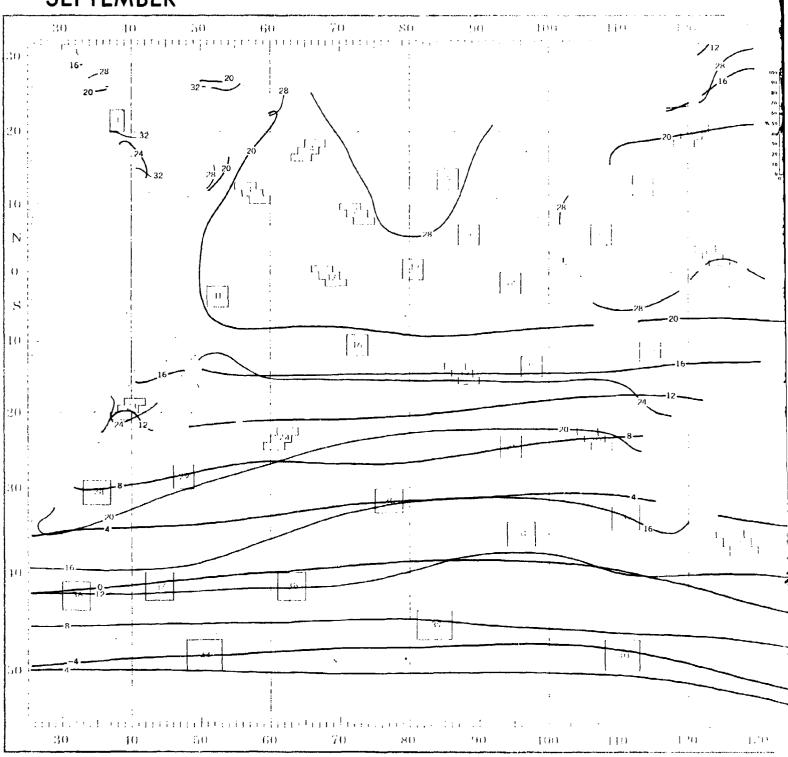


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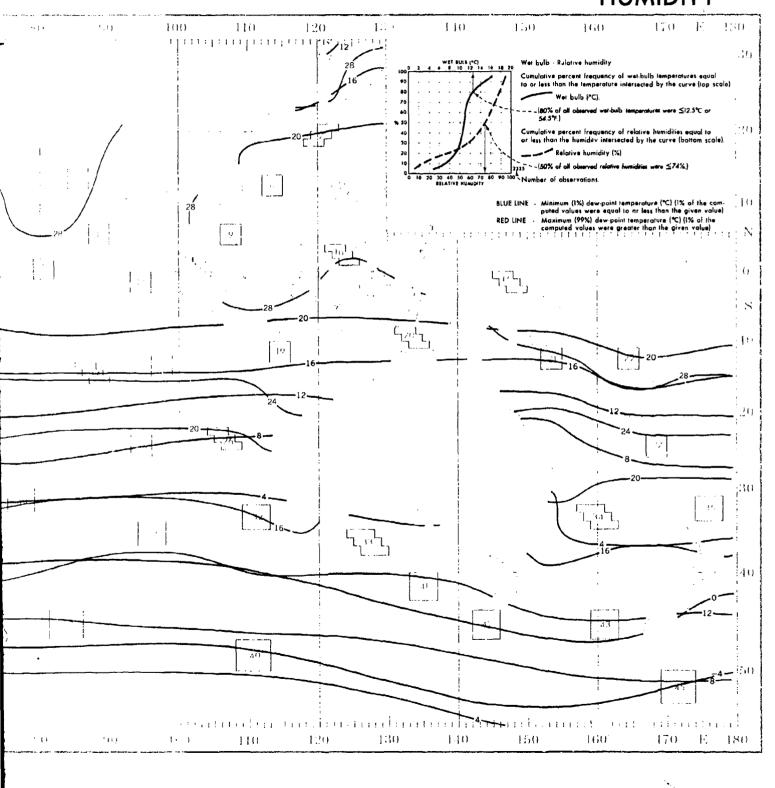


tive compilation of available data for specified areas without regard to suspected biases, osite page) are based on all available data subjectively adjusted where bias was evident.

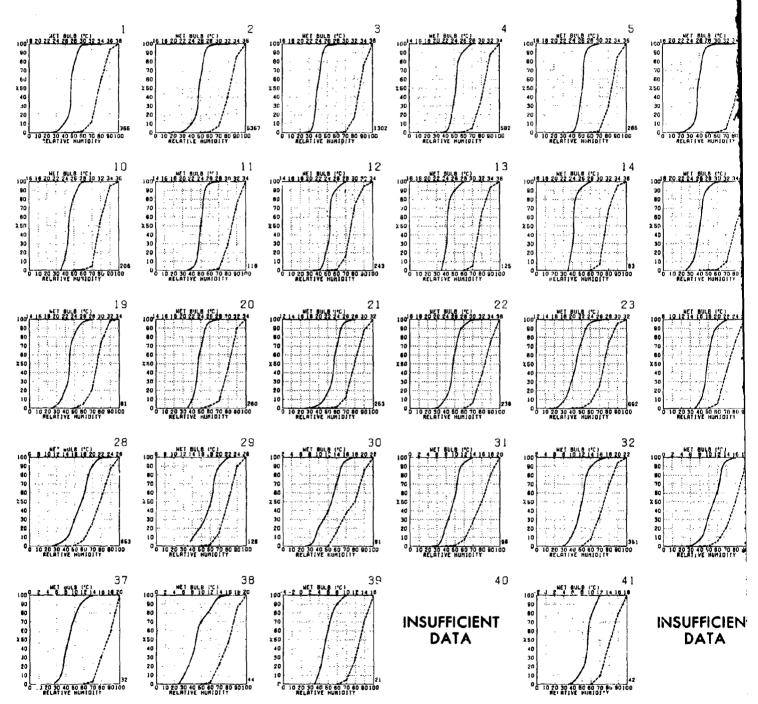
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HUMIDITY



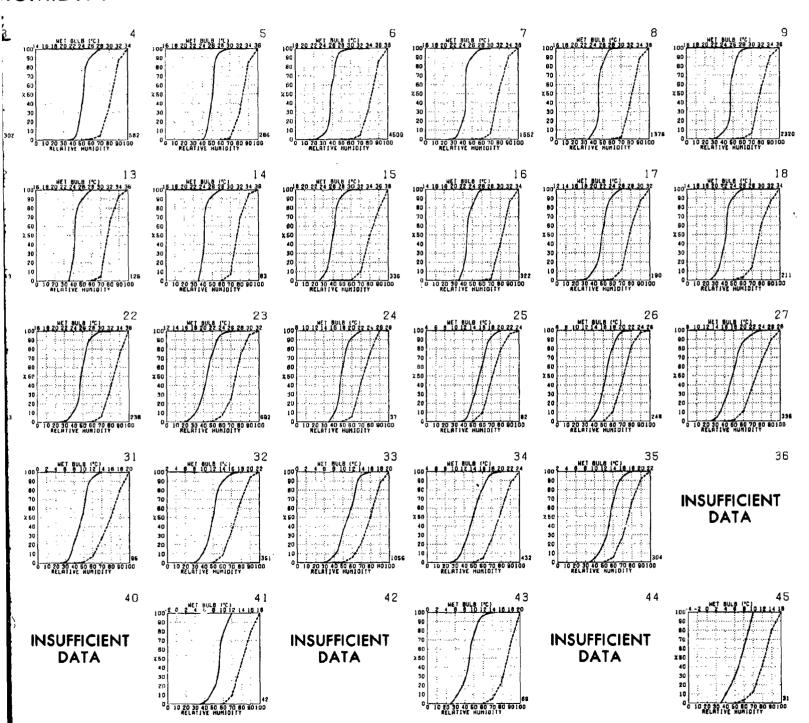
WET BULB AND RELATIVE HUMIDITY



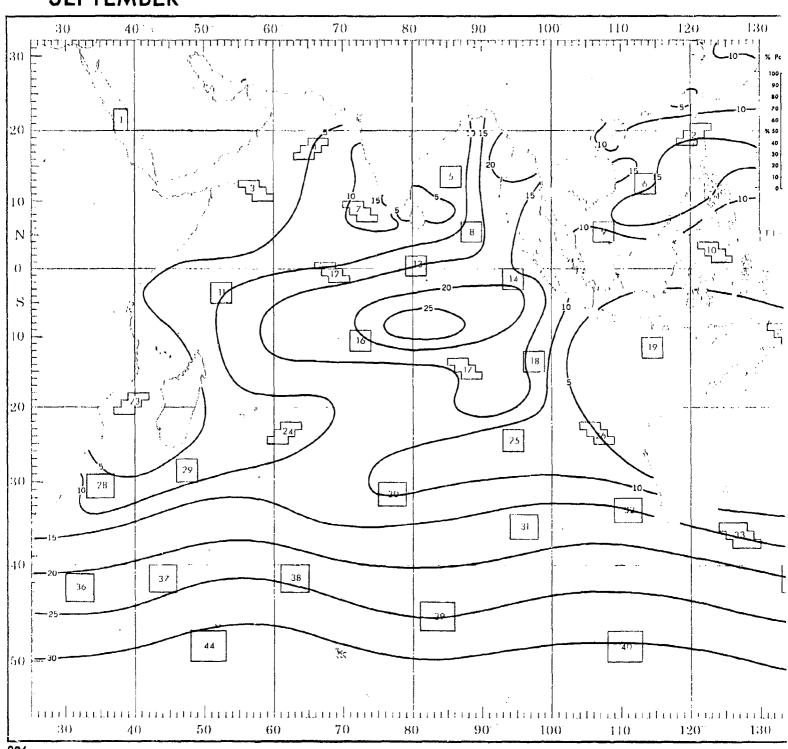
<u>Graphs</u> represent the objective compilation of available data for specified areas without The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adj

HUMIDITY

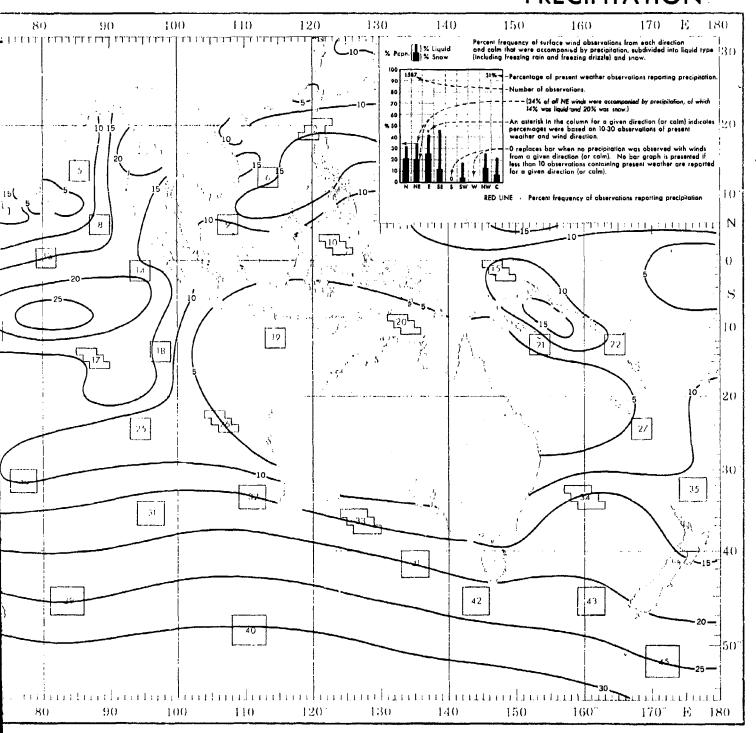
SEPTEMBER



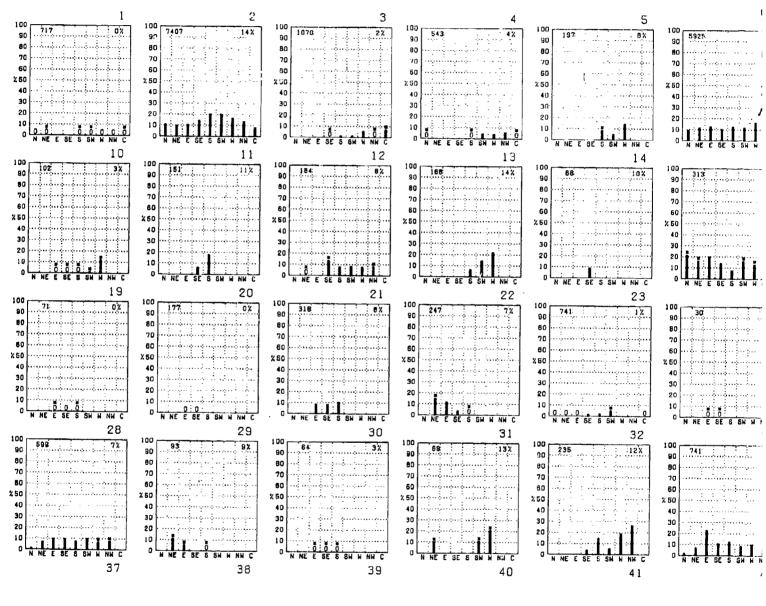
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PRECIPITATION



PRECIPITATION



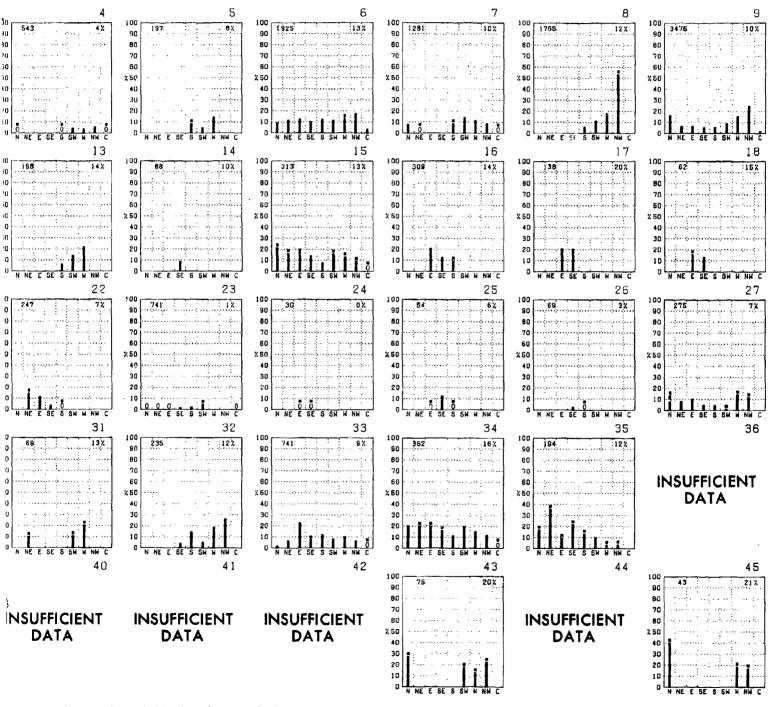
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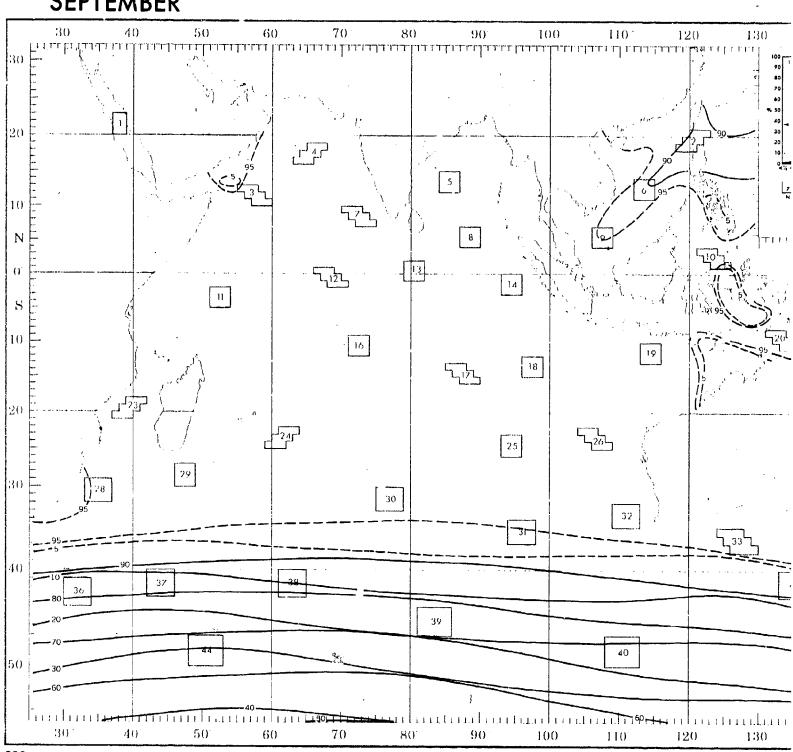
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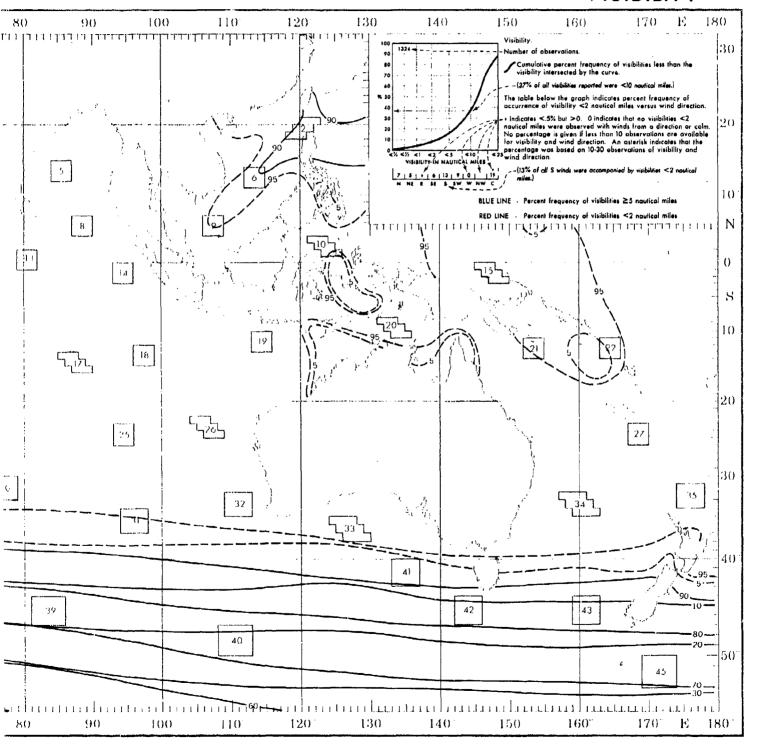


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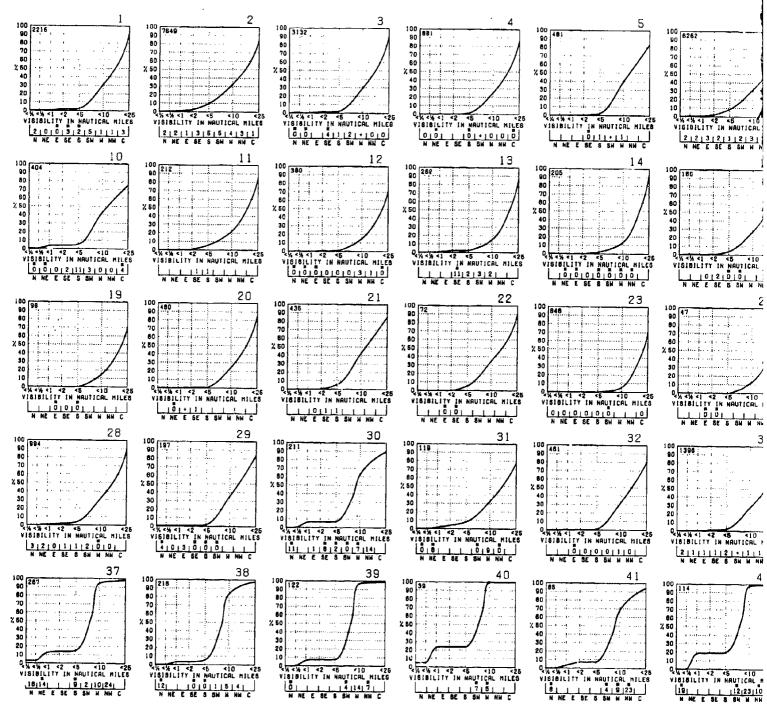
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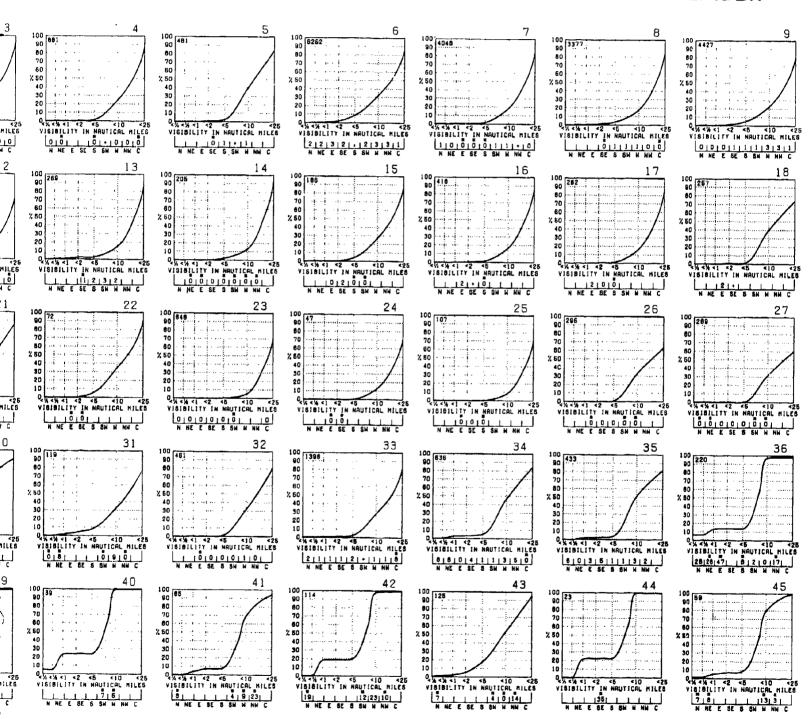


VISIBILITY

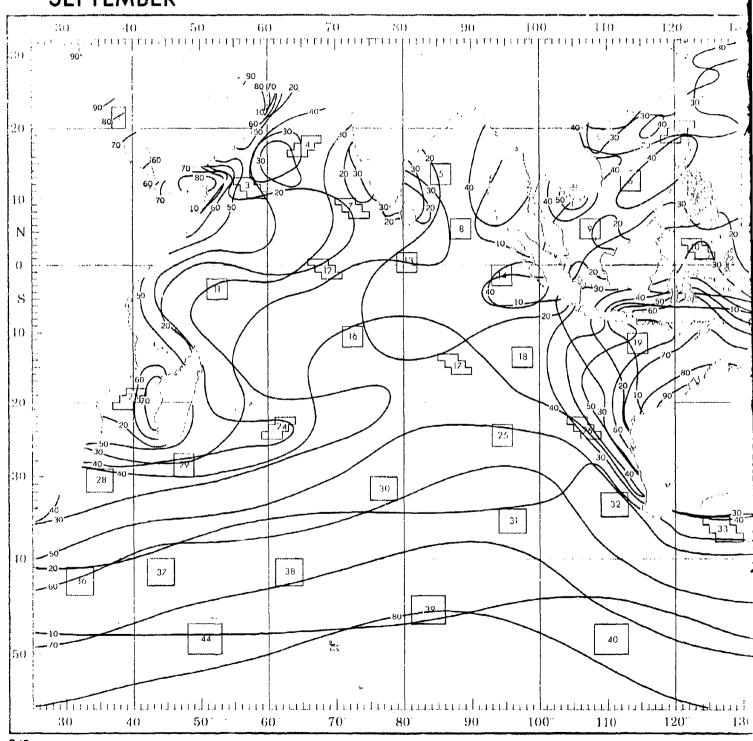


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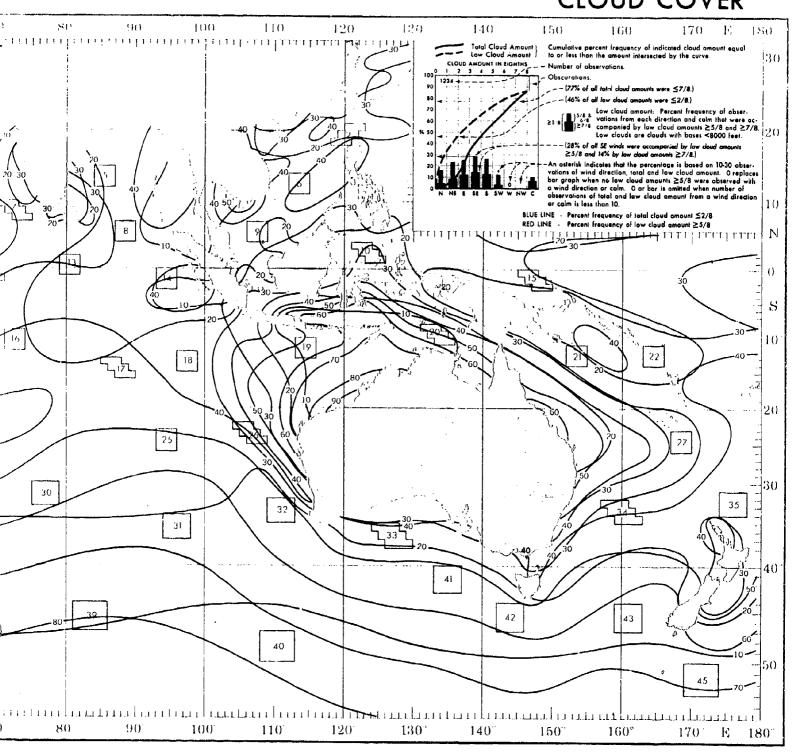
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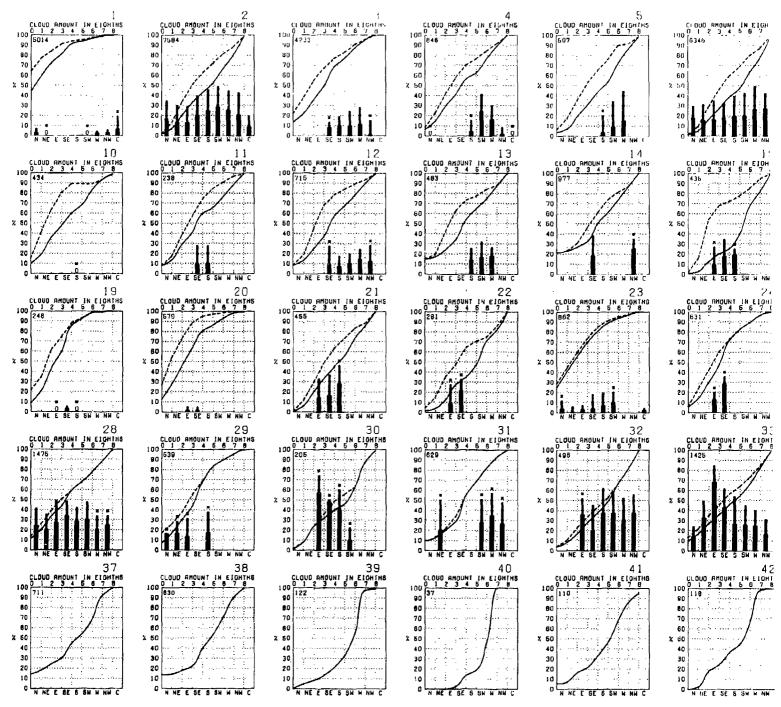
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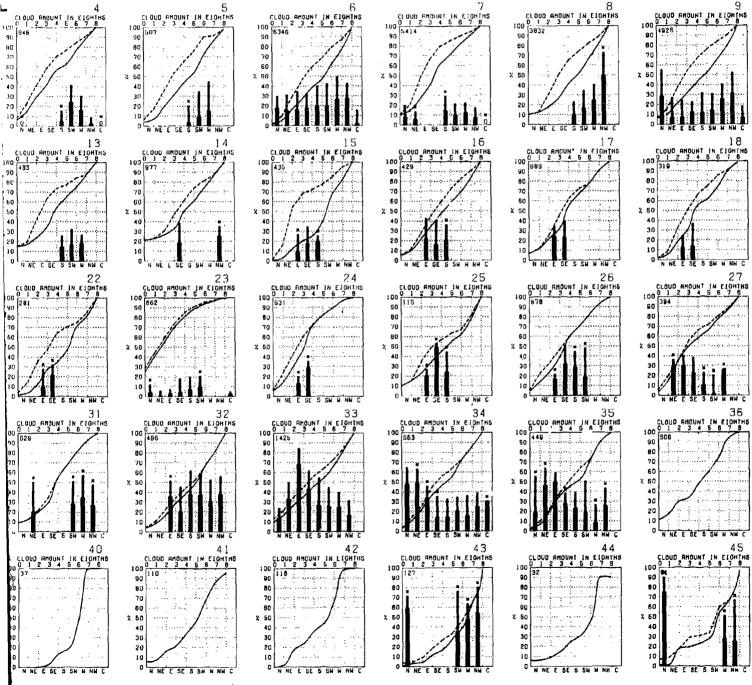
CLOUD COVER



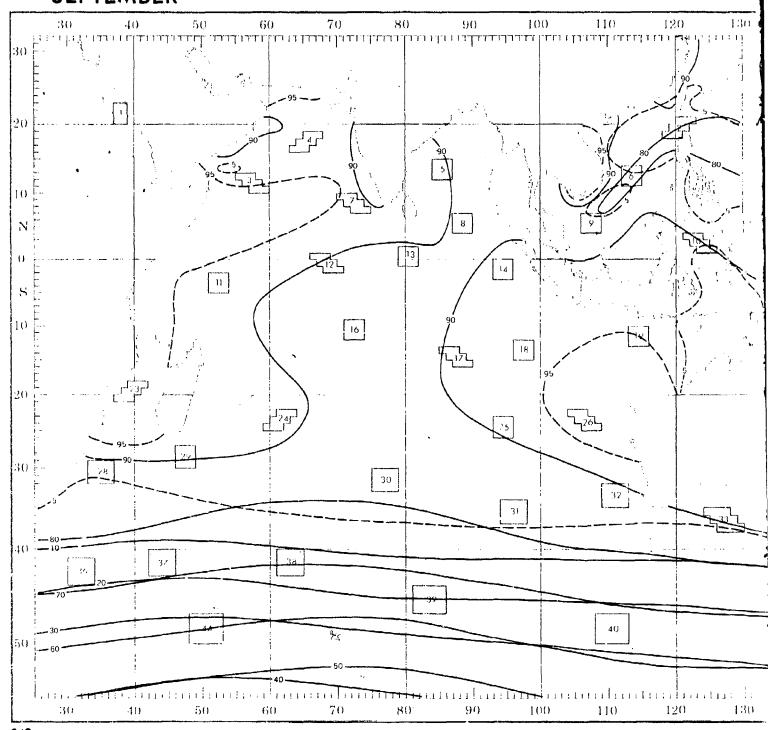
CLOUD COVER



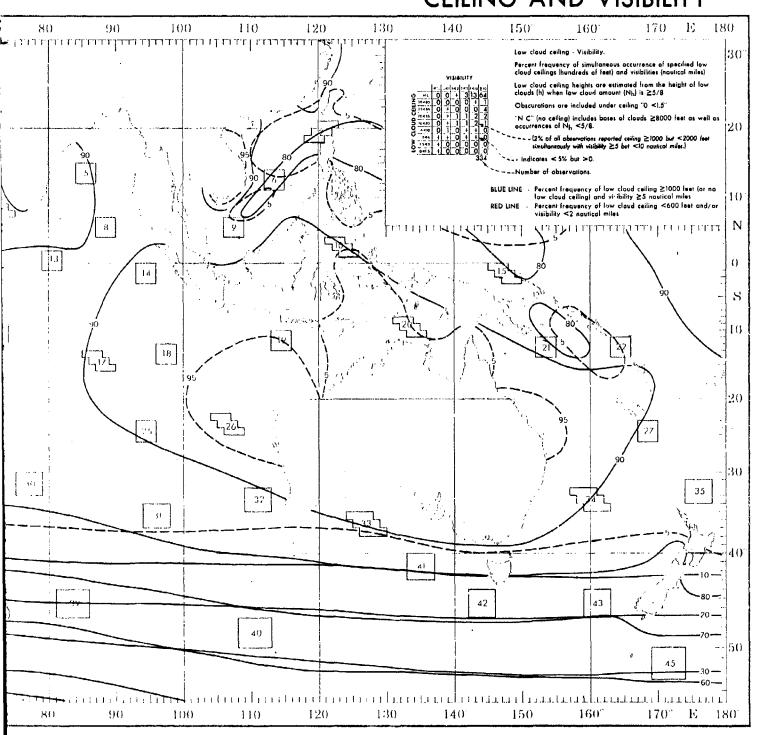
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ive compilation of available data for specified areas without regard to suspected biases. site page) are based on all available data subjectively adjusted where blas was evident.



CEILING AND VISIBILITY



CEILING AND VISIBILITY

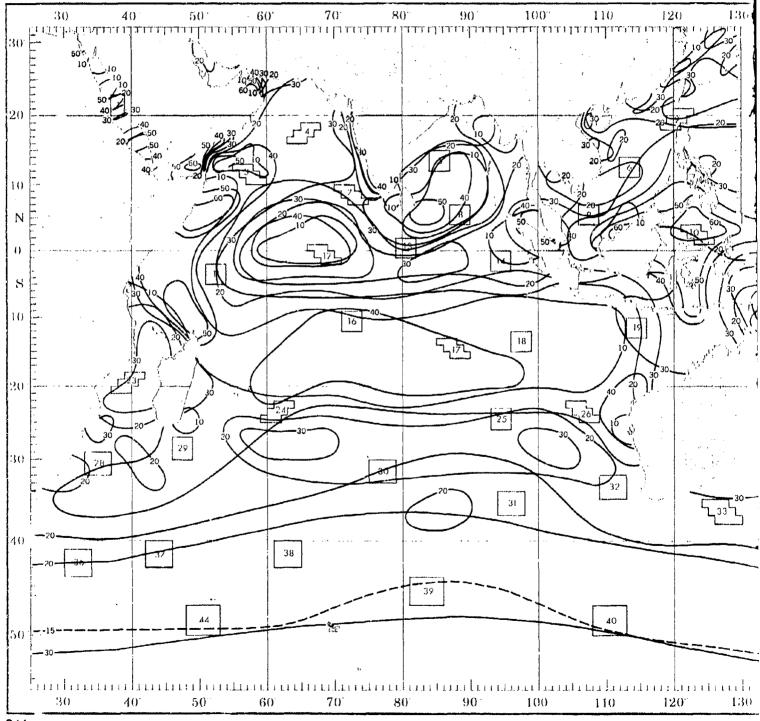
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VIBIBILITY *** ** ** ** ** ** ** ** **	VISIBILITY -*/n FACT 74 74 74 74 74 74 74 7	VISIBILITY 1.2 1.4 [Anti] 1.2 [44 [8-10] 10 1.6 0 0 0 0 0 0 0 0 2. 38-46 0 0 0 0 0 0 0 3 3. 38-46 0 0 0 0 0 1 3 3. 38-6 0 0 0 0 0 1 3 3. 38-6 0 0 0 0 0 1 3 3. 38-6 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 3. 38-6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY */A [A=1] -2 [E=4] [S-10] [10] **RC	VIETBELLIYY *********************************	VISIBILITY 4 ² /4 74 ² 14 ² 2 ⁴ 6 84 ³ 10 MC 0 0 0 0 7 60490 0 0 0 0 0 38 ⁴ 60 0 0 0 0 0 20 ⁴ 35 0 0 0 0 0 20 ⁴ 35 0 0 0 0 0 20 ⁴ 35 0 0 0 0 0 39 ⁴ 6 0 0 0 0 0 4 1,6 ⁴ 3 0 0 0 0 0 4 1,6 ⁴ 3 0 0 0 0 0 4 1,6 ⁴ 3 0 0 0 0 0 4 1,6 ⁴ 3 0 0 0 0 0 4 1,6 ⁴ 3 0 0 0 0 0 4 1,6 ⁴ 3 0 0 0 0 0 4 1,6 ⁴ 3 0 0 0 0 0 4 1,6 ⁴ 3 0 0 0 0 0 6 1,6 ⁴ 3 0 0 0 0 0 6 1,6 ⁴ 3 0 0 0 0 0 6 1,6 ⁴ 3 0 0 0 0 0 6 1,6 ⁴ 3 0 0 0 0 0 7 1,6 ⁴ 3 0 0 0 0 0 8 1,6 ⁴ 3 0 0 0 0 0 9 1,6 ⁴ 3 0 0 0 0 0 0 9 1,6 ⁴ 3 0 0 0 0 0 9 1,6 ⁴ 3 0 0 0 0 0 9 1,6 ⁴ 3 0 0 0 0 0 9 1,6 ⁴ 3 0 0 0 0 0 9 1,6 ⁴ 3 0 0 0 0 0 9 1,6 ⁴ 3 0 0 0 0 0 0 9 1,6 ⁴ 3 0 0 0 0 0 0 9 1,6 ⁴ 3 0 0 0 0 0 0 9 1,6 ⁴ 3 0 0 0 0 0 0 9 1,6 ⁴ 3 0 0 0 0 0 9 1,6 ⁴ 3 0 0 0 0 0 0 9 1,6 ⁴ 3 0 0
VISIBILITY 1-1/2 Pres 1-1/2 Pres	VISIBILITY ***********************************	VIBIBILITY -1/4 PARTI 192 PER PETIDITIO -1/4 PARTI 192 PETIDITIO	VIBIBILITY -1/8 [F/47] 1-8 [248 [5-10]-10] -1/8 [F/47] 1-8 [248 [5-10]-10] -1/8 [F/47] 1-8 [248 [5-10]-10] -1/8 [5-10] 10 0 0 0 2 00 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 0 0 0 0 -1/8 [5-10] 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY 1/4 FACT 12 246 510 10 AC	VISIBILITY 4-7-8 PA-11 1-48 E-45 B-1-101 MC 0 0 0 0 0 0 3 60-60 0 0 0 0 0 0 0 98-10 0 0 0 0 0 0 1-60-60 0 0 0 0 0 0 1-60-60 0 0 0 0 0 0 1-60-60 0 0 0 0 0 0 1-60-60 0 0 0 0 0 0 1-60-60 0 0 0 0 0 0 1-60-60 0 0 0 0 0 0 1-60-60 0 0 0 0 0 0 1-60-60 0 0 0 0 0 0 1-60-60 0 0 0 0 0 0 1-60-60 0 0 0 0 0 0 1-60-60 0 0 0 0 0 0 1-60-60 0 0 0 0 0 0 0 1-60-60 0 0 0 0 0 0 0 1-60-60 0 0 0 0 0 0 0
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INSUFFICIENT DATA	VISIBILITY 38	INSUFFICIENT DATA	INSUFFICIENT DATA	VISIBILITY 4 1 **A* [A*4] **2 [2*8	INSUFFICIENT DATA

<u>Graphs</u> represent the objective compilation of available data for specified areas without. The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjus-

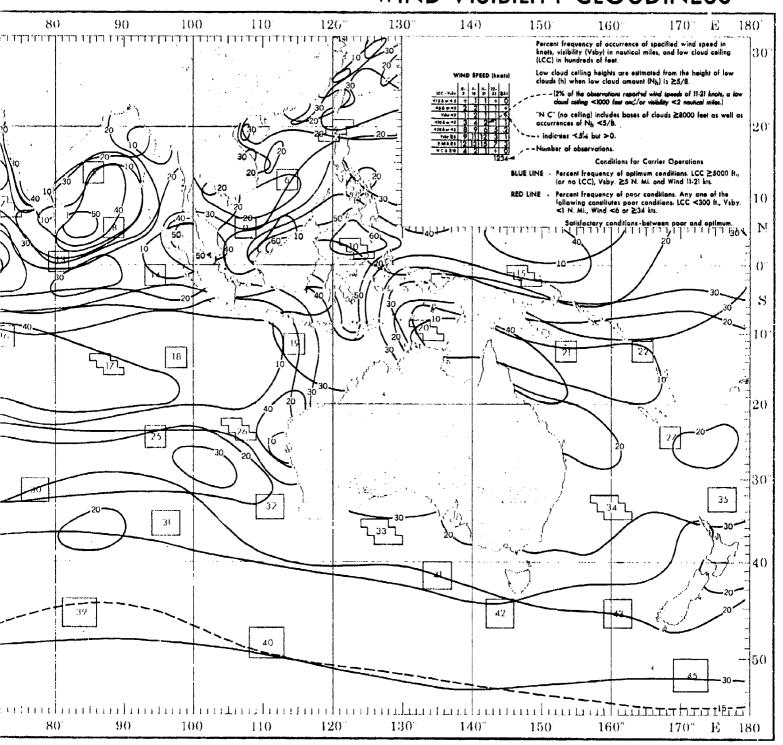
VISIBILITY *VA [74*] 142 [348 \$4:0410 MC 0 0 0 0 6 64 0*40 0 0 0 0 1 1 6*80 0 0 0 0 1 3 0*38 0 0 0 0 2 4 0*20 0 0 0 0 3 8 6*10 0 0 0 0 2 2 3*40 0 0 0 0 0 0 1*40 0 0 0 0 0 1*40 0 0 0 0 0 1*40 0 0 0 0 0 1*40 0 0 0 0 0 528	VIBIBILITY S	VISIBILITY	VIBIBILITY 7	VISIBILITY	V:SISTLITY 9
VISIBILITY 1 3	1 4	VISIBIL IT	VISIBILITY	1 7	VISIBILITY 44/9 5/40 146 248 5410 140
VISIBILITY 22	VISIBILITY 23	VISIBILITY AC 0 0 0 0 0 3 70 SC+86 0 0 0 0 0 0 3 38-80 0 0 0 0 0 0 3 38-80 0 0 0 0 0 0 3 38-80 0 0 0 0 0 0 0 3 38-80 0 0 0 0 0 0 0 3 38-80 0 0 0 0 0 0 0 12 38-80 0 0 0 0 0 0 0 6 38-80 0 0 0 0 0 0 0 6 38-80 0 0 0 0 0 0 0 0 38-80 0 0 0 0 0 0 0 0 38-80 0 0 0 0 0 0 0 0 38-80 0 0 0 0 0 0 0 0 0 38-80 0 0 0 0 0 0 0 0 0 38-80 0 0 0 0 0 0 0 0 0 38-80 0 0 0 0 0 0 0 0 0 0 38-80 0 0 0 0 0 0 0 0 0 0 38-80 0 0 0 0 0 0 0 0 0 0 0 38-80 0 0 0 0 0 0 0 0 0 0 0 0 38-80 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY 1-1/2 FACT 1-2 E-6 E-10310 NC 0 0 0 0 0 0 58 80-80 0 0 0 0 0 0 0 0 80-80 0 0 0 0 0 0 0 80-	### ### ### ### ### ### ### ### ### ##	VISIBILITY 27 4/A A-1 142 2-5 5-10 162
VISIBILITY 31 (***********************************	VISIBILITY VISIBILITY 1/2 [7/2] [7/2] [2 [2 [3 [3 (1)]] [2 [3 [3 [3 (1)]] [2 [3 [3 [3 (1)]] [2 [3 [3 [3 (1)]] [2 [3 [3 [3 (1)]] [2 [3 (1)]] [2 [3 (1)] [2 (1)] [2 [3 (1)] [2 (1)] [2 [3 (1)] [2 [3 (1)] [2 [3 (1)] [2 (1)] [2 [3 (1)] [2 (1)] [2 (1)] [2 [3 (1)] [2 (1	VISIBILITY *In Fari *2 245 340 310 *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *** *	VIBIBILITY 34	Visibal III Visibal III	INSUFFICIENT DATA
SUFFICIENT DATA	VISIBILITY 4 1 1 2 2 3 3 1 1 1 1 2 3 4 1 1 1 1 1 1 1 1 1	INSUFFICIENT DATA	VISIBILITY 4 3	INSUFFICIENT DATA	VISIBILITY 45 ***********************************

e compilation of available data for specified areas without regard to suspected biases. e page) are based on all available data subjectively adjusted where bias was evident.

WII



WIND-VISIBILITY-CLOUDINESS



LOW CLOUD CEILING-VISIBILITY-WIND

0 27 47 27 0 0 7 27 7 0

Y087 18

-20 4 00 48

2 50 4 ES

VERY AB

0 0 30 13 0

0 9 57 9 17

0 9 13 0 9

DATA

					Ì
1	2	3	4	5	•
HIND BPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	KIND SPEED (KNOTS)	HIND GBEED (HNGIS)	NIND SPEED (KNO!
LCC - Y887 0- 4- 11- 22- 33 234	LCC - VSSY 3 10 21 33 234	LCC - V88Y 3 10 21 33 234	LCC - VBBY 3 10 21 39 234	LCC - V887 3 10 21 33 294	LCC - VSBY 3 10 21 33
*1.54 GR *.5 0 + C 0 0	<1:6 t DR <-5 + 1 + +	4) - 5 4 OR 4 - B O + + O O	<1.5 4 OK <.b 0 0 + 0 0	*1.54 OR *.5 0 0 0 0 0	<1.5 t OR * . 5 0 + 1 .
<6.4 DR <2	48 4 GR *2 4 2 3 1 +	46 t 08 <5 0 + + + 0	46 4 0R 42 0 + 2 0 0	<8 t GR +2 0 0 2 0 0	<64 OR <2 4 2 3 1
VBBY <2 0 0 0 0 0	VBBY 4₽ + 1 1 + +	V68Y <2 0 + 0 0 0	VSST <2 0 0 0 0 0	Y887 <2 0 0 1 0 0	Y607 47 + + 1 +
410 4 04 44 D + + O O	*10 L QR *2 + 4 7 2 1	«10 4 0R «2 0 j 2 2 0	<10 t nR <2 + + 4 } O	<10 4 0R <2 1 1 4 1 0	*10 LOR *2 1 5 9 2
420 4 0R 46 1 1 2 0 0 0 V68Y 46 7 38 52 3 0	420 4 OR 48 1 9 17 4 1	*80 4 DR *6 + 3 8 3 0 *88 4 5 3 25 54 17 +	420 L QR 45 + 1 15 2 0	*20 4 0R *5 1 3 12 1 0 ************************************	480 ± 0R 48 1 11 19 4 V6B1 8B 7 37 42 3
v60Y = 6 7 38 52 3 0	989 4 85 5 33 43 9 +	VSBY 25 3 25 54 17 +	VAST NE 8 39 49 5 0	veev = 6 32 56 3 0	280 4 ab 6 27 24 7
HC 4 a 10 5 32 44 2 0	MC 4 = 10 3 21 24 3 +	MC 4 - 10 3 20 35 8 ·	MC 1 2 10 6 32 25 1 0	ac 4 × 10 4 25 31 1 0	MC 4 3 10 5 23 19 1
664	6294	1076	617	193	1 1 1 1 1 1
10	11	12	13	1 4	1
NING SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	WIND SPEED EKNOT
LCC - V00Y 3 10 21 83 a34	LCC - VABY 3 10 21 33 m34	LCC - VERY 3 10 21 33 234	LCC - Y08Y 3 10 21 33 284	LCC - VEST 3 10 21 35 234	LCC - YSBY 3 10 21 35
41.64 OR 5.8 0 0 0 0 0	*1.84 OR *.8 0 0 1 0 0	41:54:064:5 0 0 0 0 0	41-8 4 OR 4-8 D D 1 D D	<1.64 08 <.8 0 0 0 0 0	41.64064.8 0 0 0 0
<8 t 68 -E 0 0 0 0 0	48 4 SR 42 0 0 4 0 0	48 4 00 42 0 2 1 0 0	48 4 DR 42 D 1 1 D 0	48 48 0 0 0 0 0	48 4 DM 48 0 0 0 0
Y887 42 0 0 0 0 0	VBBY 42 0 0 1 0 0	V88Y 48 0 0 0 0 0	VASY <2 0 1 0 0 0	V88Y 4E - 0 0 0 0 0	V897 42 0 0 0 0
410 4 08 42 0 0 0 0 0	410 4 0H 42 0 2 9 0 0	-10 4 0A -1 0 B 1 0 0	«10 4 0M «2 1 6 3 0 0	420 4 6R 42 3 1 4 D O	410 4 OR 42 1 4 3 0
420 4 58 45 0 0 0 0 0	420 4 OR 48 0 3 15 2 0	420 & 0 1 4 0 0	420 4 OR 45 2 8 9 1 0	420 4 68 46 3 7 7 D O	420 4 OR 45 3 11 3 0
V007 25 36 50 15 D O	VSSY 86 4 45 44 3 C	v60Y a8 16 74 8 1 0	Veer 25 10 55 35 1 0	V85Y a5 17 53 30 0 0	V66Y 38 21 59 18 U
33 48 15 D D	asa 4 28 4 39 32 1 0	980 4 a5 14 59 3 1 D	860 4 25 8 44 22 1 0	250 4 AS 14 38 17 0 0	260 4 AS 18 46 16 O
MC 4 a 10 28 45 15 0 0	MC 4 ≥ 10 3 34 29 1 0	NC 4 3 10 14 59 3 1 0	MC 4 A 10 8 40 22 1 0	MC 4 » 10 13 32 14 0 0	HC4 = 10 17 41 14 0
·-				· -	
19 HIND SPEED (KNOTS)	20 HIND SPEED (KNOTS)	21 HIND SPEED (KNOTS)	22 HIND SPEED (KNOTS)	23 HIND SPEED (KNOTS)	2. HIND SPEED (KNOT
LCC - V46Y 9 10 21 99 234	LCC - VSBY 3 10 R1 35 294	LCC - VEST 3 10 21 35 254	LCC - Y887 3 10 21 39 334	LCC - VSBY 3 10 21 23 234	Lcc - veer 9 10 21 33
41.64 68 4.6 0 0 0 0 0 0	41.84 DR 4.8 0 0 0 0 0	41.6 4 68 4.8 0 0 0 0 0	41.54 OR 4.5 0 0 0 0 0 0	49 4 08 42 D D D D	45 4 5R 4 5 0 0 0 0
48 4 98 42 0 0 0 0 0 0 988Y 42 0 0 0 0 0	48 4 9R 42 0 0 0 0 0	18 4 8R 42	48 4 98 42 0 0 0 0 0	48 4 08 42 0 0 0 0 0	46 4 0R 42 D D O O
418 4 68 41 0 0 2 0 0	<10 4 0R <2 0 1 0 0 0	410 4 64 42 0 3 10 3 0	410 4 0R 42 D 5 5 0 0	410 4 08 42 + + 1 0 0	410 4 DR 42 D D 3 3
480 t est 46 0 2 8 0 0	420 4 9R 4B D 2 1 0 D	480 4 OR 48 0 6 24 5 0	420 4 0R 48 0 12 10 0 0	420 4 OR 48 1 2 4 1 0	420 4 Det 46 0 3 9 6
V867 25 2 63 35 G G	Y00Y NS 3 48 49 0 0	VSST BS 2 22 80 10 0	V897 46 5 33 52 2 0	VABY 85 18 49 32 3 0	VEST 25 0 52 39 9
8 50 4 96 2 58 27 O O	480 4 48 3 45 47 0 D	a 60 4 a 5 2 16 39 5 0	380 tal 5 29 31 2 0	asc 4 as 15 44 26 2 0	160 6 18 0 42 27 3
MC 6 a 10 2 58 27 D D	HC 4 a 10 3 45 48 0 0	MC 4 2 10 2 14 35 4 U	HC 4 > 10 5 21 31 2 0	MC 4 = 10 15 44 23 2 0	MC 4 B 10 0 39 27 3
52	175	231	42	699	
28	29	30	31	32	30
NIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	MIND SPEED (KNOTS)	MIND SPEED (KNOTS)	MIND SPEED (KNOT)
LCC - VOSY 3 10 21 33 484	LCC - VSSY 9 10 21 33 254	LCC - VSSY 3 10 21 35 334	LCC - V68Y 0- 4- 11- 22- 3 10 21 33 234	LCC - VSBY 0- 4- 11- 22- 3 10 21 33 484	LCC - VARY 8 10 21 33
41.64 BR 4.B 0 0 0 0 0	41.84 98 4.8 0 0 0 0 0	<1.5408 <15 0 0 0 0 0	<1.64 0R <.8 0 0 0 0 0	<1.84 on <.8 0 + 0 0 0	4).54084.8 + + 0 0
46 4 90 42 0 1 2 + 0	48 4 98 42 0 0 0 0 0 0 0 V88Y 48 0 0 0 0 0 0	48 4 68 42 0 0 0 0 0	48 4 0F 42 0 0 0 0 0	48 4 0R 42 + + + + 0	48 4 08 48 + + 1 0
410 4 00 42 + 3 6 2 1	V66Y 48 0 0 0 0 0 0 0 410 4 20 4 22 0 2 2 1 1	Y88Y <₹ D D D D D 0 <10 4 00 <2 D D 3 2 D	YEST 42 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Y88Y 42 0 0 0 0 0 0 410 4 08 42 4 2 4	410 4 5R 4E 1 3 4 1
-20 Len -5 1 7 18 B 1	410 4 de 45 0 0 0 0 1 1	420 4 08 48 3 18 13 2 0	<20 4 of 45 1 12 14 7 0	420 4 DR 45 2 12 18 4 +	420 4 0R 46 1 8 13 4
V66T 16 4 30 47 15 2	V887 15 2 30 48 15 1	4887 15 8 45 43 2 0	V88Y a5 2 38 39 14 0	VERY 35 5 36 44 11 1	7887 as 4 31 45 16
850 4 st 3 20 25 10 1	a 50 c as 2 22 35 11 D	880 4 as 5 27 21 0 0	#50 4 a5 0 23 18 5 0	180 418 2 20 19 4 ·	250 4 26 2 19 27 10
MC 4 a 10 3 19 25 9 1	NC 4 = 10 2 21 32 11 0	MC 4 a 10 3 25 19 0 0	HC 4 3 10 0 21 18 4 0	MC4 a 10 2 18 17 4 0	MC 4 2 10 2 18 28 9
587	97	63	84	290	8
37	38	39	40	4 1	4?
NIND SPEED (KNOTS)	HIND BPEED LKNOTS:			HIND SPEED (KNOTS)	
LCC - VBBY 8 10 81 38 494	LCC - VBBY 3 10 21 39 194			LCC + VODT 0- 4- 11- 22- 9 10 E1 35 034	
41-84-08-4-6 0 0 0 0 0	45.8 6 68 4.8 0 0 0 0 0		•	41-84 OR 4-8 0 0 0 0 0	
46 4 44 45 0 0 0 0 0	49 4 861 42 D D D D D	INSUFFICIENT	INSUFFICIENT	48 6 98 42 0 0 0 0 0	INSUFFICIEN1
Y80Y 48 0 0 0 0 0	V007 47 0 0 0 0 0	100111016111	" 1001 OIFL1	Y68Y -2 0 0 0 0 0	II TOOLI TOILIT

Graphs represent the objective compilation of available data for specified areas without The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjus

DATA

4 28 54 13 0

-20 4 02 46

VERY AS

DATA

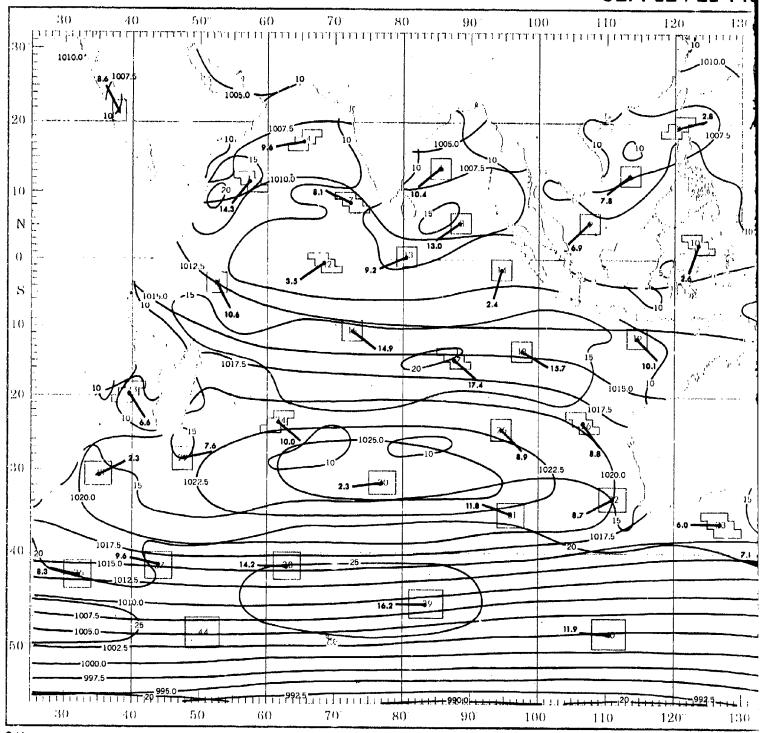
TY-WIND

SEPTEMBER

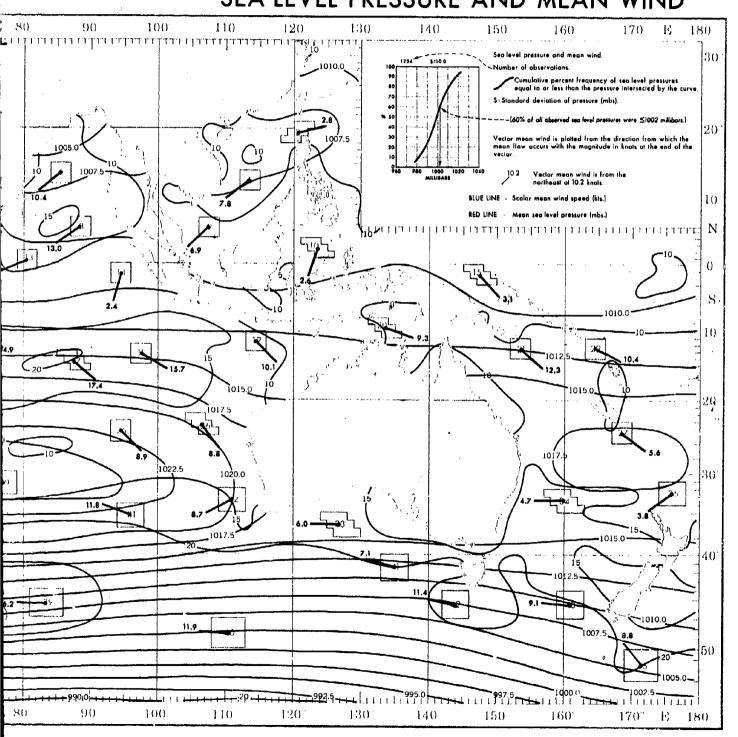
L	4	5	6	7	8	9
	INO SPEED (KNOTS)	WIND SPEED (KNOTS)	HIND BPEED (KNDTS)	HIND SPEED (KNOTS)	HIND BPEED (KNOTS)	HIND SPEED (KNOTS)
LCC - VS81		LCC - V88Y 0- 4- 11- 22- 33 a34	LCC - VBBY 3 10 21 35 >34	LCC - YERY 3 10 21 33 454	LCC - VSBY 3 10 21 33 234	LCC - V48Y 0- 6- 11- 22-
1 -5 4 DR • -1		-1.5 4 OR <.B 0 0 0 0 0	41.5 £ 0R 4.5 () + 1 + +	*1.54 GR * 18 0 0 + + D	<1.54 OR * .5 0 0 + • 0	43:8 4 dR 4:8 0 + 1 + 0
48 4 DH 47		48 4 DR 47 0 0 2 0 0	*6 + OR *2 + 2 3 1 + Y88Y *2 + + 1 + +	48 4 OR 42 + + 1 + 0	-04 0R -2 + 1 3 + 0	-(8 4 SR -(R + 1 3 1 +
*10 4 DR <		-10 4 OR -2 1 1 4 1 0	410 4 OR <p +<="" 1="" 2="" 5="" 9="" th=""><th>9889 48 0 0 + + 0 410 4 0R 42 + 2 3 + 0</th><th>VSBY 42</th><th>VBEY <p +="" +<="" 08="" 1="" 4="" 410="" 5="" <p="" b="" th=""></p></th></p>	9889 48 0 0 + + 0 410 4 0R 42 + 2 3 + 0	VSBY 42	VBEY <p +="" +<="" 08="" 1="" 4="" 410="" 5="" <p="" b="" th=""></p>
*20 4 OR 41		420 & OR 45 1 3 12 1 0	420 4 OR 45 1 11 19 4 +	420 4 0R 4E + B 7 1 0	*20 4 OR *6 + 5 19 4 +	420 4 OR 48 1 1 1 1 1 +
7887 A		Veev >5 5 32 56 3 0	V487 aB 7 37 42 5 →	V68Y a5 5 55 36 2 0	V887 35 1 25 51 8 +	V88Y AB 10 50 34 1 0
# 50 & AI		A 50 4 A 5 4 26 38 3 0	360 4 a8 6 27 24 2 +	ABO 4 28 5 47 28 1 0	a 80 4 a 6 1 20 40 4 +	250 4 25 B 37 21 + O
HC & a 10	6 32 25 1 0	HC 4 = 10 4 25 31 1 0	HC 4 & 10 5 23 19 1 +	MC 4 2 10 5 48 25 1 0	HC4 & 10 1 19 35 3 +	MC 4 a 10 7 33 17 + 0
	13		5115	1212	1345	2409
ļ.	I J IND SPEED (KNOTS)	14 HIND SPEED (KNOTS)	15 MIND SPEED (KNOTS)	16 HIND SPEED (HNOTS)	17 HINO BPEED (KNOTS)	18 Hind Speed (Knots)
LCC - VAD	0 - 4 - 112 - 00 -	LCC - VEST 0. 4- 11- 22- 24	0- 4- 11- 22-	0- 4- 11- 22-	10-14-111-1-2-1	1 1 1 1 1 1
1.5 4 OR 4.4		41.84084.8 0 0 0 0 0	LCC - V687 S 10 E1 33 884	UCC - V88Y 3 10 21 93 594		
48 & OR <2		48 4 DK 4F 0 0 0 0 0	46 4 68 42 0 0 0 0 0	46 4 00 <8 0 0 1 1 0	41.64 OR 42 0 1. 0 1 0	41.84 OR 4.8 0 0 0 0 0 0
V687 41	0 1 0 0 0	V607 42 0 0 0 0 U	Y86Y 4Z 0 0 0 0 0	V88Y -	VBBY <2 D 0 0 1 0	V88Y 4E 0 1 1 0 0
<10 4 OR <		<10 4 OR <2 3 1 4 0 0	410 4 GR 42 1 4 3 0 D	410 4 GR 42 0 1 10 3 0	410 4 DR 48 0 1 4 2 0	410 4 507 42 0 2 3 0 0
470 4 OR 41		420 4 0R 45 3 7 7 0 0	480 4 GR 45 3 11 3 0 0	420 4 SR 48 D 4 20 6 D	420 4 DR 46 0 1 15 B 1	420 4 0R 48 0 3 10 1 0
> 80 & al	110 00 30 11 0	9487 a5 17 53 30 0 0 a 50 4 a 5 14 36 17 0 0	V48Y 46 21 59 18 0 0	V88V 26 1 15 71 11 1 2 2 5 6 4 2 6 4 6 4	VSBY NS D 14 80 24 1 280 4 25 0 12 40 14 D	V68Y AB 0 11 70 16 0
HC & a Is		HC 4 2 10 13 32 14 0 0	HC A B 10 17 41 14 0 0	MC4210 1 9 40 5 +	#C4 = 10 0 12 40 14 0	a60 4 m8 0 9 47 11 0 MC 4 m 10 0 8 43 11 0
	146	76	76	305	162	122
l	22	23	24	25	26	27
1	HIND BPEED (KNOTS)	HIND SPEED (KNOTS)	MIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)
LCC - VOS		LCG - V48Y	LCC - Y88Y 3 10 21 33 234	LCC - VBBY 3 10 21 33 234	LCC - VARY 0 10 21 30 834	LCC - Y66Y 3 18 21 39 834
*8 4 OR 41		41.84 OR 4.6 0 0 0 0 0	41 - 18 4	41.6 4 SR 4.8 D D 1 D D	<1.5 t OR <.8 0 0 0 0 0	41.54 98 4.5 0 0 1 0 0
V887 4		V88Y 4E 0 0 0 0 0	V88Y 42 0 D 0 0 0	48 4 68 42 0 0 1 0 0 Y88Y 42 0 0 0 0 0	48 4 86 42 D D D 0 D D	48 4 BR 4E 0 1 1 0 0
<10 4 GR <	0 5 5 0 0	<10 4 6R 4F + + 1 D D	410 4 8R 42 0 0 3 3 0	410 4 98 42 1 3 3 0 0	410 4 SR 42 0 1 3 0 0	410 4 0R 48 1 1 B 1 O
-20 4 OR 4		420 4 OR 45 1 2 4 1 D	480 4 6R 48 0 3 9 6 0	420 4 OR 45 1 13 11 0 0	-20 4 det -6 0 1 5 2 0	420 4 GR 48 1 9 11 1 0
9687 al		VSST AB 16 49 32 3 0	Y88Y 45 0 52 39 9 0	V88V 16 B 46 45 0 0	VEBY 36 5 95 53 8 0	V68Y 25 8 41 45 8 0
HC & B II	~	#64 a B · 15 44 25 2 0	a 80 4 a 8 0 42 27 3 0 HC 4 a 10 0 39 27 3 0	B 0 4 a 6 B 31 24 0 0 B 31 24 0 0	350 445 4 26 30 3 0 HC 4 3 10 4 22 27 3 0	a 60 4 a 5 5 3 1 2 8 5 0 HC 4 a 10 4 2 9 2 7 5 0
	42	899	33	71	144	MC 4 a 10 4 29 27 5 0
l	31	32	33	34	35	36
,	RIND BPEED (KNOTS)	HIND BREED (KNOTS)	HIND SPEED (KNOTA)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	
LCC - Y881		LCC - V487 0- 4- 11- 22-	LCC - Y007 3 4- 11- 22-	LCC - VBOY 3 10 21 35 254	LCC - VBBY 3 10 21 33 234	
.6 4 OR < .1		43.56.08.4.5 0 + 0 0 0	41 :5 4 OR 4 :5 + + 0 0 0	41-8 4 0R 4.8 D D D D +	41.5404 4.5 0 1 0 1 0	
48 4 BR 41		48 4 DR 48 + + + + 0	44 6M 4Z + + 1 0 0	-84 OR -8 + 1 1 1 1	48 4 SR 42 0 1 0 1 0	INSUFFICIENT
410 4 GR 41		400 4 0R 4B + 2 4 2 +	-10 4 9R -E 1 3 4 1 0	410 4 8A 42 + 2 7 8 1	V88Y <2 0 1 0 0 0 <10 4 DR <2 1 4 9 3 1	DATA
*20 4 BR *		-20 4 9R +B 2 12 15 4 +	-20 4 SR -8 1 8 13 4 1	420 4 ex 45 1 5 15 11 2	420 4 DR 46 1 10 16 7 2	מממ
Y68Y A	1 1 1 1 1 1 1 1 1	VSSY 25 5 38 44 11 1	Y00Y AS 4 31 45 16 2	V687 26 4 20 51 19 2	VSBY 95 5 31 45 12 3	
3 50 4 31		* 60 4 ab 2 20 19 4 +	2 18 27 10 1	a 60 4 a 6 2 14 33 7 1	250 4 25 5 20 24 4 2	
NC & a' 10	0 21 15 4 0	MC A B 10 2 18 17 4 0	MC 4 a 10 2 18 26 9 1	MC 4 3 10 2 12 31 6 1	MC 4 = 10 4 18 24 2 1	
	40	41	42	43	44	45
ŀ		HIND SPEED (KNOTS)	74	MIND SPEED (KNOTS)	דיד	HIND BPEED (KNOTB)
		LCC - VERY 3 10 21 23 234		LCC - V68Y 0- 4- 11- 22-		LCC - VSOY 0- 4- 11- 88- 394
}		<1.54 DR <.5 0 0 0 0 0		41.84 98 4.6 0 1 3 0 0		41.84 0R 4.8 0 0 2 2 0
NSU	FFICIENT	-6 4 DR -E 0 0 0 D 0	INSUFFICIENT	46 4 OR 42 D 3 4 3 D	INSUFFICIENT	48 4 BR 4R 0 0 5 2 0
	ATA	V68Y 42 0 0 0 0 0	DATA	veer <# D 5 3 0 0		VSBY 42 0 0 6 2 0
l '	/A ! A	<10 4 08 <2 0 0 8 0 C	DATA	410 4 9R 42 0 3 15 / 0	DATA	410 6 00 42 0 0 7 2 0
		V887 85 4 29 54 13 0		V891 35 0 15 45 21 1		*20 4 98 *8 0 2 21 19 0 VERY 08 0 14 35 42 0
		250 4AR 4 0 33 4 0	•	a80 4 a5 D S 16 11 D		100 4 bb 0 12 12 14 0
		#C 4 0 10 4 0 29 0 0		MC 4 a 10 D 5 15 11 D	·	MC 4 to 19 0 0 5 5 0
R .		24		75		43

ive compilation of available data for specified areas without regard to suspected biases.

SEA LEVEL PR

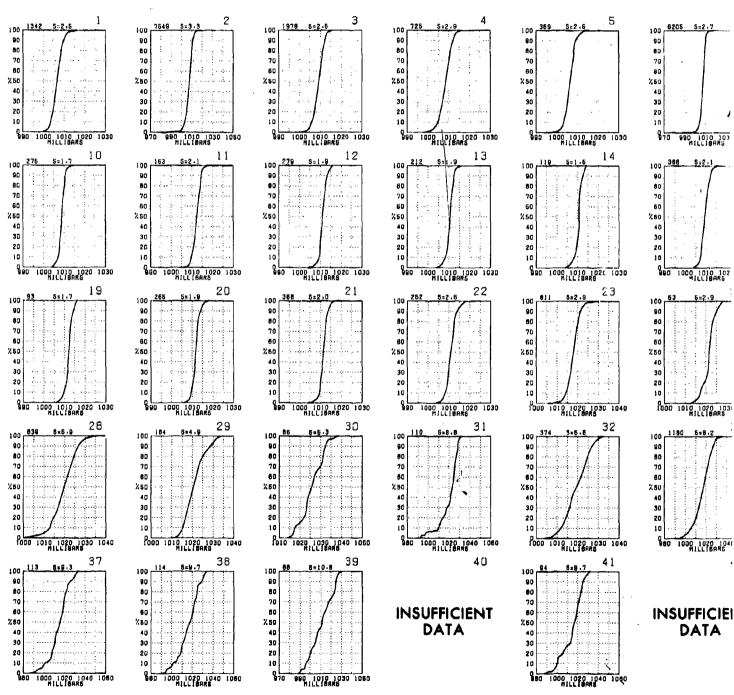


SEA LEVEL PRESSURE AND MEAN WIND

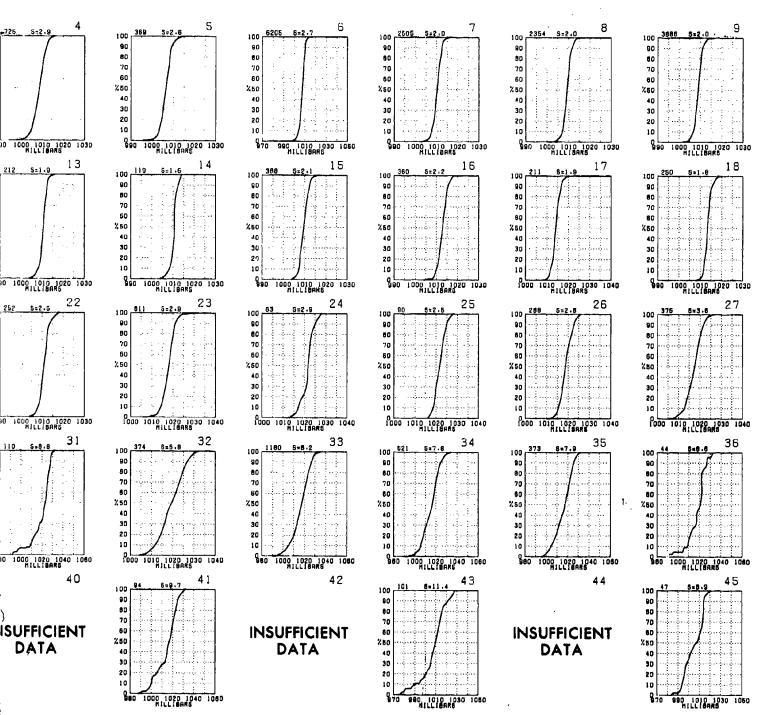


SEA LEVEL PRESSURE

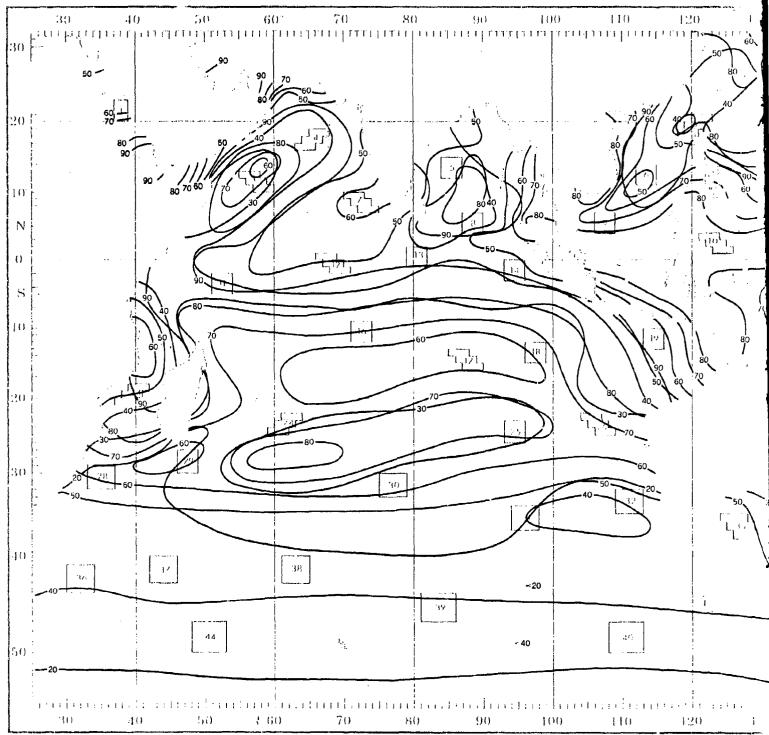
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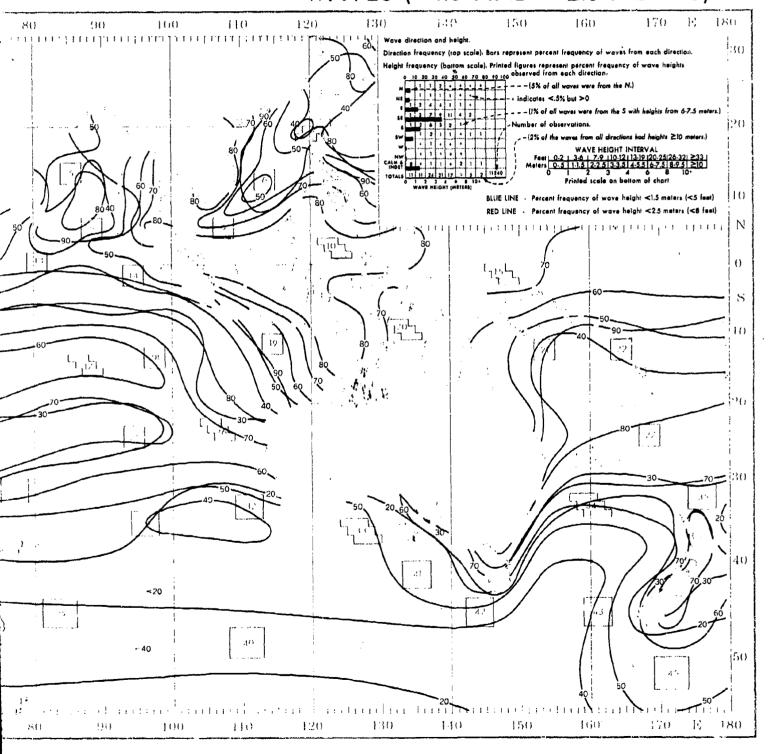
<u>Graphs</u> represent the objective compilation of available data for specified areas without the <u>isopleth</u> analyses (opposite page) are based on all available data subjectively ad



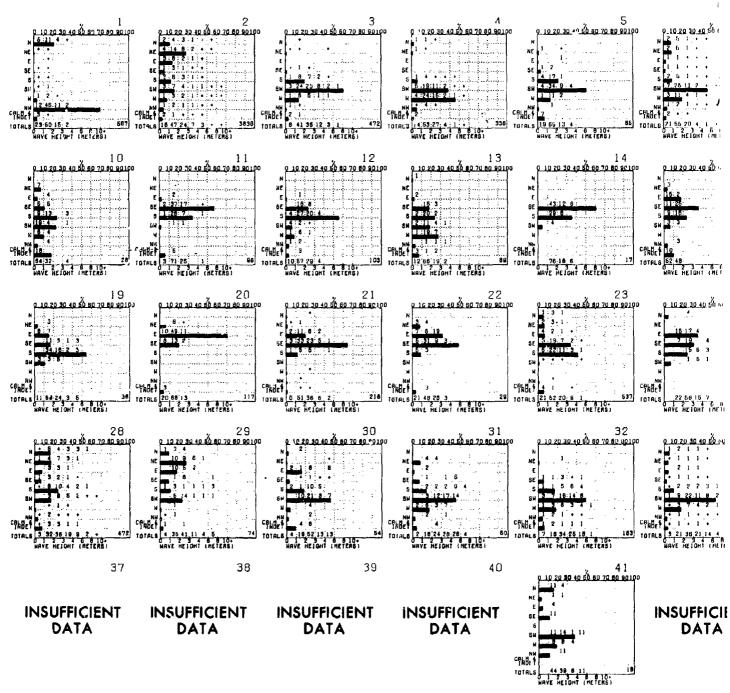
ve compilation of available data for specified areas without regard to suspected blases, ite page) are based on all available data subjectively adjusted where bias was evident.



WAVES (<1.5 AND <2.5 METERS)



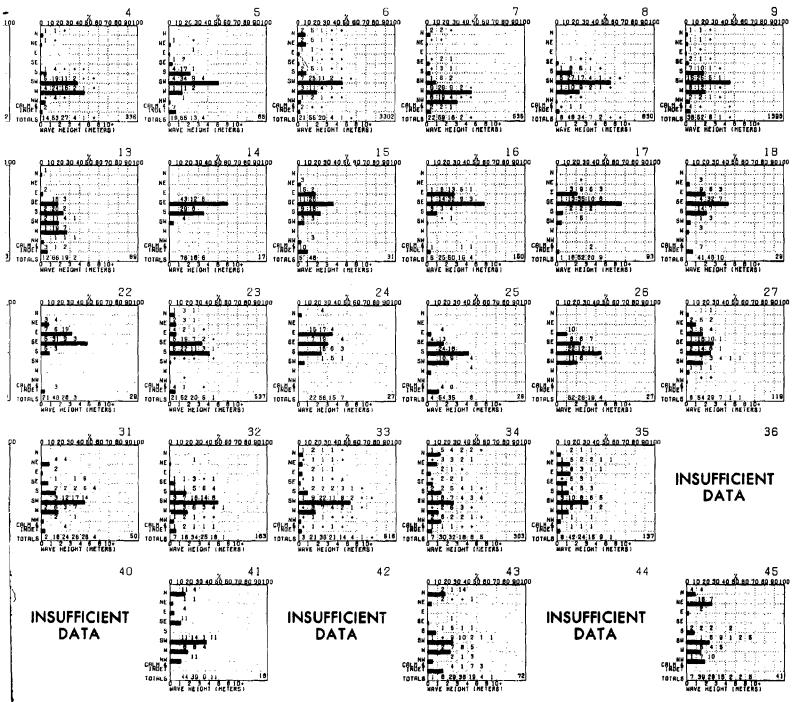
WAVE DIRECTION AND HEIGHT



<u>Graphs</u> represent the objective compilation of available data for specified areas with The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively a

IGHT

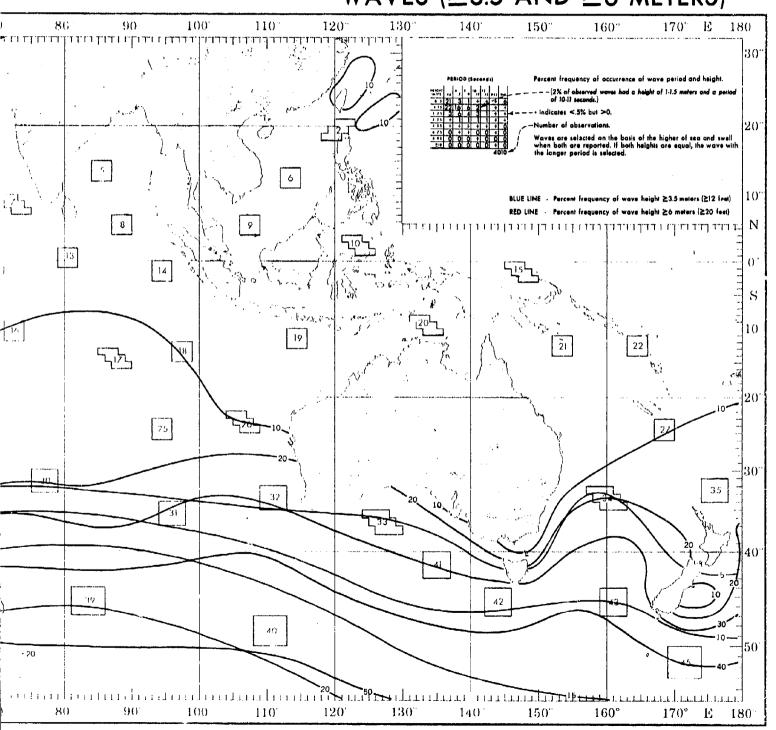
SEPTEMBER



jective compilation of available data for specified areas without regard to suspected biases, posite page) are based on all available data subjectively adjusted where bias was evident.

SEPTEMBER WAVES $G()^{\circ}$ 100. 120° 1() Ν 1)

WAVES (≥3.5 AND ≥6 METERS)



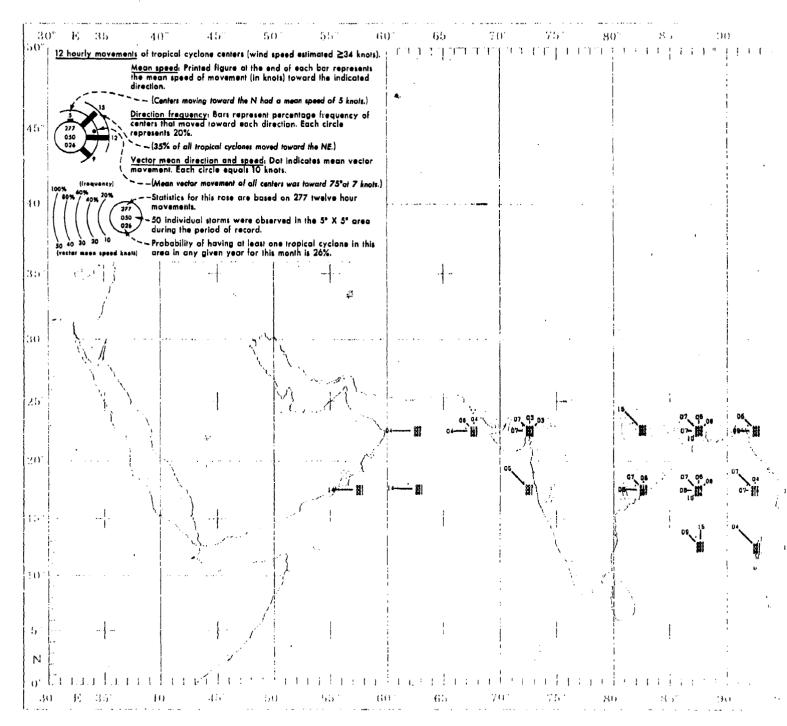
WAVE PERIOD AND HEIGHT

FERIOD SECONDS 1	PENIOD (SECUNDS) PENIOD (SECUNDS)	PERIOD (SECONDS) PERIOD (SECONDS) PERIOD (SECO	PERIOD I SECONDS MIRED 46 7 9 11 13 13 180	PERIOD (SECONDS) FATRE 8	PERIOD ISECOND: A
PEN OD	1	1 2 3 3 3 3 3 3 3 3 3	3	INSUFFICIENT DATA	PERIOD (SECONDS 1 1 1 1 1 1 1 1 1
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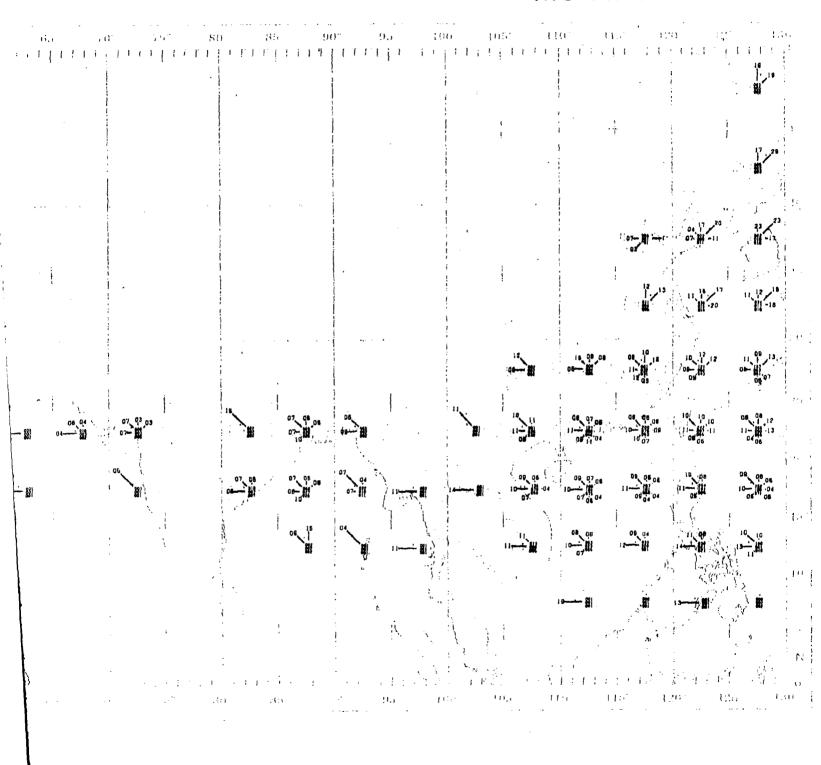
Graphs represent the objective compilation of available data for specified areas without The isopleth analyses (opposite page) are based on all available data subjectively adju-

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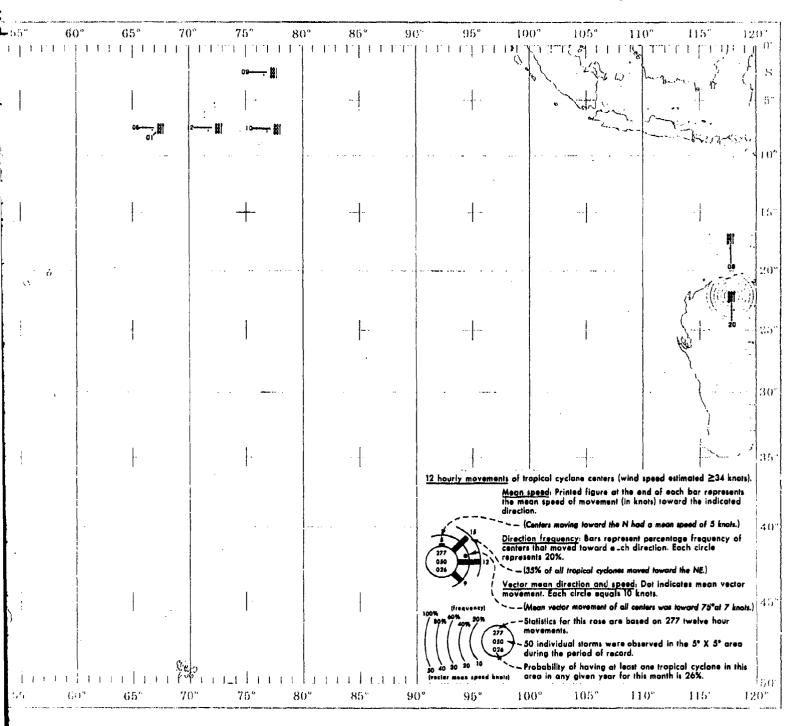


TROPICAL CYCLONE

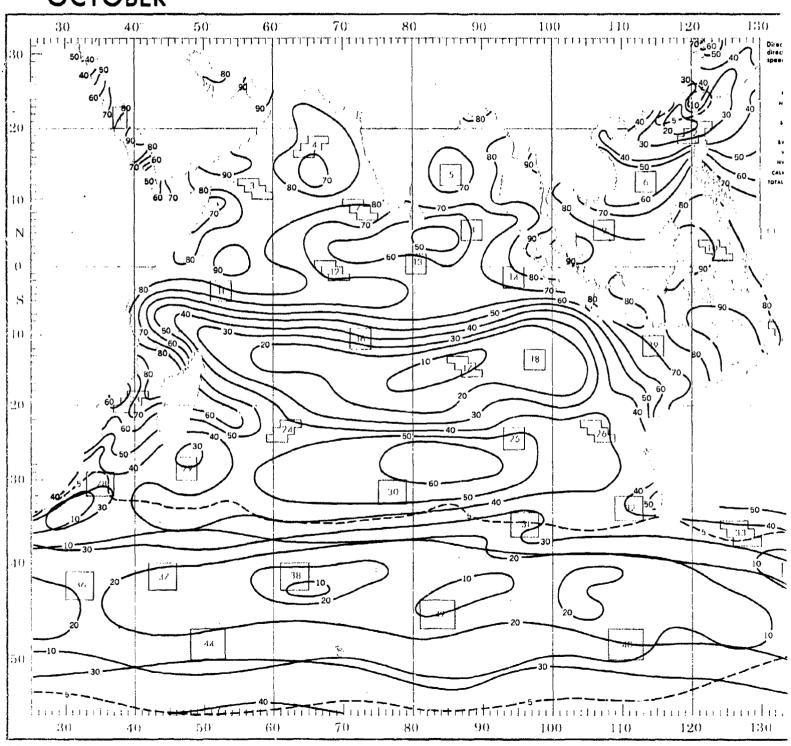


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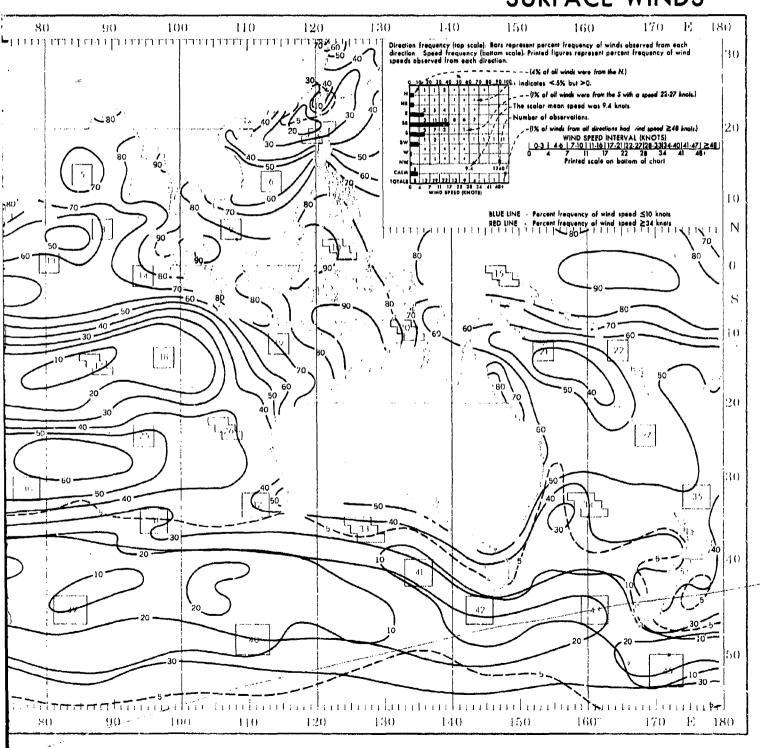
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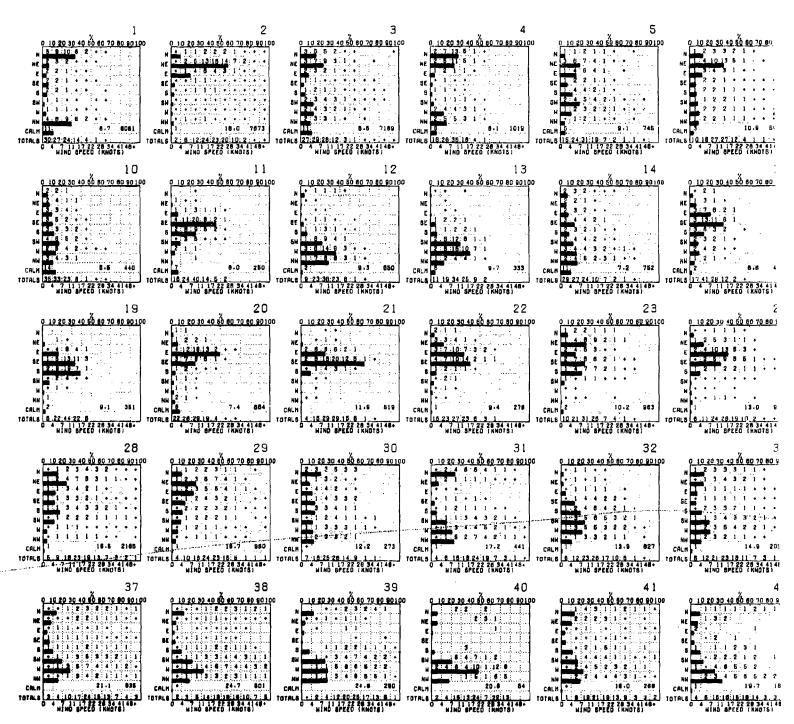
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SURFACE WINDS

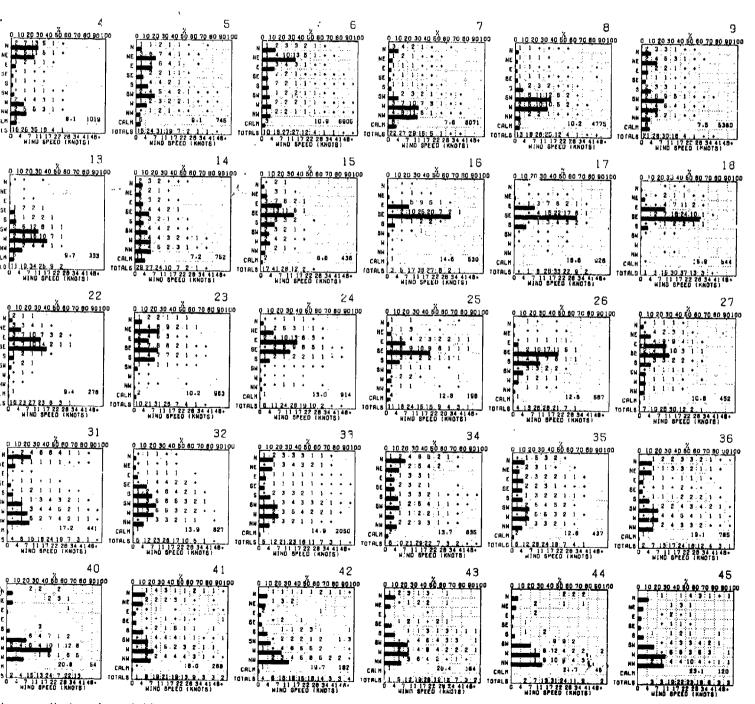


WIND DIRECTION AND SPEED



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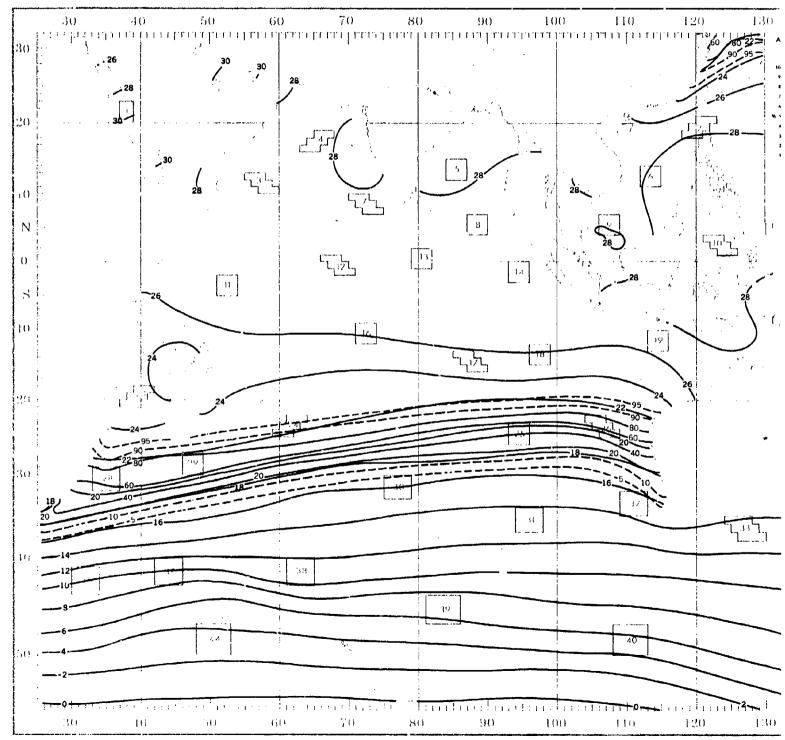


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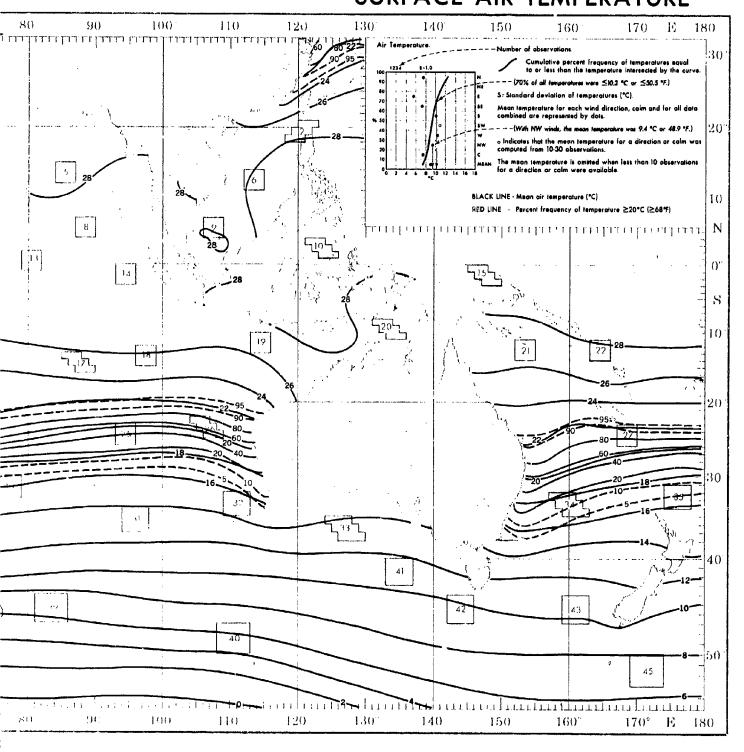
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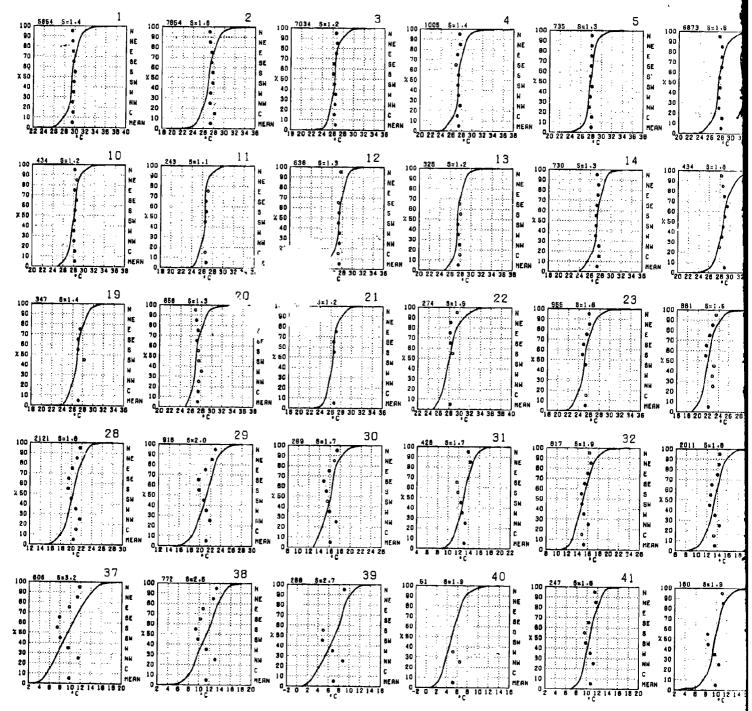


SURFACE AIR TEMPERATURE



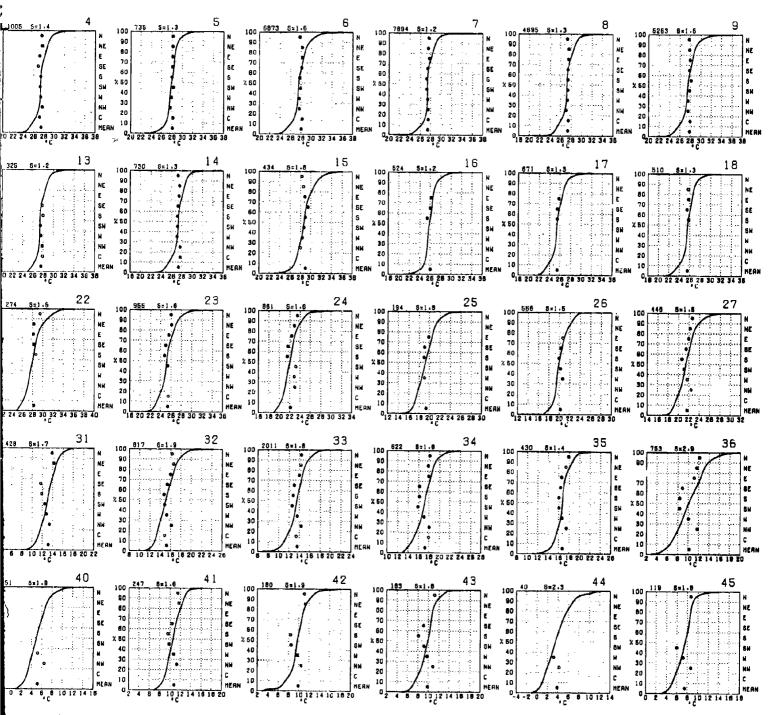
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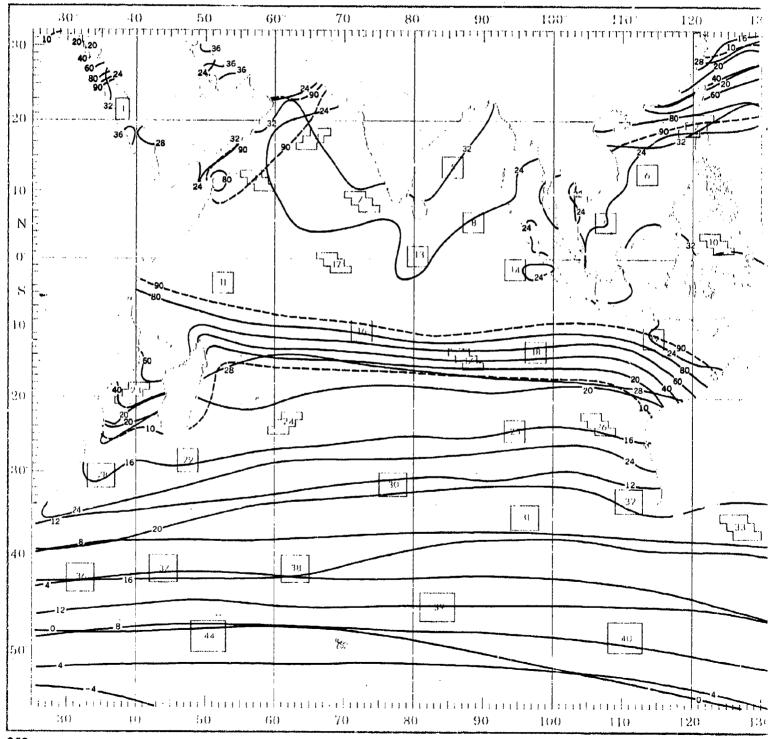
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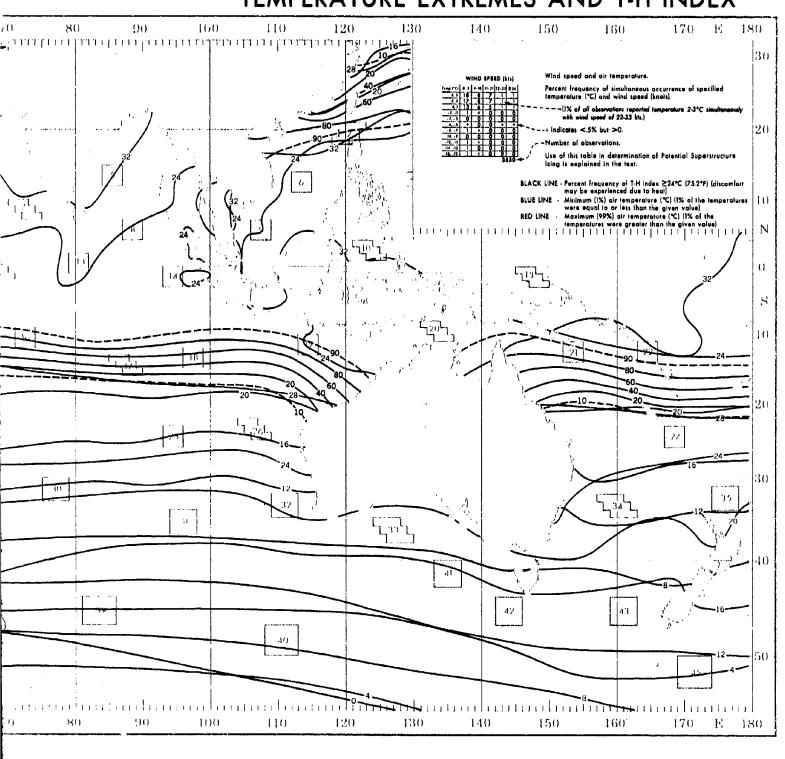
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TEMPERATURE



TEMPERATURE EXTREMES AND T-H INDEX



WIND SPEED AND AIR TEMPERATURE

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WIND BPEED (KTS)	HIND SPEED (KTB) 2	HIND SPEED (KTS) 3	HIND SPEED (KTS)	HIND SPEED (KIS) 5	HIND SPEED (KTS)
7EMF (*C) 0-9 4-10 11-21 22-93 2 34	TEMP (*C1 0-3 4-10 12-83 8E-33 = 34	7EHP (*C) 0-3 4-10 11-21 22-33 - 34	7EMP (*C) 0-3 4-10 11-21 22-33 2 34	7EMP (*C) 0-3 4-10 11-21 22-93 2 34	36.37 D + + O D
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TEMP (*C) 0-5 4-10 1-81 88-33 2 34	TEMP (*C) 0-3 4-10 11-21 22-39 2 34	TEHP (*C) 0-3 4-18 11-21 22-39 5 34	TEMP (*C) 0-3 4-10 11-21 22-33 > 94	TEMP (*C) 0-3 4-10 11-2122-33 2 34	TENP 1901 0-3 4-10 11-21 22-33 2 34
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20.20 24 37 5 + 0	28.27 11 44 11 + 0	26:28 4 27 10 + 0 26:27 4 25 15 + 0	20,20 4 27 15 1 0 20,27 5 22 15 1 0	28.27 12 26 5 1 0 24.25 1 3 2 4 4	30.31 3 14 3 0 0 4 29.28 9 35 0 0 0
24.28 + 1 + 0 0 22.83 0 0 0 0 0	22.23 0 0 0 0 0	24.25 0 3 3 0 0 22.29 0 0 0 0	24.25 0 1 2 + D 22.23 0 0 0 0 0	22.23 O + O O O O	26.27 4 11 2 0 0
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<u>Graphs</u> represent the objective compilation of available data for specified areas without regardle isopleth analyses (opposite page) are based on all available data subjectively adjusted w

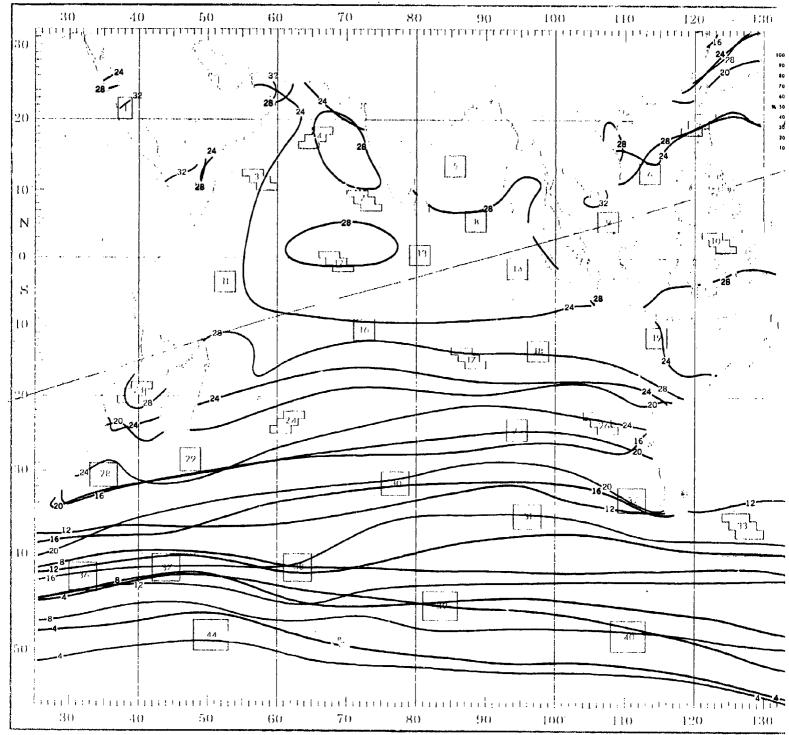
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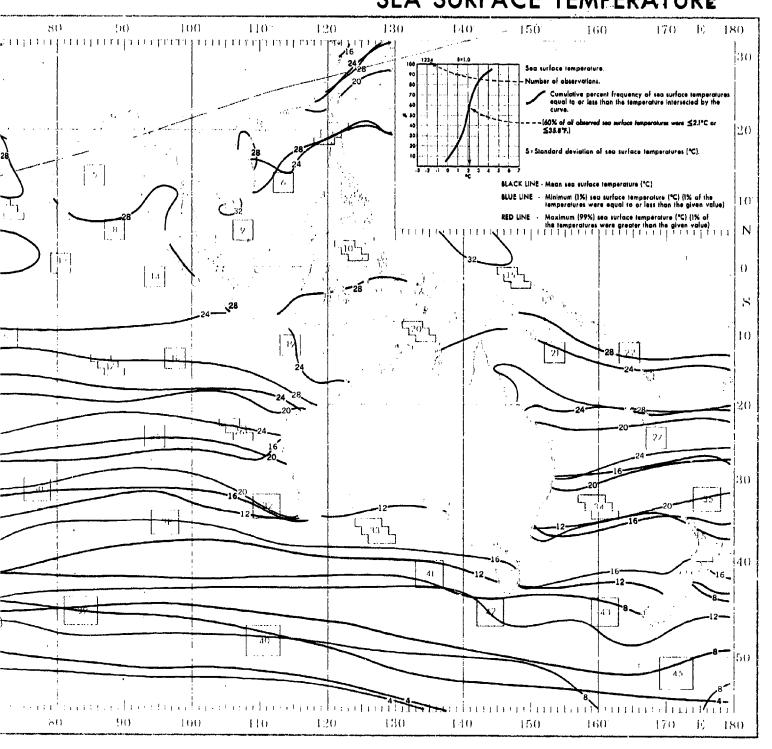
- WIND SPEED (KTS) 4	WIND SPEED (KTB) 5	WIND SPEED (KTS)	HIND SPEED (KTS) 7	HIND SPEED (KTS)	HIND SPEED (KTS)
1P 1P 0-3	1 1 2 3 3 3 3 3 3 3 3 3	38.37	TEMP 19C1 0-8 4-10 11-E1 E2-23 396 34.38 0	34.38 0 + 0 0 0 0 0 38.33 + + + + 0 0 30.31 3 2 2 + 0 0 28.28 8 19 15 2 + 28.27 7 22 16 3 0 2 1 + 22.23 0 + + + 0 0 20.21 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TEMP 19: 1 0-3 4-10 1-21 22-38 34 34 34 35 37 0 + 0 0 0 0 0 34 35 + + + 0 0 0 34 35 + + + 0 0 0 35 35 2 6 2 + 0 0 36 37 7 19 8 1 0 0 36 37 7 19 8 1 0 0 36 37 7 19 8 1 0 0 36 37 37 37 37 37 37 37
HIND SPEED (KTS) 13	RING SPEED (KT8) 14	HIND SPEED (KTS) 15	HIND SPEED (KTS) 16	HIND SPEED (KTS) 17	HIND SPEED (KTS) 18
P 1 * C 1	1600 1401 0-2 0-10 11-21 22-32 24 30.31 2 2 1 4 0 20 6 1 0 20 20 20 20 20 20	TEMP (9C)	TEMP (*G) 0-3 4-10 11-2 22-38 3-14 30.31 + 0 1 0 0	TEMP 1°C 0-9 4-10 11-E1 21-88 3 3 4 30.91 0 4 1 0 0 2 2 2 2 2 2 2 2	TEMP 1*C1
WIND SPEED (KTS) 22	HINO SPEED (KTS) 23	WIND SPEED (KTS) 24	HIND SPEED (KTS) 25	HIND SPEED (KTS) 26	HIND SPEED (KTS) 27
P (*C)	TEMP (*C) 0-3 6-10 11-21 2E-29 3 94 3E:39 0 0 + 0 0 30:31 + 1 1 + 0 16:69 1 4 2 + 0 16:67 4 18 12 2 0 16:67 4 18 12 2 0 16:67 4 18 14 2 + 0 20:81 + + + 0 0 10:19 10 0 0 0 0 16:17 0 0 0 0 0 0 16:17 0 0 0 0 0 0 16:18 0 0 0 0 0 0 16:18 0 0 0 0 0 0 18:18 0 0 0 0 0 0	TEMP (*C1 0-3 4-10 1-21 EE-39 34	TERP (10)	TEMP 19C3 0-9 4-10 11-E1 EE-39 h 94 E4.86 0 2 1 + 0 E8.73 2 8 9 1 0 E9.71 2 19 23 3 0 18.10 1 10 15 3 0 18.11 + 1 + 1 0 14.10 0 0 0 0 0 0 16.13 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 0 0 0 0 0 0 10.11 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TEMP 1/41 0 - 3 4 - 10 11 - 21 22 - 23 2 - 34
HIND SPEED (KTS) 31	HIND BPEED (KTS) 32	HIND SPEED (KTS) 33	HIND SPEED (KTS) 34	HIND SPEED (KTS) 35	HIND SPEED (KTS) 36
1°C 0-9 4-10 11-21 27-38 34 18-18 18-	TEMP (*C1 0-3 4-10 11-2) 2E-39 \ 34 EB: E3 0	TEMP (14) 0-8 4-10 11-21 22-89 8-94 80 94 80 91 91 91 91 91 91 91 91 91 91 91 91 91	TEMP 1901 0-9 4-10 11-21 88-33 34 88-83 0 0 0 0 0 0 0 0 0	TEMP (4C)	TEMP-1901 0-9 4-10 1-11 E2-18 3-24
HIND TPEED (KTB) 40	HIND SPEED (KTS) 41	HIND SPEED (KTS) 42	HIND SPEED (KTS) 43	HIND SPEED (KTS) 44	HIND SPEED (KTS) 45
10.11	TERP 1°C1 0-9 4-10 11-2: 22-39 3 34 14.18 0 1 2-1 0 0 12-11 0 12-13 14.18 0 1 2-1 0 0 12-13 15-1	16MP 1°C 0-9 4-10 11-E 21-28 24-18 16-17 0 0 1 0 0 1 16-18 16-18 24-18 24-18 16-18 0 0 1 0 0 1 1 16-18 17 6 5 1 16-18 17 7 6 5 1 16-18 17 17 12 11 3 3 6-7 2 2 3 3 0 0 0 0 0 0 0 0	TEMP (*C) 0-9 4-10 11-E E-28 h 34 14-18 0 0 1 1 1 0 15-12 0 0 1 1 1 0 15-12 0 0 1 1 1 0 15-12 0 0 1 1 1 0 0 15-12 0 0 1 1 1 0 0 1 1 1 0 0 0 0 0 0 0 0 0	TEMP 1/01 0-3 4-10 11-E1 62-38 a 26 10-11 0 B 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	TEMP (*C) 0-3 4-16 11-2 02-38 3 34 12:12 0 0 0 1 1 0 10:11 0 1 4 6 1 1 0 10:11 0 1 1 4 6 1 1 0 10:11 0 1 1 1 1 1 1 1 1 1 1 1 1 1

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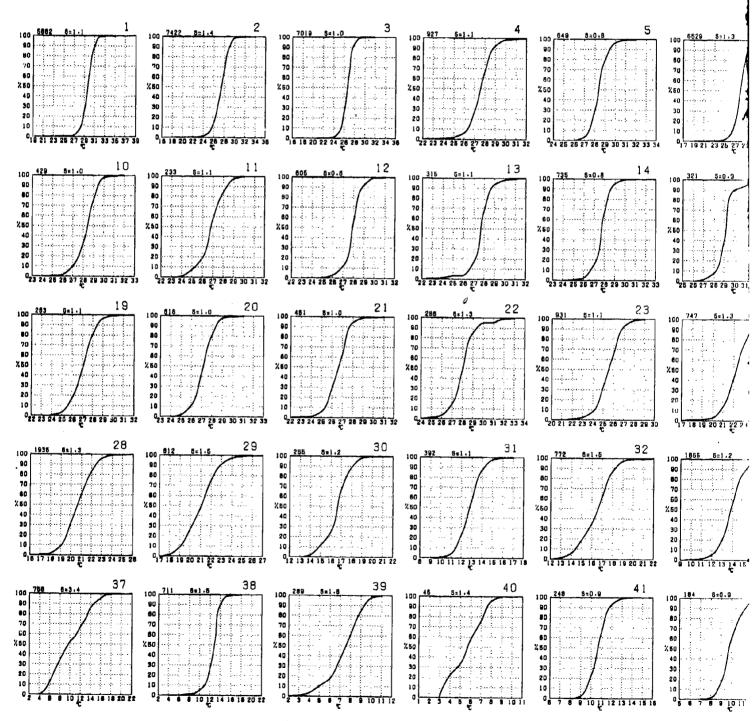
site page) are based on all available data subjectively adjusted where bias was evident.



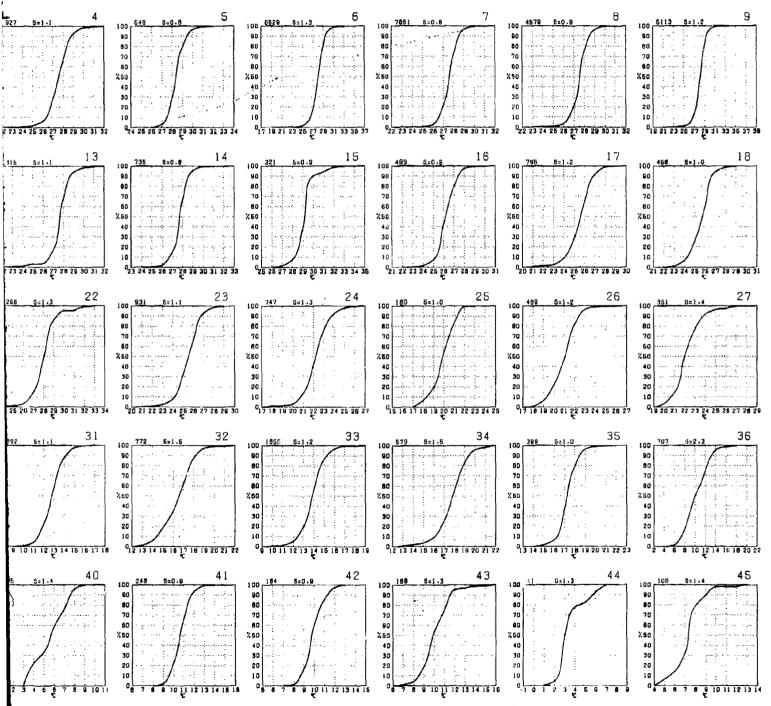
SEA SURFACE TEMPERATURE



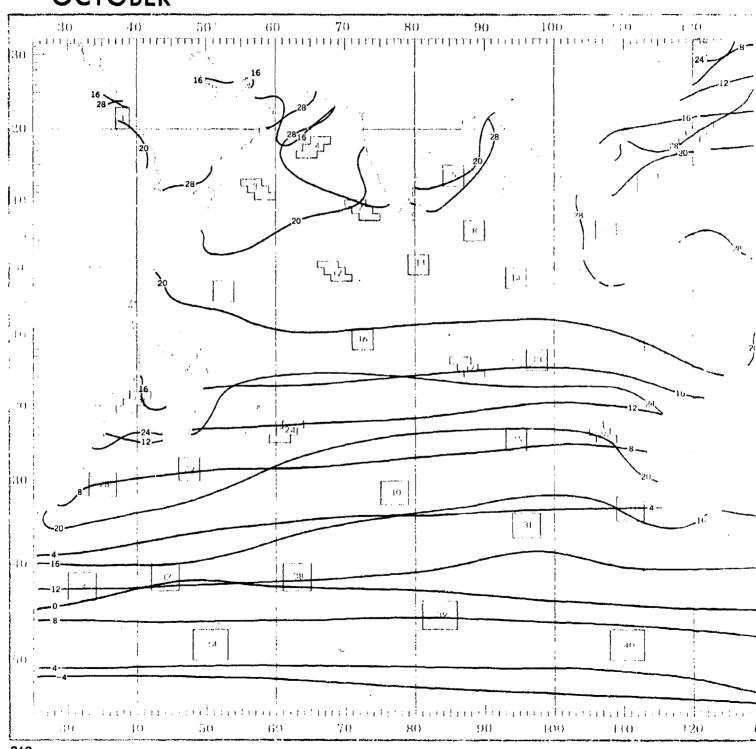
SEA SURFACE TEMPERATURE



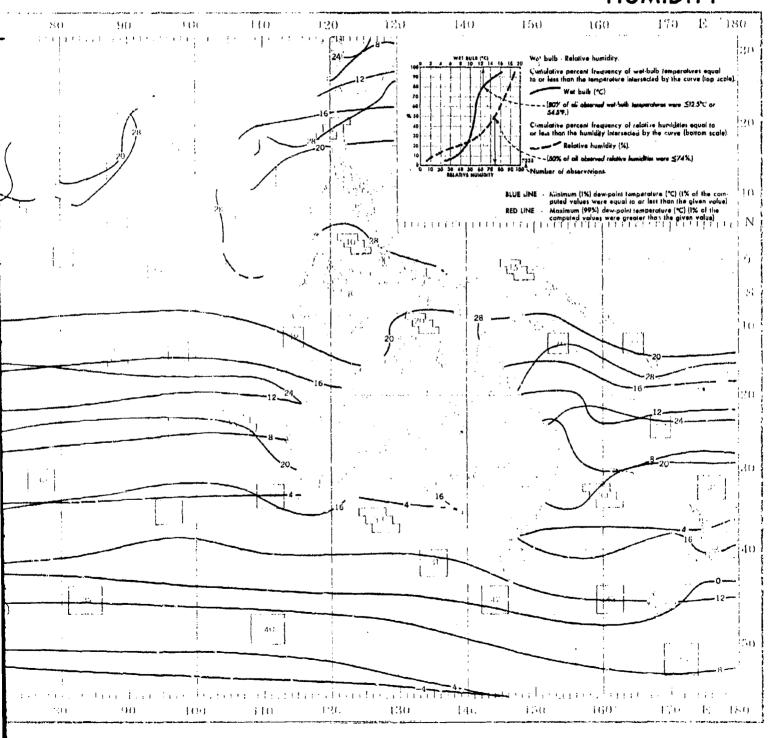
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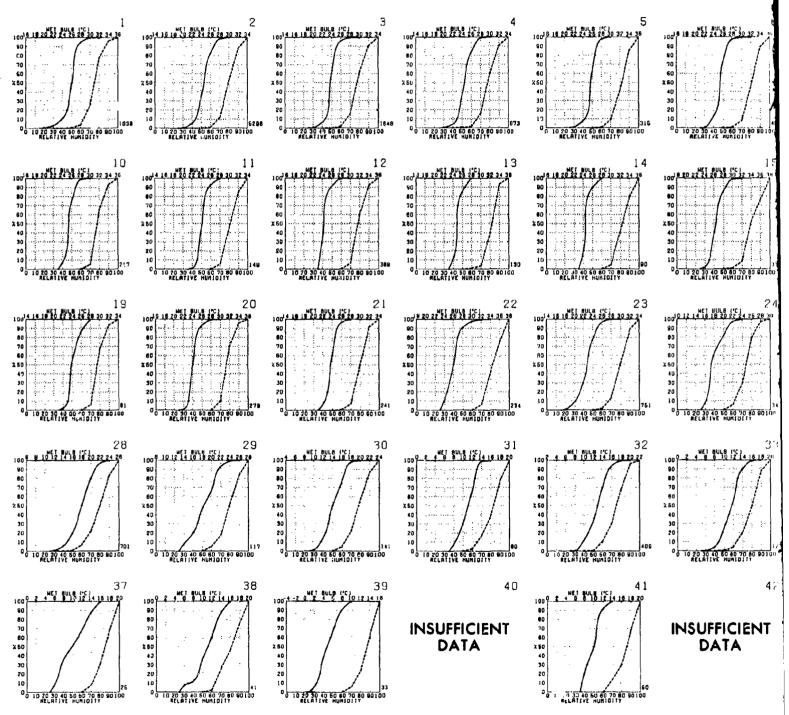
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HUMIDITY



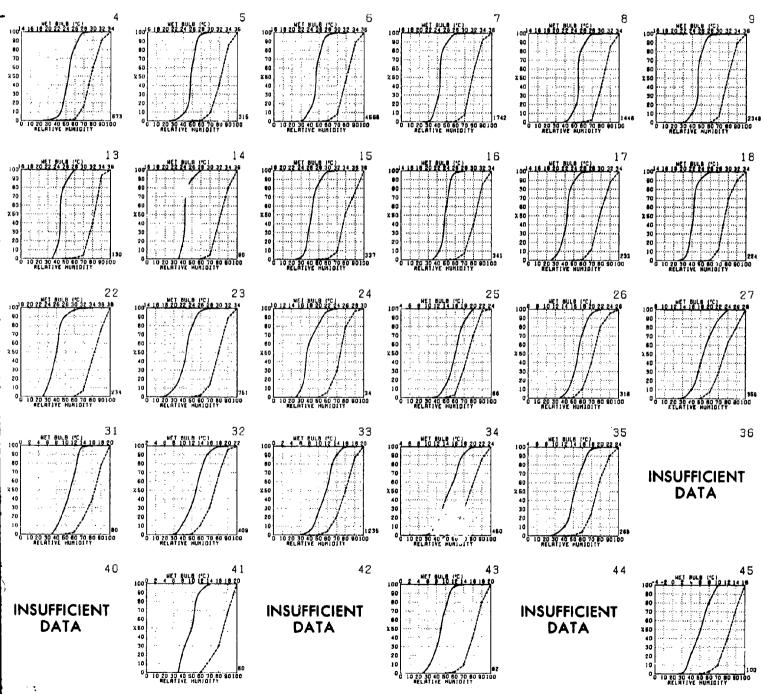
WET BULB AND RELATIVE HUMIDITY



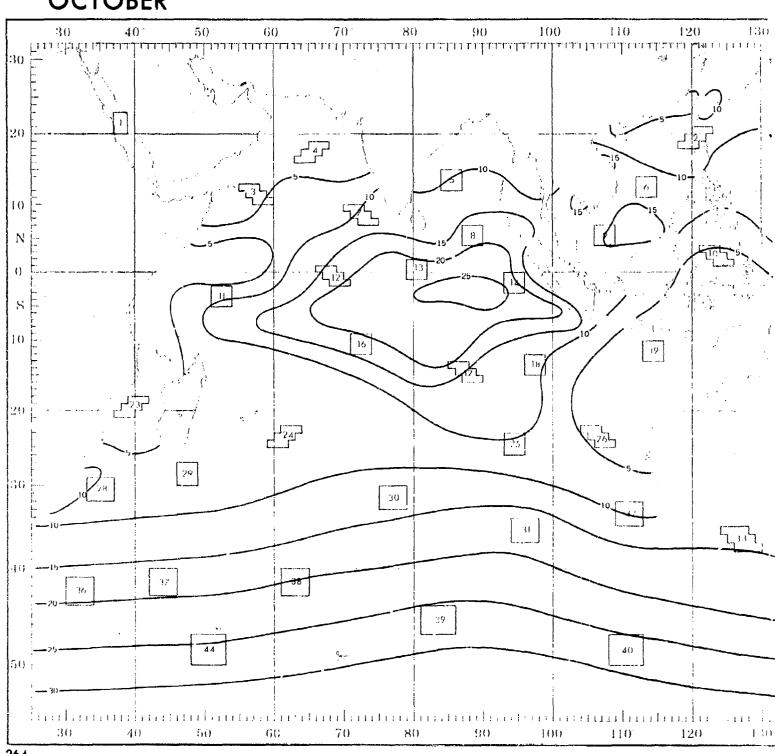
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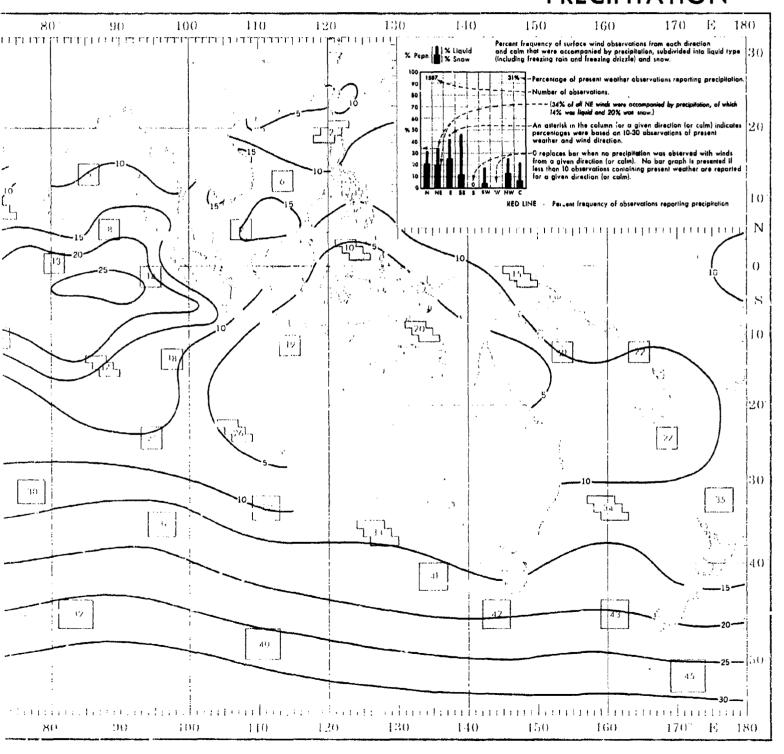
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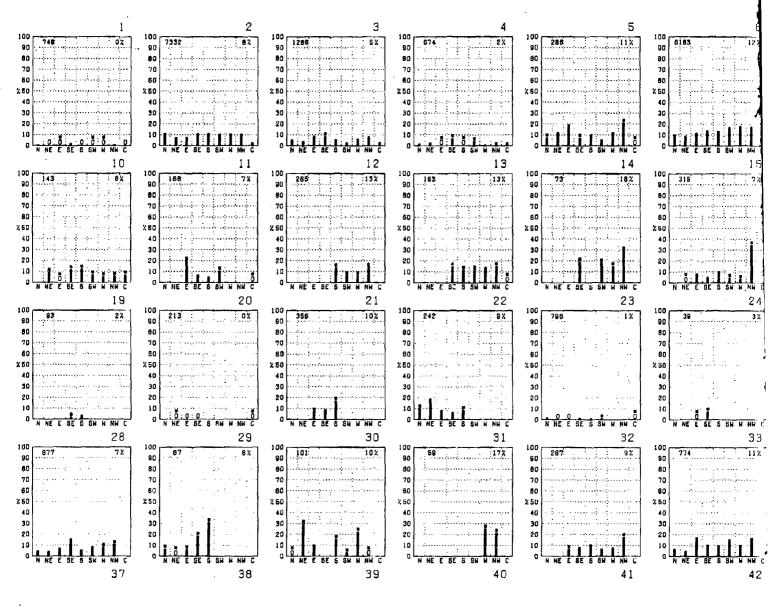
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PRECIPITATION



PRECIPITATION



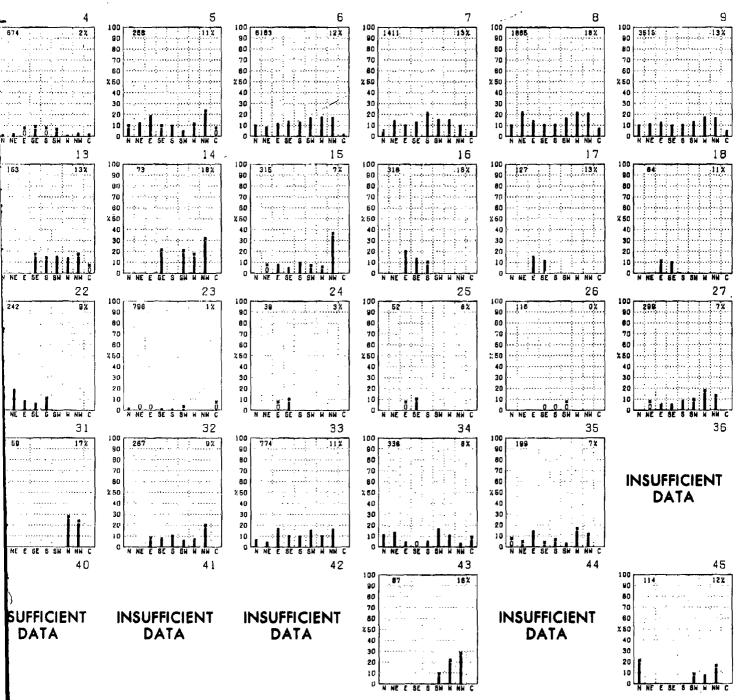
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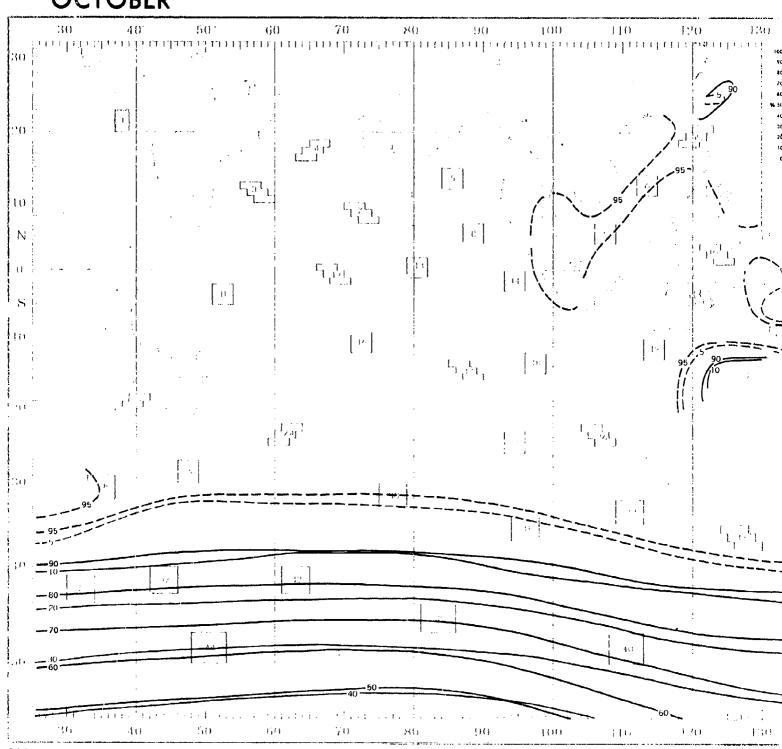
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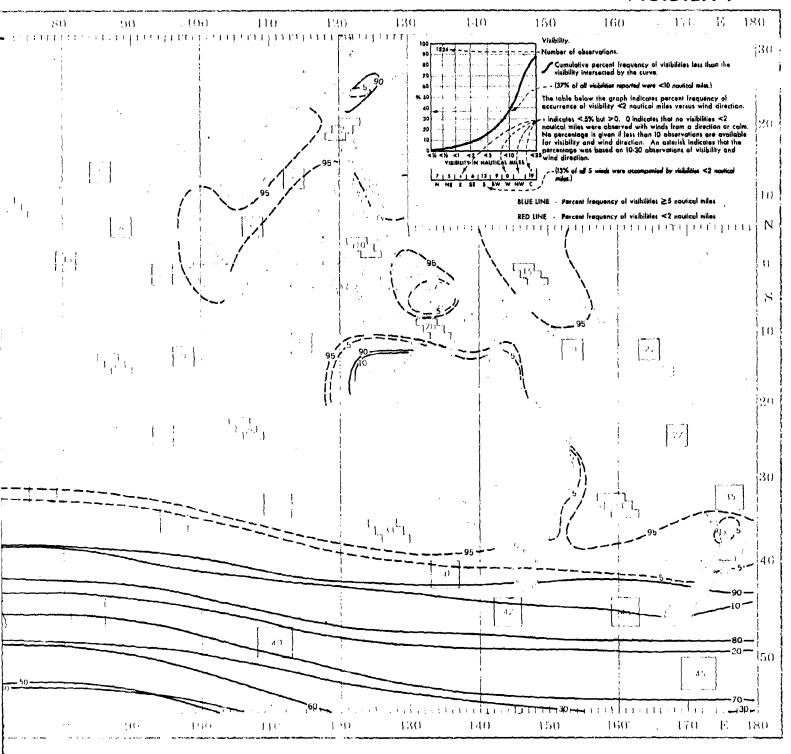
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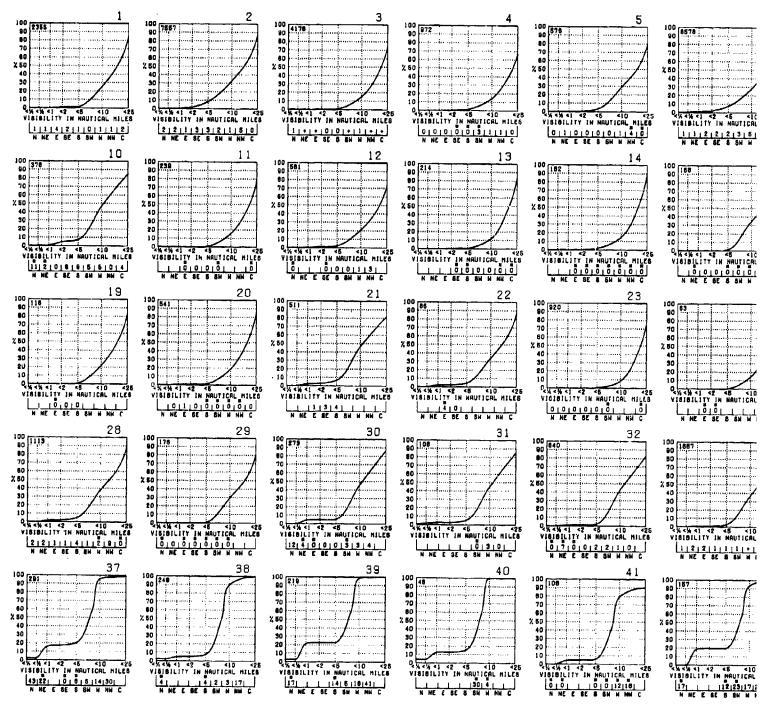
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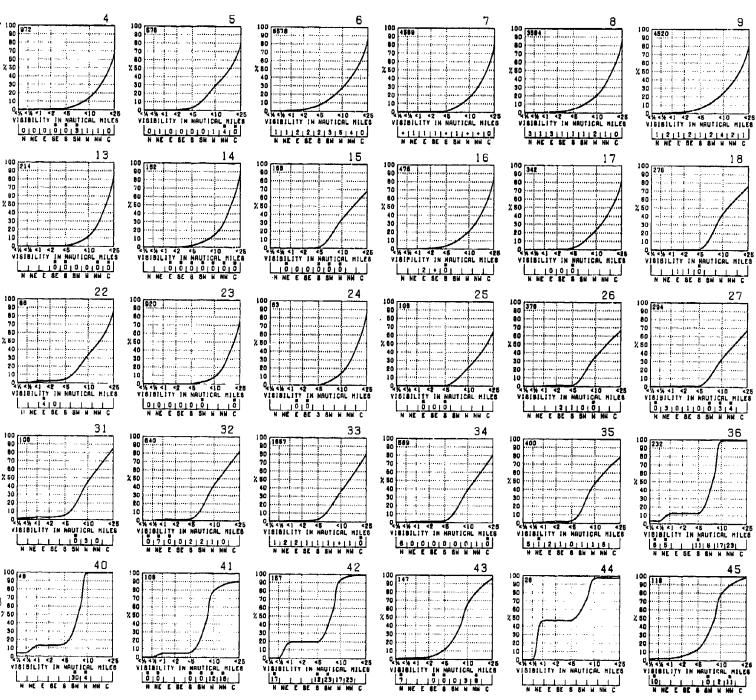
VISIBILITY



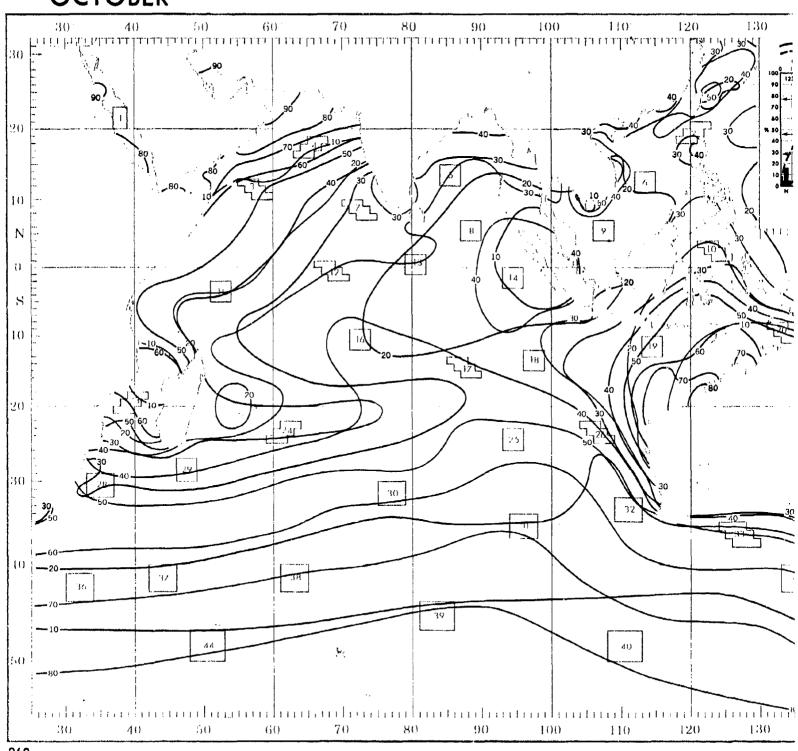
VISIBILITY



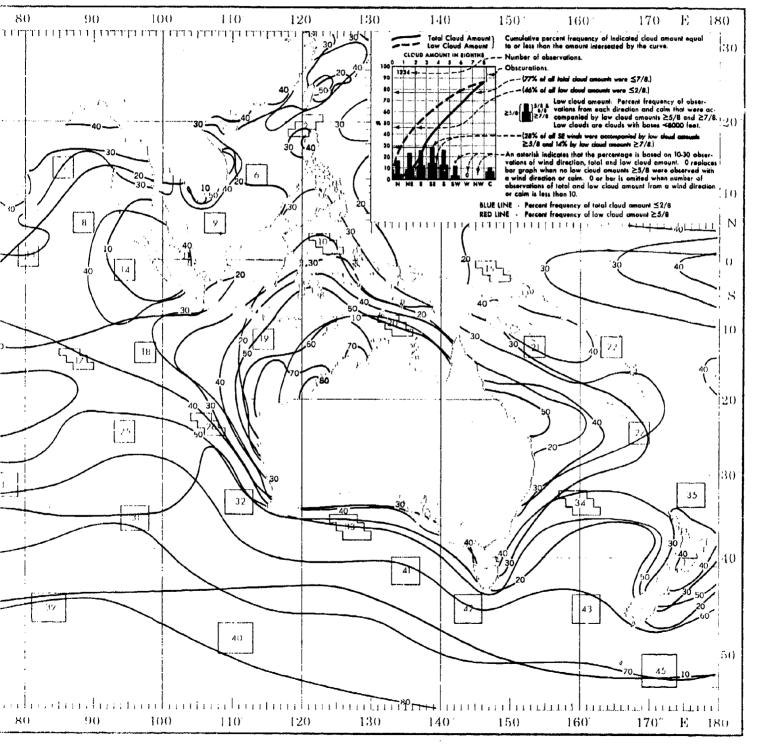
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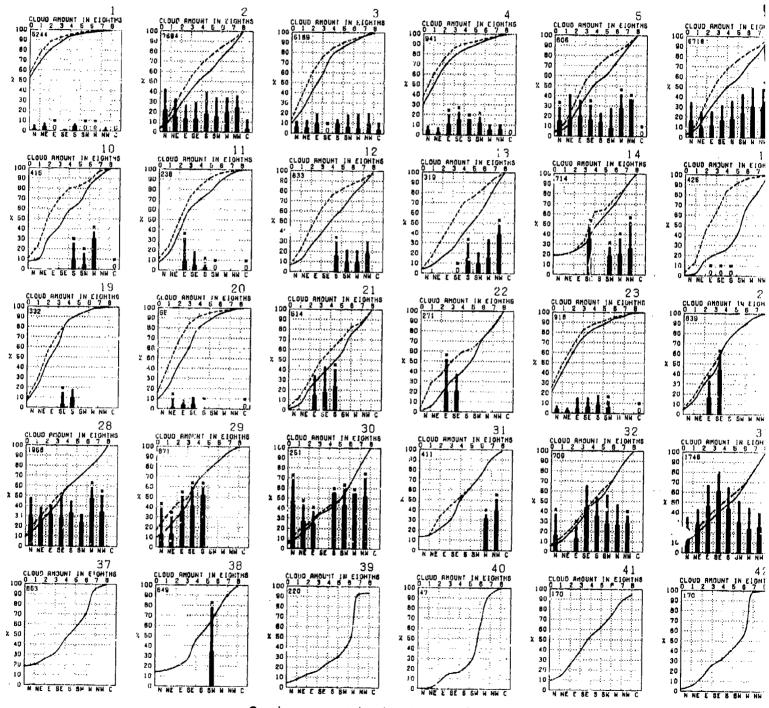
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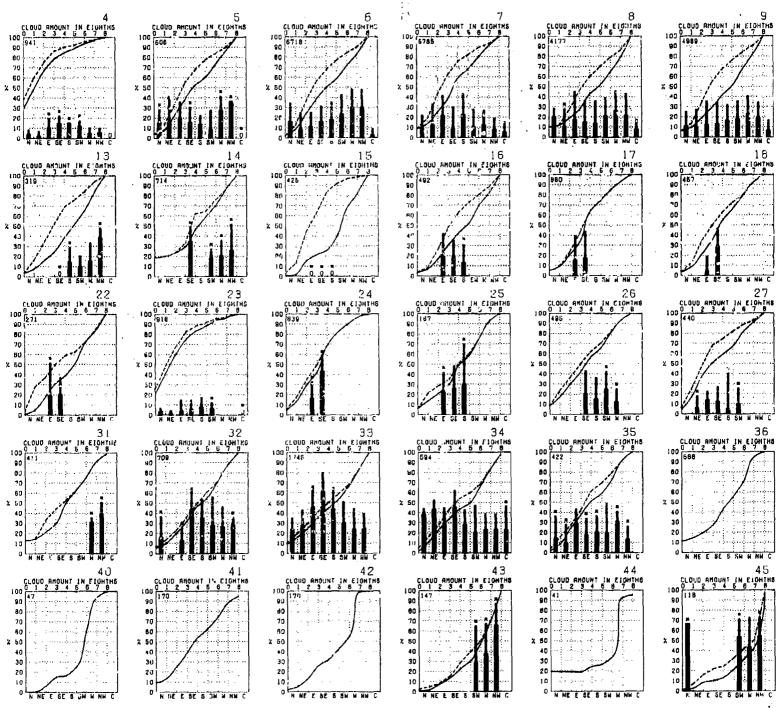
CLOUD COVER



CLOUD COVER

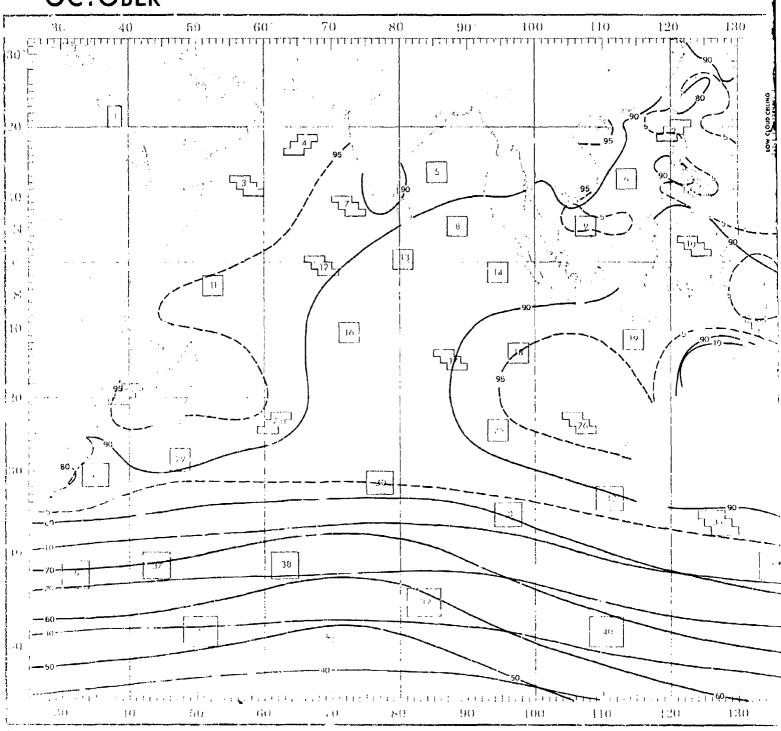


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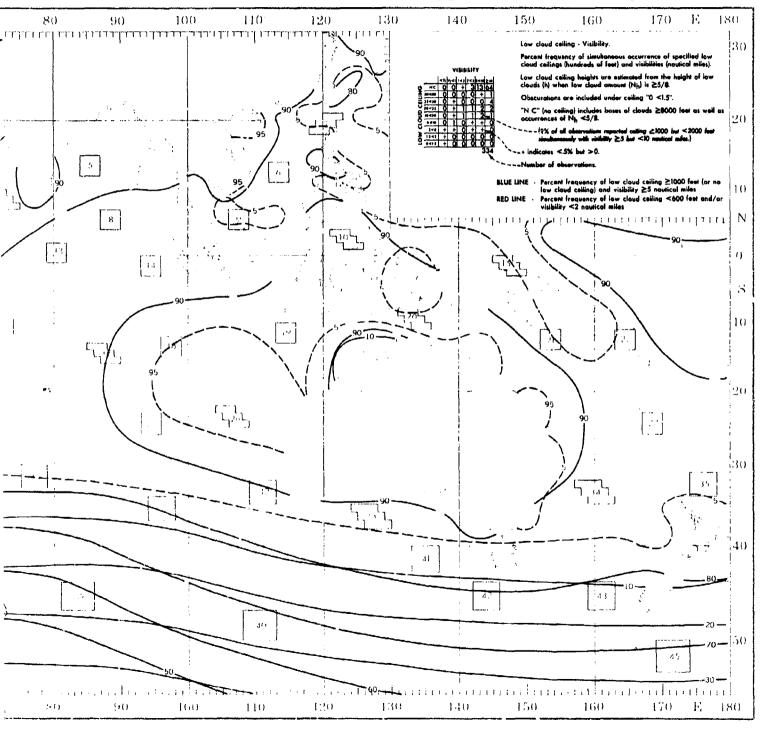


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Graphs represent the objective compilation of available data for specified areas without The isopleth analyses (opposite page) are based on all available data subjectively adjust

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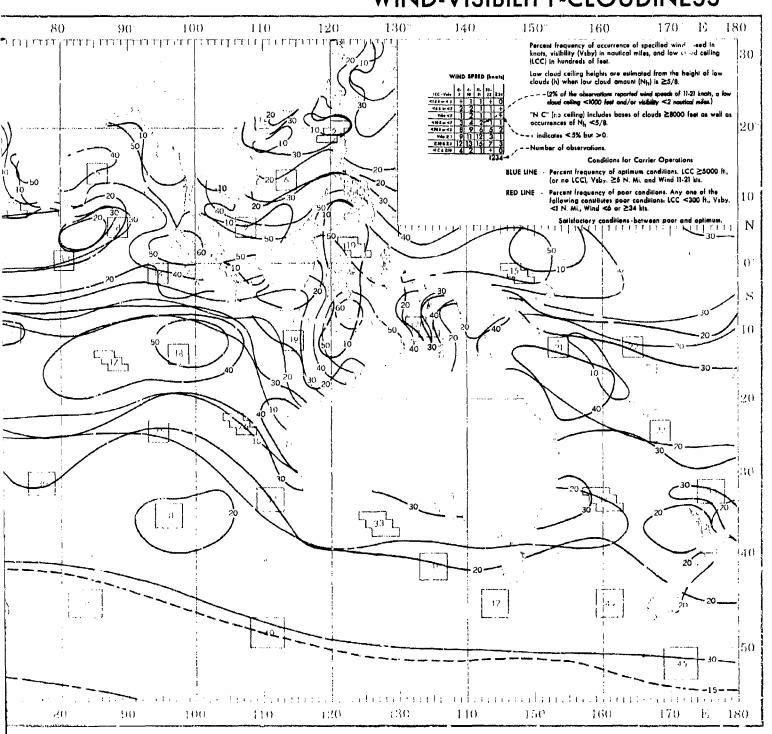
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VISIBILITY 31	VIBIBILITY -17 674-1 -18 246 6-10 317 -16 674-1 -18 246 6-10 317 -16 674-1 -18 246 6-10 317 -16 694-0 0 0 0 0 0 1 7 -16 594-0 0 0 0 0 0 1 7 -16 594-0 0 0 0 0 1 1 7 -16 594-0 0 0 0 0 1 1 7 -16 594-0 0 0 0 0 0 1 1 7 -16 594-0 0 0 0 0 0 0 1 1 7 -16 594-0 0 0 0 0 0 0 1 -16 594-0 0 0 0 0 0 0 0 0 -16 594-0 0 0 0 0 0 0 0 0 -16 594-0 0 0 0 0 0 0 0 0 0 0 -16 594-0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY Column	### 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VIETNIT VIET	INSUFFICIENT DATA
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tive compilation of available data for specified areas without regard to suspected biases.

posite page) are based on all available data subjectively adjusted where bias was evident.

OCTOBER WINE

WIND-VISIBILITY-CLOUDINESS



LOW CLOUD CEILING-VISIBILITY-WIND

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1	2	3	4	5	
WIND SPEED (KNOTS)	HINO SPEED (KNOTS)	MIND SPEED (KNOTS)	WIND SPEED (KNOTS)	WIND BPEED (KNOTS)	MIND SPEED (KNOT)
LCC - VASY 0- 4- 11- 22- 3 10 21 35 434	LCC - VBBY 9 10 21 35 494	LCC - YBBY 3 10 21 33 434	LCC - VSBY 3 10 21 33 294	LCC - VSHY 3 10 21 33 834	LCC - VSSY 3 10 21 33
<1.64 tex <.6 0 0 0 0 0	41-64 DR 4-6 D + + + +	41.8 £ 68 4.8 0 0 + 0 0	<1.54 OR <.8 0 0 + 0 0	11.8 t 98 4.8 0 + + B D	<1.54 DR <-6 + 1 -
48 Y 08 45 0 + + 0 0	48 4 0R 4E 0 + 1 2 +	<84 0M <2	48 L OR 42 0 0 + 0 0	<9.4 OR =2 O + 1 + +	46 L DR 42 4 1 2 1
V86Y 42 0 0 0 0 0	v84r <₹ 0 • 1 1 •	A88A 45 0 + 0 0 0	V007 <8 0 + 0 0 0	V857 <2 0 0 + 0 •	V88Y 42 + 1 1 ·
<10 4 0R <2 0 1 + 0 0	<10 4 0K <\$ + 1 4 4 1	<10 t 00 <2 + 2 1 0 0	<10 4 0R <2 + 1 1 + 0	410 4 0K 42 + 3 2 1 4 420 6 0K 46 1 9 6 2 4	410 4 DR 42 4 4 7 2 4 420 4 DR 45 1 9 14 3
400 4 68 45 1 1 1 0 0	480 4 DR 46 + 3 11 11 2 VBBY 35 2 17 44 28 2	420 4 0R 4B 1 4 4 + 0	120 4 0R 15	420 E OR 48 1 9 6 2 +	VBST 28 9 42 37 4
350 4 36 24 45 26 + D	360 435 2 14 35 16 1	a50 4 25 19 51 16 + C	450 A 25 13 55 22 1 0	360 4 NB 13 43 15 1 D	150 4 15 8 34 24 1
MC 4 10 23 44 25 + 0	HC 4 b 10 2 13 27 12 1	MC 4 a 10 18 49 15 + 0	HC 4 = 10 12 50 21 1 0	MG 4 = 10 12 38 14 1 0	HC4210 7 29 20 1
730	6388	1277	852	279	54
10	11	12	13	1 4	1 🖣
HIND SPEED (KNOTS)	WIND SPEED (KNOTS)	HIND SPEED (KNDTS)	WIND SPEED (KNOTS)	HINO o and (KNOTE)	HIND SPEED INNOT
LCC - VBBY 0- 4- 11-22-	LCC - Y86Y 0- 4- 11- 22-	LCC - Y887 0- 4- 11- 22- 33 434	LCC - Y00Y 0- 4- 11-22- A34	CCC - VBBY 3 10 21 33 234	LCC - VBBY 9 10 85 38
41.6 4 DR 4.8 0 0 1 0 0	<1.84 0R <.8 0 0 (1 0 0	41.84 GR 4.8 0 0 0 0 0	41 :8 4 OR 4 :6 0 0 0 0 0	41.84 0R 4.8 0 0 0 0 D	41-84 DR 4-8 D D D D
48 4 94 42 D D D D D	46 f 96 43 D D D D D	48 4 DR 42 0 0	48 4 OR 42 0 0 0 0 0	46 4 OR 42 0 0 3 0 D	10 t OR 12 O 4 O O
VESY -E 0 0 1 0 0	Y88Y 48 D D D D D	VAMY 42 0 0 1 0 0	V88Y -8 0 0 0 0 0	Vesy < R 0 0 0 0 0	760Y CZ 0 0 0 0
410 t pr <2 0 3 3 0 0	410 4 0R 42 1 3 1 0 0	410 4 0R 42 + 2 5 0 0	<10 4 0R 48 1 8 4 1 0	420 4 08 4E 0 4 8 0 0	410 4 0R 42 0 10 2 0
480 4 68 48 1 4 4 0 0 Yeav as 36 50 13 0 0	480 4 9R 46 2 5 4 1 0	420 4 OR 45 1 5 7 1 0	480 4 0R 45 2 12 9 1 0	480 4 0R 4S 0 19 10 0 0	-20 c 08 -6 2 10 2 0
250 4 hB 35 42 9 0 0	*50 4 36 19 64 11 1 0	250 4 25 5 47 25 1 0	250 225 9 41 21 0 0	250 4 25 10 30 16 0 0	>50 4 25 8 59 18 C
MC = 10 29 41 8 0 0	HC 4 2 10 16 69 10 1 0	HC410 5 43 23 1 0	HC 4 2 10 9 37 17 0 0	MC 4 a 10 10 35 18 0 0	HC 4 + 10 8 53 10 G
78	148	298	133	93	- I sloalish at
19	20	21	22	23	24
HIND SPEED (KNOTS)	NIND SPEED (KNOTS)	WIND SPEED (KNOTS)	WIND SPEED (KNOTS)	NIND SPEED (KNOTS)	HIND SPEED (KNOTS
LCC - YESY 3 10 21 33 484	LCC - VARY 3 10 21 33 334	LCC - Y887 3 10 21 33 554	LCC - V88Y 0- 4- 11- 82- 3 10 21 33 234	LCC - YEBY 3 10 21 33 954	LCC - VEST 0- 4- 11- 22-
41.8 t 04 4.5 D D D D C	<1.5 6 28 4.8 0 0 0 0 0	41-84 DR 8 0 + 0 0 0	-1.5 t OR 4.6 0 0 0 0 0	<1.54 GR <-B 0 0 + 0 0	4).54084.8 0 0 D 0
<1.8 ± 004 < .8	<1.5 à 28 < 8 0 0 0 0 0 0 0 0 48 à 82 <8 0 0 0 0 0 0 0	41 - 5 4 OR 5	1.540848 0 0 0 0 0 0 0 0 0 0 p 40 46	<1-54 OR <.8	4).5 & GR 4.8 0 0 0 0 0 0 4
-1.8 & OR -1.8 D D D D C	<1.5 à 201 <.5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41-84088 0 + 0 0 0 48 6 98 42 0 1 4 1 0 4887-42 0 0 1 0 0	-1.840R4.8 0 0 0 0 0 0 0 0 0 0 2×8048× 0 0 0 0 0 2×7048×	<1.54 GR <.B	<3.54.0R <.8
41.ELON 4.B D D 0 0 0 G 48.4 DN 4E U 0 0 0 0 0 988Y 4E 0 0 0 0 0 0 410.4 DN 4E 0 3 3 0 0	41.5 4 96 4.8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.8 4 00 · · · · · · · · · · · · · · · · ·	-1:5 & OR <:5	41.5 4.08 < 5 0 0 4 0 0 0 4 6 4.08 < 2 0 4 1 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	*1.6 4.98 4.8
-1.8 L OR -1.5 D D D D D G -84 4 9R -2 U D D D D D D D D D D D D D D D D D D	41.5 & 201 4.6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.8 4 00: -16	-1.5 £ 0R + £ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.5 4.08 < 5 0 0 4 0 0 0 4 6 4.08 < 2 0 4 1 4 0 0 0 4 6 4.08 < 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.64.08 4.8
-1.8 £ 08 4.5 D D D D D D G -9 4 08 4 £ U D D D D D D D D D D D D D D D D D D	41.6 6.7 ep 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.8 4 00 - 16 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-1.5 & OR +4 & O O O O O O O O O O O O O O O O O O	41.5 £ 00 < 5 0 0 4 0 0 0 4 6 4 0 0 0 4 6 4 0 0 0 0 0	41.6 4.68 4.6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
-1.8 £ 08 4.5 D D D D D D G	41.6 4.08 4.6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.84 08 - 16 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-1.5 £ 0R + £ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.5 4.00 < 5 0 0 4 0 0 0 4 6 4.00 < 5 0 0 4 1 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.64 SM 4.6 0 0 0 0 0 0 0 464 SM 4.6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
-1.8 LOP -1.5 D D O O O G -8 4 00 -1 U O O O O O valor -2 O O O O O O -10 400 -2 O O O O O -10 400 -2 O O O O O -10 400 -3 D O O O O O -10 400 -3 D O O O O O O O O -10 400 -1 D O O O O O O O O O O O O O O O O O O	41.6 4.04 + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.84 08 - 16 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-1.5 & OR -16	41.5 4.88 <	41.6 4 58 4 .6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
41.8 £ 08 4.5 D D D O D G 48 4 68 42 U O O O O O 410 4 68 42 D O O O O O 410 4 68 42 D O O O O O 410 4 68 42 D O O O O 410 4 68 42 D O O O 410 4 68 42 D O O 410 4 6 6 6 D O O 410 4 6 6 D O O 410 4 6 D O O 410 4 6 D O O 410 4 6 D O O 410 4 6 D O O 410 4 D O O 410 4 D O O 410 4 D O O	*1.5 & 3.6 *4.6	*1.8 4 00* -1.6	-1.5 & OR -16	41.5 4.00 4.5 0 0 4 0 0 0 4 0 0 0 4 0 0 0 4 0 0 0 4 0	41.6 4 68 4 . B
-1.8 L DN -1.8 D D D D D C -94 DR -1.8 L DN -1.8 D D D D D D D D D D D D D D D D D D D	41.8 4.98 4.8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.8 4 DR6	-1.5 & OR -1.6 O O O O O O O O O O O O O O O O O O O	41.6 4.08 4.8 0 0 4 1 4 0 0 4 4 4 0 4 4 0 4 4 0 4 1 4 0 0 4 1 4 0 0 4 1 4 0 0 4 1 4 0 0 1 4 1 4	41.6 4 68 4 . 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
-1.8 L DW -1.5 D D D D D C -9.4 D8 -1.5 L DW -1.5 D D D D D D D D D D D D D D D D D D D	41.8 4.98 4.8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.8 4 DR6	-1.5 & OR -1.6	41.5 L SN 4.8 0 0 0 + 0 0 0 48 4 0 8 42 0 + 1 1 + 0 489 42 0 0 0 0 0 0 410 4 0 8 45 0 1 1 1 1 0 420 4 0 8 45 0 3 3 1 0 480 4 8 4 10 0 0 0 0 480 4 8 10 0 0 0 0 0 480 4 8 10 0 0 0 0 0 480 4 8 10 0 0 0 0 0 0 748 32 MIND SPEED (KNDTS) LCC - 488 7 8 11 12 12 12 13 194	41.6 4 58 4 4 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
-1.8 L DN -1.5	41.8 4.98 4.8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.8 4 DR6	-1.5 & OR -1.6	41.54 0N <.5 0 0 4 0 0 0 4 4 0 0 0 4 4 0 0 0 4 4 0	41.6 4 S
	41.8 & 308 4.8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.8 4 08 - 18 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-1.5 L OR -1.6	41.5 4.00 4.5 0 0 4 1 4 0 0 48.4 08.42 0 4 1 4 0 4887 42 0 0 0 0 0 0 0 410 4.06 42 0 1 1 1 1 0 420 4.06 45 4 3 3 1 0 4887 88 11 50 34 5 0 880 4.8 10 46 28 4 0 MC 4.8 10 9 45 25 4 0 748 310 48 40 40 40 40 40 40 40 40 40 40 40 40 40	41.6 4.08 4.8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
-1.8 LOR -1.5	41.6 & 364 + 6	1.5 4 086 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-1.5 & OR -16	41.5 4.08 < 8 0 0 4 0 0 0 4 6 4.08 < 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.6 4 DR 4-8
1.8 L DN 4.5 D D O D C	41.8 4.98 4.8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.84 08 - 18	-1.5 & OR <-6	41.5 ± 08 < 5 0 0 4 0 0 0 4 0 0 0 4 4 0 0 0 0 4 1 1 1 0 0 0 0	41.64.08 + 8
1.8 L DN 4.5 D D O O C	41.8 4.98 4.8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.5 4 08 - 15	-1.5 & OR = 4 & O & O & O & O & O & O & O & O & O &	41.64 OR < 8 0 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.6 4 58 4 . 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
41.8 L D# 4.5	41.8 & 3.8 4.8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.8 4 00 - 1	-1.5 & OR = 4 & O & O & O & O & O & O & O & O & O &	41.6 4 08 48 0 0 0 4 0 0 0 4 4 0 0 0 4 4 4 0 4 2 0 0 0 0	41.64.08 4.6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	41.8 4.98 4.8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.5 4 00 - 6	-1.5 & OR -1.6	41.6 4.08 < 8 0 0 4 1 4 0 0 0 4 6 4.08 < 8 0 0 4 1 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.64.08 4.6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
41.8 £ 08 4.5	41.8 A 308 4.8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.5 4 00 - 6	-1.5 & OR = 4.6	41.5 4.08 4.8 0 0 4 1 4 0 0 48.4 08 42 0 4 1 4 0 4887 42 0 0 0 0 0 0 0 410 4.08 45 0 1 1 1 1 0 4887 88 11 50 34 5 0 4887 88 11 50 34 5 0 4887 88 10 46 28 4 0 MC 4.5 10 9 45 25 4 0 41.6 4.08 4.5 0 10 21 31 324 41.6 4.08 4.5 0 0 0 0 0 0 40 4.0 4.5 10 21 31 384 41.6 4.08 4.8 0 0 0 0 0 0 40 4.0 4.2 4 0 4 0 40 4.0 4.2 4 0 4 0 40 4.0 4.2 4 0 4 0 4 40 4.0 4.2 1 1 1 6 1 4 4887 48 1 1 1 1 1 1 1 1 4 4887 48 4 34 42 16 2 8 40 48 2 1 10 13 4 1	41.6 4.08 4.6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
1.8 L DN 4.5 D D O O C	C C C C C C C C C C	1.84 OR - 16	-1.5 & OR <-6	41.5 4 08 42 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.6 4.08 4.6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
41.8 L DR 4.8 D 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.8 & 3.8 4.8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.84 OR - 16	-1.5 & OR = 4 & O & O & O & O & O & O & O & O & O &	41.64 OR 4.8 0 0 0 4 0 0 0 4 6 4 0 0 0 4 6 4 0 0 0 0	41.6 4.08 4.6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
41.8 LOR 4.8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	C C C C C C C C C C	1.84 OR - 16	-1.5 & OR = 4 & O & O & O & O & O & O & O & O & O &	41.5 4 08 42 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	41.6 4.08 4.6 0 0 0 0 0 0 0 4 4 4 6 4 0 4 4 6 4 10 4 10

INSUFFICIENT DATA

MINE	8	EE.		401	5 :
LCC - YADY	0.	4- 10	11-	\$2 \$2	۱.
41.6 4 GR 4.0	0	0	0	0	
<0 4 DR +2	0	0	0	٥	
VBOY 42	0	0	ō	0	
410 4 00 42	٥	4	11	11	
420 4 OR 48	D	11	19	15	
V687 15	0	13	48	26	
# \$0 4 a8	0	-1	11	4	
MEAAIO	<u>Λ</u>	T-4	111	1	П

INSUFFICIENT DATA INSUFFICIENT DATA

MIN	88	EEC		NOT	8)
LCC - V88Y	0.	tio	11- #1	21. 33	-31
41 -8 4 04 4 -8	0	0	0	0	0
484 00 48	0	7	7	0	0
Y88Y 4E	0	0	0	0	0
410 4 0A 48	0	21	16	0	0
410 4 OF 46	0	21	34	7	1
YESY AS	0	42	60,	a	ĺr
# 60 4 mB	q	2 !	2	r	C
HC 1 = 10	0	21	21	\Box	[]

INSUFFICIENT DATA

Graphs represent the objective compilation of available data for specified areas without in The isapleth analyses (opposite page) are based on all available data subjectively adjust

ITY-WIND

OCTOBER

. 4	5	6	7	8	9
HIND SPEED (KNOTS)	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNDTS)
LCC - VEST 3 10 21 39 234	LCC - VSBY 3 10 21 33 234	LCC - VSSY 3 10 21 33 824	LCC - Y687 3 10 21 23 234	LCC - Y88Y 0- 4- 31- 22-	LCC - VBSY 3 10 21 33 134
-1.5 4 OR -15 0 0 + D 0	*1.54 OR *.5 D + + O D	€1.6 ± DR €.6 + + 1 + +	41.8 4 DR 4.8 0 + + D D	41.5408 4.8 0 + + + 0	41-84 0R 4-8 D + + O +
48 E OR 48 0 + + O 0	46 4 OR 42 0 + 1 + 3	-64 DR 42 + 1 2 1 +	48 4 9R 42 0 1 1 + C	48 4 BR 42 + 2 2 1 0	48 4 OR 48 1 1 2 + +
V88Y 4R 0 + 0 0 0	Y88Y 4E 0 D + 0 +	¥881 42 + 1 1 + +	V88Y 42 0 + + D D	A88A 45 + + + + 0	A88A 15 + + 1 + +
<10 4 04 <2 + 1 1 + 0	410 4 6R 42 + 3 2 1 +	<10 4 8k 42 + 4 7 2 +	410 4 0M 42 1 4 3 + D	<10 4 OR <2 1 5 7 2 +	410 4 08 42 2 8 4 + +
120 4 0R 4S + 3 1 + 0	480 4 0R 46 1 9 6 2 +	420 a GR 48 1 9 14 3 +	420 4 0R 46 2 8 6 1 0	420 4 6R 45 2 11 14 3 +	420 4 06 45 3 14 8 + + V887 25 19 55 19 1 0
Vest as 14 58 25 1 0	Y88Y 35 15 54 22 4 +	*80 4 *5 B 34 24 1 +	a 50 4 a 8 14 44 18 1 0	250 4 28 8 29 22 2 0	250 4 28 16 39 12 + 0
HC 4 10 12 50 21 1 0	HG 4 = 10 12 38 14 1 0	HC 4 = 10 7 29 20 1 0	MC 4 a 10 13 42 17 1 0	HC 4 = 10 8 27 19 1 0	MC 4 = 10 14 34 10 + 0
662	279	5440	1378	1470	2433
13	14	15	16	. 17	18
HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)
LCC - YARY 8 10 21 39 494	FCC - ANDA C 10 SF 32 034	LCC - V60Y 3 10 21 33 834	. Lec - VABY 9 10 21 33 834	LCC - VSBY 3 10 21 38 234	LCC - V887 3 10 21 33 824
*1.84 98 < .\$ 0 0 t) 0 0	41.84084.8 0 0 D 0 0	41.84 0R 4.8 D D D D D	41-8 4 OR 4-8 0 0 0 + D	<1.646R<-6 0 0 1 0 0	<1.64 DR < iff 0 0 0 0 0
*8 6 40 42 0 0 0 0 0		48 L GR 4 D 4 D 0 D	<8 4 0R 42 0 0 3 1 0	48 4 0R 42 0 0 1 1 0	*8 4 OR *2 0 0 0 1 0
*10 ± 08 <2	YERY 42 C O O O O O	487 42 0 0 0 0 0 410 4 0H 42 0 10 2 0 0	VBBY 42 0 0 1 0 0	V887 <2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	410 4 BR 42 0 0 1 2 0
-20 4 0R -5 2 12 3 1 0	420 4 OR 45 0 13 10 0 0	420 6 0R 48 2 10 2 0 0	420 4 08 48 0 3 17 8 1	420 4 OR 45 0 2 18 4 0	-20 4 OR 48 0 2 10 5 0
V667 a5 13 55 32 1 0	V887 NS 11 80 27 0 0	VERY 28 10 73 15 0 0	V467 46 + 19 67 10 1	V48Y #6 1 15 68 15 0	V68Y 26 1 14 71 13 0
, 82 4 38 9 41 21 0 0	250 4 25 10 36 18 0 0	360 4 48 8 59 16 0 0	280 4 26 + 14 48 4 D	350 4 35 1 11 3B 9 0	580 E 38 1 10 45 7 U
HC 5 = 10 9 37 17 0 U	HC 6 = 10 10 35 18 0 0	N: 4 2 10 8 63 10 0 0	HC 4 > 10 + 13 42 3 0	HC4#10 1 10 35 8 0	MC4210 1 1D 43 8 0
133	89	61	326		
22 WIND SPEED (KNOTS)	23 Wind Speed (Knots)	24 winn speed (KNOTS)	25 WIND SPEED (KNOTS)	26 WIND SPEED (KNOTS)	27 NIND SPEED (KNOTS)
	0- 4- 11- 22-	0- 4- 11-122-	10-14-111-122-1	0- 4- 11- 22-	9- 4- 21-122-
	LCC - VART \$ 10 21 35 234				1.64 00 4.6 0 0 0 0 0
41-54 OR 4.6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	49 4 0H 4P 0 + 1 - 0	<1.84 0R <.B	41.8 4.0k 4.8	48 4 98 48 0 1 0 0 0	
V807 -2 G G O O O	Vasr 42 0 0 0 C 0	VEAT 48 0 0 0 0		V88Y 4R 0 0 0 0 0	V88Y 4Z 0 0 0 0 0
410 4 OR 45 2 0 7 2 0	-10 t 3k <5 0 1 1 1 0	410 4 UR 48 0 0 3 0 0	*10 4 0R *2 0 5 3 0 0	410 4 GR 42 1 3 1 1 0	<10 4 00 42 0 3 3 3 0
<20 4 08 46 2 2 18 5 0	-20 4 GR -5 - 3 3 1 D	<20 4 5R 48 3 D 8 0 0	420 4 OR 45 0 10 14 3 0	<20 & OA 48 1 7 5 1 0	420 4 MR 48 1 8 8 4 0
V68Y 25 7 17 48 5 0	vser as 21 50 34 5 0	year 25 5 32 53 11 0	VARY 25 5 54 33 0 0	Y887 NS 4 41 48 8 0	veev =6 3 40 49 8 0
HC 4 2 10 5 30 30 0 0	160 4 8 10 46 28 4 0	» 10 4 a B 3 28 24 3 0	MC4a10 2 32 15 C 0	80 4 26 3 27 29 3 0 MC 4 2 10 3 25 25 3 0	a 50 4 a 5 1 29 40 4 0 MC 4 a 10 1 28 37 4 0
44	748	38	- HE 4 2 1 2 32 13(2) 0	104	159
31	32	33	34	35	. 36
WIND BPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEEU (ISHO)	HIND SPEED (MNO/S)	HIND BELED (KNOTS)	33
LCC - VBSY 3 10 21 33 .34	LCC - YACY 0- 4- 11- 22- 35 A34	LCC - VSSY 3 10 21 28 194	LCC - YBBY 3 10 21 33 432	LCC - VBBY 3 10 81 93 834	
41-54-004-15 0 2 0 0 0	41.8 COR 4.8 0 0 0 0 0	<1.84 SH <.8 0 + + 0 0	<1.8 4 08 < 16 D1 1 4 D 0	41.54.08 4.6 0 0 1 0 0	
4 0 4 2 0 0 0 0 0	18 4 9R 42 + C + C +	494 001 42 + 1 + 1 +	48 4 GR -2 + 1 2 0 +	49 4 9E 42 0 C 7 0	INSUFFICIENT
VADT 42 0 2 0 C 0	VSSY 42 0 0 0 0 0	V881 42 0 + 0 + +	ARRA 45 D + 0 0 0	VBBY 42 0 0 1 0 0	
410 & OR 42 2 11 7 C 0	*10 6 9R 48 1 1 B 1 •	<10 4 OR <2 + 4 5 2 1	410 4 M 42 1 2 8 + 1	416 4 0ft 42 0 2 7 3 0	DATA
**************************************	VCSY 26 4 34 42 15 2	480 4 0F 4F 1 9 13 6 2 VSBY 8F 2 52 43 16 1	489 4 58 48 3 9 17 2 1 9461 aB 7 31 50 9 2	420 4 08 46 1 11 11 4 0	
100 4.5 2 20 23 7 3	: 50 tas 2 19 22 9 2	280 4 85 2 18 24 8 2	280 4 36 3 19 26 4 1	364 4 86 8 28 29 5 0	
W 4410 2 20 21 2 3	MC 4 2 10 2 17 20 7 1	MC 5 a 10 2 16 21 7 1	MC4410 3 19 26 3 1	MC4 219 6 25 25 4 0	

INSUFFICIENT DATA

40

MINI	5#	EEC	(#	HOT	8)
LCC - 1887	٥-	19	11.	11- 33	934
41-5 4 OR 4-5	0	0	0	0	٥
48 4 88 42	0	7	7	0	0
A89.4 < 5	0	0	0	٥	0
410 4 0A +2	a	21	14	2	ב ב
450 C 08 4E	a	21	36	0	0
VOUT NO	ō	43	50,	-	٥
220 4 16	a	21	21	J	0
P7 4 1 10	0	2:	21	0	0

41

INSUFFICIENT DATA

42

					•
L26 - 1881	3	ip		8X 33	134
4) 18 4 M 418	آ آ	0	ī	0	0
46 64 48	0	3	0	5	0
1887 -5	0	٥	3	0	0
415 4 08 <2	0		17	9	3
480 4 DR 48	0	13	28	16	5
V607 55	0	17	36	20	7
160 4 40	14		13	7	3
MC 4 9 10	0	3	13		3
		_	L		77

43

INSUFFICIENT DATA

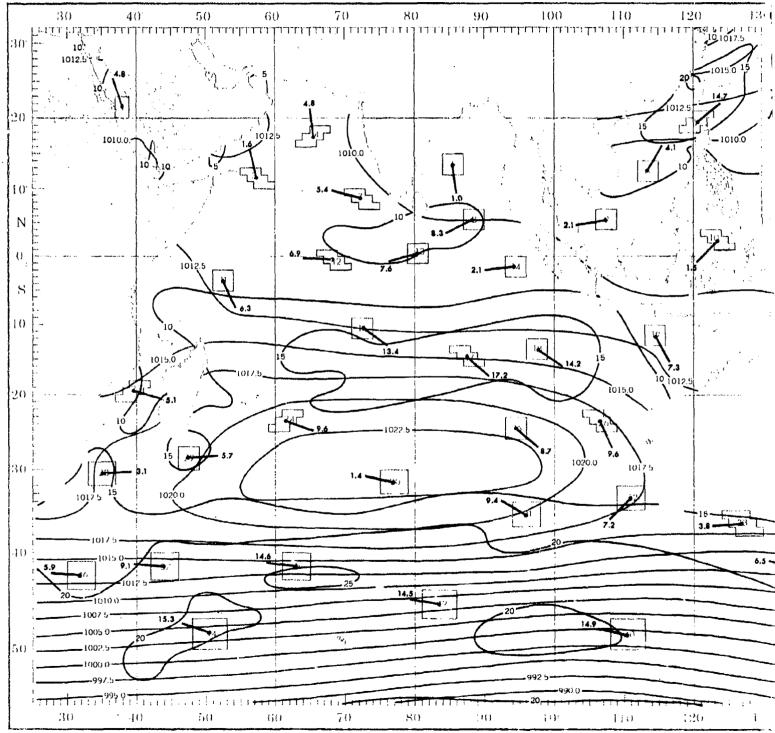
44

				4	5			
HIND SPEED (KNOTS)								
FCC - AMBA	0.8	10	11- 21	22- 39	234			
41-54-08 4-5	9	0	1	2	1			
"3 c tot =2	0	0	2	2	4			
V907 <\$	0	0	1	1	4			
40 4 BA 42	0	1	,	3	1			
-20 4 BR 45	0	3	12	17	4			
YSBY D\$	0	4	30	39	ē			
350 4 25	0	0	14	14	1			
HC 4 b 18	0	0	9		٥			

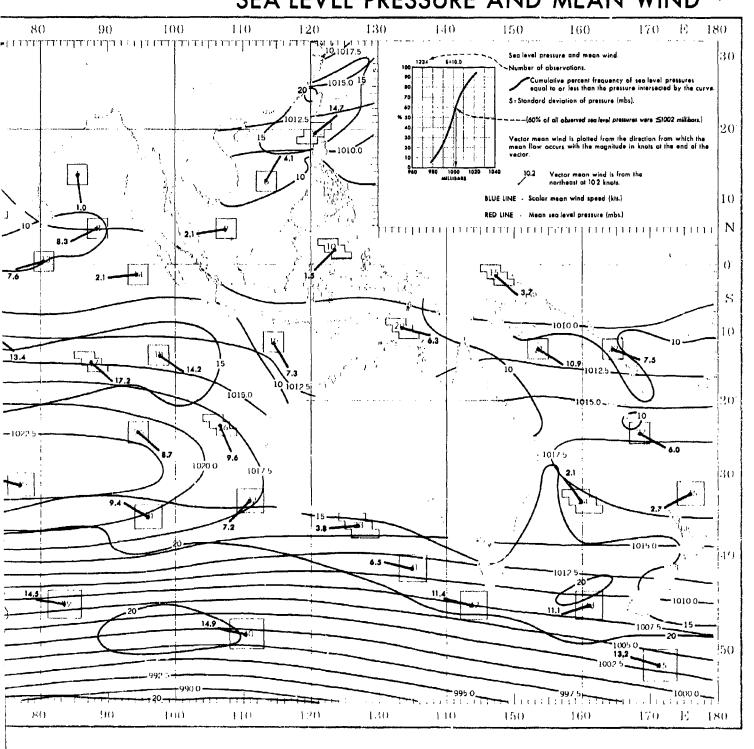
ctive compilation of available data for specified areas without regard to suspected biases.

osite page) are based on all available data subjectively adjusted where bias was evident.

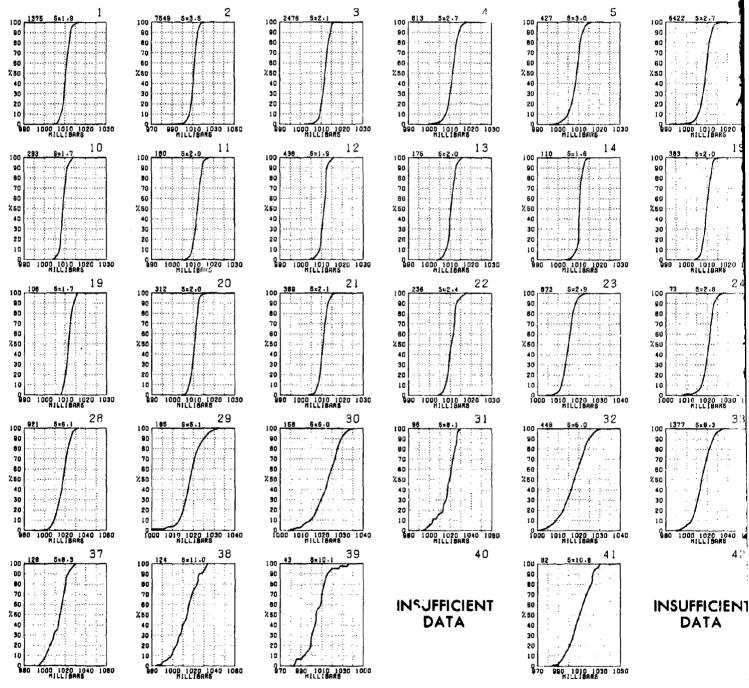
SEA LEVEL PR



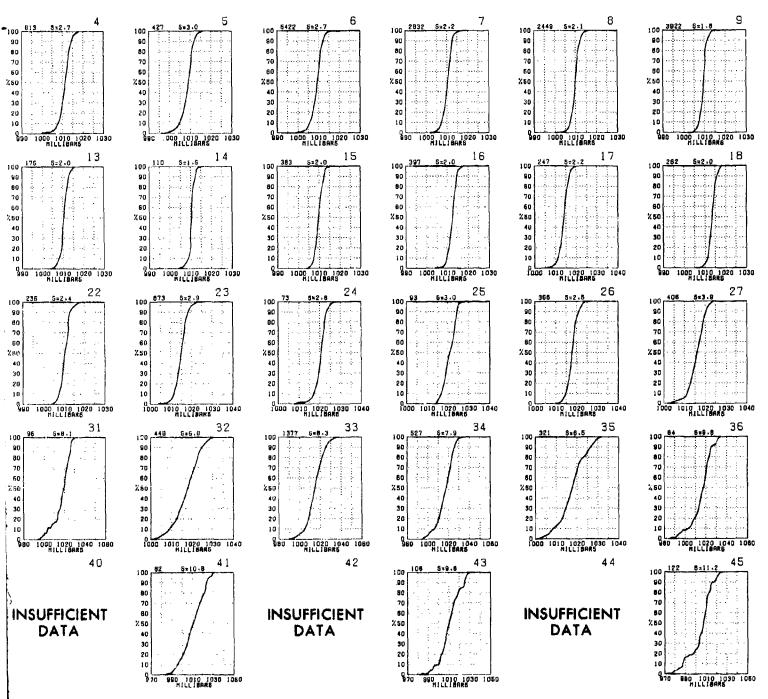
SEA LEVEL PRESSURE AND MEAN WIND



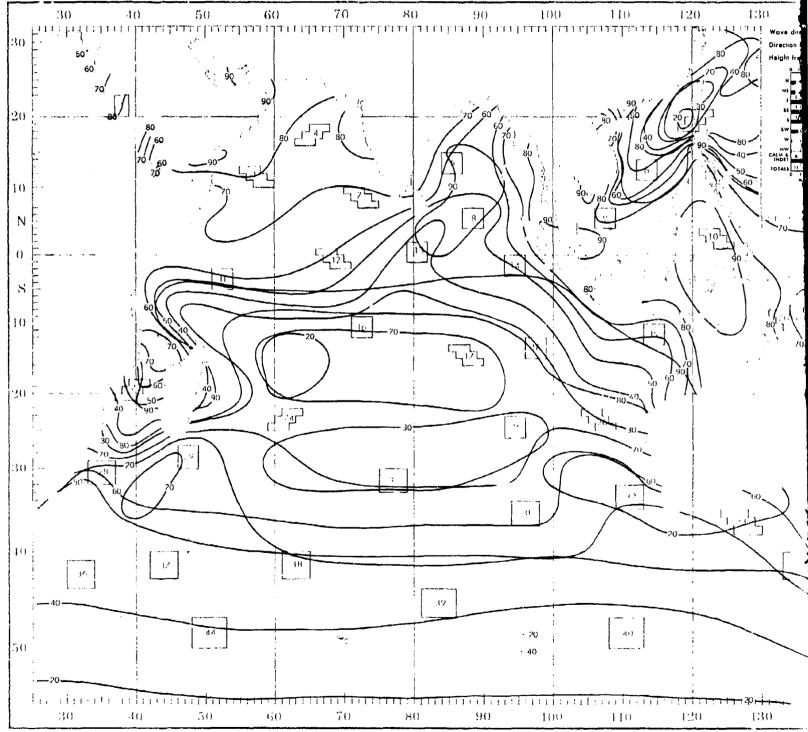
SEA LEVEL PRESSURE



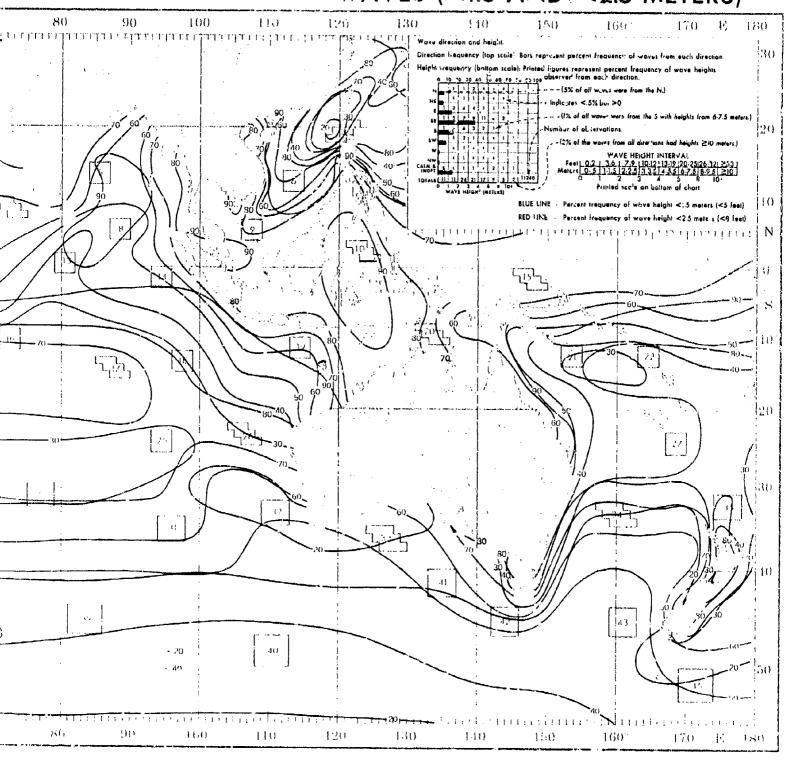
Graphs represent the objective compilation of available data for specified areas without The isopleth analyses (opposite page) are based on all available data subjectively adjusted to the control of th



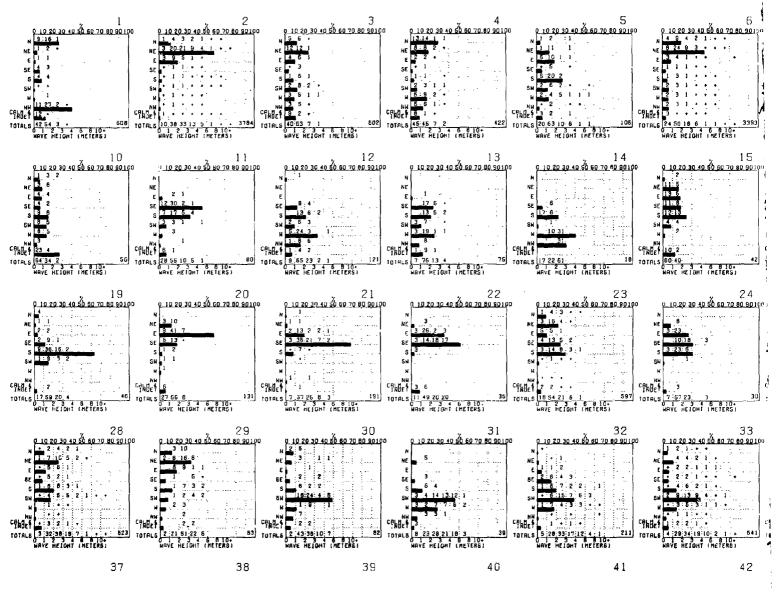
ctive compilation of available data for specified areas without regard to suspected biases, basite page) are based on all available data subjectively adjusted where bias was evident.



WAVES (<1.5 AND <2.5 METERS)



WAVE DIRECTION AND HEIGHT

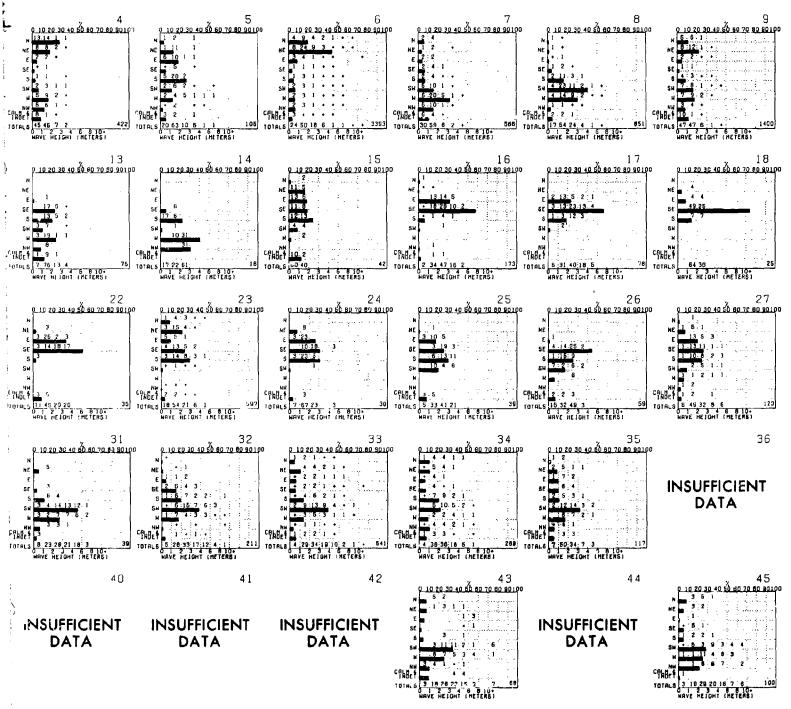


INSUFFICIENT DATA INSUFFICIENT DATA INSUFFICIENT DATA INSUFFICIENT DATA

INSUFFICIENT DATA INSUFFICIENT DATA

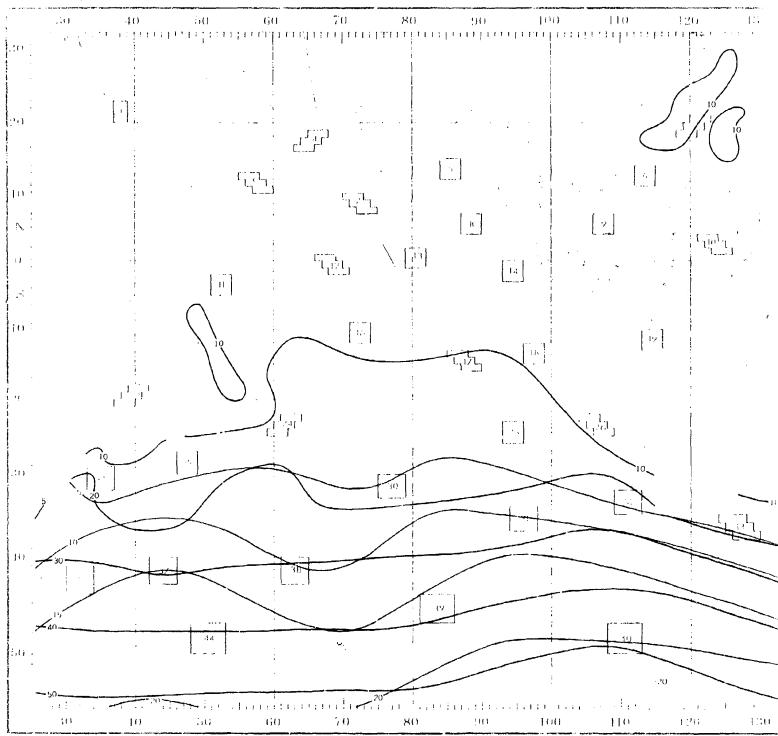
GHT

OCTOBER

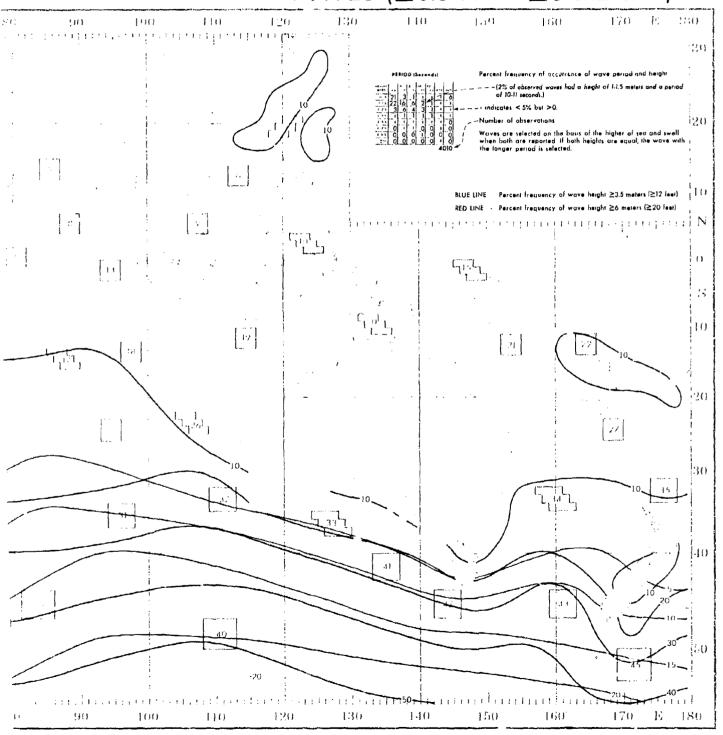


ective compilation of available data for specified areas without regard to suspected biases.

sposite page) are based on all available data subjectively adjusted where bias was evident.



WAVES (≥3.5 AND ≥6 METERS)



WAVE PERIOD AND HEIGHT

PERJOD 1.5FCOND5.1 1418.5 46 7 9 13 13 13 13 15 160 0-5 26 2 + 0 0 0 17 1-1-5 27 14 3 0 0 7 4 2-7.3 1 1 1 - 1 0 7 0 0 0 1-3.5 0 0 0 0 0 0 0 0 0 0 1-10 0 0 0 0 0 0 0 0 0 1-10 0 0 0 0 0 0 0 0 1-10 0 0 0 0 0 0 0 0	PERIOD ISECONDS 1	PERION LSECONDS	PERIOD 1 SI CONDS 1 (1291) 4 5 7 8 11 13 13 13 10 0 7 1 3 3 3 1 1 0 6 11 11 5 23 13 3 2 1 1 2 21 3 2 1 2 0 0 0 11 1 1 1 0 0 11 1 1 0 0 0 11 1 0 0 0 0	PERIOD	PERIOD (SECUNDS) OF 150: 1
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PERIOD (SECONDS) ***(104)** 4	PERIOD (SECONDS) **E10*** 5	PERIOD (SECONDS) **TION** \$\frac{1}{2} \cdot \frac{1}{2} ONDS: NEIGHT	PER-100 (SECONDE) Helder	PERIOD (5E CONDS) ***Close** - 4	
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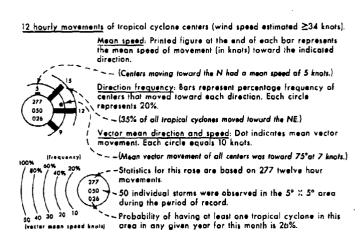
<u>Graphs</u> represent the objective compilation of available data for specified areas without re The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjuste

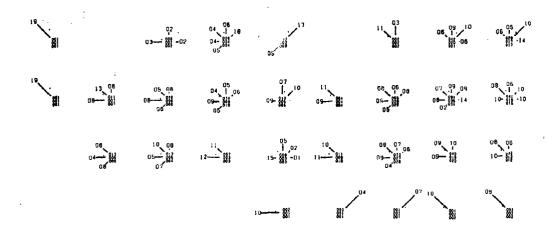
OCTOBER

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PERIOD (SECONDS) 25 4 0 0 1 1 1 1 1 1 1 25 1 0 3 0 0 0 3 0 0 0 0 5 1 3 5 3 0 0 5 1 3 5 3 0 0 5 1 3 5 3 1 0 3 6 3 8 8 5 5 0 7 1 3 5 3 1 0 3 8 3 5 0 9 0 0 0 0 0 10 0 0 0 0 11 0 0 0 0 12 0 0 0 0 39	32 PERIOD (SECONDE) ***PERIOD (SECONDE) **PERI	33 PERIOD (SECONDS) 1	3 4 MEION	35 PENIOD (SECONDS)	INSUFFICIENT DATA
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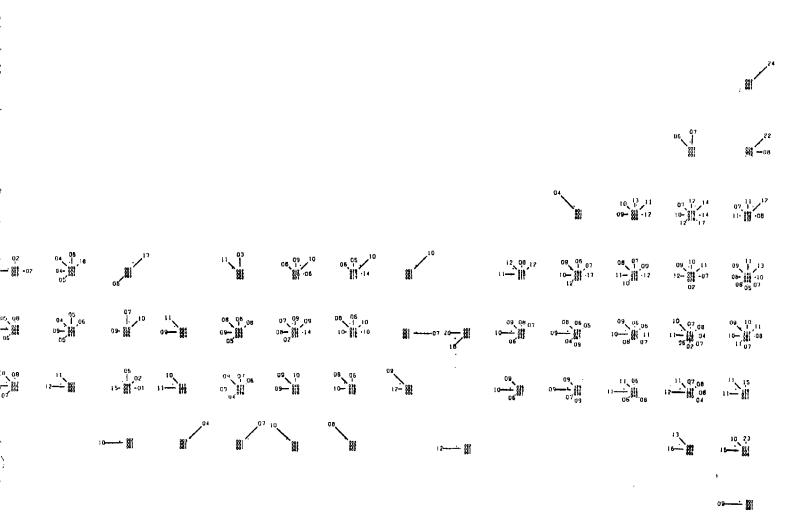
ive compilation of available data for specified areas without regard to suspected biases. site page) are based on all available data subjectively adjusted where bias was evident.

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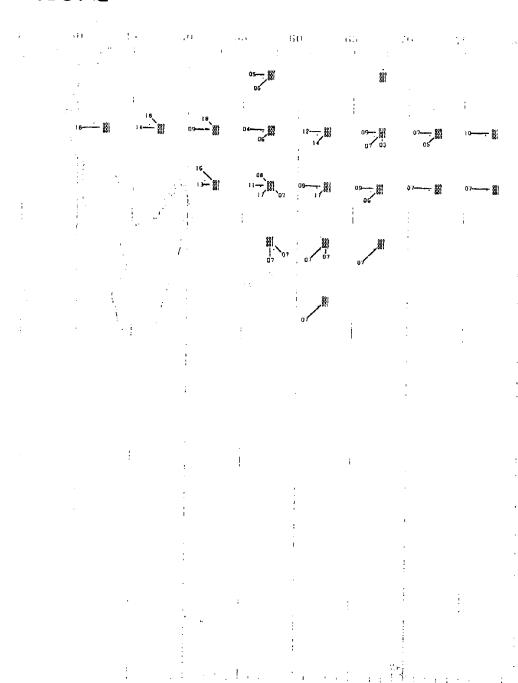




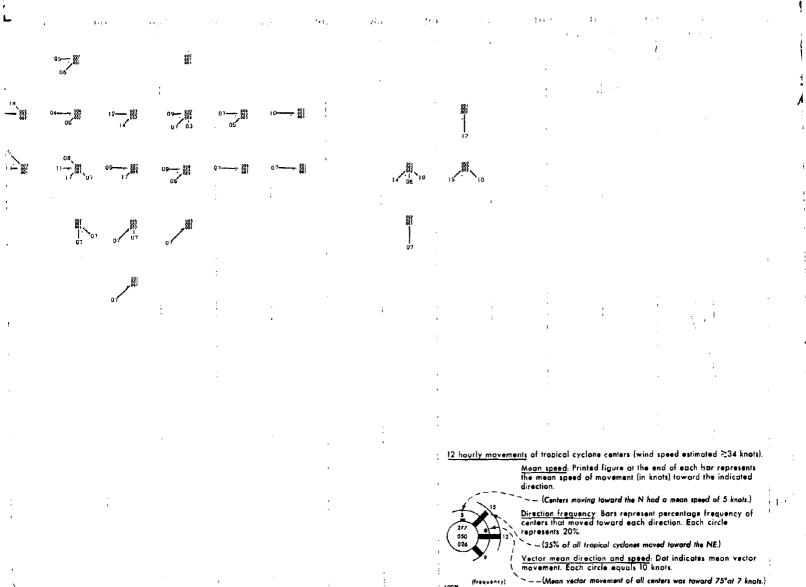
TROPICAL CYCLONE



TROPICAL CYCLONE



OCTOBER



281

-Statistics for this rose are based on 277 twelve hour movements.

-50 individual storms were observed in the 5° X 5° area

Probability of having at least one trapical cyclone in this area in any given year for this month is 26%.

(1.)

during the period of record.

105

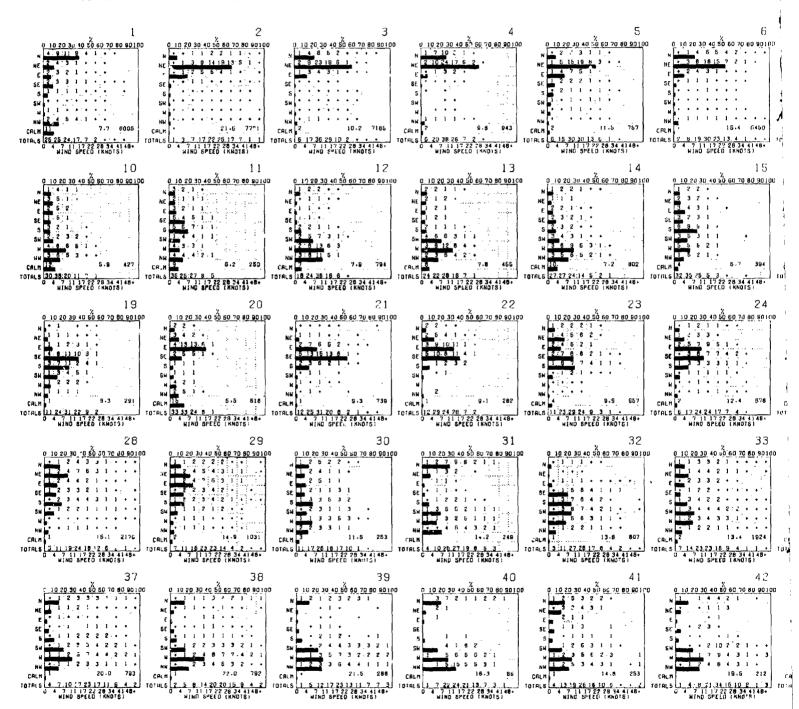
 $i \in \Omega$



SURFACE WINDS



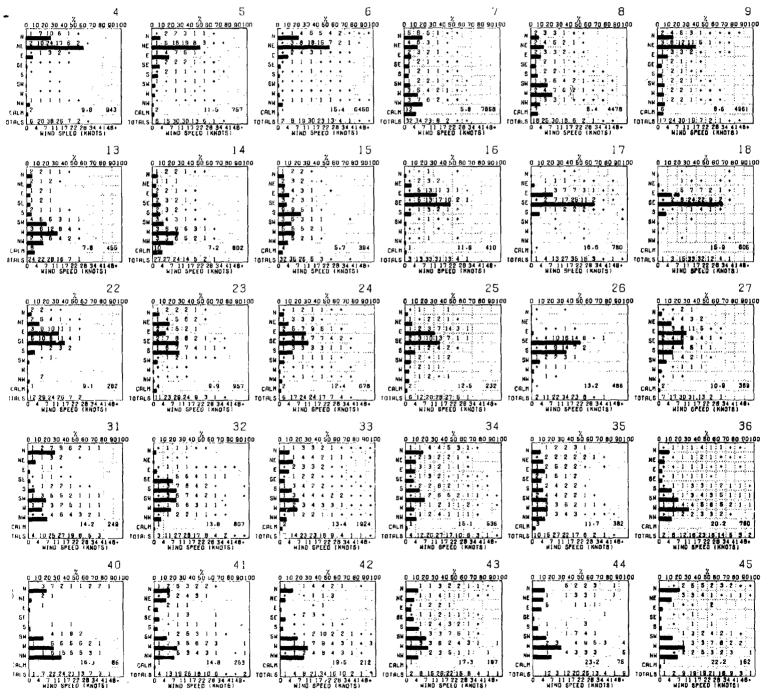
WIND DIRECTION AND SPEED



<u>Graphs</u> represent the objective compilation of available data for specified areas without regar The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjusted w

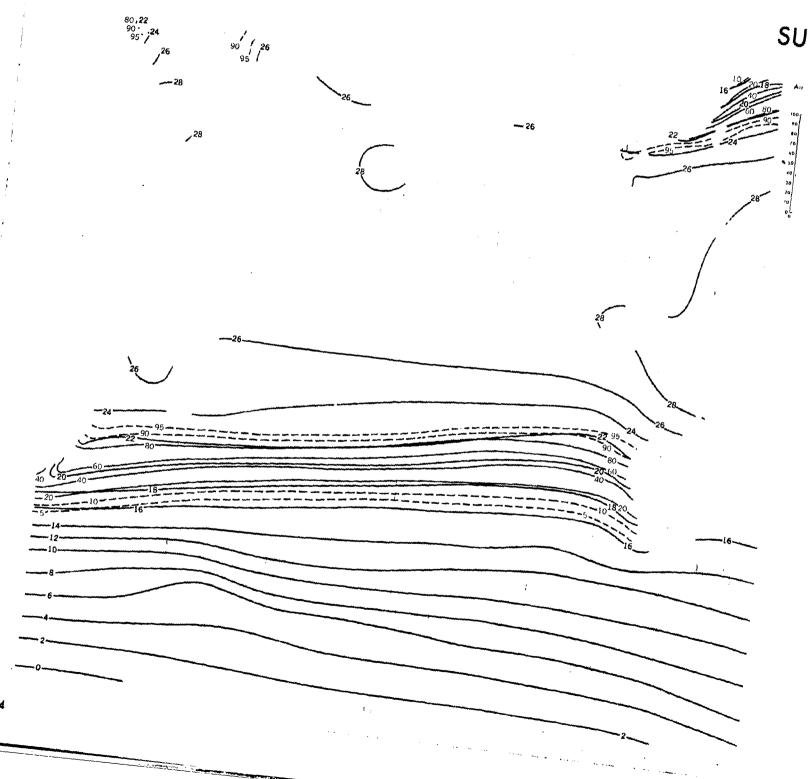
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NOVEMBER



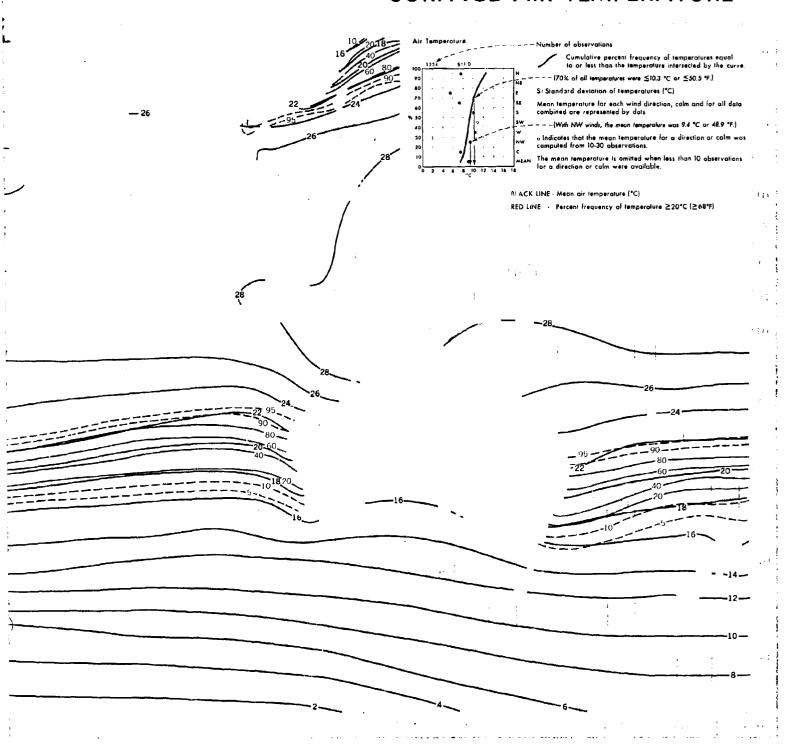
ctive compilation of available data for specified areas without regard to suspected biases.

osite page) are based on all available data subjectively adjusted where bias was evident.

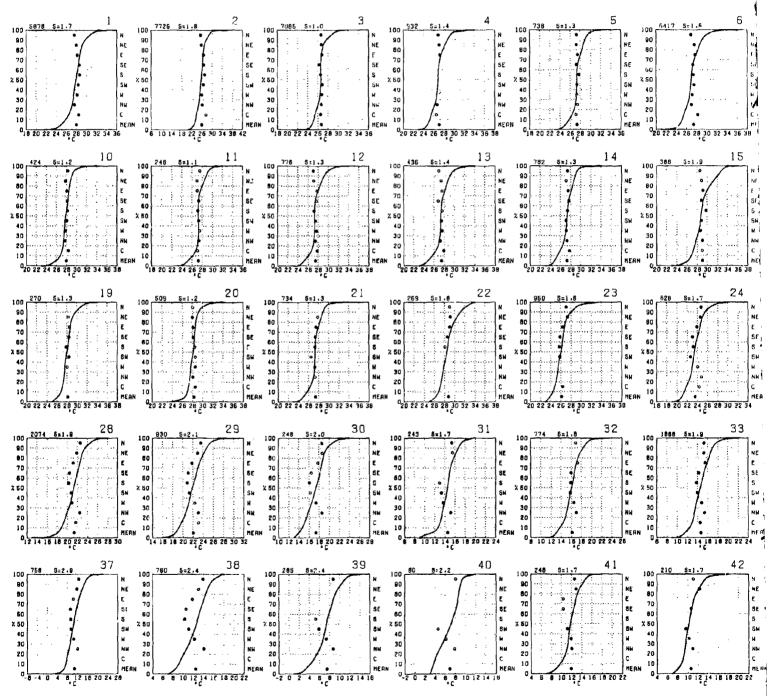


284

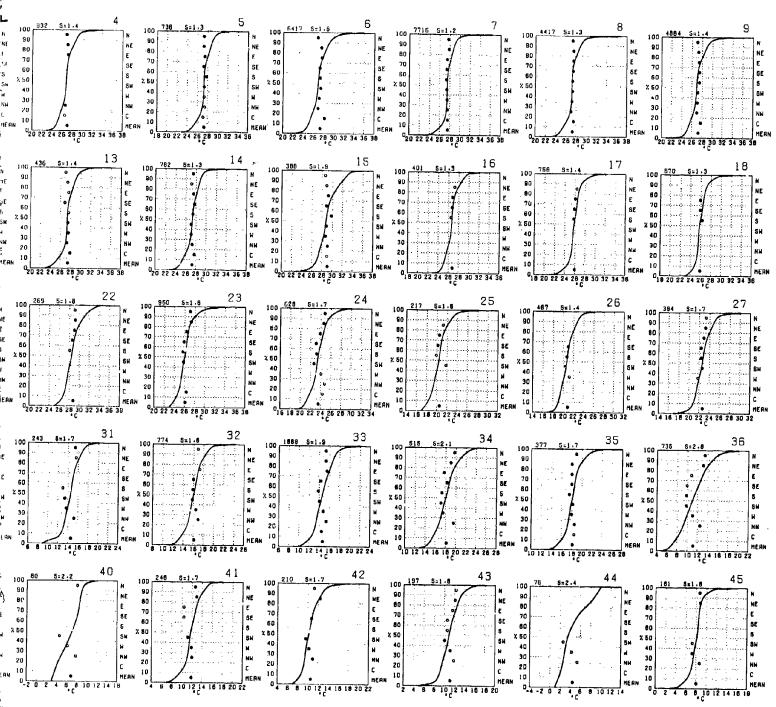
SURFACE AIR TEMPERATURE



SURFACE AIR TEMPERATURE

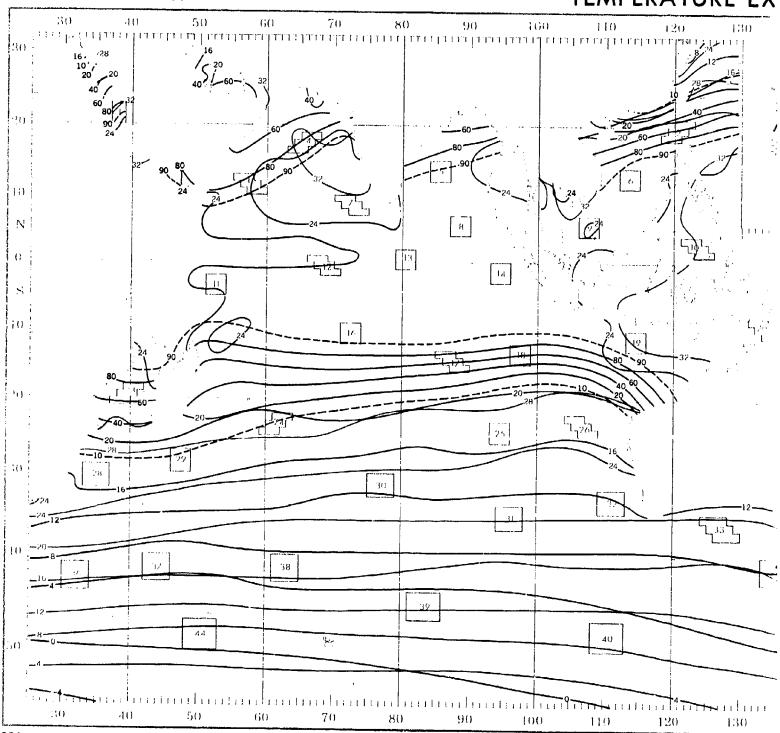


<u>Graphs</u> represent the objective compilation of available data for specified areas without re The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjuste.

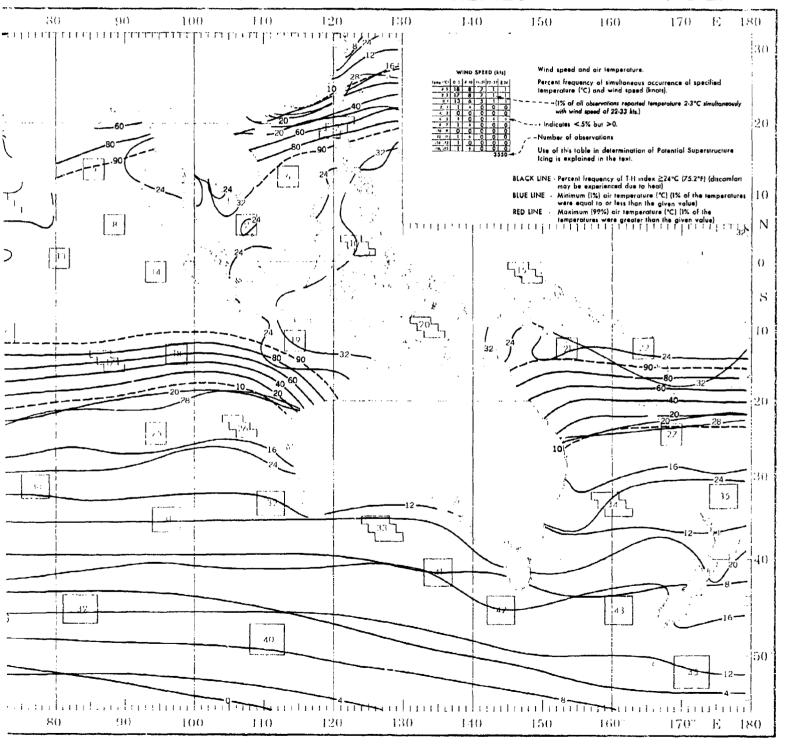


bjective compilation of available data for specified areas without regard to suspected biases. opposite page) are based on all available data subjectively adjusted where bias was evident.

TEMPERATURE EX



TEMPERATURE EXTREMES AND T-H INDEX



WIND SPEED AND AIR TEMPERATURE

WIND SPEED (KTS)	WIND SPEED (KTS) 2	WIND SPEED (KIS) 3	WING SPEED (KTS)	MIND SPEED (KIE) 5	HIND SPEED (KTS)
TEMP (4C) 0-9 4-10 11-21 22-39 = 36	TEHP (*C) 0-3 4-10 11-21 22-33 2 34	16HF (*C) 0-3 4-10 11-21 22-33 4 34	TEMP (*C) 0-3 4-10 11-21 22-33 2 34	TEMP (*C) 0-9 4-10 11-21 22-33 a 34	
90.37 + 0 0 0 0 31.35 + + 0 0	34.35 0 + + + 0 37.33 + + + 0	32.33 0 + + 0 0 30.31 + 1 + 0 0	32.33 + 1 + 0 0 30.31 + 2 2 + 0	32.33 0 0 + 0 0 30.31 1 2 1 + 0	36.37
92.33 1 1 1 + 0 30.31 5 7 2 + 0	20.31 + 1 1 + +	28.29 1 9 7 + 0 28.27 5 40 27 1 +	28.29 1 13 13 1 C 28.27 4 36 16 1 O	26.29 2 19 18 3 +	32.33 + 1 + 0 30.31 + 2 4 + 0
28.29 14 25 9 + + 28.27 5 14 9 1 +	28.27 + 5 19 18 3 24.25 + 2 10 15 3	24.25 1 4 3 + + 22.23 0 + + 0 0	24.25 1 6 2 0 0 22.23 0 0 0 0	24.25	28:29 1 11 20 4 + 28:27 1 12 23 9 1
24.25 + 2 2 1 +	22.23 + + 2 4 1	20,21 0 0 + 0 0 10,19 0 0 0 0 0	20.21 0 0 0 0 0 18.18 0 0 0 0 0	20.21 0 0 0 0 0 10.19 0 0 0 0 0	24.26 + 1 4 2 + 27.23 0 + + + + +
20.21 + + + 0 0	18.19 + O O + + 16.17 O O O O O	18.17 0 0 0 0 0 14.18 0 0 0 0 0	18.17 0 0 0 0 0 14.18 0 0 0 0 0	18.17 0 0 0 0 0 14.15 0 0 0 0 0	20:21 0 0 0 0 0 0 18:18 0 0 0 0 0 0
16.17 0 0 0 0 0	14.15 0 0 0 0 0	12.13 0 0 0 0 0	12.13 0 0 0 0 0	12.13 0 0 0 0 0	16.17 0 0 0 0 0 0 5423
NIND SPEED (KTS)	HIND SPEED (KTS) 11	WIND SPEED (KIS) 12	WIND SPEED (KTS) 13	HIND SPEED (KTS) 14	HIND SPEED (KTS) 15
7EHP (*C1 0-5 4-10 11-21 22-33 2 34	TEMP (*C) 0-9 4-10 11-21 22-39 2 34	TEHP (*C) 0-3 4-10 11-21 22-33 2 34	TEMP (MC) 0-3 4-10 11-21 22-33 2 34	TEHP (*C) 0-3 4-10 11-21 22-73 2 34	TENP (901 0-3 4-10 11-21 22-33 2 34 TE
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20.20 20 36 7 0 0 20.27 6 14 4 1 0	26.27 19 27 9 0 0 24.26 + 2 1 0 0	20.20 8 24 6 + 0	28.29 11 19 11 + 0 28.27 11 22 10 1 0	20.29 1 18 9 1 0 26.27 11 27 8 2 0	30.31 6 10 1 0 0
24.26 + 1 1 0 0 22.23 0 0 0 0 0 0	22.23 0 0 0 0 0	24.25 1 2 1 0 0 22.23 0 0 0 0 0	24.25	24.25 2 4 1 0 U 22.23 0 0 + + 0	28.27 5 8 3 0 D 24.25 1 1 1 0 0
20.21 0 0 0 0	10.19 0 0 0 0	20.21 0 0 0 0	20.21 0 0 0 0	20-21 0 0 0 0 0	22.23 0 0 0 0 0
10.17 0 0 0 0 0	14:15 0 0 0 0	16.17 0 0 0 0 0	10.17 0 0 0 0 0	16.17 0 0 0 0 0	19.19 0 0 0 0 0
14.15 0 0 0 0 0 0 12.15 0 0 0 0 0	10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0	14.15 0 0 0 0 0 0 12.13 0 0 0 0 0	14.15 0 0 0 0 0 0 12.13 0 0 0 0 0	14.15 0 0 0 0 0 0 12.13 0 0 0 0 0	18-17 0 0 0 0 0 14-18 0 0 0 0 0
427 1 Q	280 20	21	99	784 23	392
HIND SPEED (KTS) 19	HIND SPEED (KTS) 20 TENP (*C) 0-3 4-18 11-21 22-33 24	HIND SPEED (KTS) 21 TEHP (%) 0-3 4-10 11-21/22-99 2 34	HIND SPEED (KTS) 22	HIND SPEED (KTS) 23	HIND SPEED (KTS) 24
38.33 + 2 0 0 0	32,33 + 1 0 0 D	32.33 + 1 + 0 0	34.36 + + 0 0 0	34,35 0 + 0 0 0	30.31 0 + 0 0 0
90.31 2 7 3 + 0 20.20 4 32 18 1 0	30.31 5 6 1 0 0 20.25 24 36 5 0 0	30.91 + 2 2 + 0 28.29 5 24 9 1 0	32,39 1 4 1 0 0 30,31 4 12 4 + 0	32,33 + 1 + 0 0	28.27 2 7 2 1 0
28.27 8 14 8 1 0 84.25 0 0 + + 0	26.27 4 13 3 0 0 24.28 0 1 0 0 0	26.27 7 28 17 1 +	20.20 6 27 14 1 0	28.27 6 26 15 1 0	24.28 2 17 17 4 0 22.23 1 15 19 5 +
20.21 0 0 0 0 0	26.23 0 + 0 0 0	22.23 0 0 + 0 0 20.21 0 0 0 0 0	24.25 0 1 1 0 0 22.23 0 0 0 0 0	24.25 2 15 11 2 +	\$0.21 + 2 3 2 0 10.18 0 0 0 + 0
	25.23 0 + 0 0 0 26.21 0 0 0 0 0 15.15 0 0 0 0 0	22.23 0 0 + 0 0 20.21 0 0 0 0 0 10.13 0 0 0 0 0	24.25 0 1 1 0 0	24.25 2 15 11 2 + 22.23 + 1 + 0 20.21 0 0 0 0 0	20.21
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#IND SPEED (KTS)	### 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	22.23 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	E4.28 0 1 1 0 0 0 20.22 0 0 0 0 0 0 0 0 0 0 0 0 0 0	24.28 2 15 11 2 22.23 + 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	F0.F1
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10.21 0 0 0 0 0 0 0 1 10.18 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	### 10 - 1 - 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	22.23 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	### 140 0 1 1 0 0 0 1 1 1 0 0 0 1 1 1 0 0 0 1 1 1 0 0 0 1 1 1 1 0 0 0 1	24.78 2 15 11 2 + 27.23 + 1 + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	F0.E1
10.21 0 0 0 0 0 0 0 1 10.18 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	### 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	22.73 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	### 140	24.28 2 15 11 2 27.23 1 1 2 27.23 1 1 2 27.21 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	F0.F1
TEMP (*C) 0-3 0-10 11-51 12-39 2-34 14 12-51 12-13 0-10 11-51 12-39 2-34 14 15-10 11-51 12-39 2-34 14 15-10 11-51 12-39 2-34 14 15-10 11-51 12-39 2-34 14 15-10 11-51 12-39 2-34 14 15-10 11-51 12-39 2-34 14 15-10 11-51 11-5	### 100 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	22.23 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	### 180 SPEED (KTS) 16:19 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	24.28 2 15 11 2 22.23 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	FO.F1
TEMP (*C) 0-3 (-10) 1-51 (*T5-3) 1-34 (*T5-1) 10-1 (*T5-1	### 15 10 10 10 10 10 10 10	22.23 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	E4.25	24.28 2 15 11 2 2 2 22.23 4 1 1 1 1 2 3 2 2 2 1 1 1 1 2 3 2 3 2 2 2 2	FO.F1
TEMP (PC) 0-3 0-10 11-21/22-33 2-34 22-23 0 + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	REAR O O O O REAR O O O O REAR O O O O O O REAR O O O O O O O REAR O O O O O O REAR O O O O O O REAR O O O O O O O REAR O O O O O O O REAR O O O O O O O REAR O O O O O O O REAR O O O O O O O REAR O O O O O O O REAR O O O O O O O O REAR O O O O O O O O REAR O O O O O O O O REAR O O O O O O O O	22.23 0 0 0 0 0 0 0 0 0 0 10.19 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	### 100 1 1 0 0 1 1 0 0 1 1	24.28 2 15 11 2 + 27.23 + 1 + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	FORT
10.21 0 0 0 0 0 0 1 10.12 0 0 0 0 10.13 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	### 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	22.23 0 0 0 0 0 0 0 0 0 0 10.11 0 10.13 0 0 0 0 0 0 0 0 0 12.13 0 0 0 0 0 0 0 0 0 12.13 0 0 0 0 10.12 12.23 0 0 10.13 10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	### 100 1 1 0 0 1 1 0 0 1 1	24.28 2 15 11 2 27.23 1 1 0 0 0 0 0 0 0 0 0 0 0 0	FO.F1
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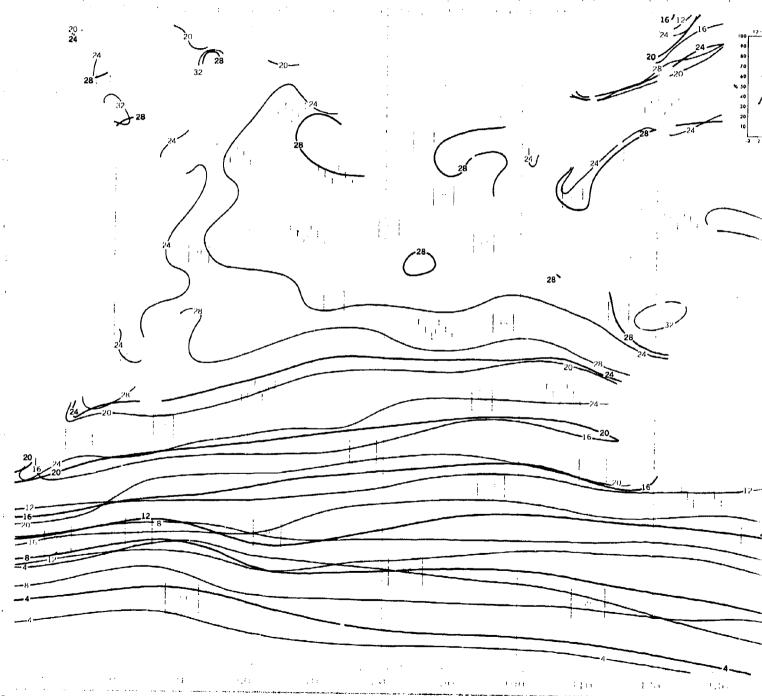
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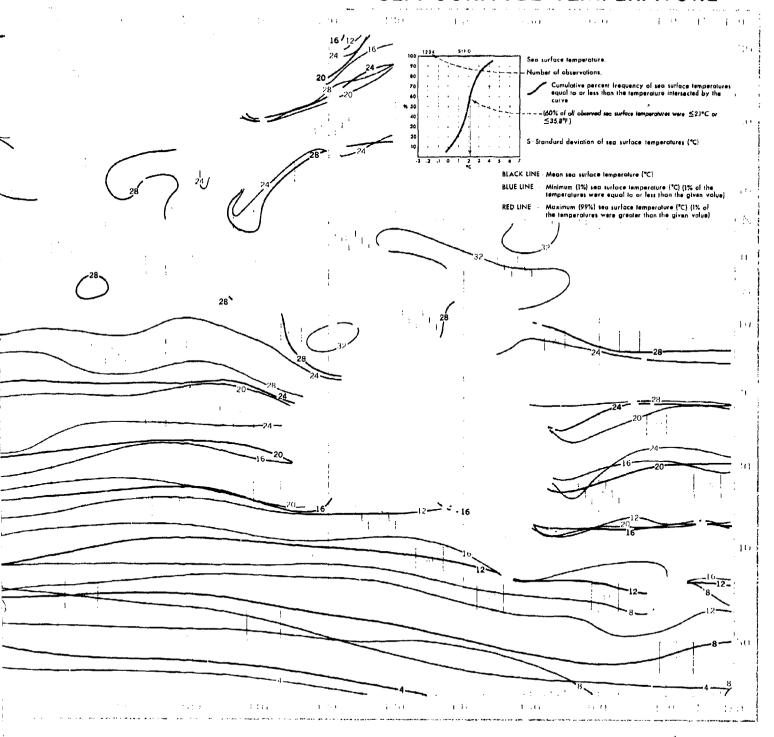
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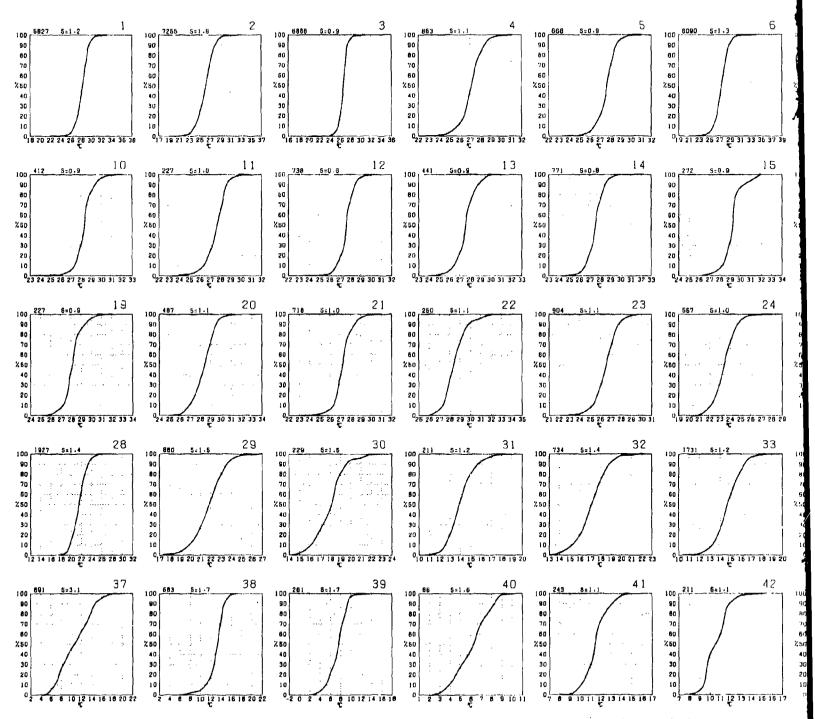
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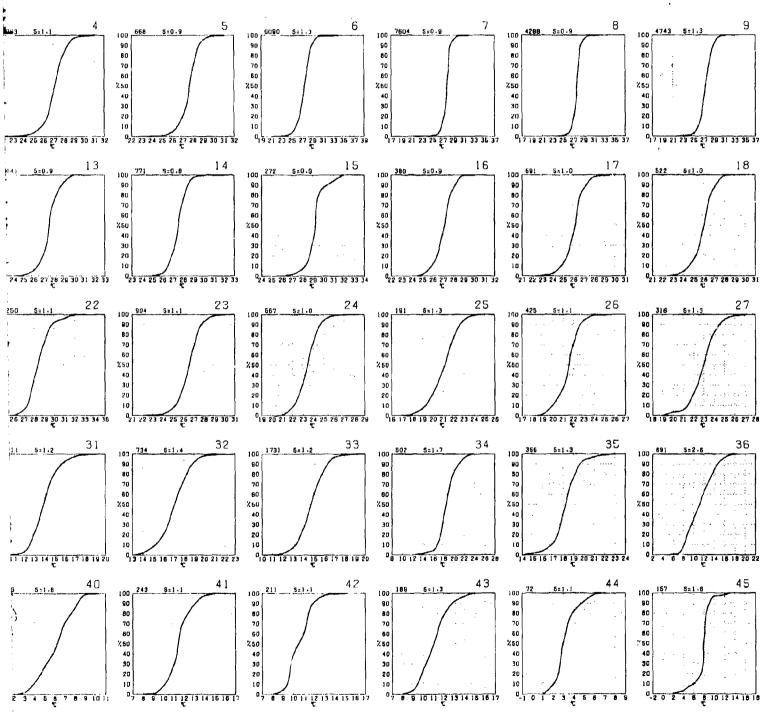
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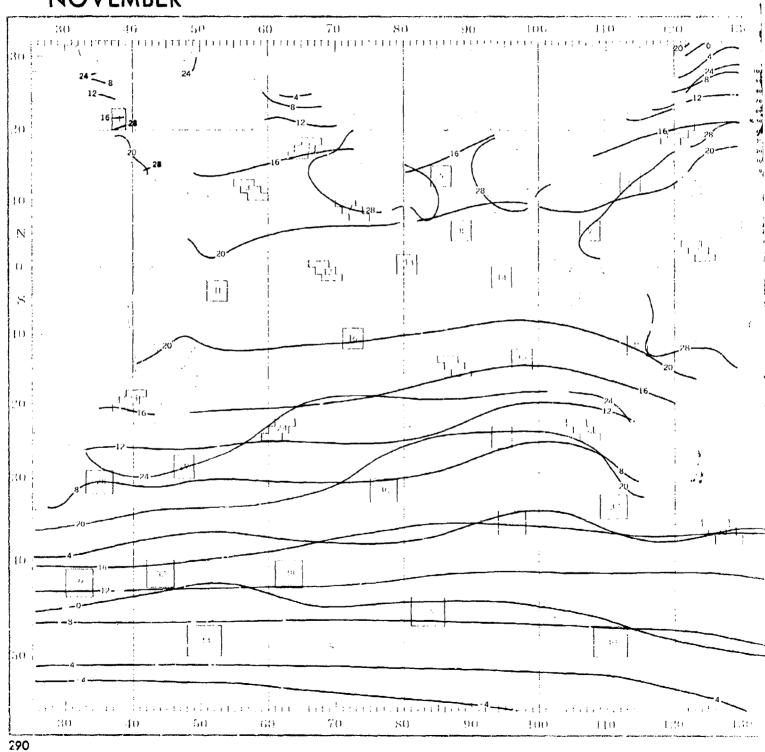
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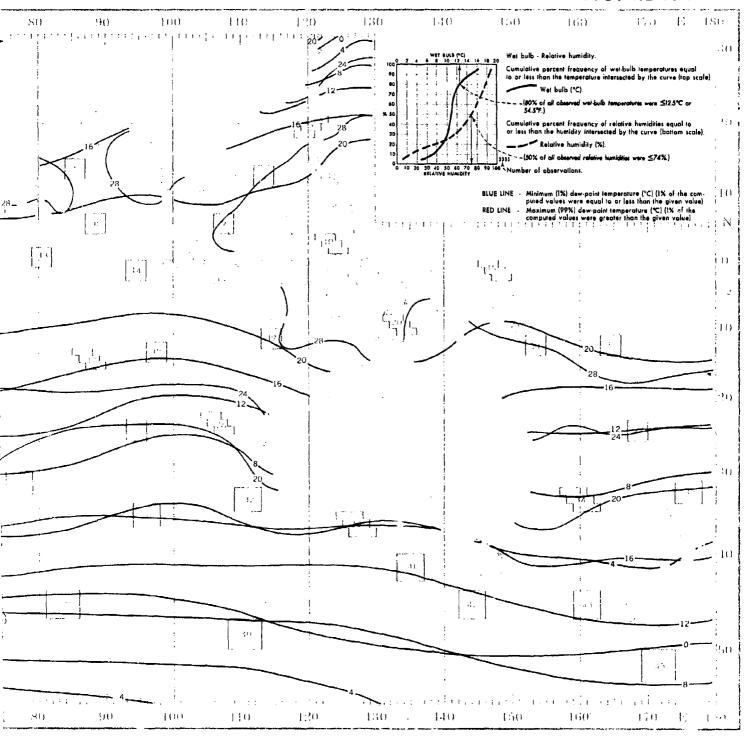
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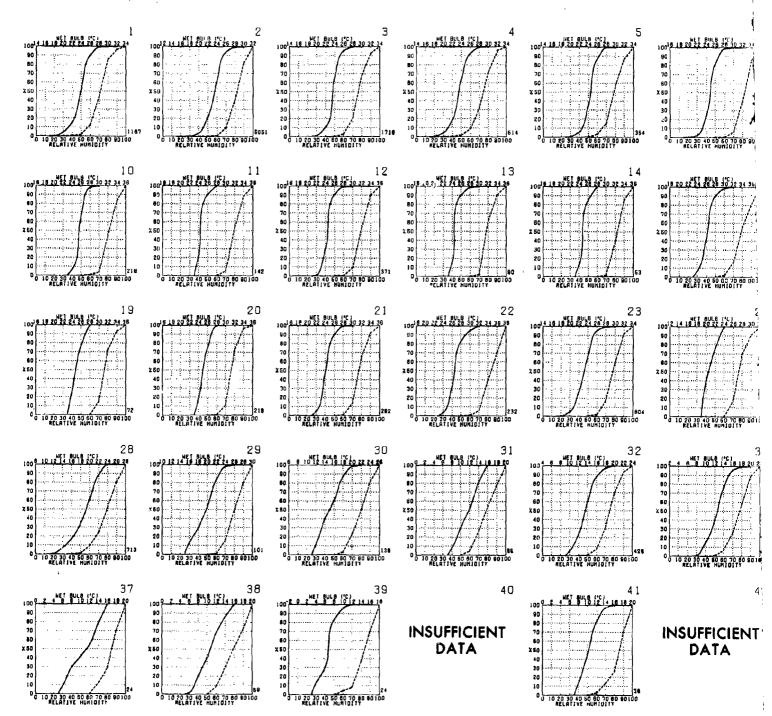
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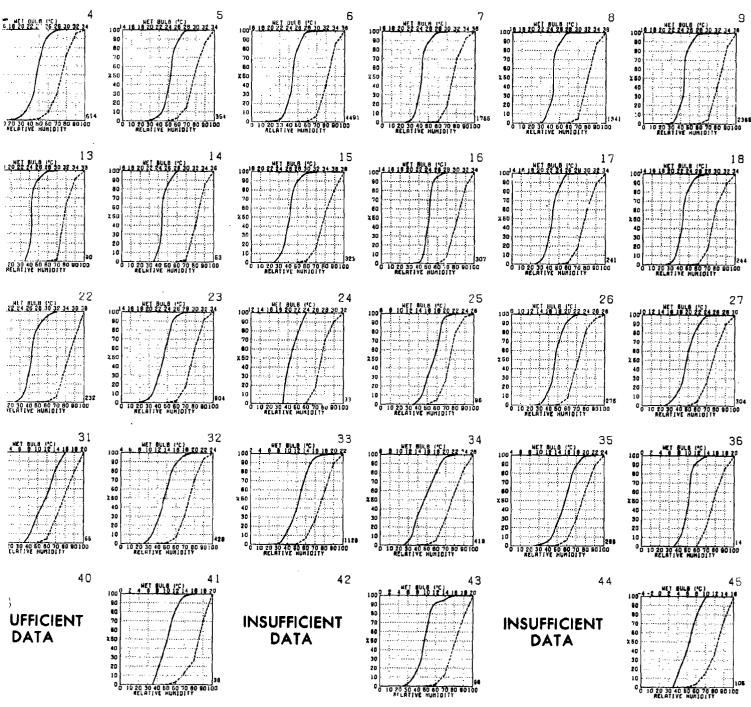
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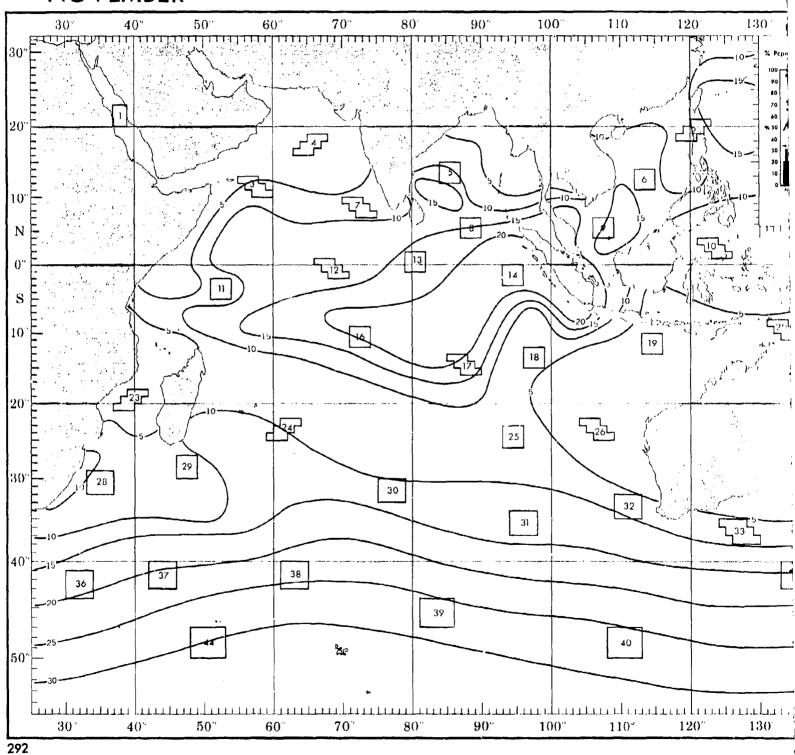
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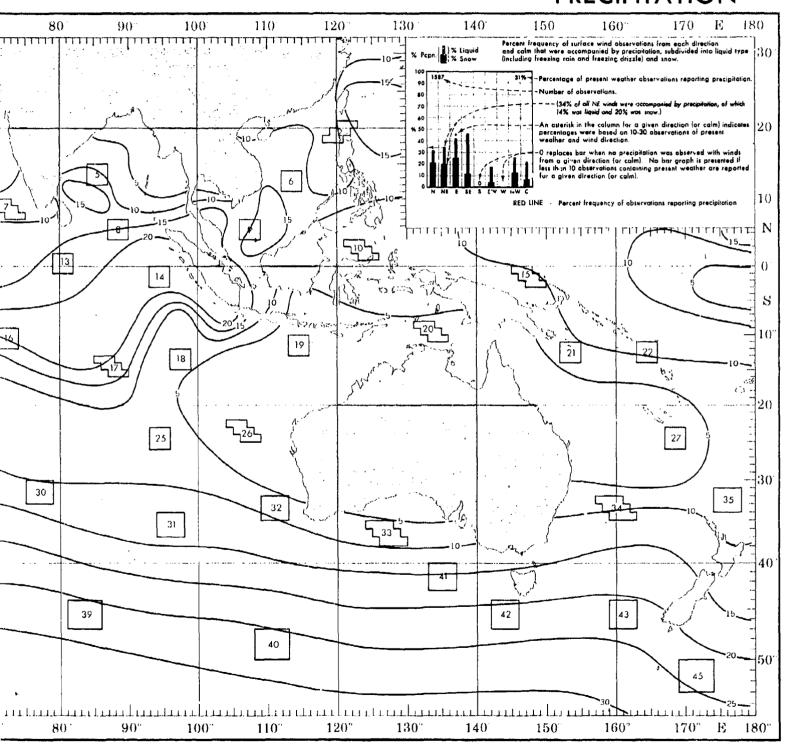


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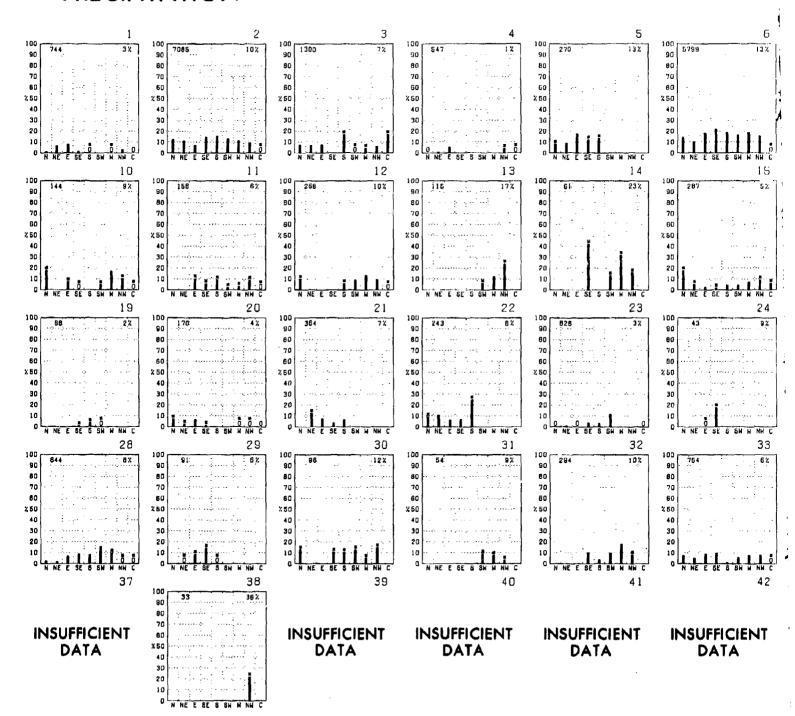
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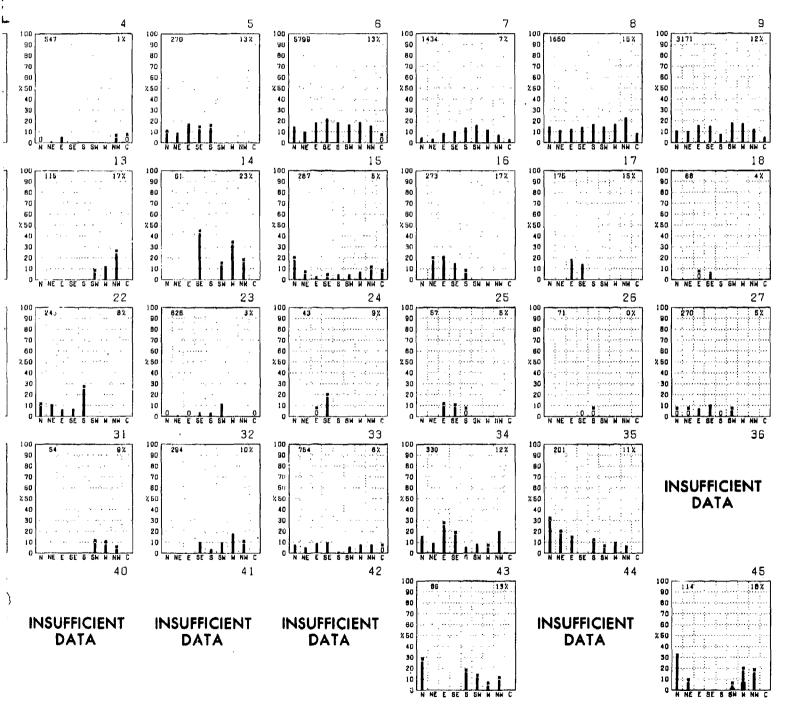
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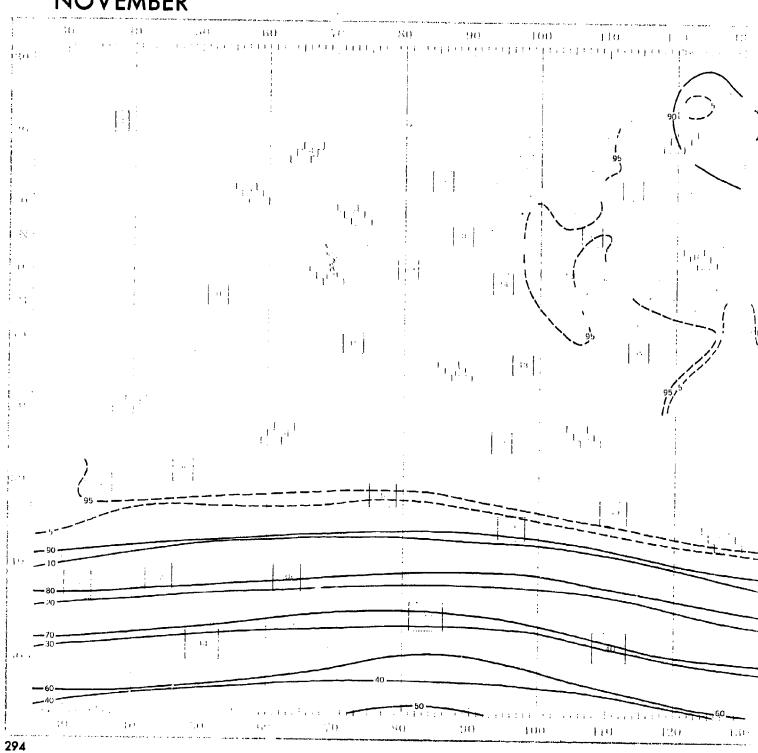


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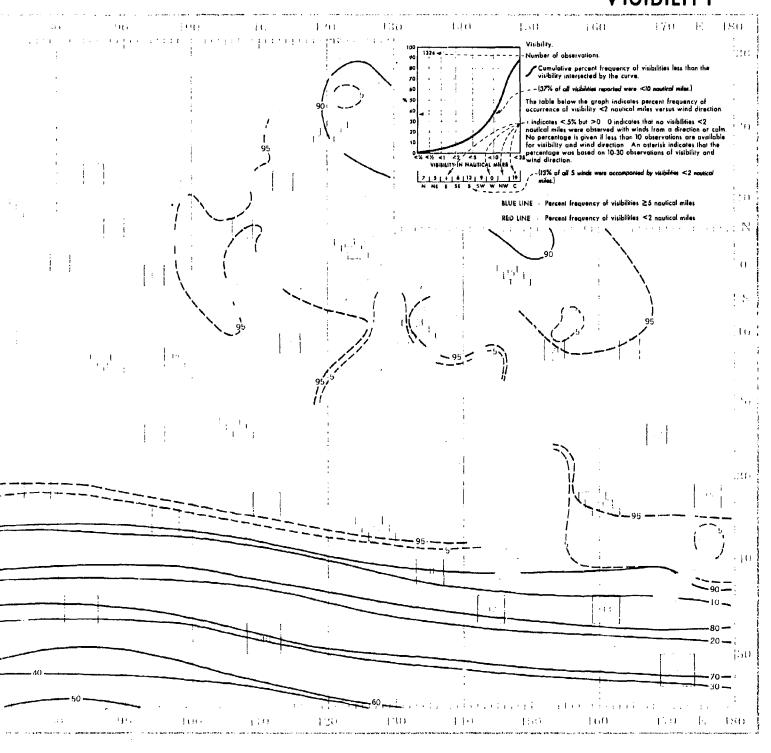


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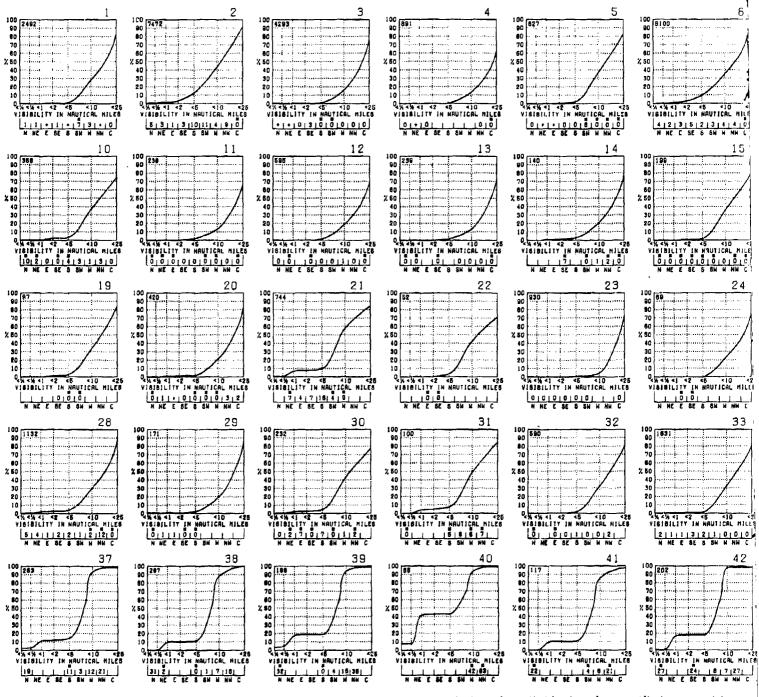
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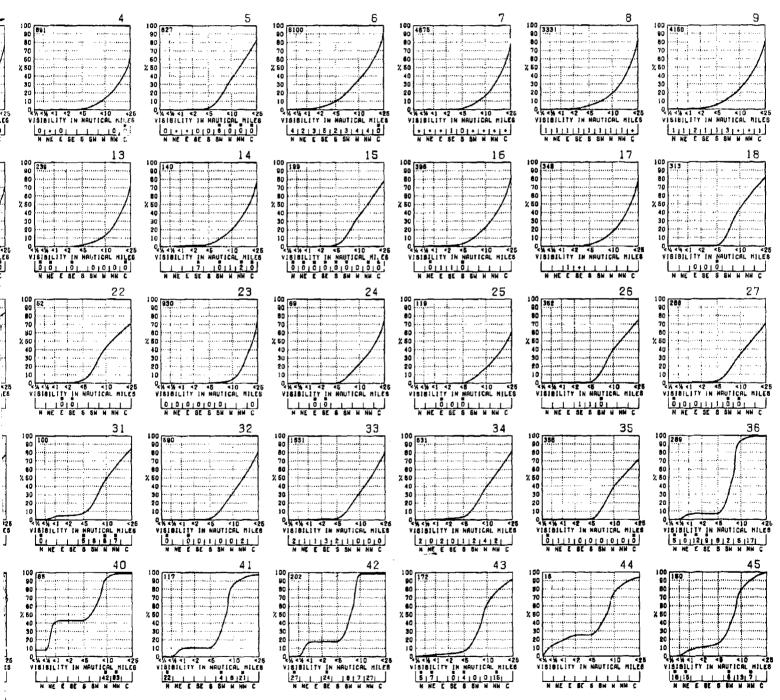
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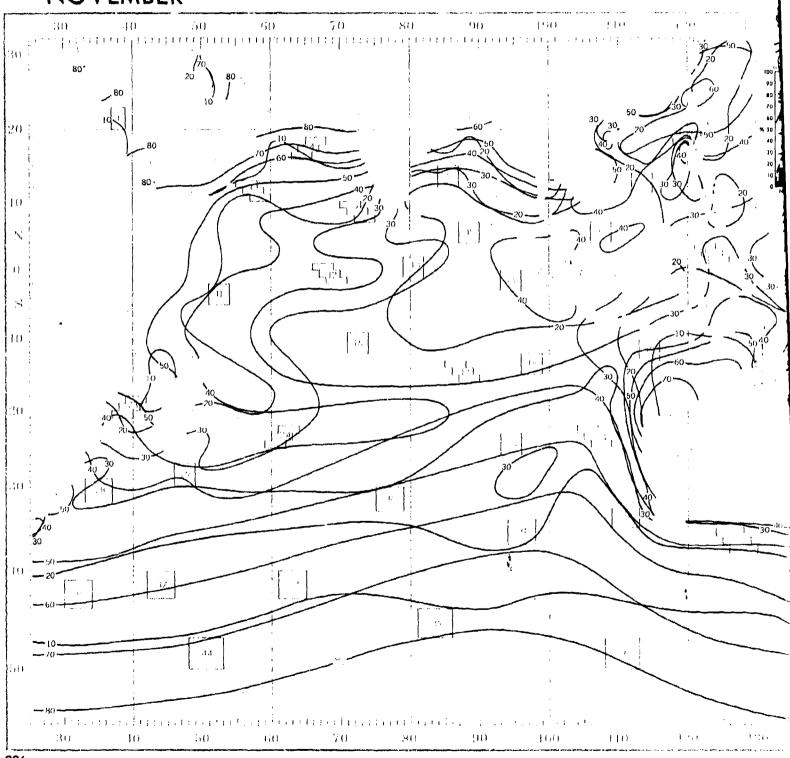
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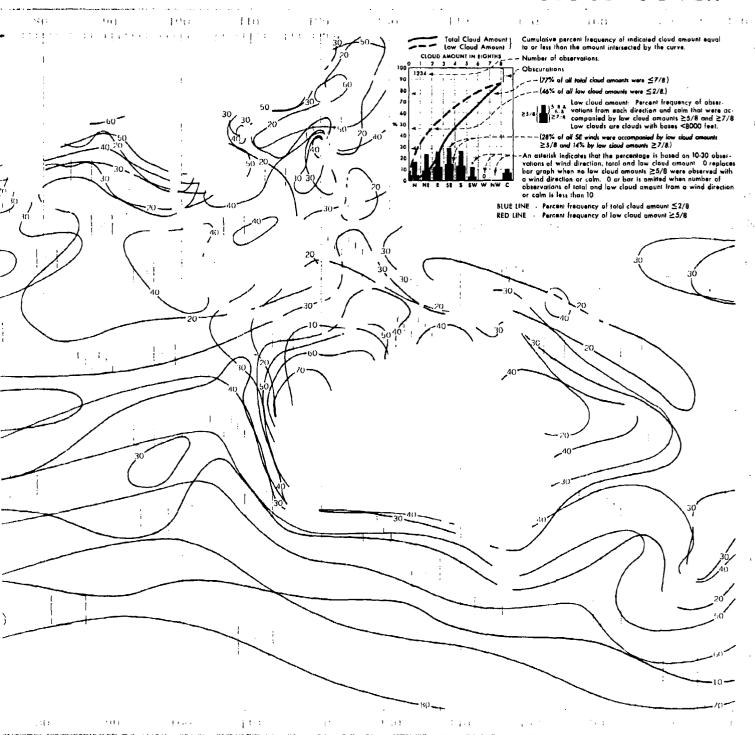
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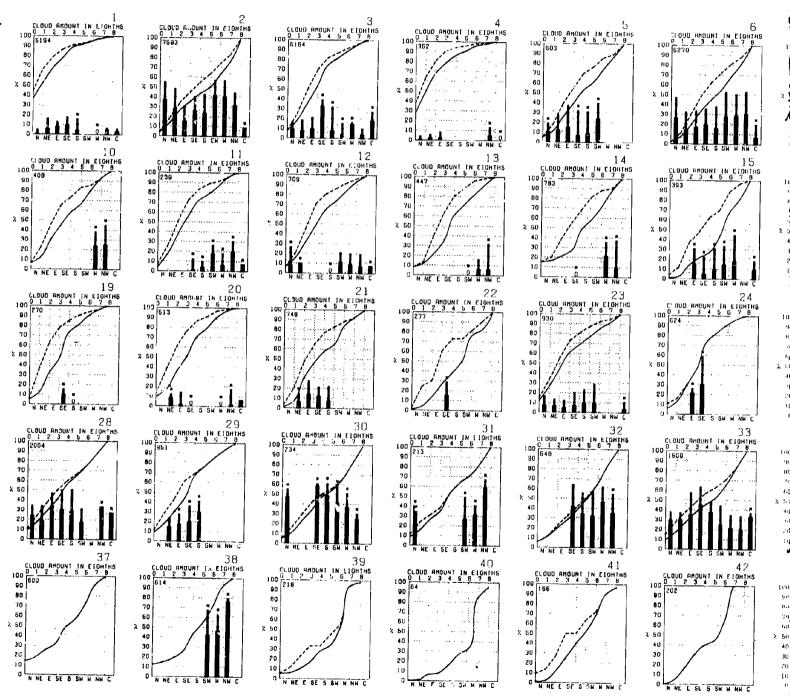
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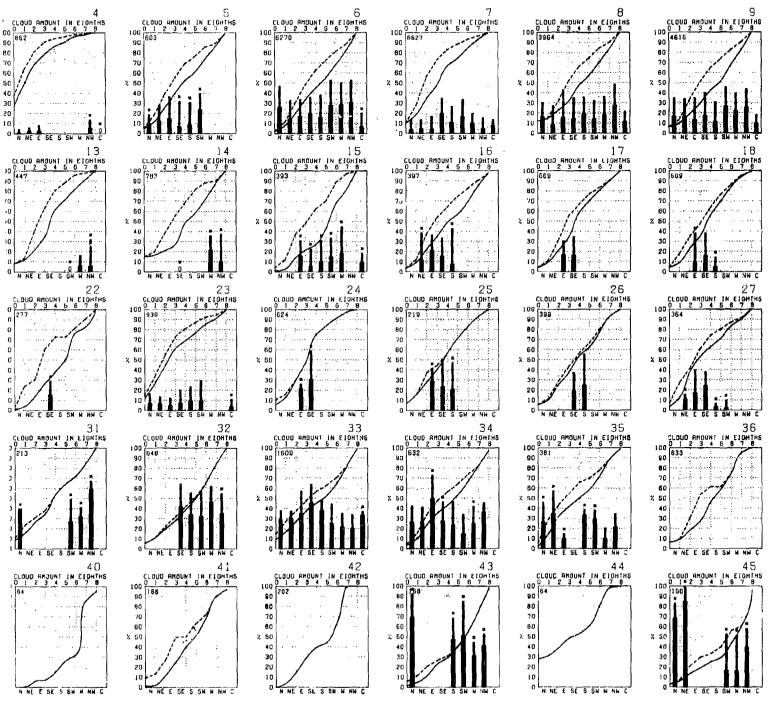
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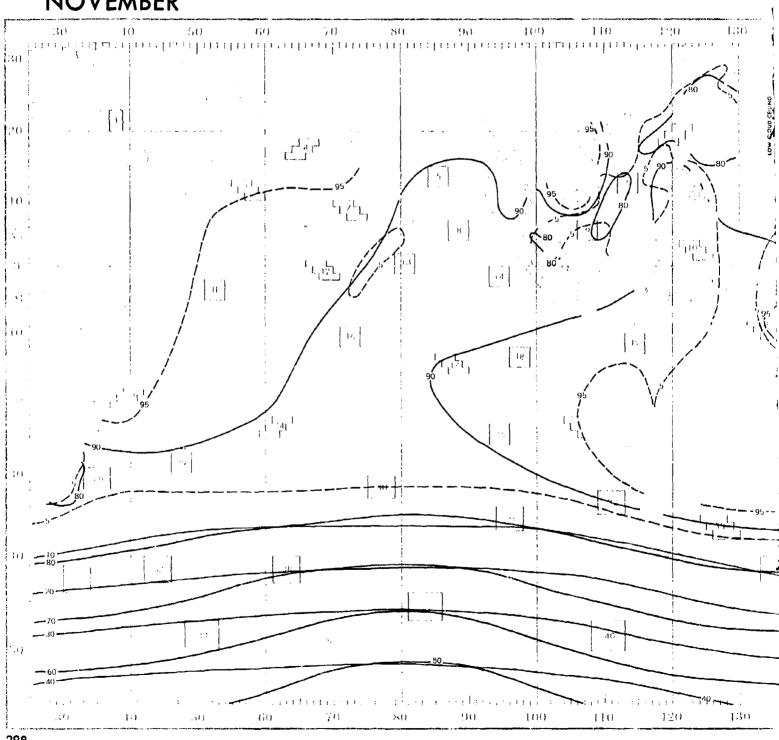
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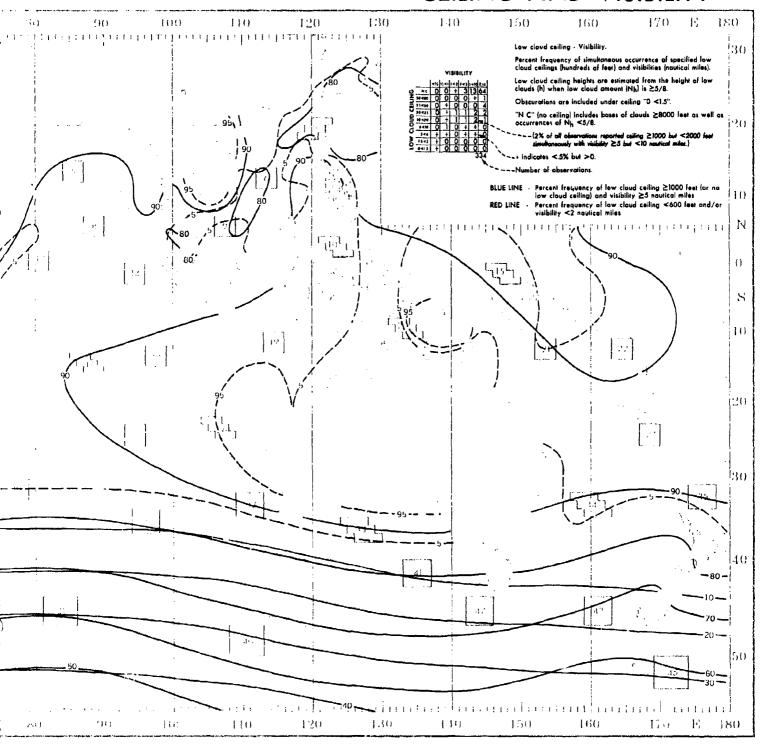
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CEILING AND VISIBILITY

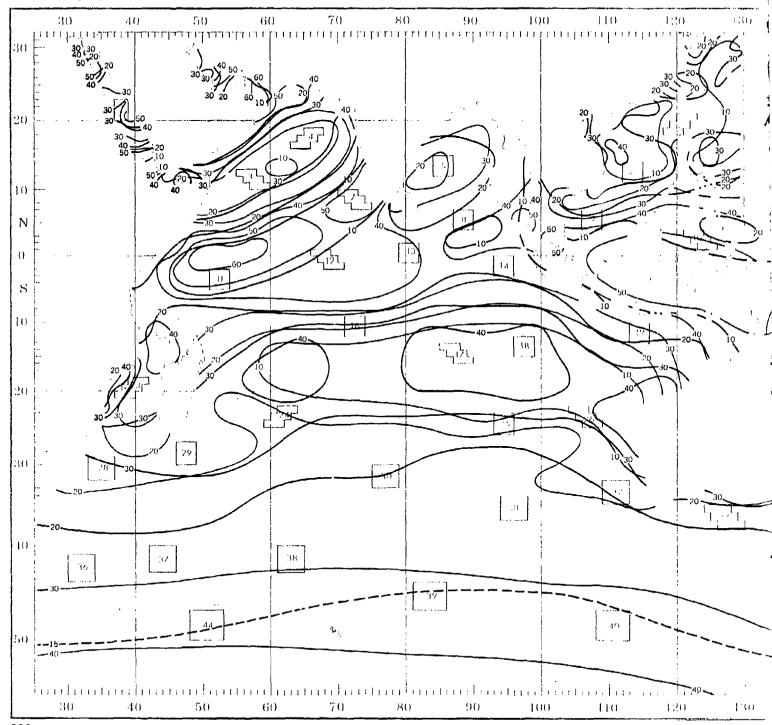
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VIBIBILITY 1 9 -1/2 fA-11 1-2 f-15 3-10-110	VISIBILITY 20 -1/4 [A-1] -1/2 1-1	VISIBILITY 21 **/A [Art]] 14 [248 [410] 10 60 40 0 0 0 0 0 0 80 840 0 0 0 0 + 1 90 1040 0 0 0 0 + 1 90 1040 0 0 0 0 + 1 90 1040 0 0 0 0 + 1 90 1040 0 0 0 0 0 0 10 40 0 0 + 1 1 1 5 90 1040 0 0 + 1 1 1 5 90 1040 0 0 0 0 0 0 1041 0 0 0 0 0 0 0 1041 0 0 0 0 0 0 0 256	VIBIBILITY 22 *** *** *** *** *** *** ***	VISIBILITY 23	VISIBILITY **A FACT 147 FACT 5-10 8C 0 0 0 0 0 5 60-60 0 0 0 0 0 0 38-80 0 0 0 0 0 0 0 38-80 0 0 0 0 0 0 0 38-80 0 0 0 0 0 0 0 60 0 0 0 0 0 0 0 0 7 0 0 0 0 0 0 0 0 0 8 0 0 0 0 0 0 0 0 0 8 0 0 0 0 0 0 0 0 0 8 0 0 0 0 0 0 0 0 0 8 0 0 0 0 0 0 0 0 0 0 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
VISIBILITY	VISIBILITY 29	VISIBILITY 4/4 8/41/14 F44 8-10/10 0 10 0 0 0 1 2 50 50-90 0 0 0 0 0 0 3 35-90 0 0 0 0 0 0 0 3 60-90 0 0 0 0 0 0 1 9 60-90 0 0 0 0 0 1 9 60-90 0 0 0 0 1 9 60-90 0 0 0 0 1 9 60-90 0 0 0 0 1 9 60-90 0 0 0 0 1 9 60-90 0 0 0 0 1 0 0 60-90 0 0 0 0 1 0 0 60-90 0 0 0 0 1 0 0 60-90 0 0 0 0 0 1 0 60-90 0 0 0 0 0 0 0 0 60-90 0 0 0 0 0 0 0 0 60-90 0 0 0 0 0 0 0 0 60-90 0 0 0 0 0 0 0 0 0 60-90 0 0 0 0 0 0 0 0 0 0 60-90 0 0 0 0 0 0 0 0 0 0 0 60-90 0 0 0 0 0 0 0 0 0 0 0 60-90 0 0 0 0 0 0 0 0 0 0 0 0 60-90 0 0 0 0 0 0 0 0 0 0 0 0 0 60-90 0 0 0 0 0 0 0 0 0 0 0 0 0 0 60-90 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY 41/4 [7/41] [48] [44] [410] [10] MC	VISIBILITY 32 ***********************************	VISIBILITY -1/4 V/4
VISIBILITY 37	VISIBILITY -c1/2 [FAct] 1-61 [C16 B-10] 110 -MC 0 0 0 0 0 4 23	INSUFFICIENT DATA	INSUFFICIENT DATA	VIBIBILITY 4 1 c1/n 7/c4 c2 8/c4 8/c1 0/c1 nc 0 0 0 0 0 6 nc 0 0 0 0 0 0 8/c40 0 0 0 0 0 10/c40 0 0 0 0 10/c40 0 0 0 0 10/c40 0 0 0 0 10/c40 0 0 0 0 10/c40 0 0 0 10/c40 0 0 0 10/c40 0 0 0 10/c40 0 0 0 10/c40 0 0 0 10/c40 0 0 0 10/c40 0 0 0 10/c40 0 0 0 10/c40 0 0 0 10/c40 0 0 0 10/c40 0 0 0 10/c40 0 0 0 10/c40 0 0 0 10/c40 0 0 0 10/c40 0 0 0 10/c40 0 0 10/c40 0 0 0 10/c40 0 0 0 10/c40 0 0 10/c40 0 0 10/c40 0 0 0 10/c40 0 0 10/c40 0 0 10/c40 0 0 10/c40 0 0 10/c40 0 0 10/c40 0 0 10/c40 0 0 10/c40 0 0 10/c40 0 0 10/c40 0 0 10/c40 0 0 10/c40 0 0 10/c40 0 0 10/c40 0 0 10/c40 0 0 10/c40 0 0 10/c40 0 0	INSUFFICIENT DATA

<u>Graphs</u> represent the objective compilation of available data for specified areas without The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjus

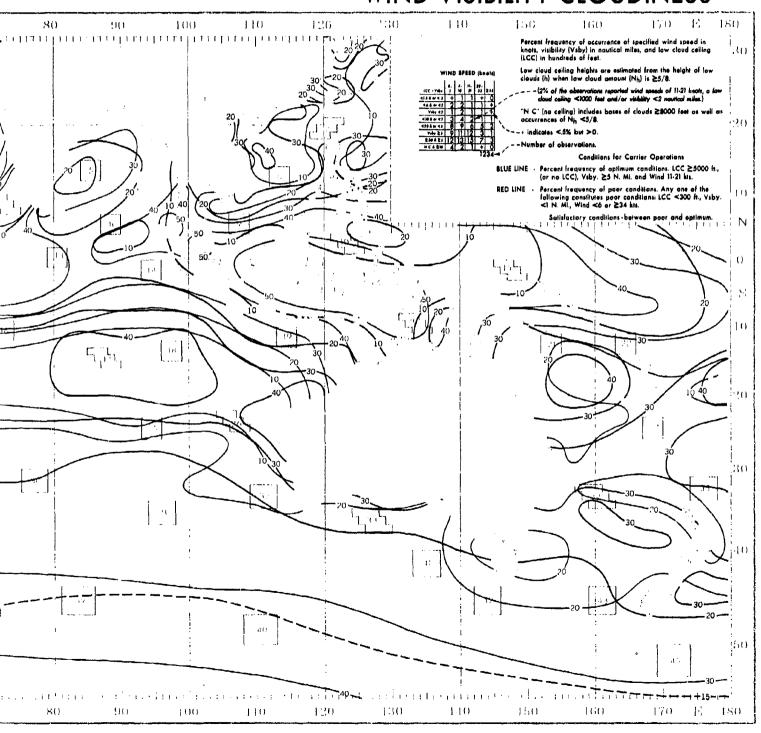
VISIBILITY ***********************************	VISIBILITY NC 0 0 + + 5 63 80-90 0 0 0 0 0 1 3 80-90 0 0 0 0 0 1 5 90-90 0 0 0 0 1 4 6 810 0 0 0 0 0 4 4 8 610 0 0 0 0 0 4 4 8 7 7 8 7 8 7 8 7 8 8 8 8 8 8 8 8 8 8	VISIBILITY G	VIBIBILITY 7	VISIOILITY	VISIBILITY 9
13 14 15 15 15 15 15 15 15	1 4	**************************************	No. No.	1 1 1 1 1 1 1 1 1 1	VISIBILITY
VIAIBILITY 22	VISIBIL TY Z 3	VISIBILITY	VISIBILITY 25	VISIBILITY 26 NC 0 0 0 0 0 1 88 80-80 0 9 0 0 0 1 84 80-80 0 0 0 0 0 0 14 80-80 0 0 0 0 0 0 15 80-80 0 0 0 0 0 0 15 80-80 0 0 0 0 0 0 15 80-80 0 0 0 0 0 0 15 80-80 0 0 0 0 0 0 0 15 80-80 0 0 0 0 0 0 0 15 80-80 0 0 0 0 0 0 0 0 0 15 80-80 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VIBIBILITY 27 -
VISIBILITY 31 ***********************************	VISIBILITY 32	VISIBILITY 3 3	VISIBILITY 4*7e*/retilist 2*6 6*10 ato NC 0 0 0 0 0 0 0 1 50*50 0 0 0 0 0 0 1 25*50 0 0 0 0 0 1 4 10*50 0 0 0 0 1 4 11 8*10 0 0 0 0 1 5 6 3*6* 0 0 0 0 0 1 1 1.5*3 0 0 0 0 1 1 3*21	VISIBILITY 35 ***** ***** **** ******	INSUFFICIENT DATA
SUFFICIENT DATA	VISIBILITY 41 VISIBILITY 41 CC 0 0 0 0 9 41 CC 0 0 0 0 0 0 0 CC 0 0 0 0 0 0 0 CC 0 0 0 0	INSUFFICIENT DATA	VISIBILITY 4 3 1 4	INSUFFICIENT DATA	VISTBILITY 45 vistBility 45 vistBility 46 0 0 1 1 18 18 0 0 0 0 0 0 1 2 0 0 0 0 1 1 2 0 0 0 0 1 1 15 7 0 0 0 0 0 1 1 2 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

e compilation of available data for specified areas without regard to suspected biases. te page) are based on all available data subjectively adjusted where bias was evident.

WIN



WIND-VISIBILITY-CLOUDINESS



LOW CLOUD CEILING-VISIBILITY-WIND

1 HIND SPEED (KNDTS)	2 WING SPEED (KNOTS)	3 HIND SPEED IKNOTS)	4 WIND SPEED (KNOTS)	5 HIND SPEED (KNOTS)	HIND SPEED (KNO
CC - YEBY 3 0 10 17 27 18 18 18 18 18 18 18 1	CC - YESY 3 10 21 33 344	CCC - view 7 9 10 22 33 33 33 33 33 33 33 33 33 33 33 33	0-4-11-22-3-10-22-3-3-54 -1-5-07-5-5-5-5-5-5-5-5-5-5-5-5-5-5-5-5-5-	CC - VARY 3 10 21 33 334	0- 4- 11-22- 10- 21-32- 11-8406+8-5
40 4 98 45 1 2 2 1 0 1 2 4 9 27 2 0 1 2 4 9 27 2 0 1 3 5 4 8 2 1 4 5 2 5 1 0 1 4 5 4 8 2 1 4 5 2 5 1 0 1 4 6 4 1 0 2 0 4 4 2 4 1 0 1 7 16	10 10 10 10 10 10 10 10	*20 4 08 *6	420 4 0R 45	420 404 46 2 7 3 4 0 V487 #8 5 49 38 C + #80 4 98 3 38 26 2 0 #C 4 8 10 3 33 25 2 0 293	-20 4 DR 45
10 HIND SPEED (KNOTS)	1 1 HIND SPEED (KNOTS)	12 HIND SPEED (KNOTS)	13 HINO SPEED (KNOTS)	14 HIND SPEED (KNOTS)	HIND SPEED CHNOT
CC - V667 3 0 4 1 1 22 3 394	CC - V88Y 8 0 0 10 21 33 344	CCC - VABAY 0 0 1 12 12 13 13 13 14	CCC - V681 9 10 21 93 394 -1.5 LOR -18 0 0 0 0 0 0 0 -6 LOR -18 0 0 0 0 0 0 0 -6 LOR -18 0 0 0 0 0 0 0 -18 LOR -18 0 0 0 0 0 0 0 -18 LOR -18 0 0 0 0 0 0 0 -18 LOR -18 0 0 0 0 0 0 0 -18 LOR -18 0 0 6 6 0 0 -18 LOR -18 0 6 6 0 0 -18 LOR -18 0 0 6 6 0 0 -18 LOR -18 0 0 6 6 0 0 -18 LOR -18 0 0 0 0 0 0 0 0 0	CCC - V687 5 10 21 33 334	CC - VBSY 3 10 21 33 32 33 34 35 37 37 37 37 37 37 37
75 19	MC4 a 10 27 45 8 0 0 129 2 0	MC4 = 10 [14 48 15 0 0] 268 2 1	MC4 = 10 23 35 17 1 0 95 2 2	nc4=10 13 31 24 0 0 56 23	MC4.#10 [25 29 8 0
HIND SPEED (KNOTS) LCC - VSSS	MIND SPEED (KNOTS) LCC - V&&T 3 0 4-1 11-127- LCC - V&&T 3 0 21 33 344 41.8 4 0M - (8 0 0 0 0 0 0 0 0 48 4 4 0M - (8 0 0 0 0 0 0 0 0 410 4 0M - (8 0 0 3 1 0 0 0 410 4 0M - (8 0 0 3 1 0 0 0 410 4 0M - (8 0 0 3 1 0 0 0 410 4 0M - (8 0 0 3 1 0 0 0 410 4 0M - (8 0 0 3 1 0 0 0 410 4 0M - (8 0 0 3 1 0 0 0 410 4 0M - (8 0 0 3 1 0 0 0 410 4 0M - (8 0 0 3 1 0 0 0 410 4 0M - (8 0 0 0 0 0 0 0 410 4 0M - (8 0 0 0 0 0 0 0 0 410 4 0M - (8 0 0 0 0 0 0 0 0 410 4 0M - (8 0 0 0 0 0 0 0 0 0 0 0 0 410 4 0M - (8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	MINO SPEED (KNOTS) LCC - VSBY 3 10 21 31 324 -11-8 4 0R 4.5 0 1 1 0 0 0 0 -18 4 0R 4.5 0 1 1 1 0 0 0 -18 4 0R 4.5 0 1 1 1 0 1 -18 4 0R 4.5 0 0 2 5 1 1 -18 4 0R 4.5 0 0 2 5 1 1 -18 4 0R 4.5 0 0 2 5 1 1 -18 4 0R 4.5 0 2 5 1 1 -18 4 0R 4.5 0 7 38 49 2 0	MIND SPEED (MNDTS) LCC - year 9 10 21 33 254 1 .54 08 - 6 0 0 3 0 0 -48 4 04 - 2 0 0 8 0 0 -48 4 04 - 2 0 0 10 0 0 -48 4 04 - 2 0 0 10 0 0 -48 4 04 - 2 0 0 3 13 0 0 -48 4 04 - 3 0 0 3 13 0 0 -48 4 04 - 3 0 0 0 0 0 0 -48 4 0 0 0 0 0 0 0 0 -48 4 0 0 0 0 0 0 0 0 -48 4 0 0 0 0 0 0 0 0 -48 4 0 0 0 0 0 0 0 0 0 -48 4 0 0 0 0 0 0 0 0 0 -48 4 0 0 0 0 0 0 0 0 0 0 -48 4 0 0 0 0 0 0 0 0 0 0 0 0 -48 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 -48 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	HIND SPEED (KNOTS) 1.02 - 11-122- 1.02 - 13 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	MIND SPEED (KNO) LCC - VSBV 3 10 21 33 1 41 11 - 12 1 33 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 2 1 41 13 1 41 1
28 NIND SPEED (MNOTS) LCC - V687	### A PART A PAR	MIND SPEED (RHOT6)	3 1 MIND SPEED (KNOTS) LCC - year 3 - 1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	32 MIND SPEED (MNDTS) LCC - VERY 3 10 21 82 824 -1.8 LOR -(8 0 0 0 0 0 0 0	#IND SPEED (KND15 LCE - Y687
37 HIND SPEED (KHOTS)	HIND SPEED (KNOTS)	39	40	4 1 HIND SPEED (KNOTS)	4.1
CC - Y687 3 4 1) - (82 33 34 34 34 34 34 34 3	CC - VBBT 3 4 11 25 33 34	INSUFFICIENT DATA	INSUFFICIENT DATA	CCC - V887 S 0 10 21 39 394 -1.84 08 -1.8 0 0 0 0 0 0 0 -44 08 -2 0 0 0 0 0 0 0 -48 08 -2 0 0 0 0 0 0 -48 08 -2 0 0 0 0 0 0 -48 08 -2 0 0 0 0 0 0 -48 08 -2 0 9 8 5 0 -48 08 -2 0 14 14 8 0 -48 08 -2 0 14 14 8 0 -48 08 -2 0 32 9 5 5 -48 04 0 0 23 9 5 5 -48 04 0 0 23 9 5 5	INSUFFICIENT DATA

<u>Graphs</u> represent the objective compilation of available data for specified areas without the <u>isopleth</u> analyses (apposite page) are based on all available data subjectively adjust

ITY-WIND

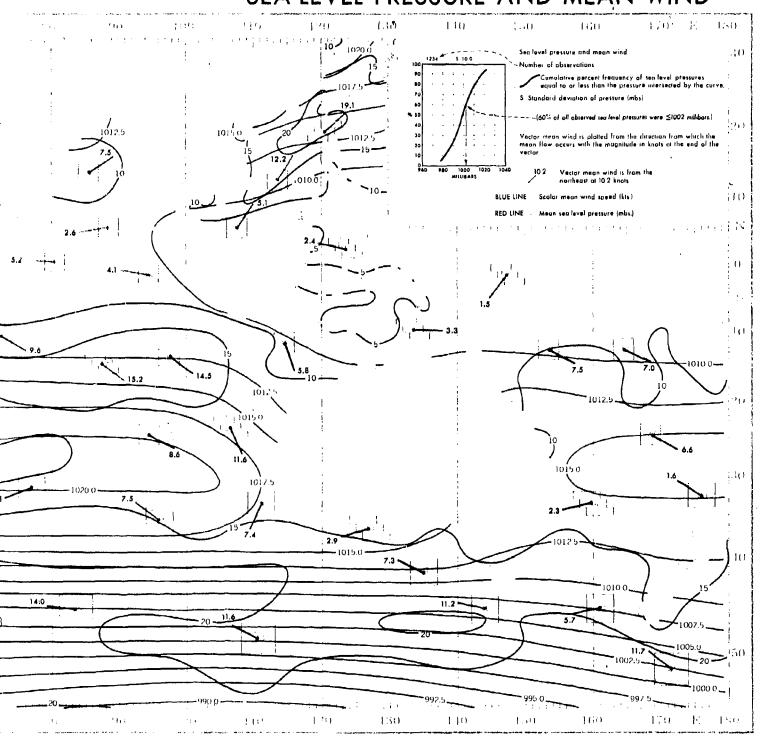
NOVEMBER

1.	5	6	7	8	9
HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	WIND SPEED (KNOTS)	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)
LCC - YEST 2 10 71 33 234	1CC - VEST 3 10 21 33 834	LCC - VBST 3 10 21 39 234	LCC - YSBY 3 10 21 33 334	LCC - VARY 3 .0 21 33 434	LCC - YEBY 3 10 21 33 294
11-5 4 09 4 16 0 0 0 0 0	*1.54 08 4.6 0 0 0 0 0	41.8 4 0g 4.8 0 + + +	*1.54 DR *.\$ D + + D D	41.5 6 0, 4.8 0 + + 0 0	41.84 QR 4.8 + + + D
*8 4 08 -2 0 0 + + 0	-64 DR -2 + 1 + + 0	+8 4 OR -8 + 1 2 2 1	*8 4 OR *2 + 1 + 0 O	48 4 (1 42) 4 2 1 4 0	48 4 58 42 4 2 2 4 0
V887 42 0 0 0 + 0	V88Y 42 0 + 0 0 0	VEBY -2 + + 1 1 +	VSBY 42 0 + 0 0 0	V687 -2 0 0	VSBY 42 + 1 1 + 0
-10 4 58 - 2 0 1 1 + 0	40 4 OR 42 1 2 5 2 0	410 4 08 42	*10 4 DM *2 + 3 1 0 0	410 4 SR 42 1 6 4 1 0	410 4 0M 49 1 5 5 1 0
120 4 08 46 0 2 2 1 0	*20 4 OR *6 2 7 9 4 0	-PO & OR -6 + 6 16 9 1	-20 4 OR -15 2 6 3 0 0	420 4 OR 45 2 13 11 1 0	420 4 DR 45 2 13 10 1 0
V587 46 7 58 36 1 D	VBBY 35 5 49 38 C +	VEST 25 2 23 51 14 1	7887 a5 26 61 12 + 0	V60Y #6 13 54 27 1 0	VSSY 25 16 47 29 2 0
A60 CAS 6 54 33 1 0	3 38 26 2 0	280 4 as 1 18 35 7 +	a 80 & a 6 24 51 9 + 12	360 4 ab 10 39 16 1 0	-50 4 -6 13 33 18 1 C
HC 4 = 10 B 62 32 1 0	MC 4 + 10 3 33 25 2 0	MC 4 8 10 1 15 28 4 +	HC 4 = 10 23 49 B + 0	MC & 2 10 10 36 14 + 0	MC 4 B 10 11 28 15 + 0
653	293	5194	1398	1352	2970
1.3	1.4	15	16	17	18
HIND SPEED (KNOTS)	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	. WIND SPEED (KNOTS)	WIND SPEED (KNOTB)	HIND SPEED (KNOTS)
				ا لمعجاديا مهامها	ا المقفلين المالما
1CC - YBBY 3 10 21 35 a34	1CC - VARY 9 10 21 33 434	LCC - Y88Y 3 10 21 35 m34	LCC - VORY 3 10 21 35 434	LCC - Y687 3 10 21 33 234	
*1.5 4 0R 2.5 0 0 0 0	41.84 OR 4.8 0 2 0 U 0	41.84 DR 4.8 D D D D	41.8 6 0R 4.8 0 0 0 0 0	*).8 4 OR *,6 0 0 0 0 0	41 - 8 4 64 4 - 8 0 0 0 0 0 0
-8 4 OR -2 0 2 0 0 0	*84 GR *2 2 2 0 0 0	46 # 0 x 4 x 1 D 0 D 0	46 4 OH 42 0 1 2 + 0	-6 4 OR +2 0 0 1 1 D	48 £ 08 42 0 0 0 1 0
vaar -2 0 0 0 0 0	V887 42 2 0 0 0 0	Y887 42 0 0 0 0 0	VB6Y <8 0 + 0 0	V847 42 0 0 0 0 0	V467 42 0 0 0 1 0
*10 4 0M *2 0 2 1 0 0	410 4 0R 42 2 9 2 0 D	*10 4 0R *2	410 1 0 4 45 4 6 6 1 0	<10 4 DR <2 0 2 8 2 1	410 4 0R 48 0 0 1 1 0
*20 4 08 *5 0 6 6 0 0	420 4 0R 45 4 11 5 D D	420 4 5R 4B B B B B B B B B B B B B B B B B B B	420 A OR 45 + 11 14 3 D	4g0 4 gm 4b 0 3 15 8 1	<80 LOR <8 0 3 10 1 1 VEST 28 1 21 71 5 1
y887 a5 25 45 27 1 0	V69Y AS 15 49 35 0 0	veer ab 32 54 10 0 0	VBSY 15 3 45 44 5 0		
250 4 25 23 38 20 1 0	240 4 88 13 31 27 0 U	*BD A *B 25 34 8 0 0	as0 4 as 2 33 28 3 0		
MC 4 = 10 23 35 17 1 0	MC 4 = 10 13 31 24 0 0 55	MC 4 = 10 25 29 6 0 0	HC 4 a 10 2 30 27 2 0	MC 4 a 10 0 13 44 7 0	AC & B ID 1 18 43 2 0
					27
22	23	24	25	26	
HIND SPEED (KNOTS)	WIND SPEED (KNOTS)	WIND SPEED (KNOTS)	WIND SPEED (KNOTS)	WIND BPEED (KNOTS)	MIND BPEED (KNOTS)
LCC - YBBT 0 4 11-22-	LCC - VBBY 3 10 21 33 694	LCC - VSBY 3 10 21 33 214	LCC - VABT 3 10 21 33 234	LCC - VARY 3 10 21 33 234	LCC - VABY 3 10 21 39 134
(1.84 pR 4.5 0 0 3 0 0	41.84 DR 4.5 0 + 0 + 0	<1.8408 *.8 0 0 0 0 0	41.84084.8 0 0 0 0 0	41.84 OR 4.8 0 0 0 0	41.84 DR 4.8 0 0 0 0 0
-a c oa -r 0 0 8 0 0	46 ± DR + ± C + + + D	48 4 OR 42 0 0 0 0 0	48 4 5R 42 0 0 0 0 0	<\$ 4 5M 4Z 0 () 0 0 D	40 4 54 48 D D D D D
Y887 42 0 0 0 0 0	V00 C C C C C C C C C C C C C C C C C C	A88A 45 D Q Q D D	V807 <2 0 0 0 0 0	VEEY +2 0 0 0 0 0	V007 <p 0="" 0<="" th="" u=""></p>
-10 4 GR =2 0 0 10 0 0	*10 4 UR <2 + 1 2 1 +	/10 4 QR = Z	<10 4 0A 42 0 1 6 0 0	410 4 68 48 0 1 4 0 0	<10 4 9R <2 0 0 6 0 0
-20 4 OR -8 0 3 13 0 0	420 4 OR 46 1 5 5 1 •	420 4 DA 48 D U 19 3 D	420 4 0R 46 0 1 18 0 0	420 4 OR 45 0 2 7 2 0	420 4 OR 48 0 2 13 U 0
V687 35 3 45 48 0 0	veer as 13 50 33 4 ·	V667 +3 0 43 54 3 0	V667 AB 1 40 57 1 0	v887 a5 1 27 88 8 0	Y88Y 25 4 36 55 2 0
* 60 6 26 3 35 29 0 0	a 50 4 a 5 11 43 28 2 ·	a 80 4 4 5 0 32 92 0 0	# 60 4 MB 1 29 30 1 0	960 4 a \$ 0 17 42 1 0	380 4 a 8 4 34 37 1 0
NC 4 + 10 3 19 23 0 0	#C 4 2 10 11 43 25 2 +	MC 4 = 10 0 30 27 0 0	ME 4 a 10 1 24 27 1 0	MC 4 a 10 D 16 38 1 3	MC 4 0 10 4 33 35 1 0
•,	·	- /	2,	•••	·
31 Hind Speed (Knots)	32	33	34	35 HIND SPEED (KNOTS)	36
	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNDTS)		
LCC - YESY 3 10 21 33 254	LCC - YBBY 3 10 21 33 #34	LCC - Y887 3 10 21 33 234	LCC - Yest 3 10 21 33 634	LCG - Y88Y 2 10 E1 38 134	
11.84 d# 1.8 0 0 0 0 0	43 - E 4 OR 4 - E 0 0 0 0 0	<1.64 OR <.6 0 0 0 0	<1.84 gR <.8 () + () } ()	41.54 0R 416 0 0 0 1 0	
48 4 DR 17 D D D D D	48 4 DR 42 0 0 1 + 0	48 4 02 42 + 6 3 D +	<8 4 OR <2 0 + 2 2 0	48 4 DR 42 0 1 3 1 0	INSUFFICIENT
VERY <2 0 0 0 0 0	7887 *F 0 0 0 0 0	Y887 42 0 0 0 0 +	YEST - 2 0 0 0 + 0	V887 48 0 0 0 0 0	DATA
4)0 4 OR 49 0 2 4 4 2	*10 4 OR *2 0 3 3 1 1	<10 4 OR <e +="" +<="" 1="" 3="" 4="" th=""><th><10 4 de <2 0 3 10 5 1</th><th>410 & 0R 42 0 3 5 3 1</th><th>DATA</th></e>	<10 4 de <2 0 3 10 5 1	410 & 0R 42 0 3 5 3 1	DATA
-20 4 GH 45 2 8 B B 7	-20 4 OR +5 0 10 13 4 2	-20 4 GR -8 1 8 9 2 +	420 4 OR 48 + 7 19 8 2	<20 4 OR <8 1 B 12 4 1	
VSBT 25 6 32 40 13 4	VEHY AS 1 31 50 12 3	VSBT AS 7 36 40 12 1	VBBY AS 4 30 47 14 3	VSSY as 5 42 43 B 1	
* 80 4 ss 0 18 21 B 0	380 4 38 1 18 23 6 O	a 50 4 all 5 24 25 B 1	3 1 B 25 B 1	260 4 as 4 30 28 4 1	
MC 4 > 10 0 19 19 B 0	HC 4 = 10 1 14 20 4 0	MC 4 4 10 5 21 22 7 +	HC4 = 10 3 18 24 6 1	ac 4 a 10 4 30 27 4 0	
					4.5
40	41	42	43	44	45
Ü	MIND SPEED (KNOTS)		HIND SPEED (KNOTS)		WIND SPEED (KNOTS)
· ·	LCC - V487 0 4- 11- 22-		LCC - VERY 3 10 21 38 434		LCC - VBST 3 10 21 29 334
}	41.84084.5 0 0 0 0 0		41.5 4.08 4.8 0 1 1 1 0		41.84084.6 0 2 5 0 1
NSUFFICIENT	48 4 5R 42 0 0 5 0	INSUFFICIENT	484 OR 42 0 1 5 1 1	INSUFFICIENT	-84 SR <8 () 4 5 1 2
DATA	veev -2 0 0 0 0 0		VBRY 42 0 1 0 0 0	DATA	V681 48 0 2 5 1 2
UAIA	-10 4 OR -2 0 9 9 5 0	DATA	-10 4 SR -2 D 4 21 4 1	DAIA	<10 4 OR <2 0 5 9 1 2
	-20 s oz =6 0 14 14 9 0	•	-PO LOR -E 0 5 38 6 5		-E0 4 DA -E 0 7 18 12 4
	veev ats 0 45 32 14 5		V487 25 1 19 50 19 5		1407 48 2 9 35 32 7
	a 80 4 a 8 0 32 9 5 5 MC 4 a 10 0 23 9 5 5	·	3 60 4 3 B 13 10 1		#C 4 2 0 1 3 6 3 1
	MC 4 3 10 1 7 7 7 1 0 1 S 1 S 1		MC 4 3 10 0 9 10 9 0		MC 4 3 10 3 5 5

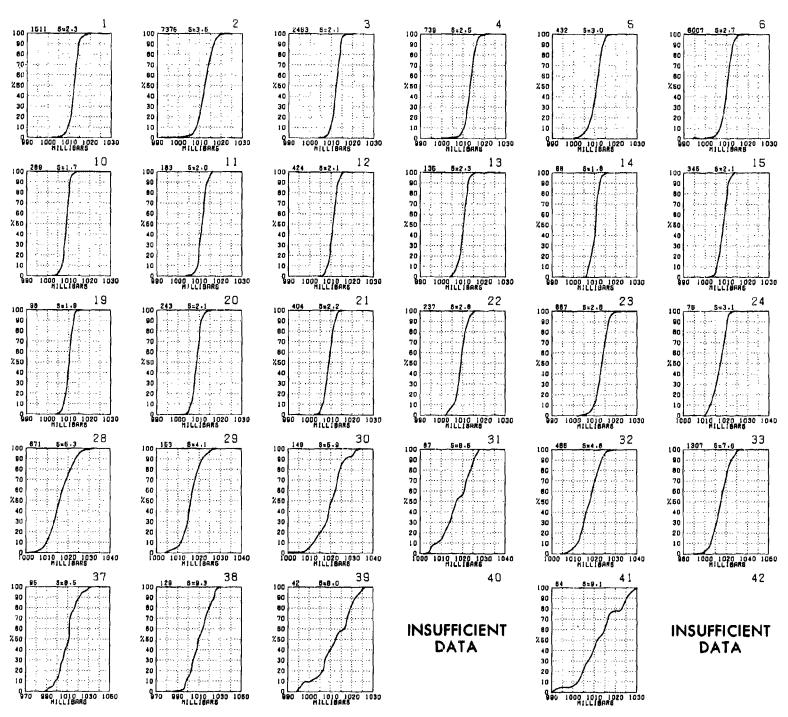
itive compilation of available data for specified areas without regard to suspected biases. saite page) are based on all available data subjectively adjusted where bias was evident.

NOVEMBER SEA LEVEL PRES

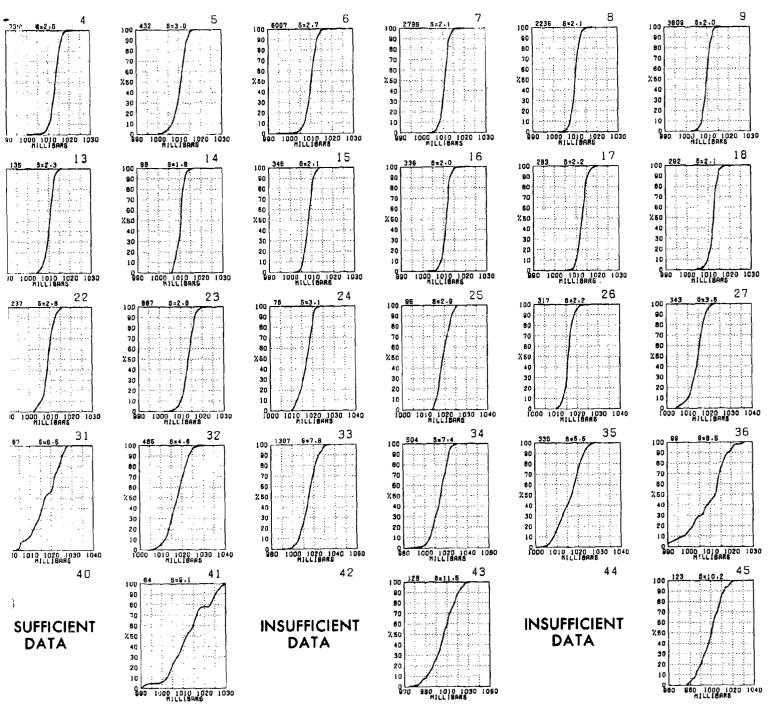
SEA LEVEL PRESSURE AND MEAN WIND



SEA LEVEL PRESSURE

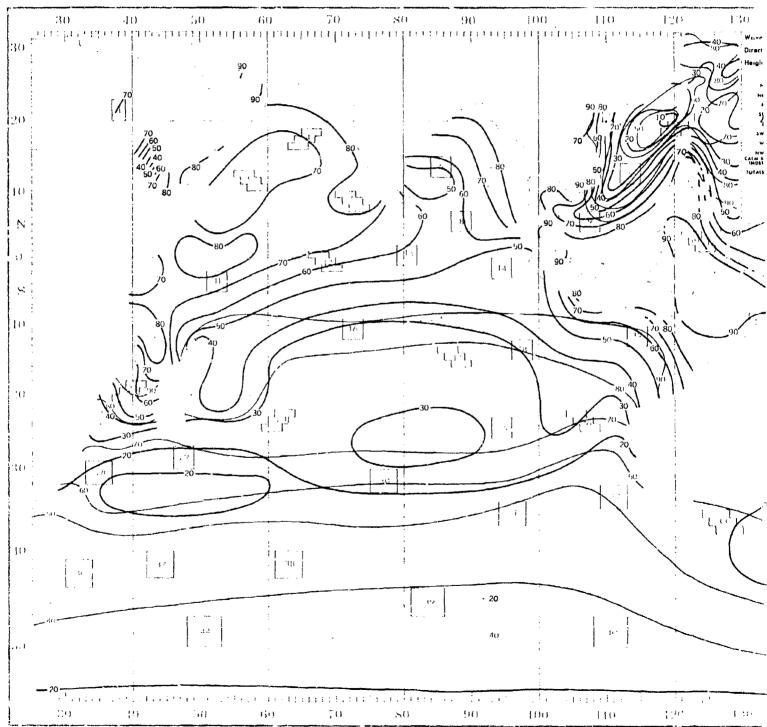


Graphs represent the objective compilation of available data for specified areas without regar. The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjusted w

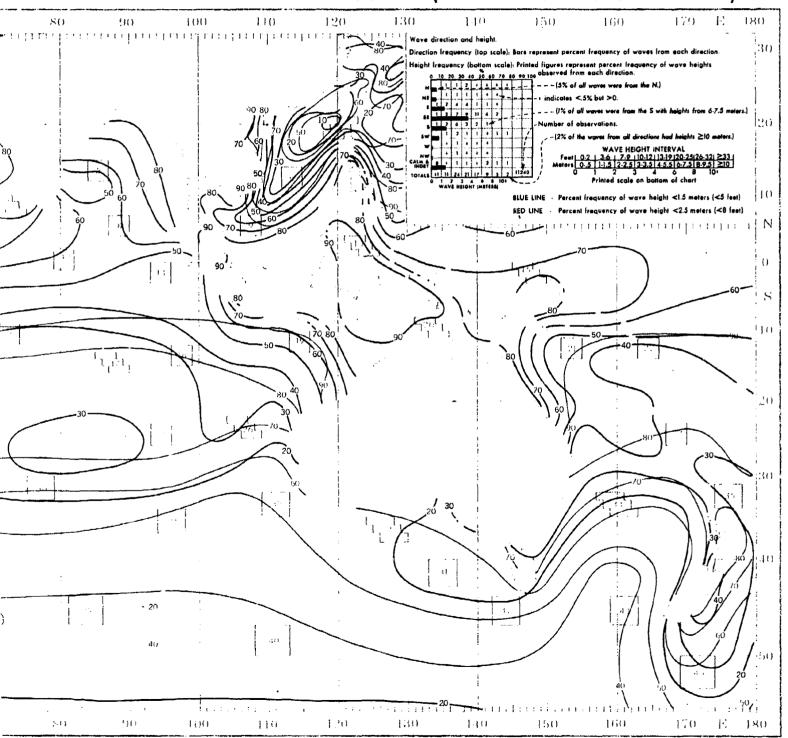


re compilation of available data for specified areas without regard to suspected biases. to page) are based on all available data subjectively adjusted where bias was evident.

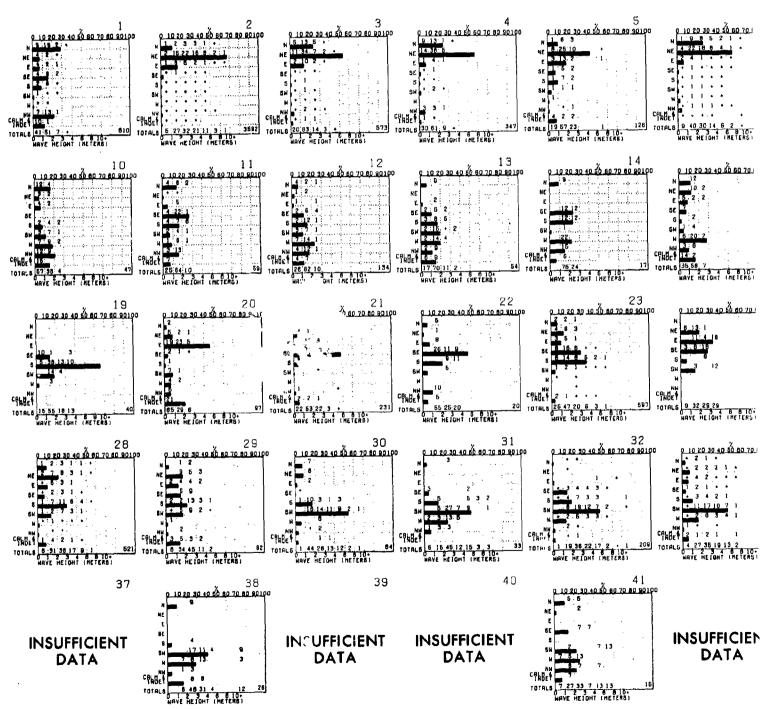
WAVES



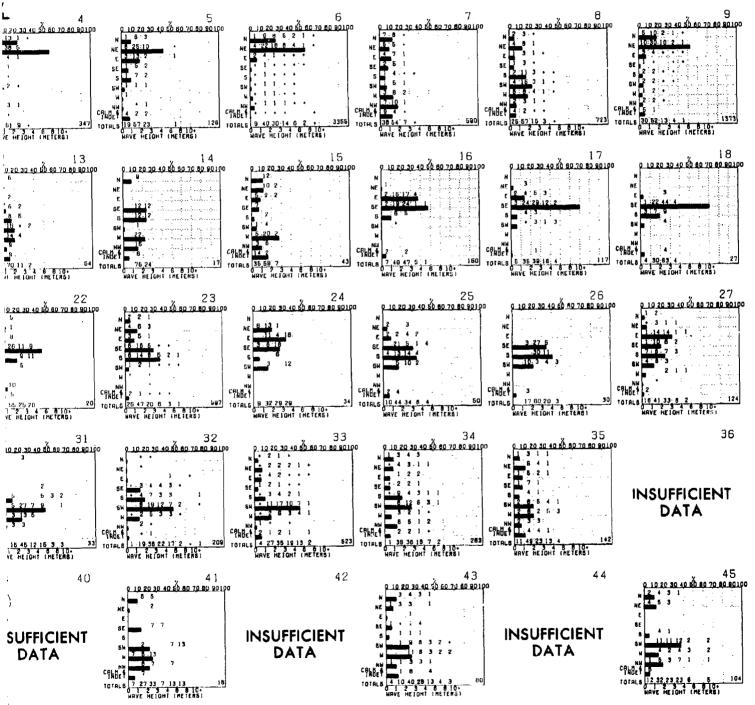
WAVES (<1.5 AND <2.5 METERS)



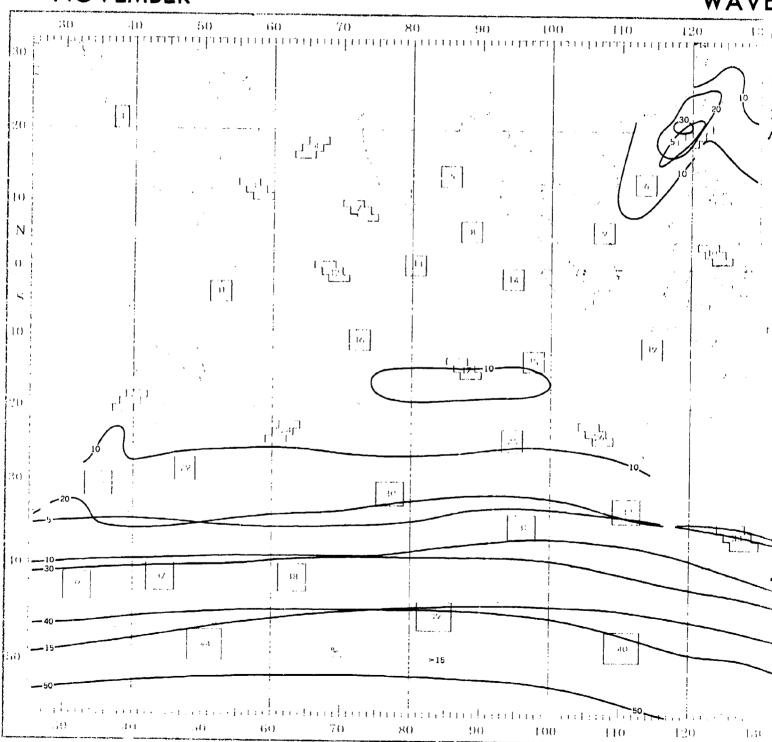
WAVE DIRECTION AND HEIGHT



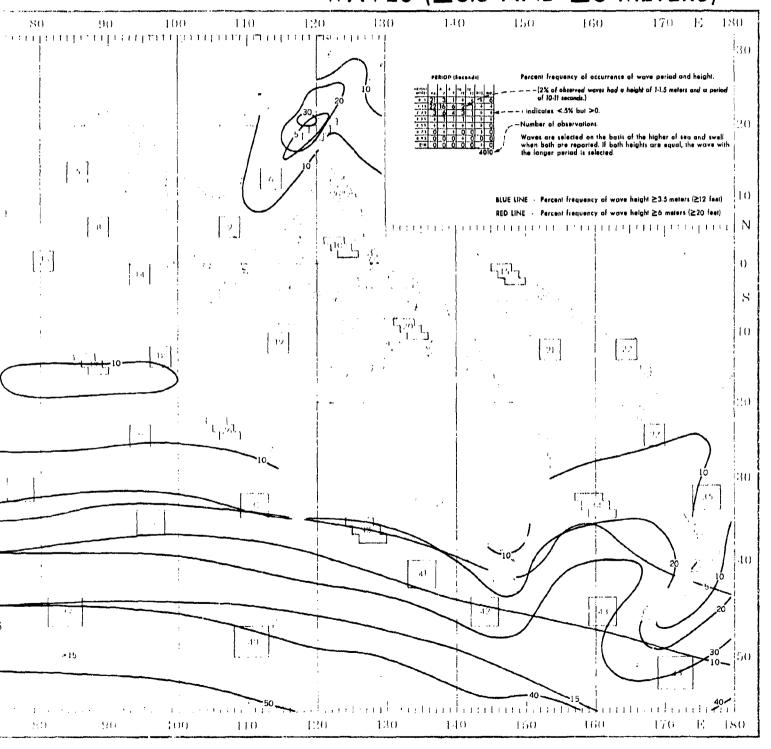
Graphs represent the objective compilation of available data for specified areas witho The isopleth analyses (opposite page) are based on all available data subjectively adj



B compilation of available data for specified areas without regard to suspected biases. The page are based on all available data subjectively adjusted where bias was evident.



WAVES (≥3.5 AND ≥6 METERS)



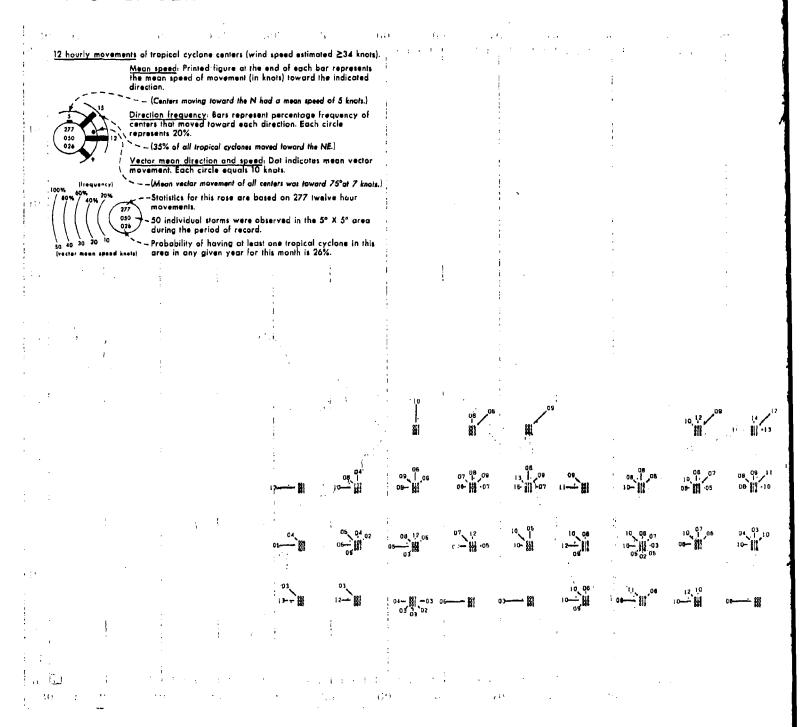
WAVE PERIOD AND HEIGHT

INSUFFICIENT DATA	38 PERIOD I SECONDE) ***TRAB** 46 7 9 111 13 213 149 ***	INSUFFICIENT DATA	INSUFFICIENT DATA	INSUFFICIENT DATA	INSUFFICIEN DATA
28 PERIOD (SECONDB)	29 PERIOD (SECONDE) ***********************************	30 PERIOD (SECONDE) ***I	3 PERIOD (SECONDS)	#E1001 (EECONDS)	PERIOD (SECOND: (n/As) ** 1
PERIOD (SECONDS)	PERIOD (SECONDE) **Cloud 48 0 0 10 10 10	PERIOD (SECONDE) PERIOD (SEC	PERIOD (SECONDS) 18 10 10 10 10 10 10 18 18 18 10 10 10 18 18 18 18 18 18 18	23 **COUNT 6-7 10-11 13 13 140 **COUNT 6-7 -1 10-11 13 13 140 **COUNT 6-7 -1 10-11 13 13 140 **COUNT 6-7 -1 10-11 13 13 140 **COUNT 7 7 7 7 7 7 **COUNT 7 7 7 7 **COUNT 7 7 7 7 **COUNT 7 7 7 7 **COUNT 7 7 7 **COUNT 7 7 7 **COUNT 7 7 7 **COUNT 7 7 7 **COUNT 7 7 7 **COUNT 7 7 7 **COUNT 7 **COUNT 7 7 **COUNT 7	PERIOD (SECOND) HE [OH] 16
PERIOD (SECONDS) ***********************************	1	1 1 1 1 1 1 1 1 1 1	1 3 PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) **PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) ***PERIOD (SECONDS) **PERIOD	INSUFFICIENT DATA	PERIOD (SECOND: NETON: 1
PERIOD (SECONDS) **Etenti a	PERIOD (SECONDS) 18	MEIONI PERIOD (SECONDS) MEIONI PERIOD (SECONDS) MEIONI	PERIOD (SECONDS) **TOM** 6- 0- 10- 11 13 13 140	FERIOD (SECONDS) MCIONI	PERIOD (SECON) HEIONT 6 7 8 10 13 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

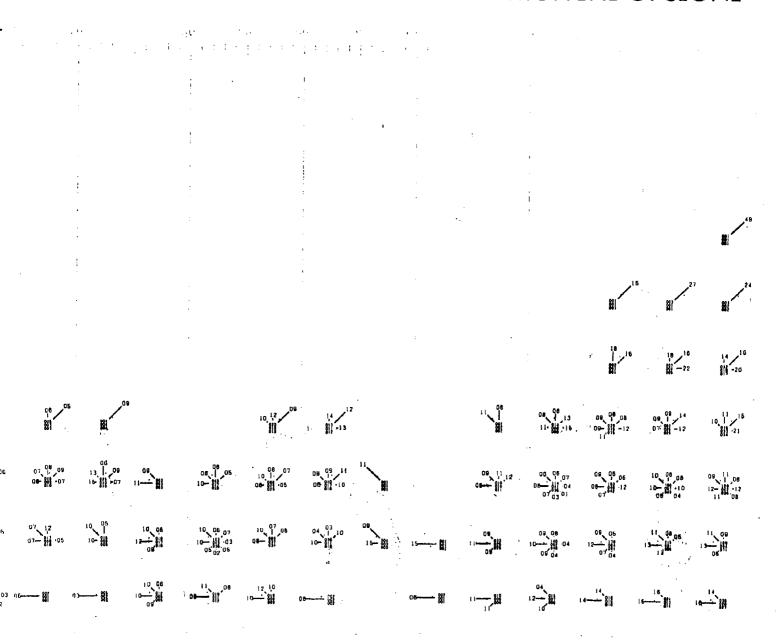
Graphs represent the objective compilation of available data for specified areas without The isopleth analyses (opposite page) are based on all available data subjectively adju-

jective compilation of available data for specified areas without regard to suspected biases.

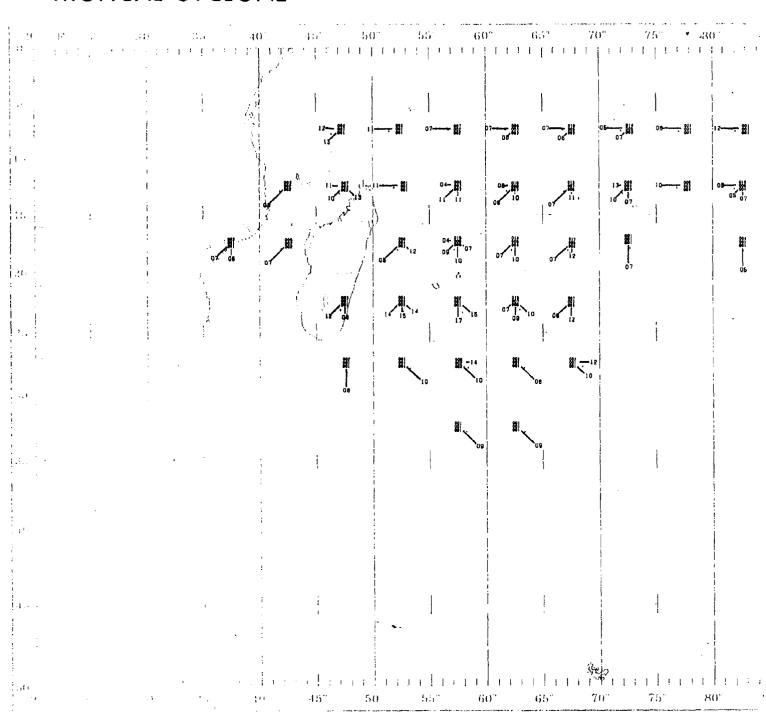
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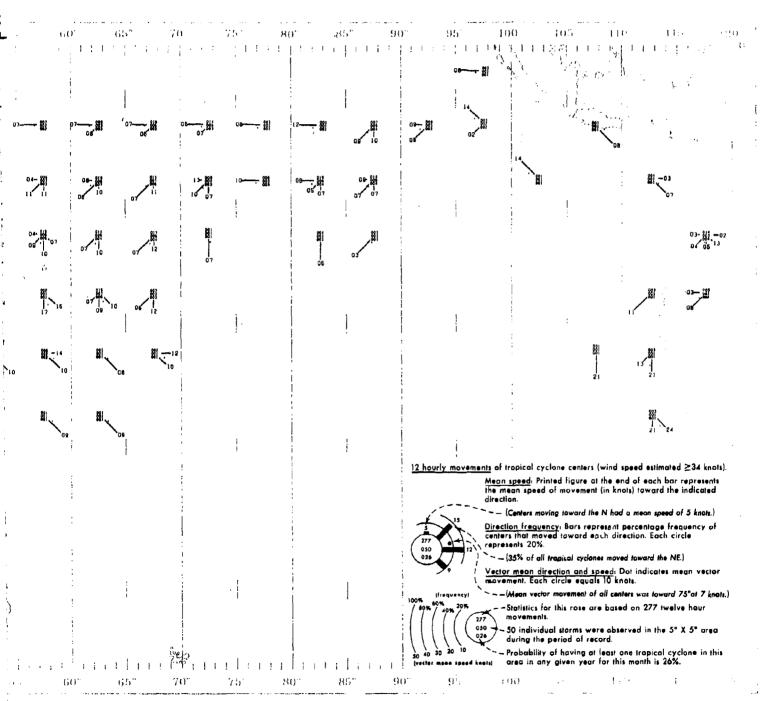


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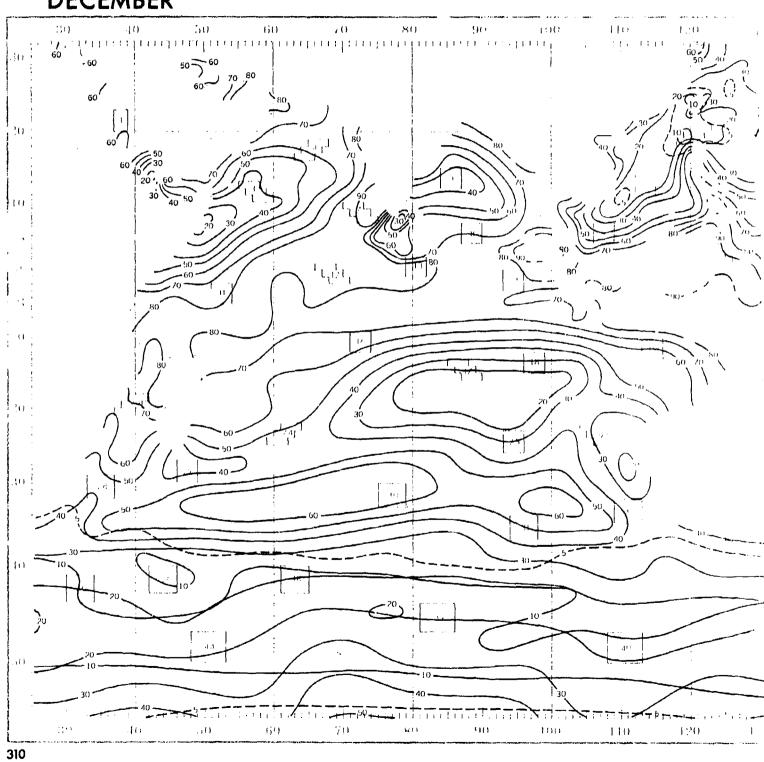


TROPICAL CYCLONE

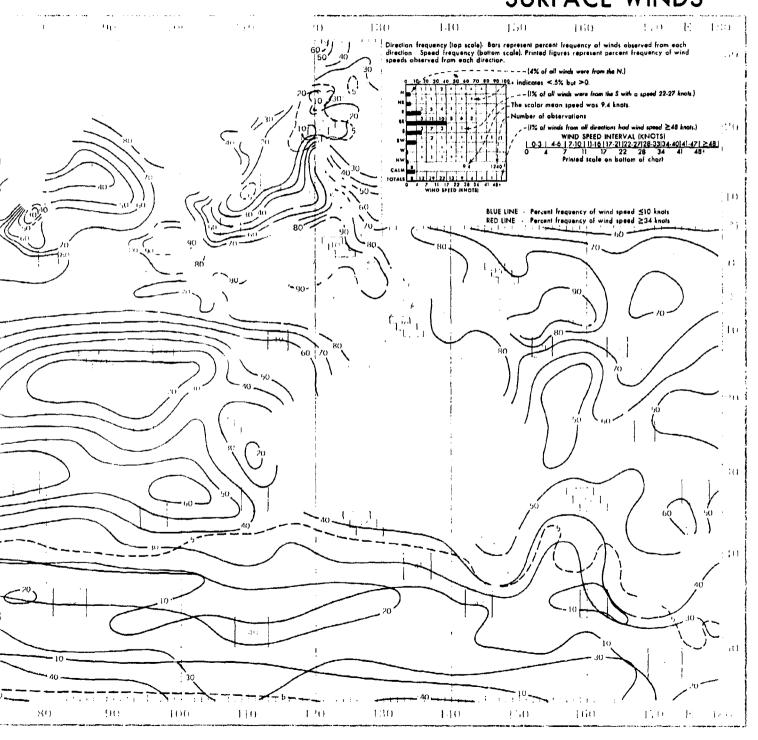




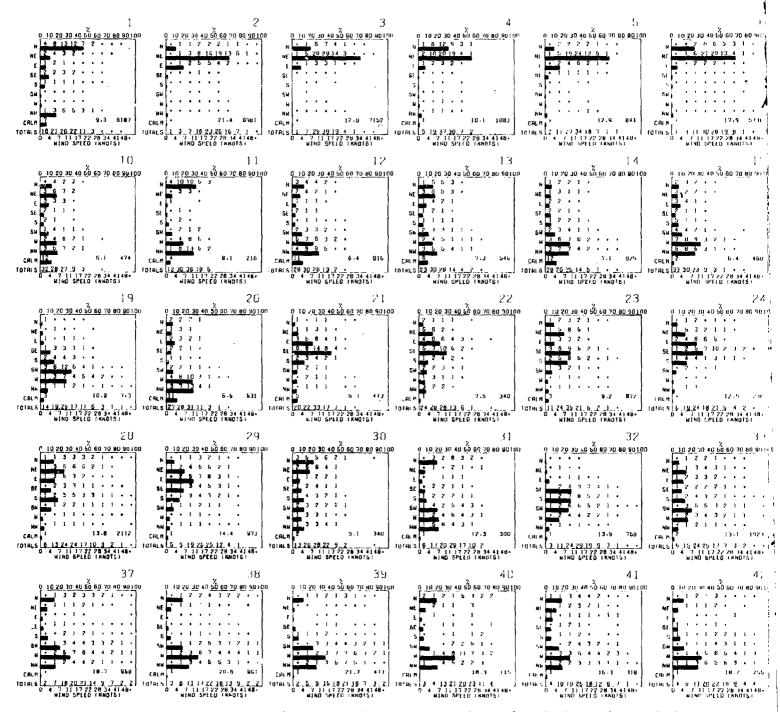
DECEMBER



SURFACE WINDS

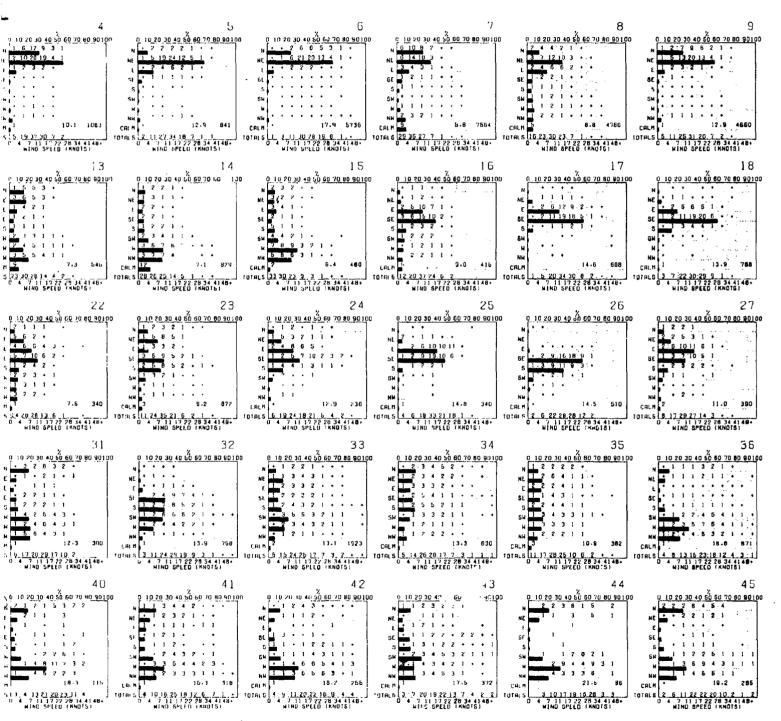


WIND DIRECTION AND SPEED

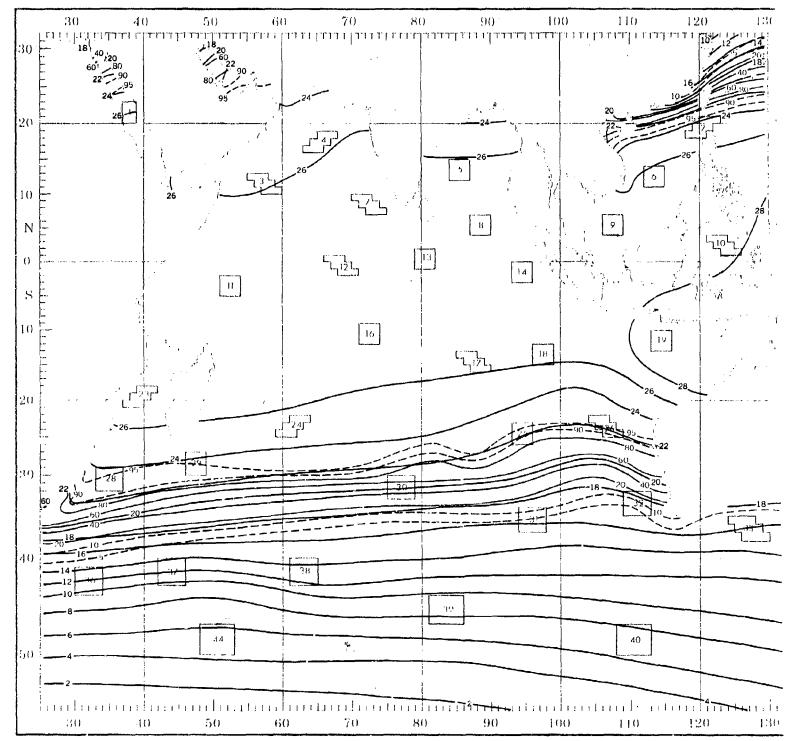


Graphs represent the objective compilation of available data for specified areas without rec The isopleth analyses (apposite page) are based on all available data subjectively adjusted

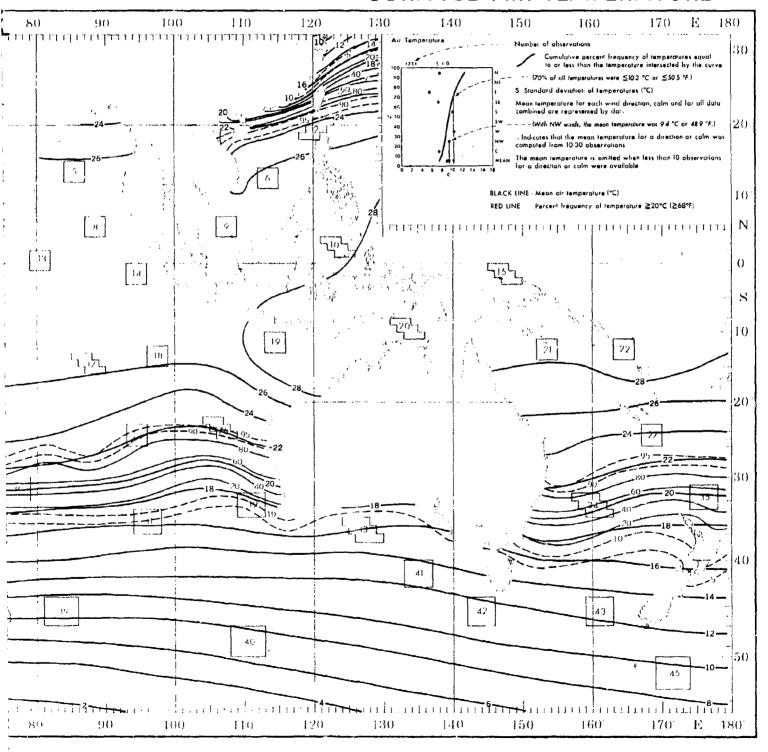
DECEMBER



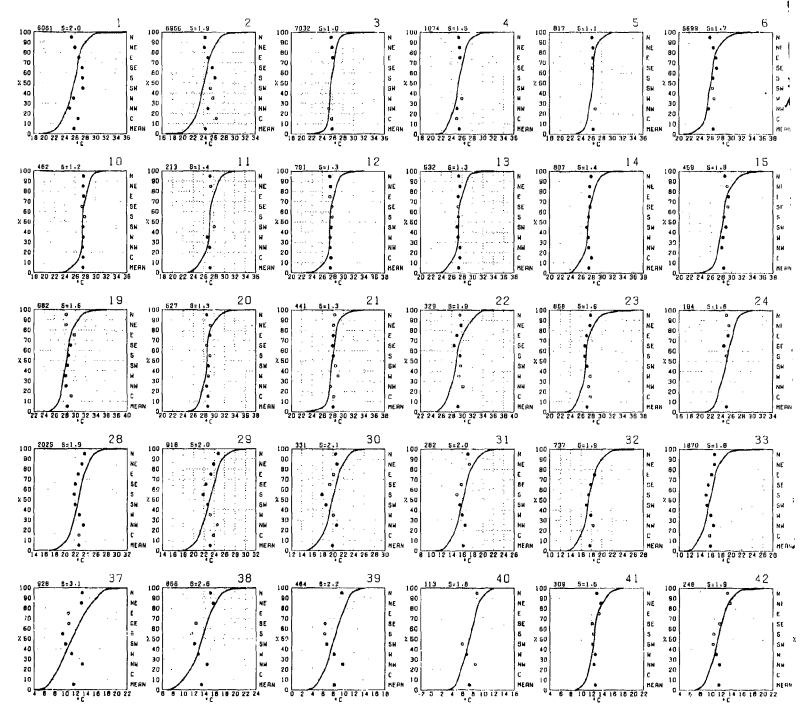
ive compilation of available data for specified areas without regard to suspected biases, site page) are based on all available data subjectively adjusted where bias was evident.



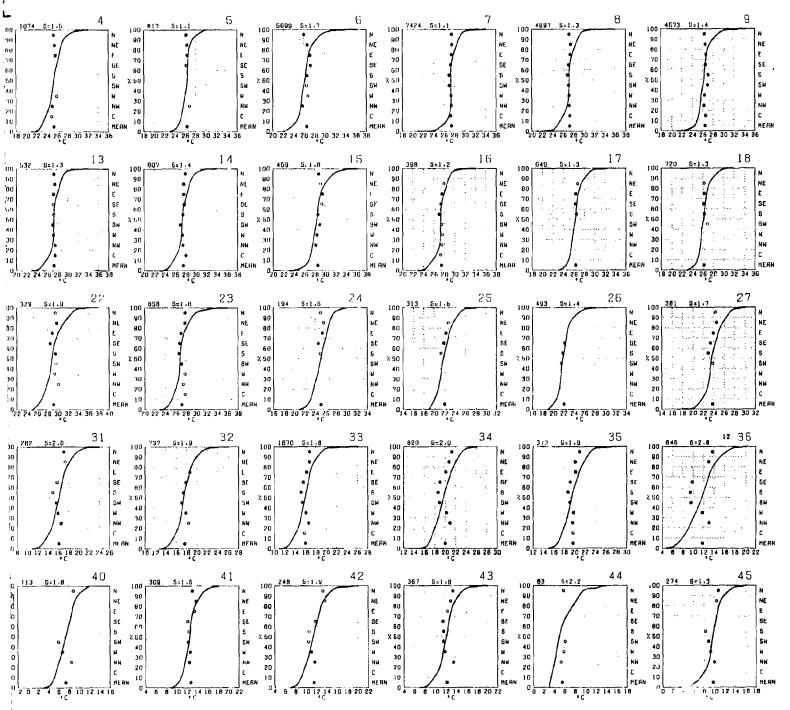
SURFACE AIR TEMPERATURE



SURFACE AIR TEMPERATURE

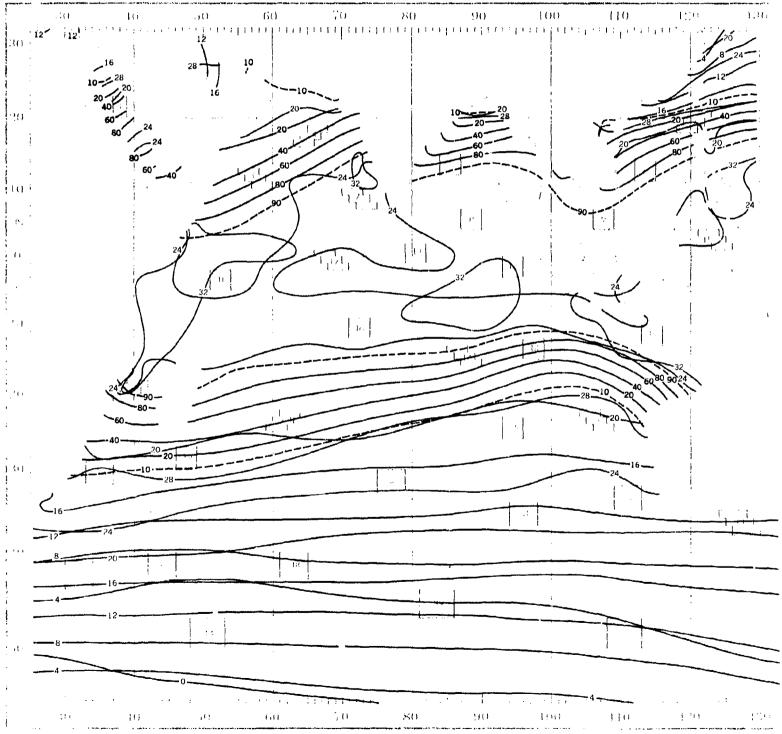


Graphs represent the objective compilation of available data for specified areas without reg The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjusted

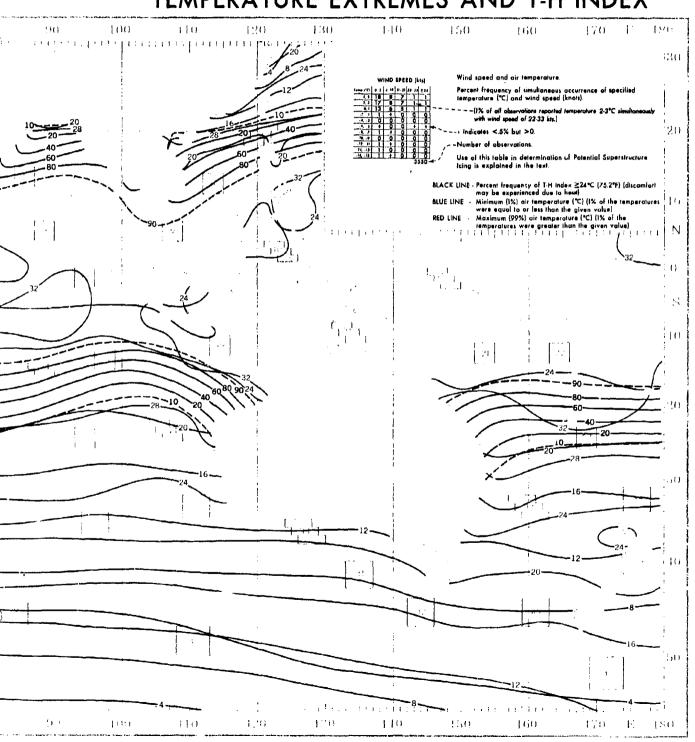


ctive compilation of available data for specified areas without regard to suspected biases.

TEMPERATURE E



TEMPERATURE EXTREMES AND T-H INDEX



WIND SPEED AND AIR TEMPERATURE

HIND SPEED (KTS)	HIND SPEED (KIS) 2	HIND SPEED (KTS) 3	WIND SPEED (KTS) 4	WIND SPEED (KTS)	HIND SPEED (KIS) 6
1EMP (*C) 0-9 4-10 11-21 22-33 2 34	TEMP (*C) 0-9 4-10 11-2122-38 ± 94			TEMP (4C) 0-9 4-10 11-21 22-33 a 34	TEMP (4C) 0-3 4-10 11-21 22-33 4 34 5
32.33 + + + 0 C	30.31 + + + + + + + + + 20.60 + 1 2 1 +	30.31 + + + + 0 28.28 + 3 4 + +	30,31 0 1 + 0 0 28,28 1 5 3 + 0	28.28 • 7 7 1 0 28.27 1 24 38 5 •	32.33 + 1 1 · U
28.28 4 8 4 + 0 26.27 10 20 10 1 + 24.25 3 12 11 1 4	26.27 1 4 12 8 1 24.25 - 4 17 17 3 22.23 + 1 7 12 3	28:27 1 21 37 3 + 26:28 + 12 17 2 + 82:23 + + + + +	28,27 2 22 16 1 0 21,28 2 23 10 1 0 22,23 + 4 3 + 0	24.75 1 8 5 1 + 22.23 0 + + 0 0 20.21 0 0 0 0 0	28.29 + 3 13 3 · 28.27 + 7 30 14 1 24.25 + 2 10 8 1
22 .23 1 4 6 1 +	20.21 + + 1 3 1	20.21 0 0 + + 0 19.19 0 0 0 0 0	20.21 0 0 + 0 10.19 0 0 0 0 0	10.19 0 0 0 0 0 0 18.17 0 0 0 0 0 0	22:23 0 + 1 + · · · · · · · · · · · · · · · · ·
10-10 0 + + 0 0 0 10-11-11-11-11-11-11-11-11-11-11-11-11-1	18.17 0 0 + 0 0 14.18 0 0 0 0 0 0 12.13 0 0 0 0 0	18:17 0 0 0 0 0 0 14:15 0 0 0 0 0 0 12:13 0 0 0 0 0	14.15 0 0 0 0 0 14.15 0 0 0 0 0 0 12.13 0 0 0 0 0	14.15 0 0 0 0 0 0 17.13 0 0 0 0 0 0 10.11 0 0 0 0 0	19-19 0 0 0 0 0 0 19-17 D 0 0 0 0 0 14-18 0 0 0 0 0
6084	6956	7032	1076	617	5690
HIND SPEED (KTS) 10	HIND SPEED (KTB) 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	MIND SPEED (KTS) 12	MIND SPEED (KTS) 13	NING SPEED (KTS) 14	HIND SPEED (NTS) 15
30.31 1 3 1 0 0 20.20 20 26 5 0 0	90.91 2 3 1 0 0 28.28 4 22 9 0 0	32:33 + 1 0 0 0 30:31 2 3 1 0 0	32.33 D + + O O 30.31 2 2 1 1 0	32,33 1 + 0 0 0 0 30,31 3 5 2 0 0	34.98 1 4 0 0 0 38.39 3 3 0 0
26.27 12 24 4 + 0 24.25 + 2 1 0 0	26.27 6 36 10 0 0 24.25 0 4 2 0 0	28.29 12 25 6 • 0 28.27 14 26 8 • 0	28.27 12 24 10 1 0	28.29 14 22 5 0 0 28.27 11 21 10 1 0	30.31 6 6 1 0 0 20.20 10 31 7 + 0
20.21 0 + + 0 0 20.21 0 0 0 0 0 18.10 0 0 0 0 0	22.23	24.25 1 1 2 0 0 22.23 0 + + 0 0 20.21 0 0 0 0 0	24.25 1 4 1 + U 22.23 0 + D 0 D 20.21 0 0 U 0 0	24.25 1 3 2 1 + 21.23 0 0 0 0 0 0 20.21 0 0 0 0 0	26.27 6 11 4 1 · 24.25 + 1 1 0 0 22.23 0 0 0 0 0
18-17 0 D 0 D 0 D 0 14-16 0 D 0 D 0 D 0	18.17 Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q Q	18-18 0 0 0 0 0 0 18-17 0 0 0 0 0 0	19.19 0 0 0 0 0 18.17 0 0 0 0 0	18.17 O O O O O	20:21 0 0 0 0 0 10:10 0 0 0 0 0
18.13 0 0 0 0 0 0 19.11 0 0 0 0 0 0	10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0	14-15 0 0 0 0 0 0 12-13 0 0 0 0 0 0	14.18 0 0 0 0 0 0 12.19 0 0 0 0 0 0	14,15 0 0 0 0 0 0 12,13 0 0 0 0 0 0	14-14 0 0 0 0 0
MINO SPEED (KTS) 19	HIND SPEED (KTS) 20	MIND SPEED (KTS) 21	HIND SPEED (KTS) 22	WIND SPEED INTS. 23	HIND SPEED (KTS) 24
TENP 1*C) 0-3 4-10 11-21 22-31 2 34	16HP (4C) D-9 4-10 11-21 22-23 A 34	TEHF (PC) 0-3 4-10 11-51 22-33 8 84	TENP (*C) 0-3 4-10 11-2122-33 34	TEMP (*C) 0-3 4-10 11-21 22-33 a 34	TEMP (*C) 0-9 4-10 11-81 82-93 a 34
34.35 1 + 0 0 0 0 32.33 2 3 + 0 0 30.31 4 9 5 + +	34.36	32,33 1 2 0 0 0 30,31 3 6 1 + 0 28,20 12 33 13 1 0	26.98 1 1 0 0 0 28.92 3 7 1 0 0 20.21 6 12 3 0 0	34.35 + + 6 0 0 32.33 + 1 + 0 0 30.31 1 3 1 0 0	20:20 2 4 2 D 0 26:27 3 15 15 1 0 24:28 2 20 16 7 1
28.28 6 26 16 6 • 26.27 2 10 6 3 1	28.28 17 37 8 + 0 28.27 2 6 2 + 0	28,27 6 13 9 1 0 24,25 0 1 1 0 0	20:20 12 26 11 1 0 26:27 2 10 3 0 •	28.26 3 17 8 0 0 28.27 6 31 14 2 0	20.21 0 0 0 0 0
t4.f6 0 + 1 0 + tr.23 0 0 0 0 0 0	24.25 + + + 0 D 21.23 0 0 0 0 0	22.21 0 0 0 0 0 0 0 0 0	24.25 0 + 0 + 0 22.23 0 0 0 0 0	22.25 1 5 2 + + 22.25 0 0 + 0 0	10·10 0 0 0 0 0 10·17 0 0 0 0 0
10.10 0 0 0 0 0 10.10 0 0 0 0 0 0	20,21 0 0 0 0 0 0 18.18 0 0 0 0 0 0 16.17 0 0 0 0 0	10,10 0 0 0 0 0 10,17 0 0 0 0 0 0 14,18 0 0 0 0 0	20,21 0 0 0 0 0 0 19,18 0 0 0 0 0 0 18,17 0 0 0 0 0	20.21 0 0 0 0 0 0 10.19 0 0 0 0 0 0 19,17 0 0 0 0 0 0	14-18 0 0 0 0 0 0 0 0 1 10-11 0 0 0 0 0 0
14.16 0 0 0 0 0 0 802	14.16 0 0 0 0 0 0 529	12.13 0 0 0 0 0 0 449	18-17 0 0 0 0 0 0 14-18 0 0 0 0 0 0 329	14.16 0 0 0 0 0 878	0 0 0 0 0 195
HIND SPEED (KTS) 28	HIND SPEED (KTS) 29	HIND SPEED (KTS) 30	WIND SPEED (KTS) 31	HIND SPEED (KTS) 32	HIND SPEED (KTS) 33
TEMP (PC) D-3 4-10 11-21 22-38 à 34 20-28 + + + + + D	1ERF I*C1 0-3 4-10 11-21 22-33 2 34 30-31 0 + + 0 0	7ERP (*C) 0-5 4-10 11-21 22-33 3 34	7EMP 1'C1 0-9 4-10 11-21 22-33 2 34 22-23 0 1 0 0 0	TEMP (4C) 0-9 4-10 11-21 22-33 = 34	TEMP 1451 0-3 4-10 11-21 22-33 2 34 ,
24.25 1 9 12 3 +	20.29 + 1 1 + 0 26.27 1 4 6 1 0	24.24 + 2 1 0 0 22.23 4 10 7 0 +	90.21 0 2 1 1 0 18.18 1 8 9 1 0	22.23 0 1 1 1 0 20.21 1 6 5 1 0	22,83 0 + + 0 0 1 1 + +
22.23 3 16 18 6 1 20.21 2 7 7 3 1 10.10 4 2 2 1 +	24.28 2 0 17 4 + 22.23 2 10 15 7 1 20.21 + 4 11 2 +	20,21 4 17 11 1 0 10.10 3 10 6 + 0 16.17 1 6 3 + 0	18.17 2 21 18 4 0 14.18 1 7 12 3 0 18.19 1 2 4 2 0	10.10 1 13 17 4 0 10.17 1 12 22 6 1 10.18 0 2 3 1 1	18,17 3 17 19 4 1 14,18 2 11 12 4 1
10-17 + • 0 0 0 0 14-18 0 0 0 0 0 0	18.18 0 + 2 1 0 18.17 0 0 0 0 0	14.16 0 1 + 1 0 12.13 0 0 0 0 0	10.11 0 0 + 0 0 0.0 U 0 C 0 0	12.13 0 + + 0 0 10.11 0 0 0 0 0	18:13 · 2 3 1 · 10:11 0 · · · 0 · .
12.13 0 0 0 0 0 0 10.11 0 0 0 0 0 0	14.16 0 0 0 0 0 0 12.13 0 0 0 0 0 0 10.11 0 0 0 0 0	10.11 0 0 0 0 0 0 0.0 0 0 0 0 0 0 0.7 0 0 0 0 0 0	6.7 0 0 0 0 0 0 4.8 0 0 0 0 0 0 2.3 0 0 0 0 0	8.8 0 0 0 0 0 0 8.7 0 0 0 0 0 0 4.6 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
2043	918	331	262	740	1874
WIND SPEED (KTS) 37	WIND SPEED (KTS) 38	HIND SPEED (KTS) 39			MIND SPEED (KTS) 42
#0.21 0 + + + 0	22.23 + 0 0 0 0 0 20.21 + + + + 0	TEMP (#C) 0-3 4-10 11-21 22-33 2 34 14-16 + 0 0 + 0 12-13 + + 2 4 1	18-19 0 0 2 0 0 10-11 1 1 4 3 1	10:10 0 + 0 0 0 10:17 1 1 4 + 0	10.19 0 1 0 0 0 16.17 + 1 0 0 0
16.17 + 2 4 3 1 14.16 + 4 6 5 1	18.10 + 1 2 2 + 18.17 + 3 7 6 1	10.11 1 2 9 11 1 8.8 1 4 10 12 3	0.0 2 10 11 10 1 0.7 1 6 18 17 1	14.16 2 6 13 3 1 12.13 1 14 21 10 5	14.15 + 6 5 1 0 12.13 2 5 15 8 0
18.13 + 5 9 5 2 10.11 + 6 8 5 2	14.15 1 6 12 8 3 12.15 1 4 10 8 4	4.5 0 2 3 3 1	4.8 0 1 5 5 2 2.3 0 0 0 0 0 0	10.11 1 4 8 5 2 0.0 0 0 1 0 0	10.11 1 4 13 10 6 6.8 0 1 6 6 1
10.11	10.11 + 1 B 4 4 0.0 0 + 2 3 1 6.7 0 0 + + +	8.9 0 0 + 0 U 0.1 0 0 0 0 0 -21 U 0 0 0 0	4.4 0 1 5 5 2 2.3 0 0 0 0 0 0 0.1 0 0 0 0 0 0 -21 0 0 0 0 0 0 -43 0 0 0 0 0 0 -57 0 0 0 0 0 0	0.0 0 0 1 0 0 0 0 0 0	6.7 0 0 0 0 1 4.8 0 0 0 0 0 0 2.3 0 0 0 0 0
2.3 0 0 0 0 0 0.1 0 0 0 0 0	4.6 0 0 0 0 0 0 2.3 0 0 0 0 0 0	-43 0 0 0 0 0 0 -68 0 0 0 0 0	-43 0 0 0 0 0 0 0 0 0 -87 0 0 0 0 0 0 0	0.1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
928	856	484	113	309	248

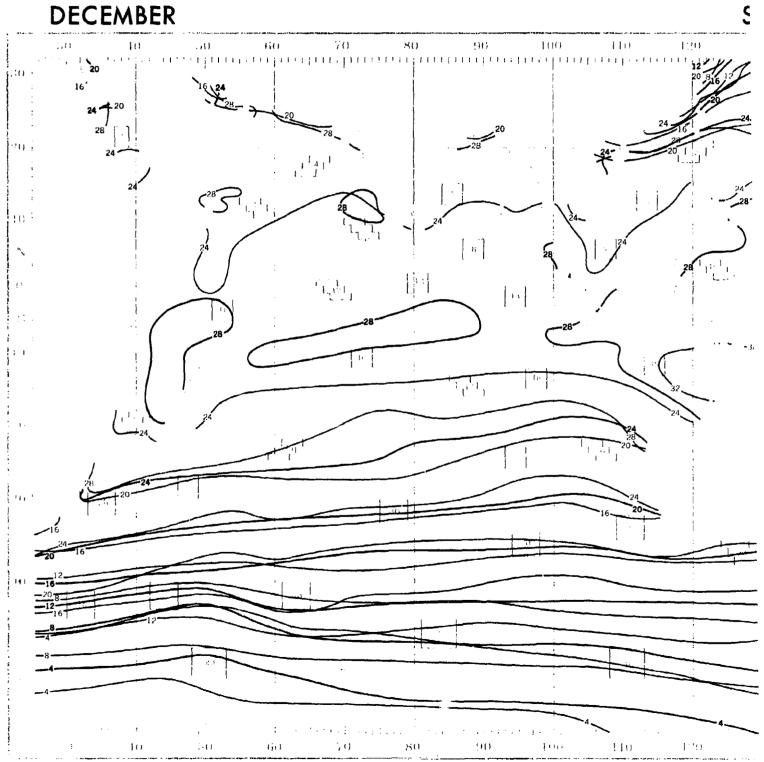
<u>Graphs</u> represent the objective compilation of available data for specified areas without reg The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjusted

ERATURE

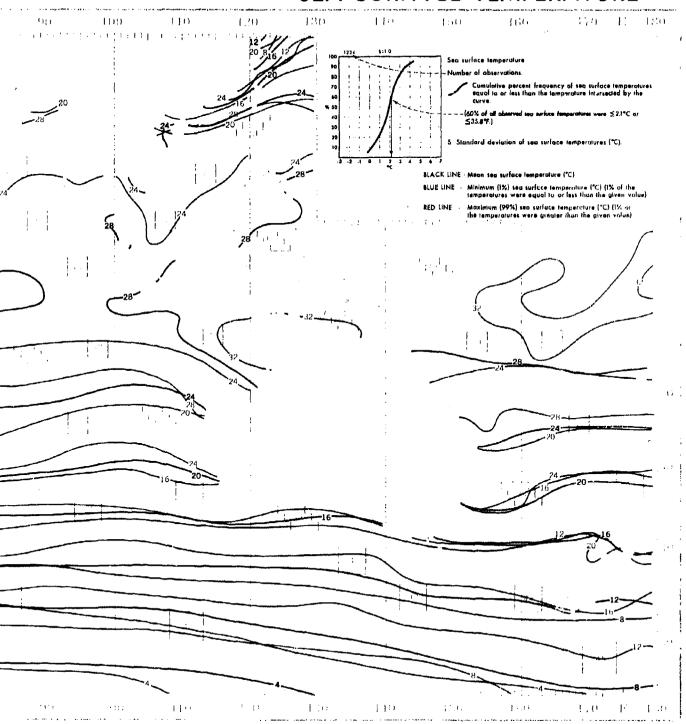
DECEMBER

HIND SPEED (HTS) 4	NIND SPEED (KTS) 5	WIND SPEED (KTS) 6	WIND SPEED (KTS)	WIND SPEED (KIS)	HIND SPEED (KTB)
	TEMP (*C) 0-9 4-10 11-81 22-23 2-34	TEMP (*C) 0-3 4-10 11-21 22-33 4 34		TEMP (*C) 0-8 4-10 11-21 22-33 a 34	
32.33 0 0 + 0 0 30.31 0 1 + 0 0 78.29 1 5 3 + 0	20:31 0 + + 0 0 28:28 + 7 7 1 0 28:27 1 24 38 5 +	34.35 0 + + 0 32.35 + + 1 + 0 30.31 + 1 3 + 0	34:38 0 + 0 0 0 32:33 + + + 0 0 30:31 1 2 1 0 U	34.35	34.38 0 0 + 0 0 38.33 0 + + + 0
78.29 1 5 3 + 0 28.27 2 22 16 1 0 24.28 2 23 15 1 0	24.25 1 B 6 1 + 22.23 0 + + 0 0	28.24 + 3 13 3 + 28.27 + 7 30 14 1	76.28 11 28 4 + 0 26.27 16 30 4 + 0	20.29 6 20 13 1 0 20.27 9 27 13 1 +	20.20 1 7 9 1 0 20.27 3 21 31 5 4
27.23 + 4 3 + 0	20,21 0 0 0 0 0 10,19 0 0 0 0 0	24.25 + 2 10 B 1 22.23 0 + 1 + +	24.28 + 2 + + 0 22.23 + + 0 0 0	24:28 1 3 2 · 0 22:23 · · · 0 0	24,28 1 6 9 2 + 22,23 4 + + + 0
10.10 0 0 0 0 0	18:17 0 0 0 0 0	19.19 0 0 0 0 0	20.21 O O O O O O O O	10.10 0 0 0 0 0	20.21 0 0 0 0 0
14-15 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	14.15 0 0 0 0 0 0 17.13 0 0 0 0 0 10.11 0 0 0 0 0	18-17 0 0 0 0 0 0 14-16 0 0 0 0 0	16.17 0 0 0 0 0 0 14.18 0 0 0 0 0	18.17 0 0 0 0 0 14.18 0 0 0 0 0	16.17 D O O O O
1075	817	5688	7453	4714	4576
WIND SPEED (KTS) 13 EHP (*C: 0-3 4-10 11-21 22-33 23-34	HIND SPEED (KTS) 14	NIND SPEED (KTS) 15	WIND SPEED (KTS) 16		NIND SPEED (KTS) 18
32.33 0 + + 0 0	32,33 1 + 0 0 0	94.95 1 4 0 0 0	32,33 0 1 + 0 0	30,21 0 1 1 0 0	30.31 + 1 1 0 0
90.31 2 2 1 1 0 20.28 9 27 6 + 0	30:31 3 5 2 0 0 20:20 14 22 6 0 0	38.33 3 + 0 0 30.31 6 6 1 0 0	30.3i 1 3 1 0 0 20.20 5 24 13 0 0	28.29 0 5 12 2 + 28.27 + 14 39 6 +	28.27 2 16 36 5 0
28:27 12 24 10 1 0 24:28 1 4 1 + 0 27:23 0 + 0 0 0	24.25 1 2 10 1 0 24.25 1 3 2 1 4 22.23 0 0 0 0 0	20:20 10 31 7 + 0 20:27 6 11 4 1 4 24:28 + 1 1 0 0	28.27 6 26 15 1 0 24.25 1 2 1 1 0	24.25 + 5 12 2 + 22.23 0 0 + 0 0 20.21 0 0 0 0 0	24.25 1 7 12 3 + 22.23 0 + + + 0 20.21 0 0 0 0 0
27.23 0 + 0 0 0 20.21 0 0 0 0 0 10.10 0 0 0 0 0	20.21 0 0 0 0 0 0 10.10 0 0 0 0 0	24.28 + 1 1 0 0 22.23 0 0 0 0 0 0 20.21 0 0 0 0 0	#2.23 0 0 0 0 0 0 #0.21 0 0 0 0 0	10.11 0 0 0 0 0 0 10.10 0 0 0 0 0 0 10.17 0 0 0 0 0	10:10 0 0 0 0 0 10:10 0 0 0 0 0 16:17 0 0 0 0 0
18.17 0 0 0 0 0 0 14.18 0 0 0 0 0 0	16.17 0 0 0 0 0 0 14.16 0 0 0 0 0 0	10.10 0 0 0 0 0	18-17 0 0 0 0 0 0 14-18 0 0 0 0 0 0	14.15 0 0 0 0 0 12.13 0 0 0 0 0	14:15 0 0 0 0 0 12:13 0 0 0 0 0
12-13 0 0 0 0 0	12.13 0 0 0 0 0	14-18 0 0 0 0 0	12:13 0 0 0 0 0	10.11 0 0 0 0	10.11 0 0 0 0 0
WIND SPEED (KTS) 22	WIND SPEED (KTS) 23	HIND SPEED (KTS) 24	WIND SPEED (KTS) 25	HIND SPEED IKTS: 26	HIND SPEED (KTS) 27
the (40) 0-9 4-10 11-21 22-33 a 34	TEHP (*C) 0-3 4-10 11-21 22-33 4 34	TEMP (*C) 0-9 4-10 11-8188-39 2 34	TERP 1*C1 0-5 4-10 11-21 22-33 3 34	TEMP (*C) 0-3 4-10 11-8188-33 a 34	1EMP (*C) 0-3 4-10 11-21 22-33 34
34.38 1 1 0 0 0 32.33 3 7 1 0 0	34.95 + + + 0 0 32.33 + 1 + 0 0	#8.#8 2 4 2 0 0 #8.#7 3 13 15 1 0	26,27 0 1 1 + 0 24,25 1 6 8 4 0	29.27 0 1 1 + 0	20.21 + 0 0 0 0 20.22 + 1 1 0 0
90.91 6 12 3 0 0 20.98 12 28 11 1 0	30.31 1 3 1 0 0 20.29 3 17 8 0 0	24.26 2 20 16 7 1 22.23 1 5 5 2 3	20.21 1 5 23 4 0	24,25 1 4 7 + 0 21,23 1 14 27 8 0	#8-27 Z 10 7 0 0 #4-28 3 18 15 1 0 #2-23 3 17 16 2 +
28:27 2 10 3 0 + 24:28 0 + 0 + 0 22:23 0 0 0 0 0	28.27 6 31 14 2 0 24.25 1 6 2 + + 27.23 0 0 + 0 0	##: 423	18.17 0 0 0 0 0 0 14.15 0 0 0 0 0	20,21 + 8 20 4 0 18,18 0 1 1 1 0 18,17 0 0 0 0 0	#2.23 3 17 16 2 + #0.21 0 2 3 + 0
20.21 0 0 0 0 0 0 0 1 10.10 0 0 0 0 0	20.21 0 0 0 0 0 10.10 0 0 0 0 0	14-16 0 0 0 0 0	12:13 0 0 0 0 0 10:11 0 0 0 0 0	14-15 O O O O O O O O	18-17 0 0 0 0 0
18:17 0 0 0 0 0 14:18 0 0 0 0 0	16.17 0 0 0 0 0 14.16 0 0 0 0 0	10.11 0 0 0 0 0 0 1.9 0 0 0 0 0 0	8.9 0 0 0 0 0 6.7 0 0 0 0 0	10.11 0 0 0 0 0 0 10.11 0 0 0 0 0 0	12.13 0 0 0 0 0 10.11 0 0 0 0 0
329	97 5	195	313	493	381
HIND SPEED (MTS) 31	WIND SPEED (KTS) 32	HIND SPEED (KTS) 33	WIND SPEED (KTS) 34		NIND SPEED (KTS) 36
22.29 0 1 0 0 0	TEMP (*C) 0-3 4-10 (1-21 22-33 2 34)	24.25 0 + 0 0 0	26.27 0 0 + 0 0	20.27 + 1 0 0 0	20.21 0 0 + + 0
20:21 0 2 1 1 0 10:10 1 6 9 1 0	22,23 0 1 1 1 0 20,21 1 6 5 1 0	82.83 0 + + 0 0 80.81 + 1 1 + +	21.25 + 1 1 1 0 22.23 1 6 10 3 +	24.25 0 1 1 0 0 22.23 3 8 3 0 0	10:10 0 1 + + + 10:17 0 2 3 1 +
16.17 2 21 16 4 0 14.16 1 7 12 3 0	18.17 1 13 17 4 0 18.17 1 12 22 6 1	10.10 1 7 7 1 + 18.17 3 17 19 4 1	20.21 2 12 14 3 1 18.10 2 14 14 2 1	20.21 3 17 14 2 + 10.10 3 16 13 3 0	14.18 1 4 6 4 1 12.13 1 7 12 7 2
19.19 1 2 4 2 0 10.11 0 0 + 0 0	14.16 0 2 3 1 1 16.13 0 + + 0 0 10.11 0 0 0 0 0	14.18 2 11 12 4 1 12.13 + 2 3 1 + 10.11 0 + + 0 +	18:17 + 6 3 2 0 14:18 0 0 + 0 0 12:19 0 0 0 0 0	10-17 2 4 4 2 + 14-18 0 0 + 0 0 12-13 0 0 0 0 0	10·11 1 4 9 9 2 6.8 1 2 5 6 2 6.7 0 1 2 2 1
#.0 0 0 0 0 0 #.7 0 0 0 0 0 0 4.8 0 0 0 0 0 0	0.0 0 0 0 0	0.0 0 0 0	10:11 0 0 0 0	10.11 0 0 0 0 0 10.11 0 0 0 0 0 0.9 0 0 0 0 0	0.7 0 1 2 2 1 4.8 0 0 + + + 2.8 0 0 0 0 0 0
8.3 0 0 0 0 0 0 282	9.7 0 0 0 0 0 1.6 0 0 0 0 0	6.7 0 0 0 0 0 4.8 0 0 0 0 0 0	6.7 0 0 0 0 0 6.7 0 0 0 0 0	0.7 0 0 0 0 0	0.1 0 0 0 0 0
, HIND SPEED (KTS) 40	HIND SPEED (KTS) 41	HIND SPEED (KTS) 42	HIND SPEED (KTS) 43	HIND SPEED (KTS) 44	HIND SPEED (KTS) 45
MF (*C) 0-3 4-10 11-81 88-33 a 34	TEMP 1401 0-3 4-10 11-81 28-33 2 34	TENF (*C) 0-3 4-10 11-2122-33 4 34	TEHP (40) 0-9 4-10 11-2122-38 2 34	TEMP (*C) 3-9 4-10 11-2122-99 2 94	TEMP (*C) 0-3 4-10 11-2122-33 & 34
19:13 0 0 2 0 0 10:11 1 1 4 3 1	19:19 0 + 0 0 0 16:17 1 1 4 + 0	19.19 Q 1 0 0 0 19.17 + 1 0 0 0 14.18 + 6 8 1 0	19,10 0 1 + 0 0 19,17 0 1 3 + 0	10.11 0 0 0 2 1 10.11 0 0 0 2 0	14.18 0 0 2 1 0 12.13 1 5 4 3 0
6.7 1 6 18 17 1	12.19 1 14 21 10 5	18.13 2 8 15 8 0	18,19 1 15 21 8 2	6.7 0 4 10 5 1	10.11 1 9 23 9 1 0.9 + 4 14 12 1 5.7 0 1 4 3 2
9.5 0 1 5 5 2 2.3 0 0 0 0 0 0 0.1 0 0 0 0 0	0.0 0 0 0 0	10.31 1 4 13 10 6 1.0 0 1 6 6 1 1.7 0 0 0 0 1	10.11 • 6 7 5 4 9.9 1 0 1 3 1 6.7 0 0 0 0 1	4.5 0 7 18 14 5 2.3 0 1 6 7 0 0.1 0 0 0 0 0	4.5 0 0 0 1
-21 0 0 0 0 0 -43 0 0 0 0 0	6.7 0 0 0 0 0 1.6 0 0 0 0 0 2.3 0 0 0 0 0	4.8 0 0 0 0 0 0 2.3 0 0 0 0 0	4.6 0 0 0 0 0	-t1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2:3 0 0 0 0 0 0:1 0 0 0 0 0 -2:-1 0 0 0 0 0
-06 0 0 0 0 0 -07 0 0 0 0 0	0.1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.1 0 0 0 0 0 -21 0 0 0 0 0	-85 0 0 0 0 0 -87 0 0 0 0 0	-49 0 0 0 0 0 -66 0 0 0 0 0
113	309	248	367	83	274

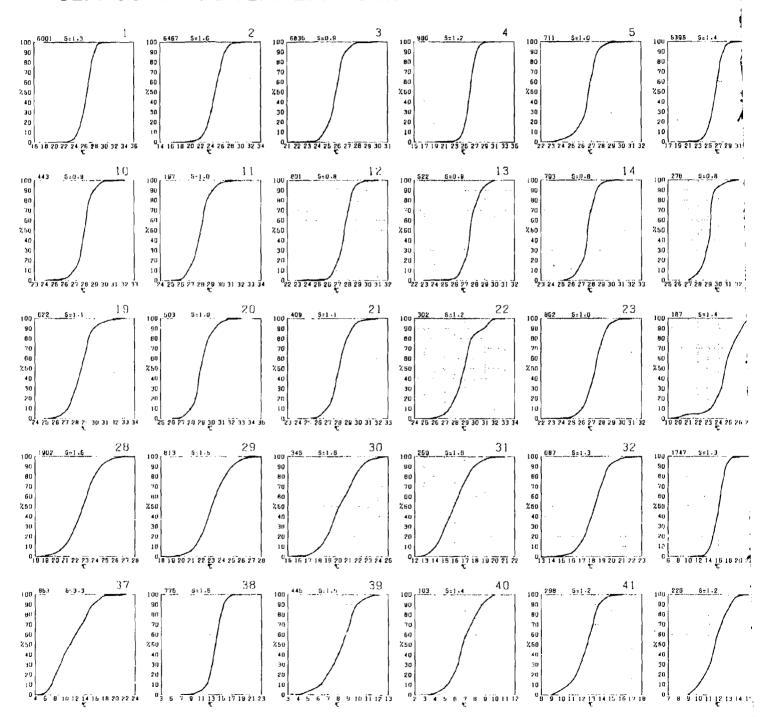
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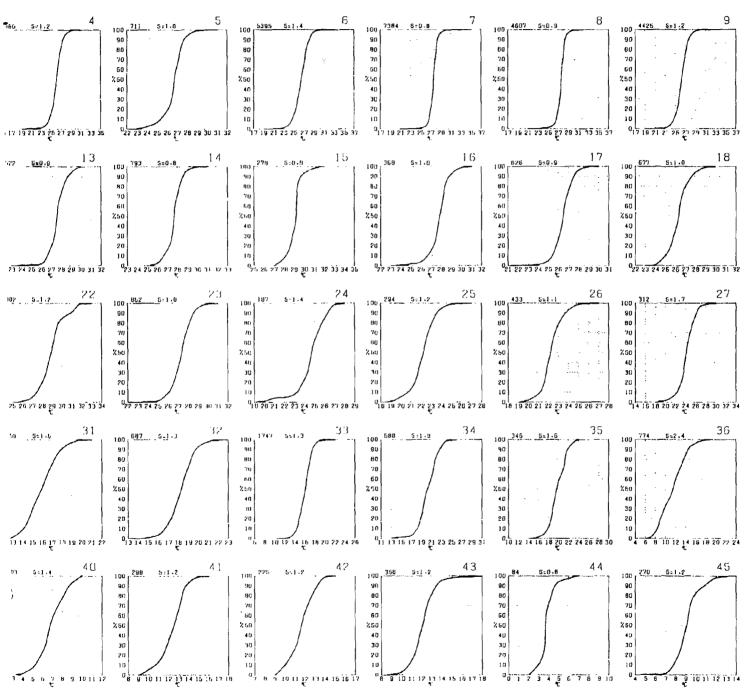
SEA SURFACE TEMPERATURE



SEA SURFACE TEMPERATURE

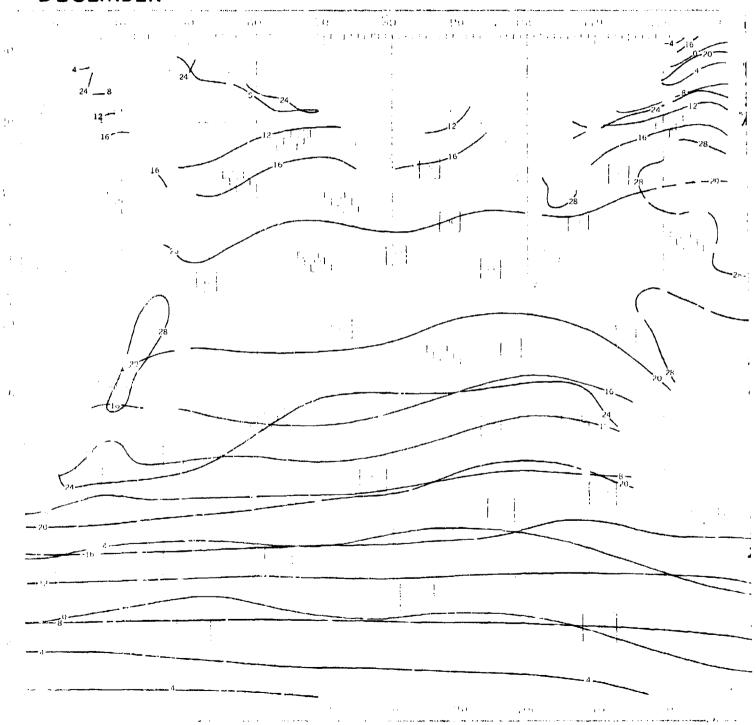


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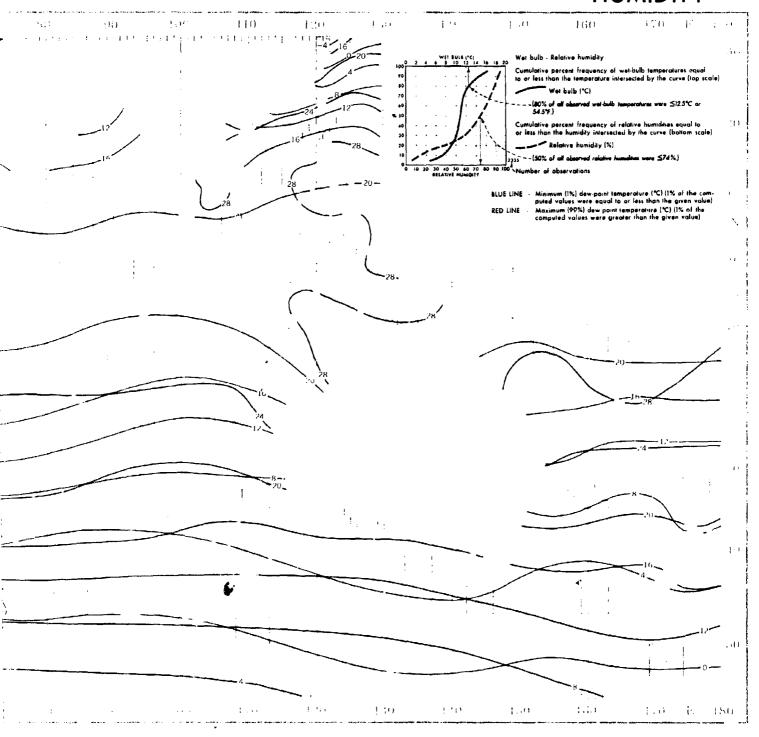


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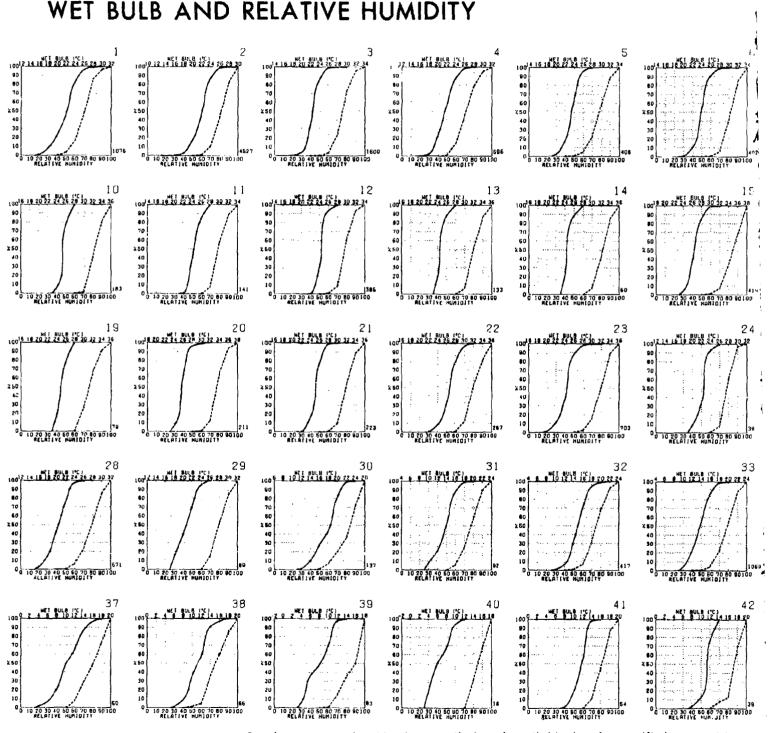
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HUMIDITY



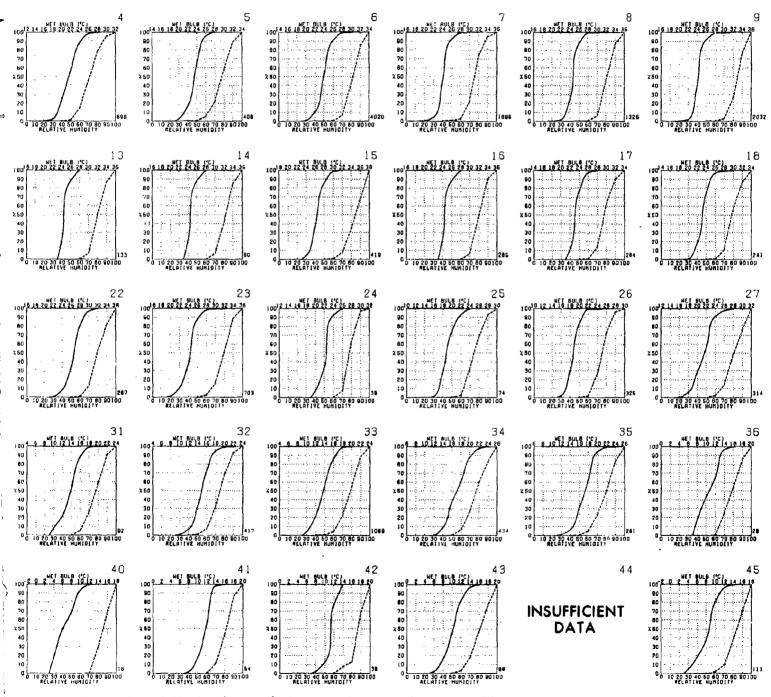
WET BULB AND RELATIVE HUMIDITY



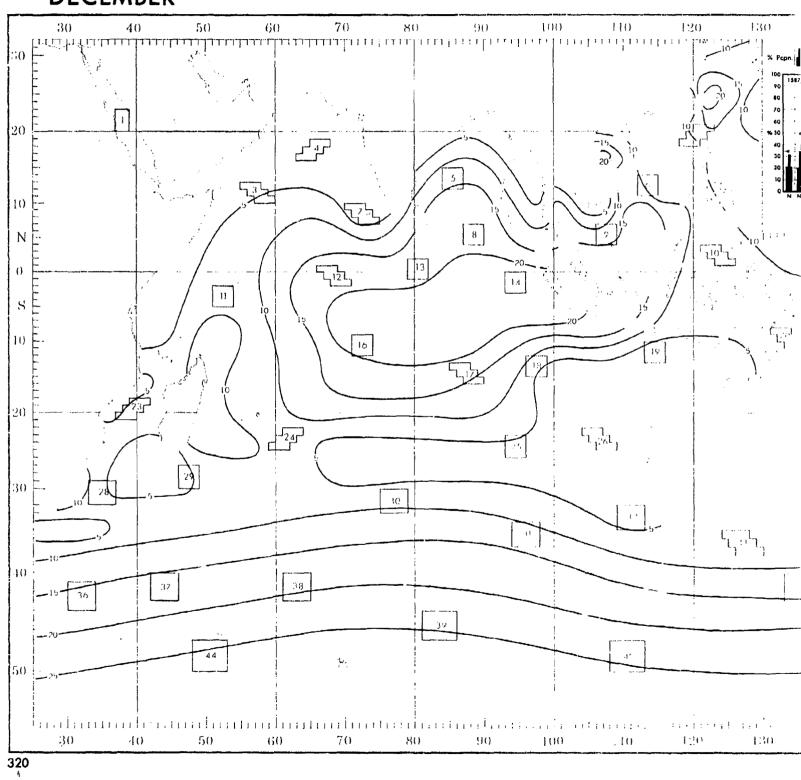
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IUMIDITY

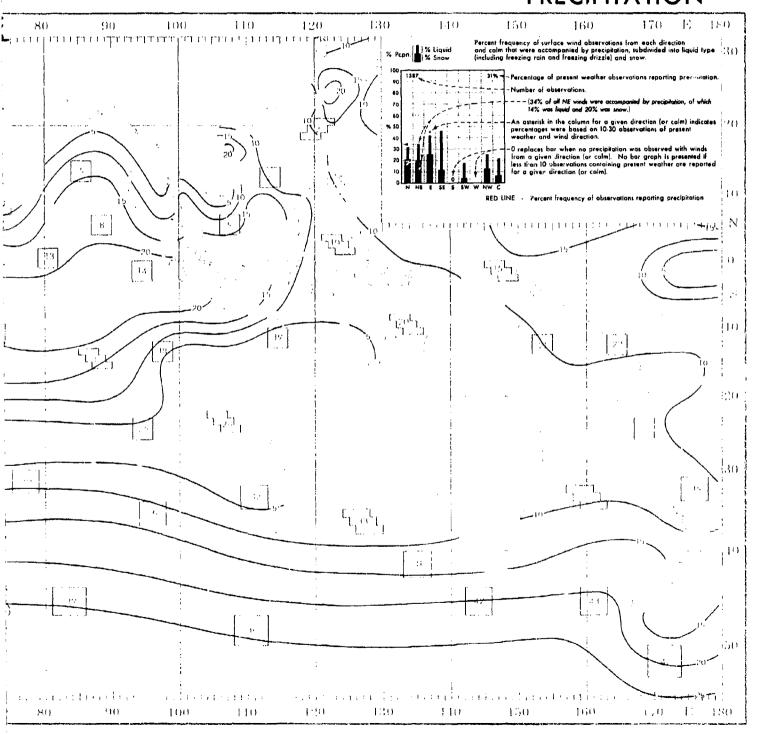
DECEMBER



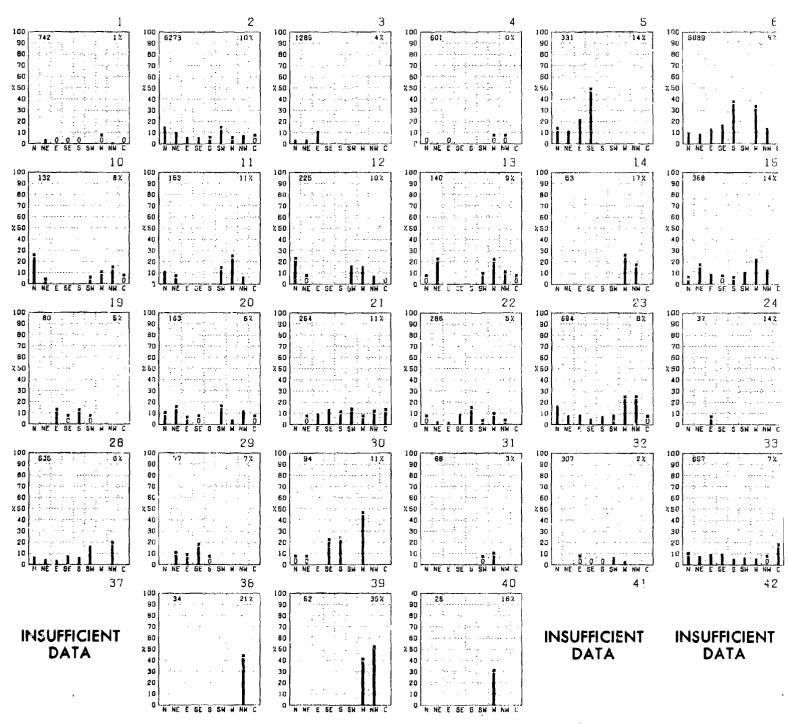
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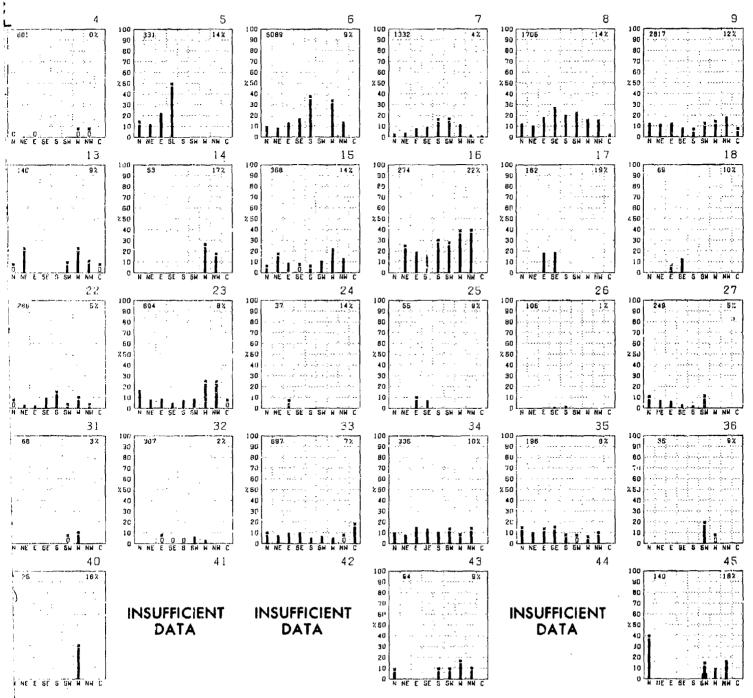
PRECIPITATION



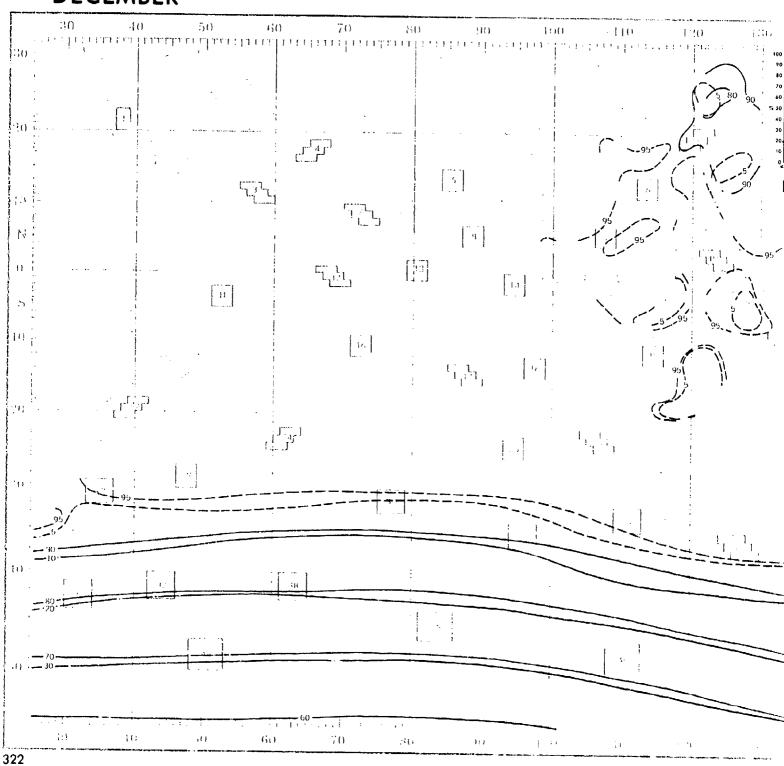
PRECIPITATION



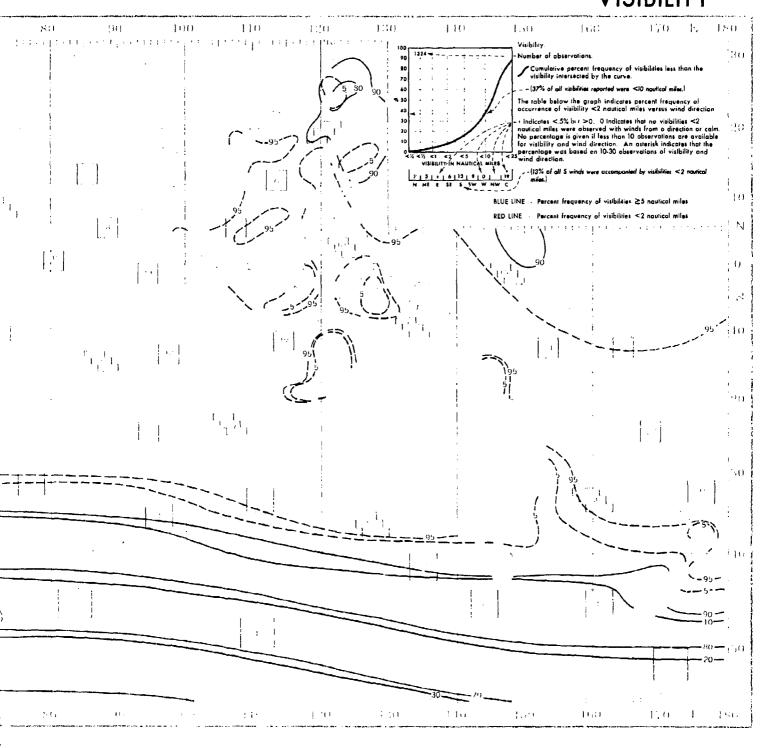
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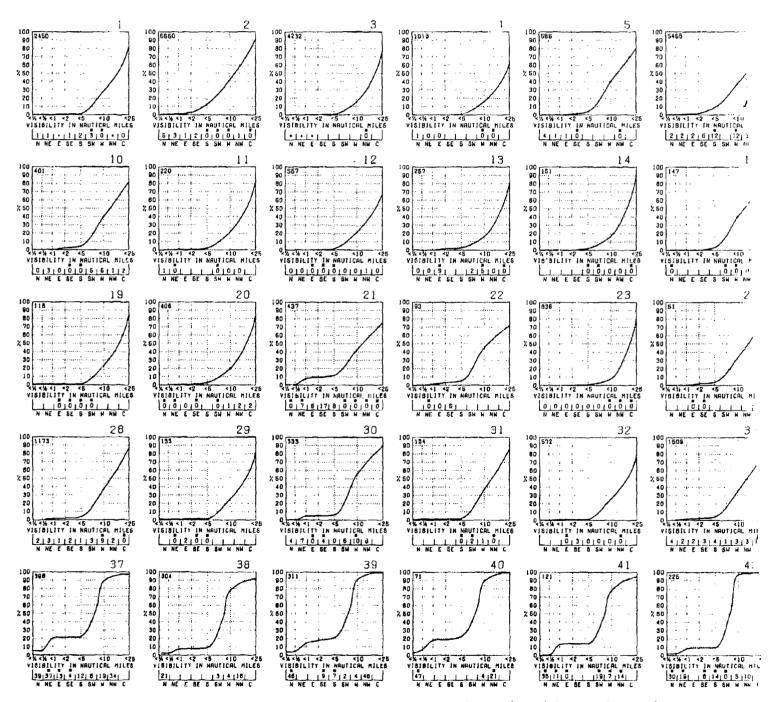
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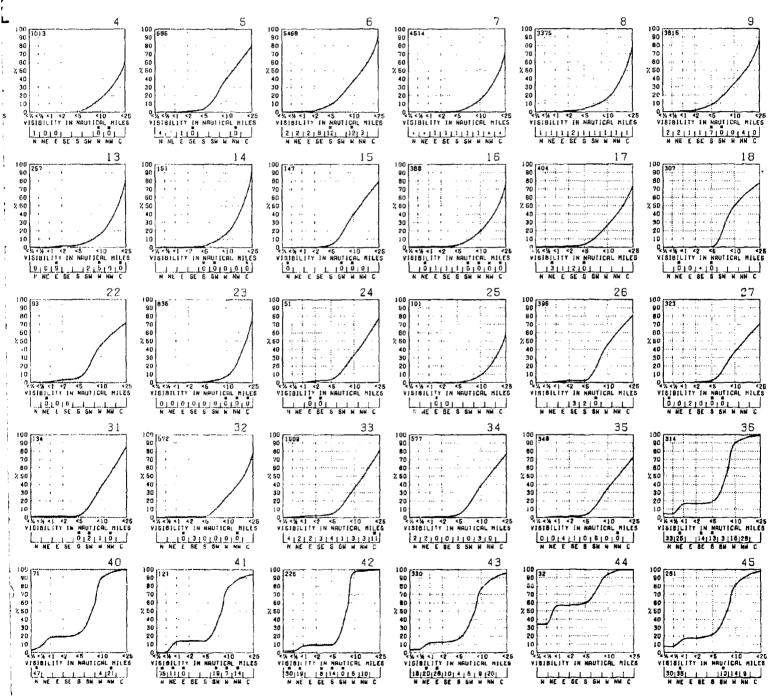
VISIBILITY



VISIBILITY



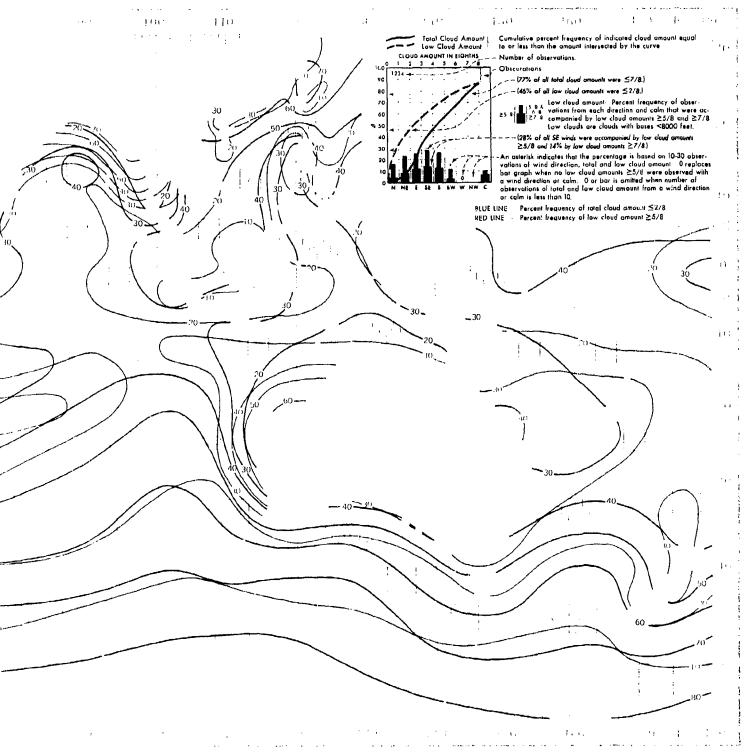
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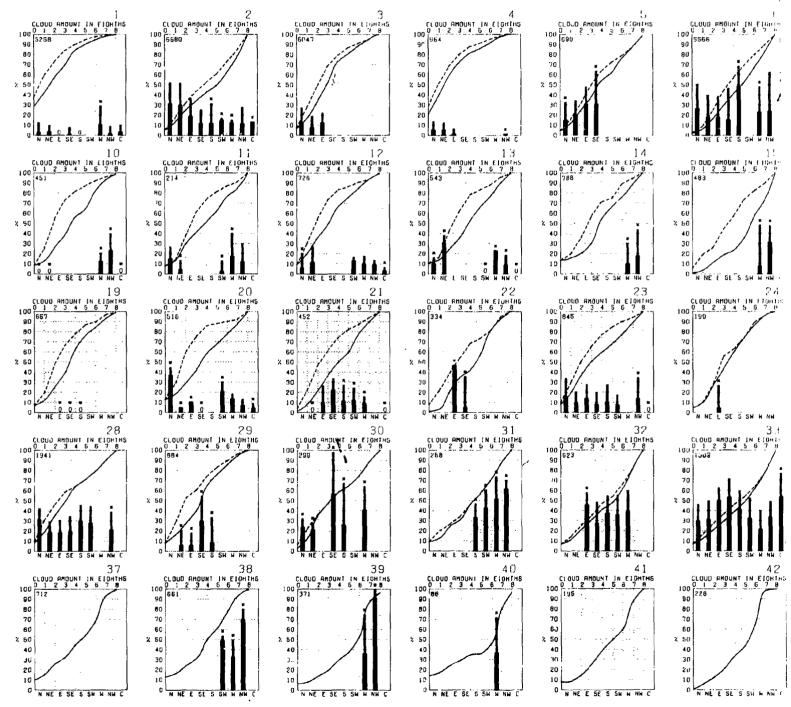
ective compilation of available data for specified areas without regard to suspected biases, posite page) are based on all available data subjectively adjusted where bias was evident.



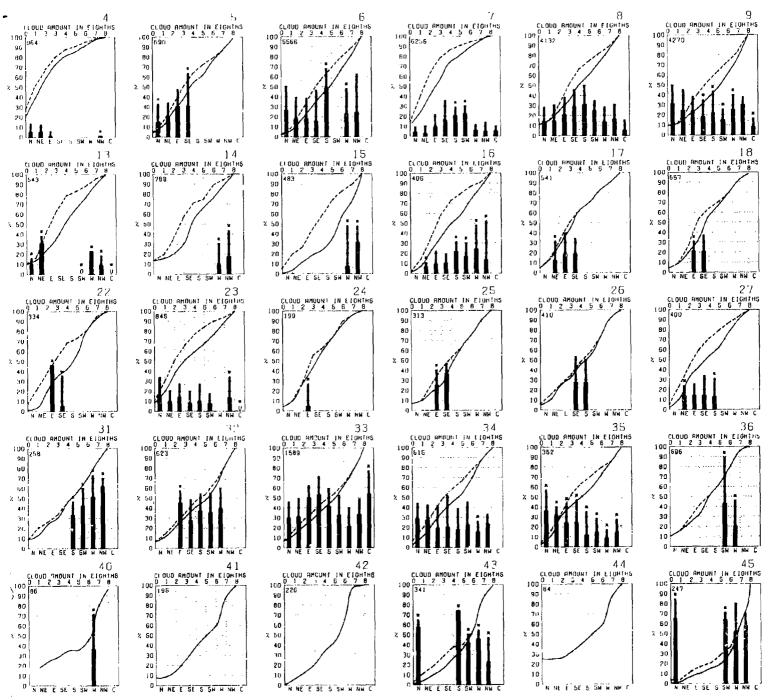
CLOUD COVER



CLOUD COVER



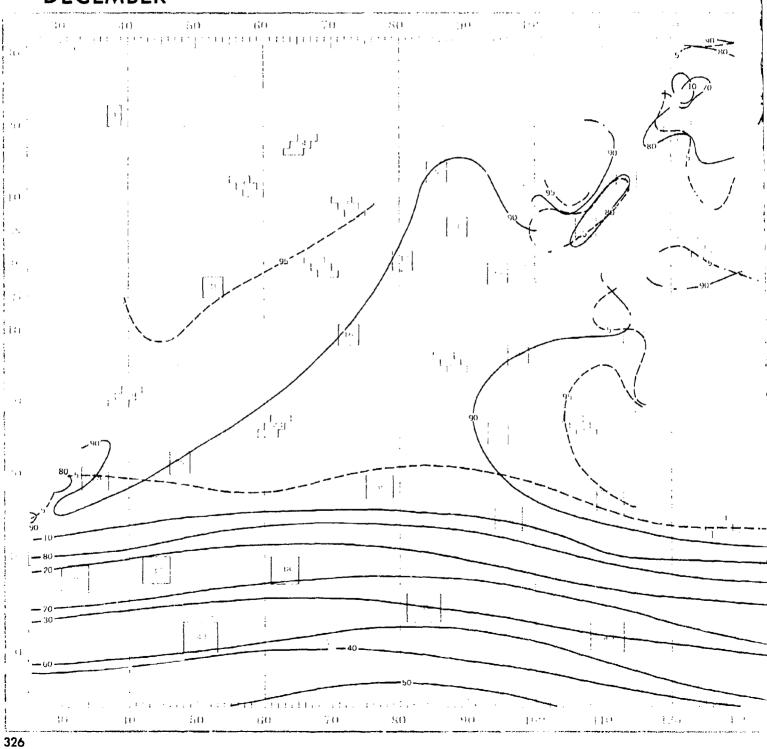
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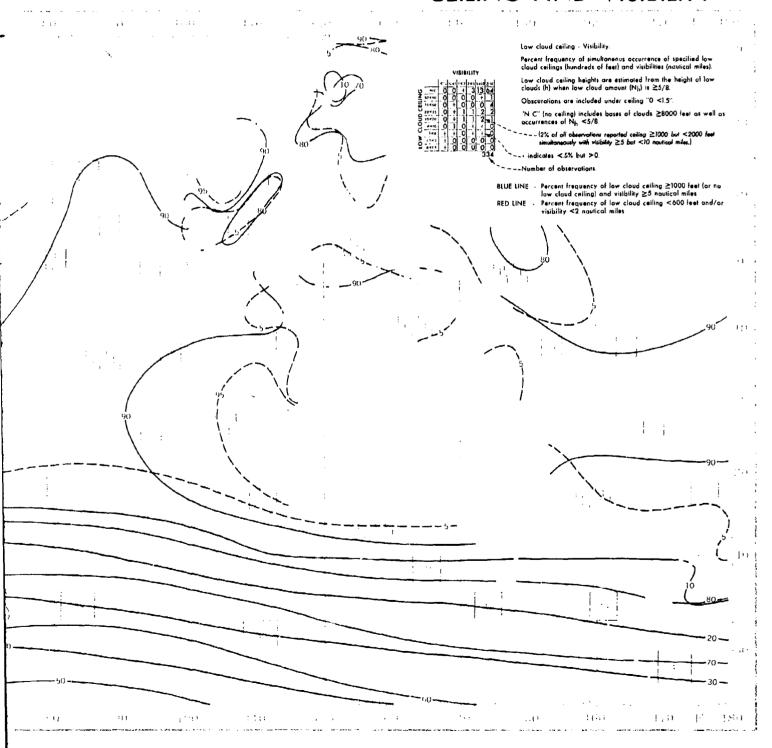
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CEILING AND VISIBILITY



CEILING AND VISIBILITY

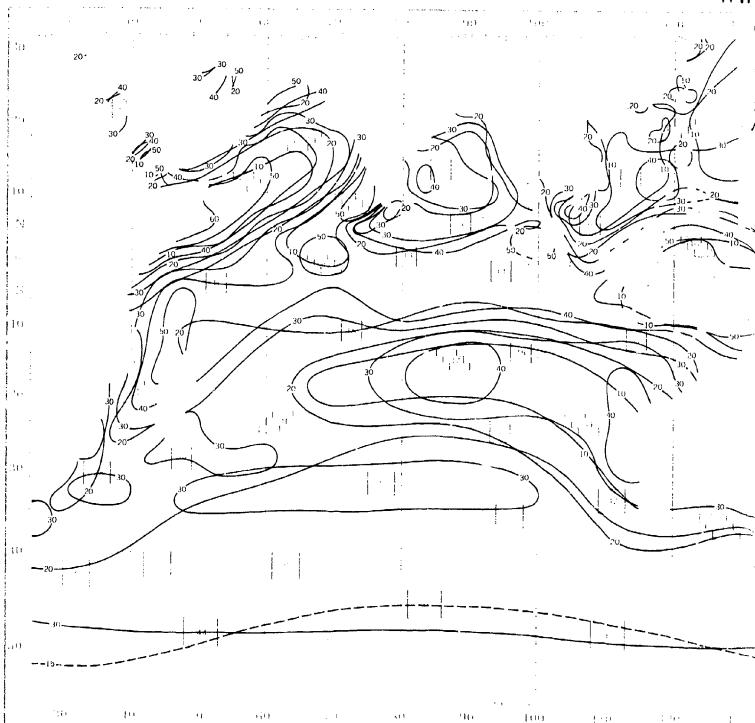
VISIBILITY 1	VISIBILITY	VISIBILITY 3 **C 0 0 0 0 0 0 1 1 **South 0 0 0 0 0 0 1 1 **South 0 0 0 0 0 0 1 5 **South 0 0 0 0 0 0 1 5 **South 0 0 0 0 0 0 1 5 **South 0 0 0 0 0 0 1 5 **South 0 0 0 0 0 1 5 **South 0 0 0 0 0 1 5 **South 0 0 0 0 0 1 5 **South 0 0 0 0 0 1 5 **South 0 0 0 0 0 1 5 **South 0 0 0 0 0 1 5 **South 0 0 0 0 0 0 1 5 **South 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 **South 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY VISIBILITY 4 1-10	VISIBILITY	VISIBILITY (-1)#
VISIBILITY *1/2 7/2 1/2 1/2 8/2 8/2 1/2 1/2	WISIBILITY 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	VISIBILITY 1 2	VIGIBILITY 1 3 **In *In	VISIBILITY 1 4 ***	VISIBILITY
VISIBILITY 416 PA1 141 E 248 B 10 B 10 BE 0 0 0 0 0 0 2 74 60480 0 0 0 0 0 0 0 34480 0 0 0 0 0 0 2 8 BE 10400 0 0 0 0 0 0 6 6410 2 0 0 0 0 3 2 3480 0 0 0 0 0 0 0 6 6410 2 0 0 0 0 0 0 0 1.843 0 0 0 0 0 0 0 61.843 0 0 0 0 0 0 0 62.65	VISIBILITY 20	VISIBILITY 2 1 **C 0 0 0 1 1 6 67 **B0440 0 0 0 0 1 0 1 **B0480 0 0 0 0 1 0 1 **B0480 0 0 0 0 1 0 1 **B0480 0 0 0 0 1 1 7 **B0480 0 0 0 0 1 1 7 **B0480 0 0 0 0 1 1 7 **B0480 0 0 0 0 1 1 7 **B0480 0 0 0 0 1 1 1 7 **B0480 0 0 0 0 0 1 1 1 **B0480 0 0 0 0 0 1 1 1 **B0480 0 0 0 0 0 1 1 1 **B0480 0 0 0 0 0 1 1 1 **B0480 0 0 0 0 0 1 1 1 **B0480 0 0 0 0 0 1 1 1 **B0480 0 0 0 0 0 1 1 1 **B0480 0 0 0 0 0 0 1 1 1 **B0480 0 0 0 0 0 0 0 1 1 **B0480 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY 22 -1/a	VISIBILITY **/**	VISIBILITY
VISIBILITY 28 **In	VISIBILITY 29	VISIBILITY ACC 0 0 0 1 1 1 61 50490 0 0 0 0 0 1 3 50490 0 0 0 0 0 0 1 3 50490 0 0 0 0 0 0 5 50490 0 0 0 0 0 0 1 3 50490 0 0 0 0 0 0 5 50490 0 0 0 0 0 0 0 1 50490 0 0 0 0 0 0 0 5 50490 0 0 0 0 0 0 0 0 5040 0 0 0 0 0 0 0 0 5040 0 0 0 0 0 0 0 5040 0 0 0 0 0 0 0 5040 0 0 0 0 0 0 0 5040 0 0 0 0 0 0 0 5040 0 0 0 0 0 0 0 5040 0 0 0 0 0 0 0 5040 0 0 0 0 0 0 0	VISIBILITY 3 1	VISIBILITY 32 ***********************************	VISIBILITY -1/4 P/4-1] 1-2 P4-6 B4-10 MC 0 0 0 0 1 2 50-60 0 0 0 0 0 1 55-50 0 0 0 0 0 1 67 00-96 0 0 0 0 0 1 67 00-96 0 0 0 0 0 1 68 10 0 0 0 0 1 70 10-90 0 0 0 1 70 10-90 0 0 0 0 1 70 10-90 0 0 0 0 0 71 10-90 0 0 0 0 0 71 10-90 0 0 0 0 0 71 10-90 0 0 0 0 0 71 10-90 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 0 0 0 0 0 0 71 10-90 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
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Graphs represent the objective compilation of available data for specified areas without The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjust

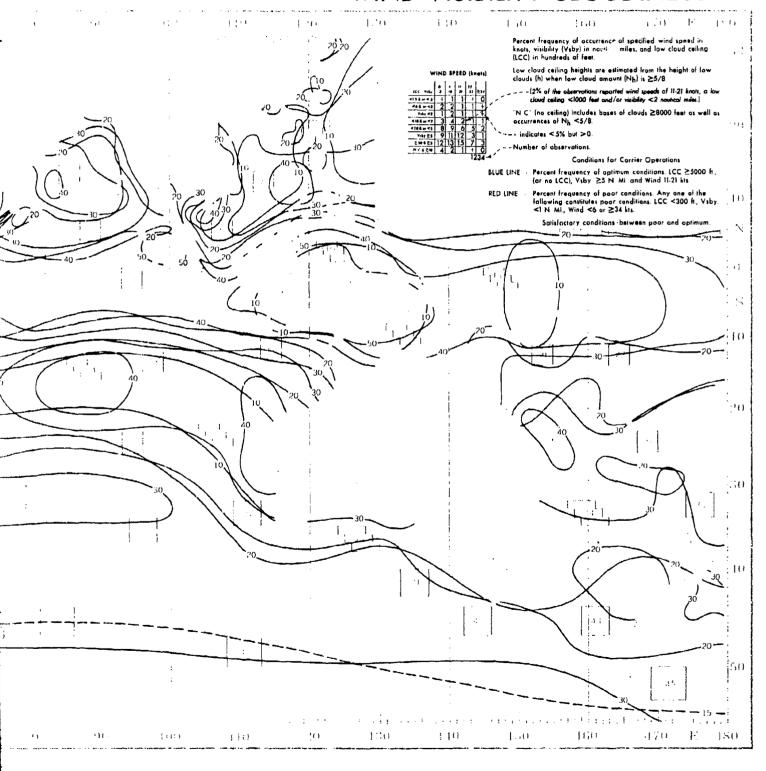
VISIBILITY 4 1/19 74+11 1-2 2+8 8-10 10 MC 0 0 0 0 1 4 86 50-60 0 0 0 0 0 0 1 1 1 35-50 0 0 0 0 0 0 3 3 2 20-38 0 0 0 0 0 0 2 2 0 10-20 0 0 0 0 0 0 1 5 346 0 0 0 0 0 0 0 1 5 346 0 0 0 0 0 0 0 0 1 5-3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY 5 **********************************	VISIBILITY RC 0 0 0 1 1 14 43 50-60 0 0 0 0 0 0 0 50-60 0 0 0 0 0 0 0 20-35-60 0 0 0 0 1 1 3 4 0-0-10 0 0 0 0 1 7 9 6-10 0 0 0 0 1 7 9 6-10 0 0 0 0 0 0 0 1-6-3 0 0 0 0 0 0 0 1-6-3 0 0 0 0 0 0 0 1-6-3 0 0 0 0 0 0 0 1-6-3 0 0 0 0 0 0 0 1-6-3 0 0 0 0 0 0 0 1-6-3 0 0 0 0 0 0 0 0 1-6-3 0 0 0 0 0 0 0 0 1-6-3 0 0 0 0 0 0 0 0 1-6-3 0 0 0 0 0 0 0 0 0 1-6-3 0 0 0 0 0 0 0 0 0 0 1-6-3 0 0 0 0 0 0 0 0 0 0 1-6-3 0 0 0 0 0 0 0 0 0 0 0 1-6-3 0 0 0 0 0 0 0 0 0 0 0 0 1-6-3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY	VISIBILITY	VISIBILITY 9
VISIBILITY 1 3 ** ** ** ** ** * **	VISIBILITY 1 4	VISIBILITY -1/2 V/41 1-2 U-6 6-10 10 -1/2 V/41 1-2 U-6 6-10 10 -1/2 V/41 1-2 U-6 6-10 10 -1/2 U-6 10 10 0 0 0 -1/2 U-6 10 10 0 0 0 -1/2 U-6 10 10 0 0 0 -1/2 U-6 10 10 0 0 0 -1/2 U-6 10 10 0 0 0 -1/2 U-6 10 10 0 0 0 -1/2 U-6 10 10 0 0 0 -1/2 U-6 10 10 0 0 0 -1/2 U-6 10 0 0 0 0 -1/2 U-6 10 0 0 0 0 -1/2 U-6 10 0 0 0 0 -1/2 U-6 10 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 0 0 0 -1/2 U-6 10 0 0 0 0 0 0 0 0	VISIBILITY 16/2 PARE 1 et 2 e 5 e 10 10 16 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 1 1 1 1 1 1 1 1 1	VISTBILL 17 1 8
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VISIBILITY 31	VISIBILITY 32 -1/a P/4+1 1+2 2+8 +10 +10 -1/a P/4+1 1+2 2+8 +10 -1/a P/4+1 1+2	VISIBILITY 3 3	VISIBILITY 34 VISIBILITY 34 NC 0 0 0 1 2 57 S040 0 0 0 0 0 1 S040 0 0 0 0 0 1 S040 0 0 0 0 0 1 S040 0 0 0 0 0 1 S040 0 0 0 0 0 1 S040 0 0 0 0 0 0 1 S040 0 0 0 0 0 0 1 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 S040 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	VISIBILITY 35	VISIBIL TY 3 6
Y1818JLITY 4 () **\text{**} *\text{**} VISIBILITY 41 AC 0 0 0 0 0 0 12 BOWD 0 0 0 0 0 3 3 STANDARD 0 0 0 0 0 3 STANDARD 0 0 0 0 0 15 STANDARD 0 0 0 0 0 0 15 STANDARD 0 0 0 0 0 0 15 STANDARD 0 0 0 0 0 0 0 0 STANDARD 0 0 0 0 0 0 0 STANDARD 0 0 0 0 0 0 0 STANDARD 0 0 0 0 0 0 0 STANDARD 0 0 0 0 0 0 0 STANDARD 0 0 0 0 0 0 0 STANDARD 0 0 0 0 0 0 0 STANDARD 0 0 0 0 0 0 0 STANDARD 0 0 0 0 0 0 0	INSUFFICIENT DATA	**************************************	INSUFFICIENT DATA	VISIBILITY 45 VISIBILITY 45 VISIBILITY 45 VISIBILITY V	

ective compilation of available data for specified areas without regard to suspected biases.

Iposite page) are based on all available data subjectively adjusted where bias was evident.



WIND-VISIBILITY-CLOUDINESS



LOW CLOUD CEILING-VISIBILITY-WIND

410 4 OR +2

420 4 00 4K

V88Y 16

2 BO 4 a F

MC 4 & 10

-10 4 OR -2

100 4 08 48

V891 45

+ 60 4 15

HC 4 2 10

0 0 8 4 0

0 4 32 44 16

0 0 16

0 4 2 0 0 0 8 6 0 0 0 13 15 8 0 6 13 64 19 0 4 2 31 8 0

410 A OR 42

420 4 08 45

V887 26

- 60 4 45

MC & a 10

2 6 8 27 8

2 8 10 35 8

0 10 10 27 8

0 4 2 8 0

0 4 2 6 0

				_	i
NIND SPEED (KNOTS)	2 Wind Speed (knots)	3 HIND SPEED (KNOTS)	4 WIND SPEED (KNOTS)	5 WIND SPEED (KNOTS)	MIND SPEED :
0-14-111-122-1	10-14-121-122-1	10-14-111-122-1	0 4 11-22-	10- 4- 111-122-	lo-la-lu
#2.8 4.08 = 15 0 0 D D D		41.6 4 68 4.5 D D D D D	+1.64 DR +.6	LCC - VSBY 3 10 21 33 234	1.640k6
*8 4 OR *2 D + + O O	*# 4 OR *2 + 2 3 1	-84 OR -2 D + 1 + +	-6 4 08 42 0 0 + 0 0	*6 4 OR *2 0 • 2 1 0	75 L OR 42
V68Y -9 0 0 + 0 0	V887 42 U + 1 1 1	¥887 +2 □ □ 0 + □ □	V887 <2 0 0 0 0 0	V5B7 *2 0 0 1 1 0	V587 -7 U
*10 t 68 *2 + 1 1 0 0	<10 4 0R <2 + 1 5 B 3	*10 A GR 42 + 1 4 + +	<10 4 0R <2 D + 1 + D	-10 4 dR =? 0 2 5 2 •	-10 4 08 -2 + 1 -20 4 08 -5 + 3 15
420 4 08 45 1 2 4 · 0 Yulit a5 13 44 39 2 0	*20 4 0R 46 + 2 13 19 5 YEBY #8 1 9 36 35 6	420 4 CR 45 → 2 10 1 → V88Y >5 1 31 53 4 →	*20 & OR *5 0 2 3 + 0		
V.BT 25 13 44 39 2 0	7687 a5 1 9 36 35 6 250 4 a6 1 7 23 18 2	280 425 1 27 49 2 2	VSBY 25 6 51 41 2 0	#50 4 25 1 27 36 4 0	V\$87 ≥5 ← 11 5√7 ≥50 4 ≥5 ← 9 3 °1
MC 4 > 10 12 39 33 1 0	HC 4 > 10 1 7 19 12 1	NC 4 2 10 1 25 47 2 +	NC 6 2 10 6 44 34 1 0	ME 4 & 10 + 25 30 1 0	NC 4 3 10 + 7 2
712	5369	1287	625	307	
10	11	12	13	1 4	
WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HINO SPEED (KNOTS)	MIND SPEED (KNOTS)	WIND SPEED (KNOTS)	WIND SPEED IN
CC - Y887 3 10 21 39 234	LCC - VARY 3 10 21 33 834	LCC - VEET 3 10 2) 33 434	LCC - VARY 3 10 21 33 234	LCC - YEST 3 10 21 33 234	LCC - VERY 3 10 21
41.54.09 4.6 0 0 3 0 0	41-84084-8 0 1 1 0 0	*1.6 c 0 *** 0 0 0 0 0	41.8 & OR 4.5 D D D D D D D D D D D D D D D D D D D	<1.64 0R <.8 0 0 0 0 0 0 0 <64 0R <2 0 4 2 0 0	<1.5 4 0H + .B
V887 <2 0 0 0 0 0	V8AY 42 0 0 1 0 0	V887 42 U O O O O	V S P P P P P P P P P P P P P P P P P P	V88T 42 0 0 0 0 0	VSSY 42 0 0 1
110 4 0R -2 1 4 3 D D	410 4 0R 42 0 5 3 0 0	*10 L OR *2 1 3 1 + G	410 4 OR 48 2 5 2 0 0	-10 4 OR -2 2 6 2 0 0	<10 ¢ 3 € 42 6 6 6
420 4 0R 48 3 6 4 9 D	420 4 DR 48 G 13 b O G	480 4 DR 45 1 7 2 + 0	420 4 DR 45 2 5 6 0 0	420 4 02 45 2 12 2 U D	420 4 45 B 15 10
v887 a6 40 54 4 0 0 a 60 4 a6 37 44 1 0 0	Y48Y 46 11 64 24 D D	v487 ≥6 28 59 12 + 0 ≥60 4 ≈6 26 48 10 0 0	7887 x6 21 58 20 0 0	V88Y a6 27 53 20 0 0 a 80 4 a 5 24 35 12 0 0	vsu <6 31 48 15
MC & 2 30 37 37 1 0 0	NC 4 ± 10 11 44 15 0 0	MC 4 + 10 24 48 10 0 0	HC4 = 10 19 45 12 0 0	MC 4 2 10 24 33 12 0 0	MC 4 a 10 21 31 4
68	143	284	126	12 13 149	
19	20	21	22	23	
HIND SPEED (KNSTS)	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	WIND SPEED (KNOTS)	WIND SPEED (KNOTS)	HIND SPEED CK
LCC - YBOT 3 10 21 33 234	LCC - VSSY 3 30 71 39 494	LCC - YARY 3 10 21 33 334	LCC - VOBY 3 10 21 39 234	LCC - Y8BY 3 10 21 33 334	LCC - VARY 3 10 2)
41.E4884.8 0 0 2 0 0	41.6 £ 08 4.5 0 0 1 0 0	41.54 OR 4.5 0 1 1 0 0	<1.5 t 0f <.5 0 0 0 0 0	<1.840R4.5 0 0 + 0 0	43.54.084.8 0 0 U
*# 4 9R *\$ 0 0 2 0 0	48 4 DR 42 0 0 1 0 0	46 4 0R 42 D 1 3 0 0	48 4 OR 42 3 3 0 0 0	*6 4 0R <z< th=""><th>*8 4 DR 42 0 0 3</th></z<>	*8 4 DR 42 0 0 3
410 4 dR 42 0 2 5 0 0	410 4 08 42 0 4 3 0 0	-10 4 0A -2 0 5 5 0 0	*50 4 OR *E 3 5 0 3 0	<10 4 OF <2 + 4 2 1 0	-10 L OR -2 3 3 13
420 L OR 46 2 2 8 2 0	<20 € 08 <8 2 5 4 1 0	-20 4 OR -6 2 10 10 0 0	420 4 6R 4B 8 10 0 3 3	-20 4 OR -6 1 9 5 1 0	420 L OR 48 3 11 21
VBBY 46 15 51 31 2 0	VERY #8 33 54 10 1 0	vasy 25 18 55 23 1 0	V487 a5 21 46 26 3 3	V881 38 14 55 28 2 0	VBBY >5 5 39 50
#66 4 25 11 43 21 0 0 MC 4 2 10 11 43 20 0 0	as0 4 as 32 49 7 0 0 MC 4 a 10 28 47 7 0 0	#60 4 #5 17 44 13 0 0 HC 4 2 10 15 39 12 D 0	#60 6 25 15 36 21 0 0 #C 6 2 10 13 33 21 0 0	#60 4 a5 13 44 21 1 0 MC 4 a 10 13 42 20 1 0	MC 4 a 10 3 29 32
61	166	198	39	658	3 59 35
28	29	30	31	32	1
HIND SPEED (KNOTS)	NIND SPEED (KNOTS)	WIND SPEED (KNOTS)	WIND SPEED (KNOTS)	WIND BPEED (KNOTS)	NIND SPEED INN
LCC - V48Y 3 10 21 33 234	LCC - VSST 3 10 21 33 234	LCC - VMMY 0- 4- 11- 22- 3 10 21 33 234	LCC - Y88Y 3 10 21 33 454	LCC - VBY 3 10 21 33 234	LCC - YASY 3 10 71 3
<1.8 4 SR 4.8 U + O O O	<1.5 4 SR < 18 0 0 0 0 0	<1.5 t OR <.5 0 1 0 0 0	1.640R 4.6 0 0 0 0 0	41.6 4 OR 4.6 1 0 0 0 0	<1.5 4 OR 4.5 + 1 +
<8 ← DR ≪2	0 0 0 0 25 NG 5 BP	<84 dR <2 D 1 D U D	-0 ± OR +2	<64 OR <2 1 0 · U 0 VBBY -2 · 0 0 0 0	48 t OR 42 + 1 + V&BT 48 + 1 D
410 4 00 42 + 3 5 2 1	-10 4 6A -2 1 0 4 2 0	*10 4 OF *P 0 9 5 1 D	-10 4 OR 42 0 2 3 2 0	-10 4 OR -2 1 1 3 1 0	<10 4 08 42 1 4 4
420 4 0R 48 1 8 11 4 1	480 4 OR 48 1 2 11 2 C	-20 4 df <8 2 19 14 2 1	420 4 0R 48 1 20 13 7 0	420 4 OR 48 1 8 14 3 0	480 4 08 48 2 12 14
Y48Y 25 6 38 42 11 1	V48Y 3E 6 37 42 14 1	VSST 25 B 52 35 1 0	V60Y a6 7 45 34 14 0	V487 25 3 35 51 9 1	Y66Y VE 5 38 44
#60 4 B5 4 27 27 7 +	MC 4 NO 5 31 27 9 1	#60 4 16 8 29 18 0 D	-50 4 a 5 2 23 11 5 0	NC4 a 10 2 17 22 5 1	860 485 3 19 23 8:4 a 10 3 17 19
619	81	114	88	373	
37	38	39	40	4 1	
WIND SPEED (KNOTS)	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	HIND SPEED (KNOTS)	•
LCC - VASY 3 10 21 33 254	LCC - V887 9 10 21 33 234	LCC - YEST 0- 4- 11- 22- 33 +34	LCC - Y887 0- 4- 11- 22- 3 10 21 33 434	LCC - V881 3 10 21 35 234	
*1.5 & DR *.8 0 0 0 0 0	41.84 69 4.5 0 2 0 0 0	<1.540R*.5 0 0 2 8 2	41.84 GR 4.5 0 0 4 8 0	<1.8 & OR = . B	
*8 & GR <2 0 0 0 4 0	*8 & 0R =P D 4 2 0 0 Y88Y =2 0 4 2 0 0	<84.08 <2	48 4 DR 42 D D 4 B D	VSSY 42 0 3 3 0 0	INSUFFICIEN
10 4 08 12 0 0 5 4 0	10 4 gR - 2	410 A 08 42 2 8 8 27 B	10 4 0R 12 0 0 B B (2)	10 4 08 42 0 13 16 3 3	DATA

Graphs represent the objective compilation of available data for specified areas withou The <u>isopleth</u> analyses (apposite page) are based on all available data subjectively adju

0 8 8 0

4 17 13 4

B 46 13 13 D 8 4 13

0 0 0 4 6

0

0

0

ᆎ

410 4 OR 42

-20 4 OR <8

7887 a6

180 4 28

HC L . 10

0 3 3 0 0

0 28 25 9 3

3 34 41 13 3 0 3 9 3 0 0 0 9 0 0

DATA

10 4 DR 12

170 4 00 46

VEST LE

180 4 18

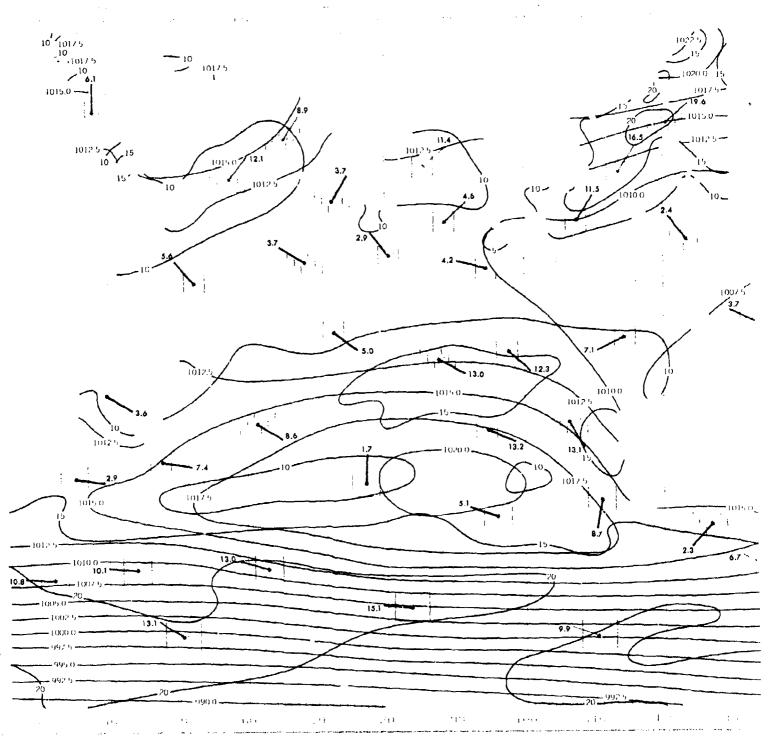
HC 4 9 10

ITY-WIND

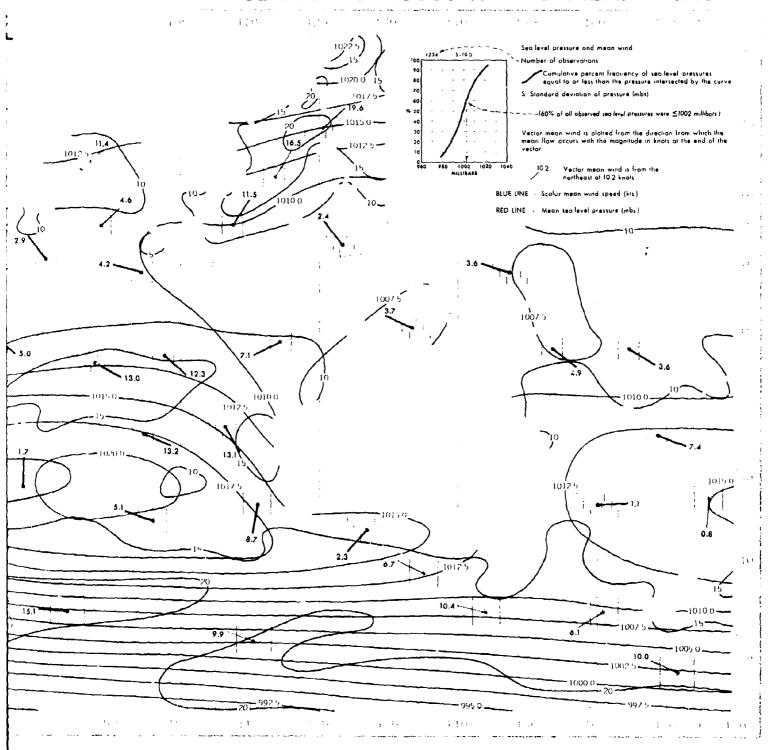
DECEMBER

4	5	6	7	8	9
MIND SPEED (KNOTS)	WIND SPEED (KNOTS)	HIND SPEED (KNOTS)	NIND SPEED (KNOTS)	WIND SPEED (KNOTS)	WIND SPEED (KNOTS)
110 - V687 0- 4- 11- 22- 33 234	LCC - V887 3 10 21 33 231	LCL - VSST 3 10 21 33 234	LCC - 17 0 4- 11- 27- 3 10 21 33 434	LCC - V6BY 3 10 71 35 434	CCC - VSBY 3 10 21 33 234
11.54.08 13. O O O O O	<1.6 4 OR * P	*1.5 4 DR *2 + + + + + + + + + + + + + + + + + +	41.540K+2 0 + 0 0	<1.5 L QR <-5 () + + • () <8 4 QR <2 + 1 2 • ()	<1.5 4 0R <.B 0 + 1 + 0
8 4 0 *7 0 0 0 0 0 U	*6 4 ON *P 0 + 2 1 0	*6 4 OR *? + + 2 2 + VUBY *? O + 1 1 +	46 F OH +5 0 + + 0 0	*8 4 OR *2 + 1 2 + U	
*10 4 08 *7 D + 1 + D	111 4 108 -2 0 2 5 2 •	10 4 0R <z +="" 1="" 1<="" 7="" th=""><th>*10 4 0 * *2 + 2 1 + 0</th><th>-10 4 0R -2 1 5 5 1 G</th><th>410 4 DR 42 - 3 11 3 0</th></z>	*10 4 0 * *2 + 2 1 + 0	-10 4 0R -2 1 5 5 1 G	410 4 DR 42 - 3 11 3 0
*20 & DK 45 10 2 3 • 0	*20 LGR *5 0 6 15 3 •	420 4 OR 45 + 3 18 13 1	420 4 OR 45 8 2 1 0	<20 4 08 45 1 11 13 1 0	+20 4 OR +5 1 7 25 5 0
vs87 +6 6 51 41 7 0	¥887 ∌5 1 34 52 7 +	v5er ≥5 + 11 56 22 1	VS87 aG 22 57 10 1 0	VB8Y 35 10 48 35 2 D	vany as 2 27 53 8 · aso tas 2 19 28 4 ·
50 tas 6 47 36 1 0	350 4 a5 1 27 35 4 O	250 4 25 4 9 37 11 +	abo 4 ab 20 60 7 0 0	250 4 25 8 36 22 1 D	
HC 4 + 10 6 44 34 1 0	HC 4 & 10 • 26 30 1 0	HC & > 10 + 7 29 6 +	MC 4 a 10 19 5B 7 0 0	MC 4 3 10 8 33 18 1 0	MC 4 a 10 1 16 20 2 0 2050
13	1 4	15	16	17	18
HIND SPEED (KNOTS)	WIND SPEED (MNOTS)	WIND SPEED (KNOTS)	MINO SPEED (KNOTS)	WIND SPEED (KNOTS)	WIND SPEED (KNOTS)
LCC - VEBY 3 10 21 33 334	LCC - YBB7 3 10 21 33 834	LCC - YSBT 0- 4- 11- 22-	LCC - YERY 3 10 21 33 334	LCC - V887 3 10 21 33 234	LCC - VEST 3 10 21 33 234
41-5 LOR 4-6 0 0 0 0 0	41.8 4 DR 4.8 D U D D		4)-5 4 GR 4-5 0 0 0 0 0	*1.64 0R *.5 U O C O O	41.84 DR 4.8 0 0 1 0 0
-6 4 0A -2 D 3 1 D 0	-8 4 OR -2 0 4 2 0 0	41.5 4 0R 4.5 0 0 0 0 0 0	<8 4 DK ≤2 0 2 + + 0	*8 \$ OR 12 D 1 1 0 0	45 4 0A 42 0 0 3 0 0
V887 42 D () () () D	4864 <5 0 0 0 0 0	V6BY 42 0 J 0 0 0	Y48Y 42 0 0 + 0 0	V5BY <2 () () + () ()	Y887 49 D 0 1 0 D
10 4 08 -9 7 5 2 0 0	<10 4 0R +2	410 4 DR 48 6 6 6 0 0	4:0 4 OR 42	-10 4 0R -2 0 1 8 2 0 -10 4 0R -5 0 4 15 4 0	430 4 6R 48 D 3 10 2 D
vsm1 a5 21 5B 20 0 0	VSBY 45 27 53 20 0 0	VSBY 86 31 48 15 2 0	*70 4 04 <6 + 12 6 2 0	Y687 as 0 30 62 4 0	V601 35 4 33 57 4 0
250 4 25 19 46 12 0 0	260 4 26 24 35 12 0 0	3 ED 4 35 23 33 6 0 D	3 60 6 38 7 47 18 + O	250 4 25 0 23 40 1 0	a 80 4 as 4 24 38 2 0
HC 4 a 10 19 45 12 0 0	MC 6 a 10 24 33 12 0 0	MC 4 + 10 21 31 4 0 D	HC 4 > 10 7 44 17 + 0	NC & & 10 0 21 36 + 0	MC 4 3 10 4 22 35 2 0
125	49	52	286	207	138
22 WIND SPEED (KNDTS)	23 HIND SPEED (KNOTS)	24 WIND SPEED (KNOTS)	25 WIND SPEED (KNOTS)	26 WIND SPEED (KNOTS)	27 HIND SPFED (KNOTS)
LEC - V887 3 10 21 33 =34	0- [4-]11-[22-]	0- 4- 11- 22-	10-14-111-122-1	LCC - V487 9 10 21 39 294	LCG - YERY 3 10 21 33 294
-1.64 dH -18 0 0 0 0 0	LCC - Y887 3 10 21 39 234 41.54084.5 0 0 + 0 0	LCC - V88V 9 10 21 35 234 <1.5 4 0R < 18 0 0 0 0 0	LCG - VABT 3 10 21 33 134	41.8 4 OR 4.5 0 0 0 0 0	41.5 4 58 4.8 0 0 0 0 0 0
48 F DM 45 3 3 D D D	*6 & OR *2 0 * 1 1 G	48 4 OR 42 0 0 3 0 0	48 4 OR 42 G O 2 O O	484 DR 48 0 0 1 0 0	46 4 OR 42 0 0 0 1 0
YEST 42 3 0 D 0 0	Y887 *2 0 0 0 0 0	Y88Y 42 0 0 3 0 0	Y887 48 0 0 0 0 0	V8BY -P 0 0 0 0 0	YEST 12 0 0 0 0 0
410 & OR 42 3 5 U 3 D	-10 4 DR -2 - 4 2 1 D	<10 4 DR <2 3 3 13 0 0	-10 4 0H -2 D 0 12 D 0	«10 4 GR «¥ D 1 2 D D	410 4 08 -9 0 4 2 2 0
*20 4 68 46 8 10 0 3 3 *488* 45 21 46 26 3 3	*20 4 OR *5 1 9 5 1 0	<20 4 0R <6 3 11 21 0 0 9887 25 5 39 50 0 0	420 4 UR 45 2 2 21 0 0 9687 a6 3 30 62 3 2	*20 4 OR *5 0 3 6 3 0	*20 4 OR *8 2 7 8 2 0 *88* 35 9 42 43 5 1
350 4 38 15 36 21 0 0	a 50 4 ah 13 44 21 1 0	3 28 32 0 0	280 4 25 2 17 33 3 2	480 436 0 10 37 10 9	#80 4 ab 5 31 31 2 1
HC 4 # 10 13 33 21 0 0	NC 1-10 13 42 20 1 0	MC 4 2 10 3 28 32 0 0	MC 4 > 10 2 17 33 3 2	NC 4 # 10 0 8 33 7 0	HC 4 9 10 5 30 31 2 1
39	058	38	56	192	184
31 WIND SPEED (KNOTS)	32 WIND SPEED (KNOTS)	33 HIND SPEED () NOTS)	34	35 WIND BPEED (MNDTS)	36 (stonk) daags drijn
10-14-14-14-1	10-14-111-129-1	ا امراد الحدادة ا	0-14-111-22-1	ا المعاملات المامي	LCC - VARY 3 10 21 33 394
1.5 4 0R *-5 0 0 0 0 0	1.54 MK < .5 1 0 0 0 0	LCC - VABY 3 10 21 33 234 <1-64 OR <15 + 1 + () ()	1.54 OH <-15 0 0 0 0 0	-1.64 OR -18 1 1 0 0 0	41-8 L OR 4-8 0 0 0 0 0
-64 d# 42 () () 1 () ()	+6 4 08 +2 1 0 • D 0	48 4 DR 42 + 1 + O D	-6 4 OR -2 0 0 + + 0	48 4 OR 48 1 2 1 1 0	46 4 DR 42 D D D D
V607 -2 0 0 0 0 0	VBAT -2 - 0 0 0 0	V687 -2 + 1 0 U U	VSBY <2 0 0 + + 0	Y887 4 0 1 0 0 0	V88Y -2 0 0 0 0 0
*10 4 08 42 0 2 3 2 0	-10 1 08 42 1 1 3 1 0	=10 4 OR 42 1 4 4 1 +	410 4 dH 42 0 2 5 2 4	<10 4 0R <2 1 6 4 2 0	10 4 0f +2 0 0 0 0
*70 4 DR *5 1 20 13 7 0	420 4 OR 45 1 8 14 3 0 VBBT 96 3 35 51 9 1	420 6 OR 45 2 17 14 3 1 VEST 26 5 3B 44 B +	470 4 OR 46 1 9 1B 4 → VERY ab	*20 4 0R *8 1 11 9 3 0	10 4 08 18 0 3 0 14 3 10 14 3 0 14 3
*50 4 *5 2 23 11 5 0	450 4 45 2 18 25 5 1	160 4 25 3 19 23 5 O	250 425 5 22 28 5 D	380 4 38 6 31 26 4 0	150 4 26 3 14 28 8 D
NC 4 2 10 2 20 10 3 0	MC 4 > 10 2 17 22 5 1	4C 4 > 10 3 17 19 4 0	MC 4 = 10 6 21 27 5 0	HC 4 a 10 5 28 24 4 C	850 4 a 5 3 1 4 28 8 0 MC 4 a 10 3 1 1 2 5 6 U
88	379	852	328	190	36
40	41	42	43	4 4	45
WIND SPEED (KNOTS)	HIND SPEED (KNOTS)		WIND SPEED (KNOTS)		HIND SPEED (KNOTS) 0-14- 11- 22-
1CC - VOBT 3 10 21 33 434	LCC - V881 3 10 21 33 354		LCC - VBBY 3 10 21 99 154		LCC - VARY 3 10 21 35 434
1-54 OR 4-5 0 0 4 8 0	*1.6 ¢ 0k *.5	IN 101 IEE: 01EN IE	41.640R 4.8 0 2 0 1 0	IN ICUITE CIENT	*1.84 OF *.8 0 1 1 1 0
V887 -2 0 0 4 8 0	VBRY 42 0 3 3 0 0	INSUFFICIENT	V887 42 0 2 1 0 0	INSUFFICIENT	1887 -2 0 1 1 1 0
*10 4 D# *2 0 0 B 8 0	-10 4 OR -2 0 13 18 3 3	DATA	*10 4 OR *2 2 5 6 8 0	DATA	410 4 OR 42 0 1 6 4 1
<20 4 08 <5 () 4 17 1 1 4	-20 4 0H -5 0 28 25 9 3		-20 4 de -6 2 12 15 19 2		470 4 OF 4 0 4 25 13 4
vsav a5 0 8 46 13 13	VSBT +6 3 34 41 13 3 +60 4 46 0 3 9 3 0		VEST #6 2 27 37 21 3		veev as 0 7 47 30 5
					U * * E U 1
MC 6 a 10 0 0 0 4 8	NC 4 + 10 0 0 9 0 0		MC4+10 D 9 18 5 D		HC 4 = 10 0 1 9 1 0

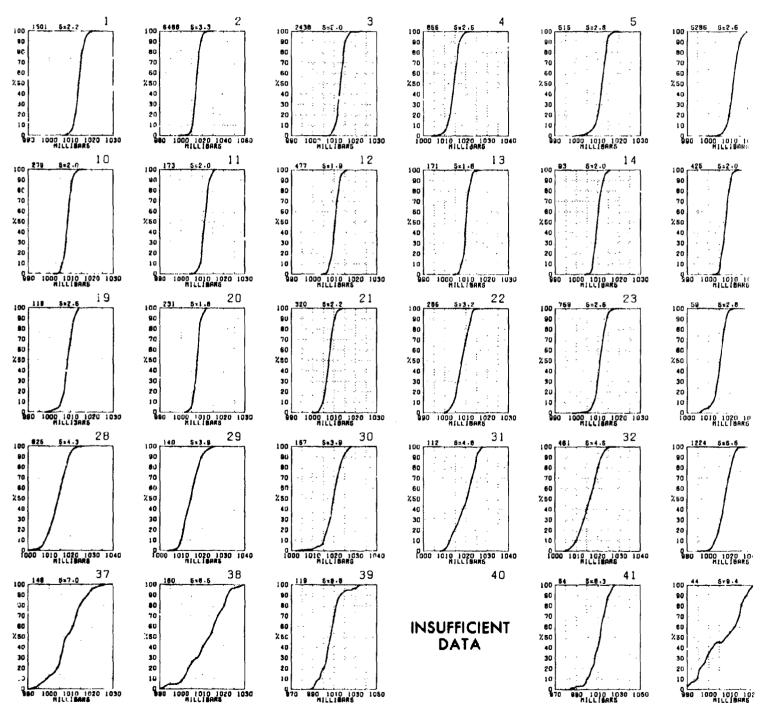
SEA LEVEL PRE



SEA LEVEL PRESSURE AND MEAN WIND

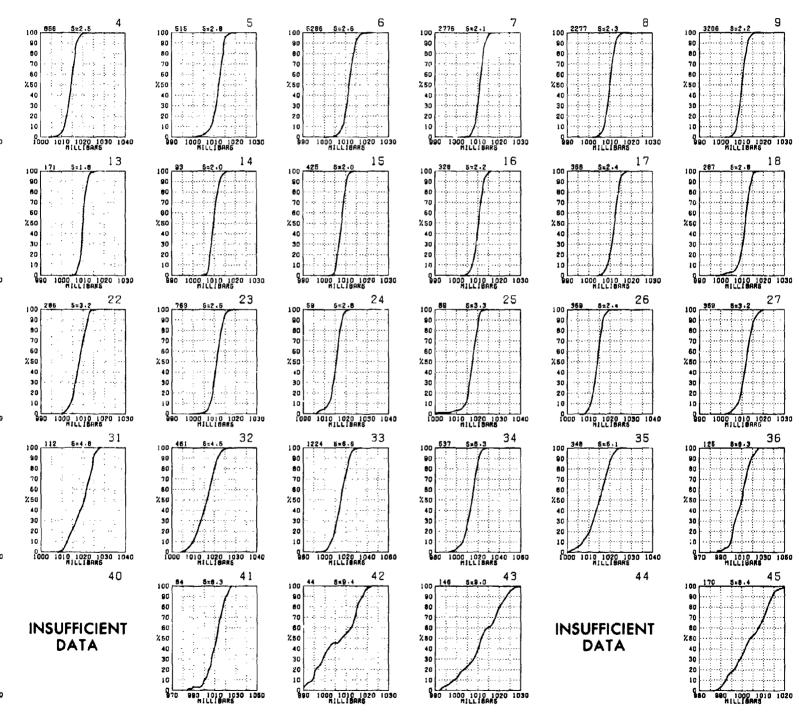


SEA LEVEL PRESSURE



Graphs represent the objective compilation of available data for specified areas with The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively ac

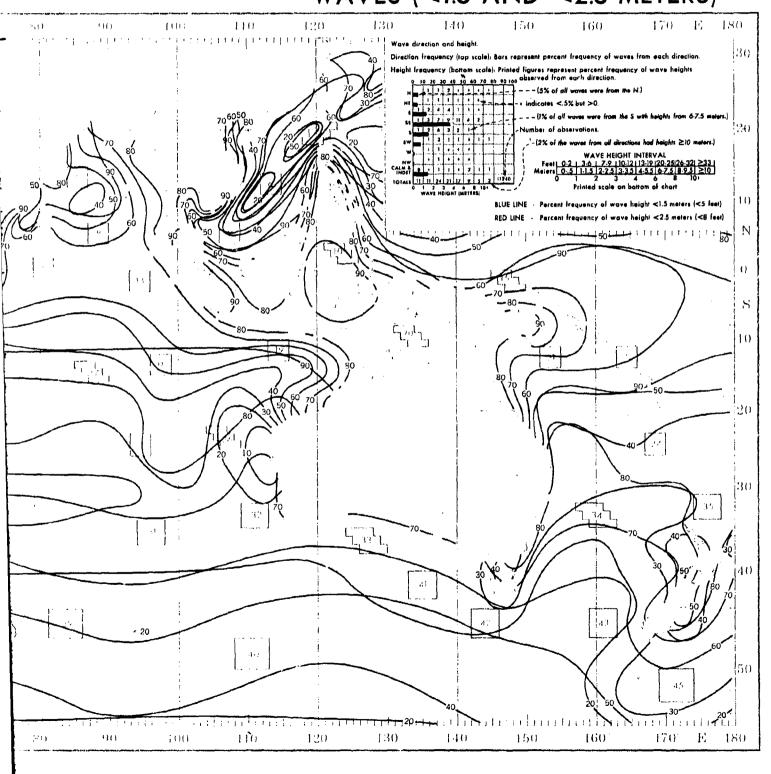
DECEMBER



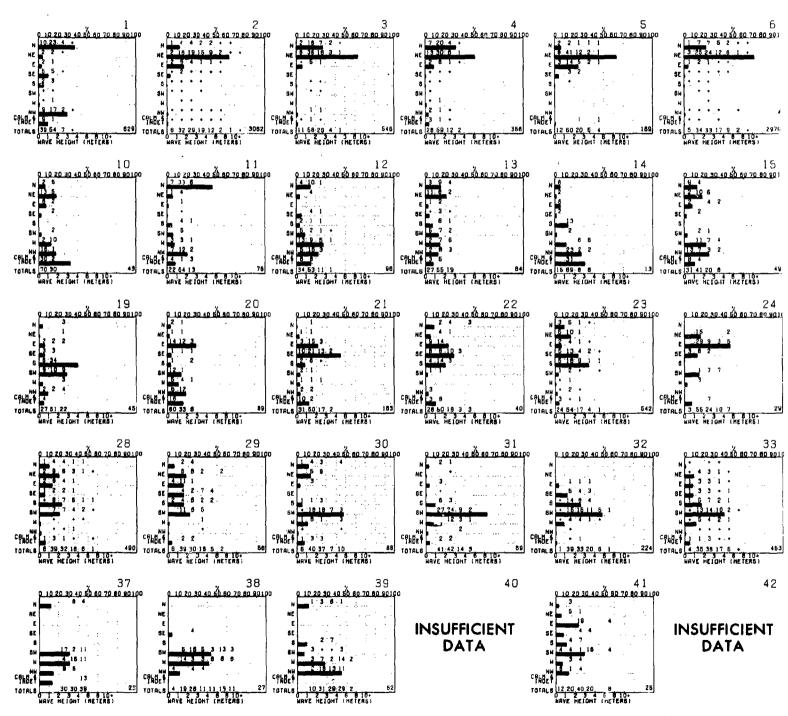
objective compilation of available data for specified areas without regard to suspected biases. (opposite page) are based on all available data subjectively adjusted where bias was evident

WAVES (**DECEMBER** kir aminaimuliatios ja mainalmismalamininia mahada da kariso **(**;()

WAVES (<1.5 AND <2.5 METERS)



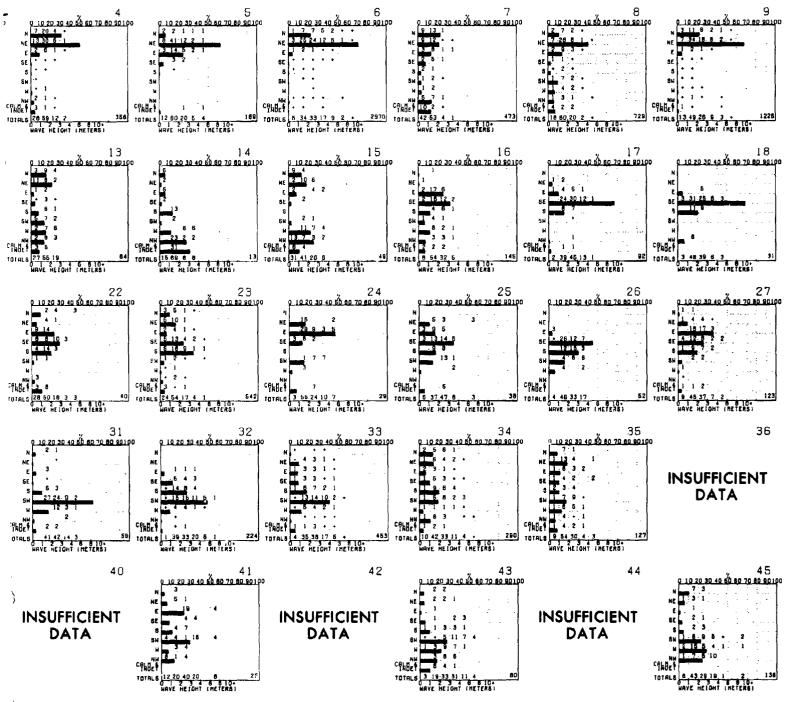
WAVE DIRECTION AND HEIGHT



Graphs represent the objective compilation of available data for specified areas without re The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjuste

GHT

DECEMBER

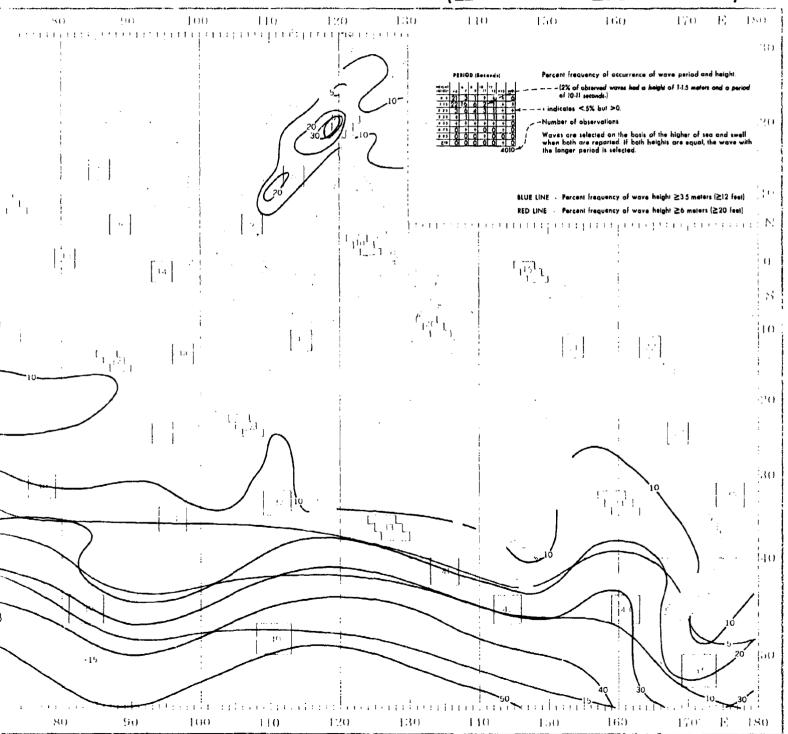


scrive compilation of available data for specified areas without regard to suspected biases. posite page) are based on all available data subjectively adjusted where bias was evident.

DECEMBER WAVES terrifered a film ferral militari de mante de mante de mante de mante de mante de mante de mante de mante de m An 180 de mante de mante de mante de mante de mante de mante de mante de mante de mante de mante de mante de m 303 10 ! $\tau_{1,1,1}$ [h $[1]_{T}^{T}$ 14 ٠; $\left[u_{0}\right]$ 110 18 1.10 filiadimikan birda iz zadroda. Secretaria de la contra del contra de la contra de la contra de la contra de la contra de la contra de la contra de la contra de la contra de la contra de la contra de la contra de la contra de la contra de la contra de la contra de la contra de la contra de la contra de la contra del contra de la contra del la contr 70 90 100 11() 120

334

WAVES (≥3.5 AND ≥6 METERS)



WAVE PERIOD AND HEIGHT

PERIOD SECONDS	PERIOD I SECONDS 1 (19161) - 4	PERIOD (SECONDS)	#E10+1 5 5 10 12 13 140	S	PERIOD (SECONDS) (1918a) -4 - 2 - 9 - 11 - 13 - 13 - 14 - 15 - 16 - 17 - 18 - 18 - 19 - 18 - 18 - 18 - 18 - 18
	1	2 PERIOD (SECONDS) 10 10 10 10 10 10 10 1	1 3 PERIOD (SECONDS) 1 3 PERIOD (SECONDS) 1 1 1 1 1 1 1 1 1	INSUFFICIENT DATA	Columbia Columbia
PERSON (SECONDS) ***INTERS** 48	PERIOD (SECONDS) **Electron 4-7 5-1 15-1 15-1 15-1 15-1 **Electron 5-1 15-1 15-1 15-1 15-1 **Electron 5-1 15-1 15-1 15-1 **Electron 5-1 15-1 15-1 15-1 **Electron 5-1 15-1 15-1 15-1 **Electron 5-1 15-1 15-1 15-1 **Electron 5-1 15-1 15-1 **Electron 5-1 15-1 **Electron 5-1 15-1 **Electron 5-1 15-1 **Electron 5-1 15-1 **Electron 5-1	PERIOD (SECONDS)	PERIOD (SECONDS) No. 10 10 12 13 14 15 16 16 17 16 17 17 18 18 18 18 18 18	PERIOD (SECONDS) NECTOR 4- 3- 10- 11- 11- 110	PERIOD (SECONDS)
PERIOD (SECONDS)	PERIOD (SECONDS) NETERING	30 PERIOD (SECONDS) 161848) -6 -7 -6 -11 -13 -13 -130 0-3 -4 -0 -0 -0 -0 -1 1-1-1 -13 -10 -7 -3 -3 -0 -3 1-1-1 -13 -10 -7 -3 -3 -0 -3 1-1-1 -13 -10 -7 -3 -3 -0 -3 1-1-1 -13 -10 -7 -3 -3 -0 -3 1-1-1 -13 -10 -7 -3 -3 -0 -3 1-1-1 -13 -10 -7 -3 -3 -0 -3 1-1-1 -13 -10 -7 -3 -3 -0 -3 1-1-1 -13 -10 -7 -3 -3 -0 -3 1-1-1 -13 -10 -7 -3 -3 -0 -3 1-1-1 -13 -10 -0 -0 -0 -0 -0 1-1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1	31 PERIOD (SECONDS) ***PISSON 10 17 17 17 18 ***O'-1 0 0 0 0 0 0 ***O'-1 0 0 0 0 0 0 ***O'-1 0 0 0 0 0 0 ***O'-1 0 0 0 0 0 0 ***O'-1 0 0 0 0 0 0 ***O'-1 0 0 0 0 0 0 ***O'-1 0 0 0 0 0 0 ***O'-1 0 0 0 0 0 0 ***O'-1 0 0 0 0 0 0 ***O'-1 0 0 0 0 0 0 ***O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 ***O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 0 **O'-1 0 0 0 0 0 **O'-1 0 0 0 0 0 **O'-1 0 0 0 0 **O'-1 0 0 0 0 **O'-1 0 0 0 0 **O'-1 0 0 0 **O'-1 0 0 0 **O'-1 0 0 0 **O'-1 0 0 **O'-1 0 0 0 **O'-1 0 0 **O'-1 0 0 **O'-1 0 0 **O'-1 0 0 **O'-1 0 0 **O'-1 0 0 **O'-1 0 0 **O'-1 0 0 **O'-1 0 0 **O'-1 0 **O'-1 0 0 **O'-1 0 **O'-	32 PERIOD (SECONDS) **Total 4	Femilion
PERIOD (SECONDS) ***PERIOD (S	3 8 PERIOD (SECONDS) 18781 8	PERIOD (SECONDS) PERIOD (SECONDS)	INSUFFICIENT DATA	PERIOD (SECONDS)	INSUFFICIENT DATA

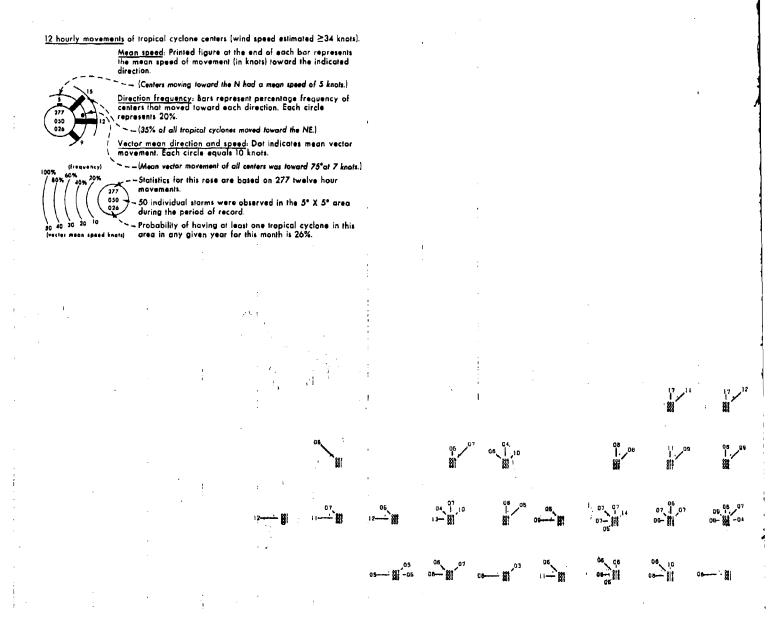
Graphs represent the objective compilation of available data for specified areas without re The <u>isopleth</u> analyses (opposite page) are based on all available data subjectively adjuste

DECEMBER

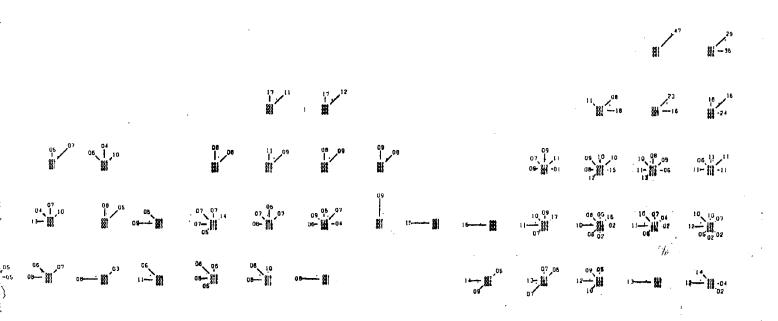
-	PERIOD (SECONOS) 12 2 0 0 0 0 0 2 1-14 27 14 7 2 11 1 6 1-2-14 0 2 2 2 0 0 0 0 0 1-14 0 1 1 2 0 1 1 0 0 1 1-2-14 0 0 2 2 2 0 0 0 0 1-2-14 0 0 0 0 1 2 0 1 1-2-14 0 0 0 0 0 0 0 0 1-2-14 0 0 0 0 0 0 0 0 1-2-14 0 0 0 0 0 0 0 0 0 1-2-14 0 0 0 0 0 0 0 0 0 1-2-14 0 0 0 0 0 0 0 0 0 0 1-2-14 0 0 0 0 0 0 0 0 0 0 1-2-14 0 0 0 0 0 0 0 0 0 0 1-2-14 0 0 0 0 0 0 0 0 0 0 0 1-2-14 0 0 0 0 0 0 0 0 0 0 0 1-2-14 0 0 0 0 0 0 0 0 0 0 0 0 1-2-14 0 0 0 0 0 0 0 0 0 0 0 0 1-2-14 0 0 0 0 0 0 0 0 0 0 0 0 0 1-2-14 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1-2-14 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1-2-14 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	PERIOD (SECONDS) 10	7 PERIOD (SECONDS) 1 1 1 3 13 180 0 - 8 30 2 1	PERIOD (SECONDS) 11186; *6	9 PERIOD SECONDS
1 3 PERIOD (SECONDE) ***********************************	INSUFFICIENT DATA	PERIOD SECONDS	PERIOD (SECONDS)	1 7 7 7 7 7 7 7 7 7	1 1 1 1 1 1 1 1 1 1
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NSUFFICIENT DATA	PERIOD (SECONDS)	INSUFFICIENT DATA	## PERIOD (SECONDS) FERIOD (SECONDS) FINE 14	INSUFFICIENT DATA	### PERIOD : SECONDS

ive compilation of available data for specified areas without regard to suspected biases. site page) are based on all available data subjectively adjusted where bias was evident.

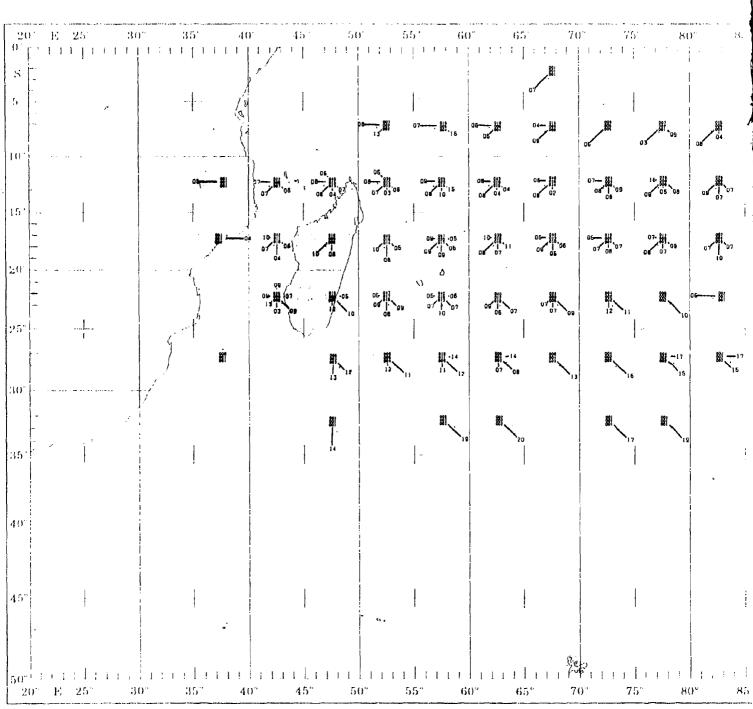
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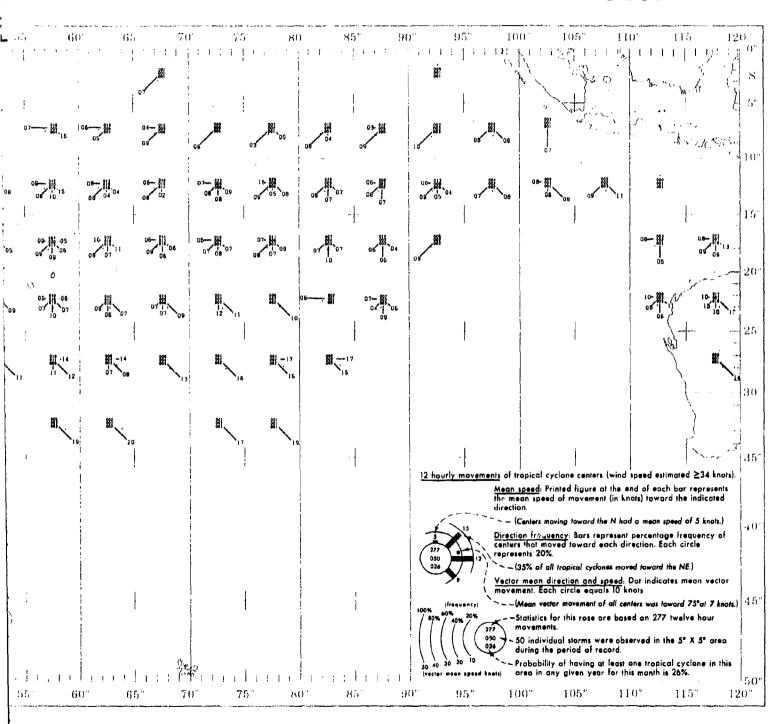
TROPICAL CYCLONE



TROPICAL CYCLONE

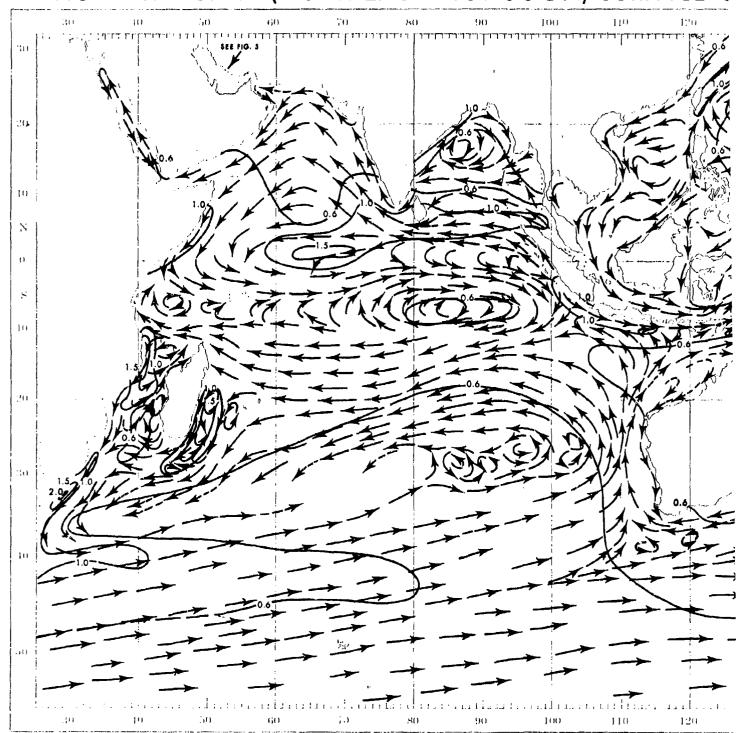


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PART II OCEANOGRAPHY

FIG. 1 JANUARY (NORTHEAST MONSOON) SURFACE (



EAST MONSOON) SURFACE CURRENTS

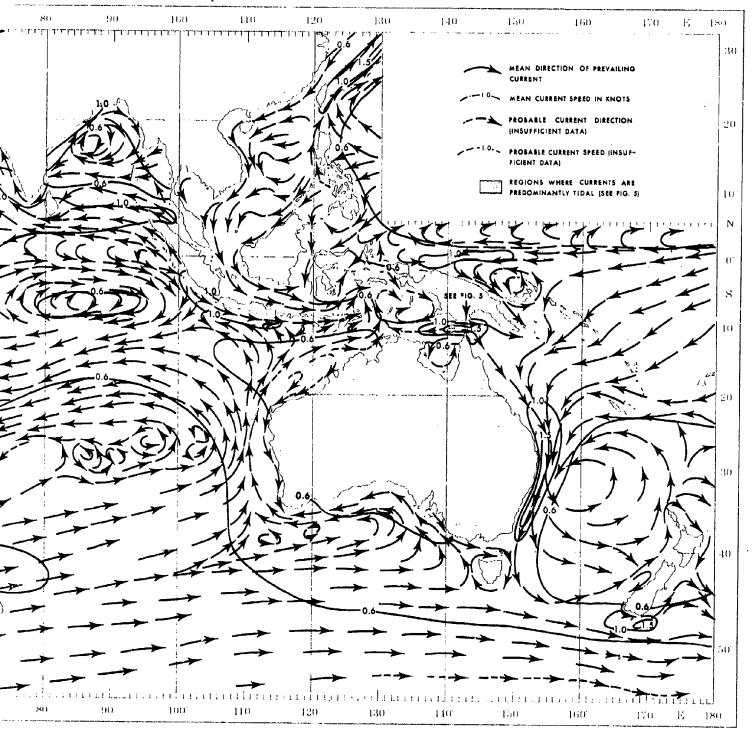
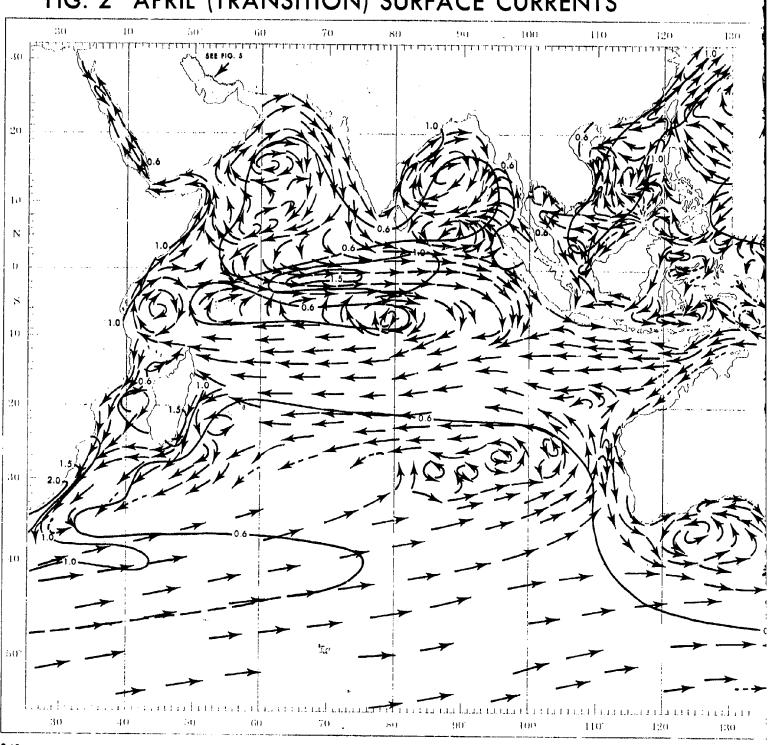


FIG. 2 APRIL (TRANSITION) SURFACE CURRENTS



ON) SURFACE CURRENTS

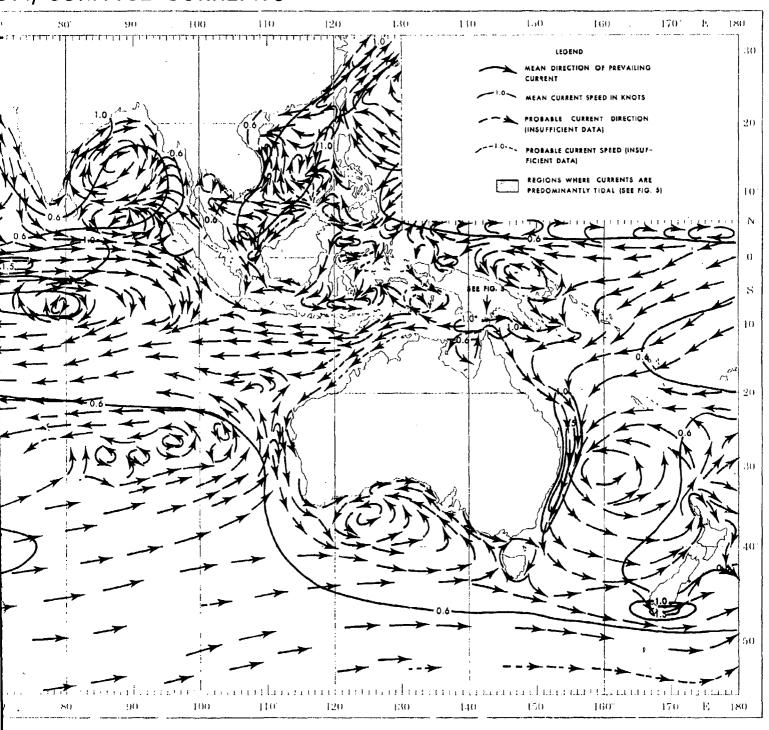
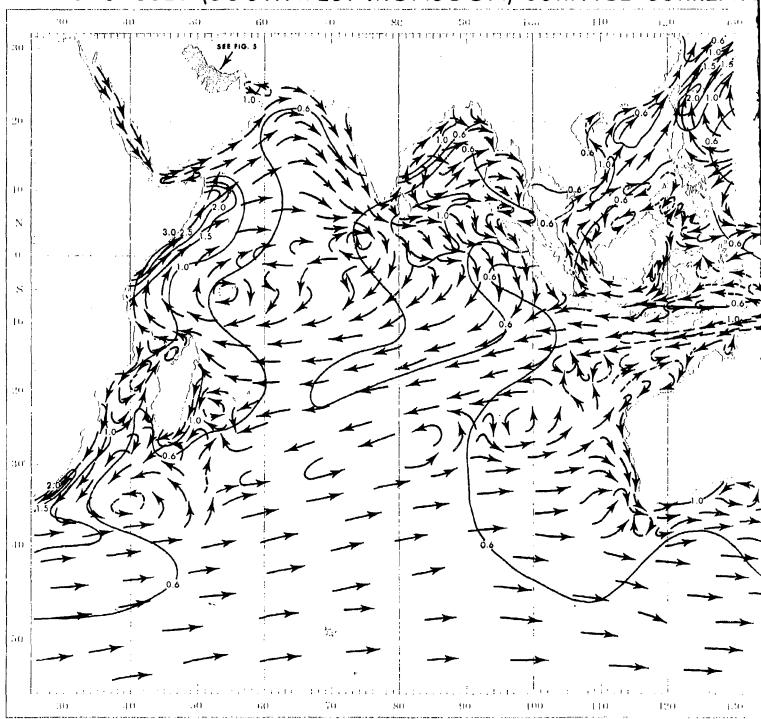


FIG. 3 JULY (SOUTHWEST MONSOON) SURFACE CURRENTS



EST MONSOON) SURFACE CURRENTS

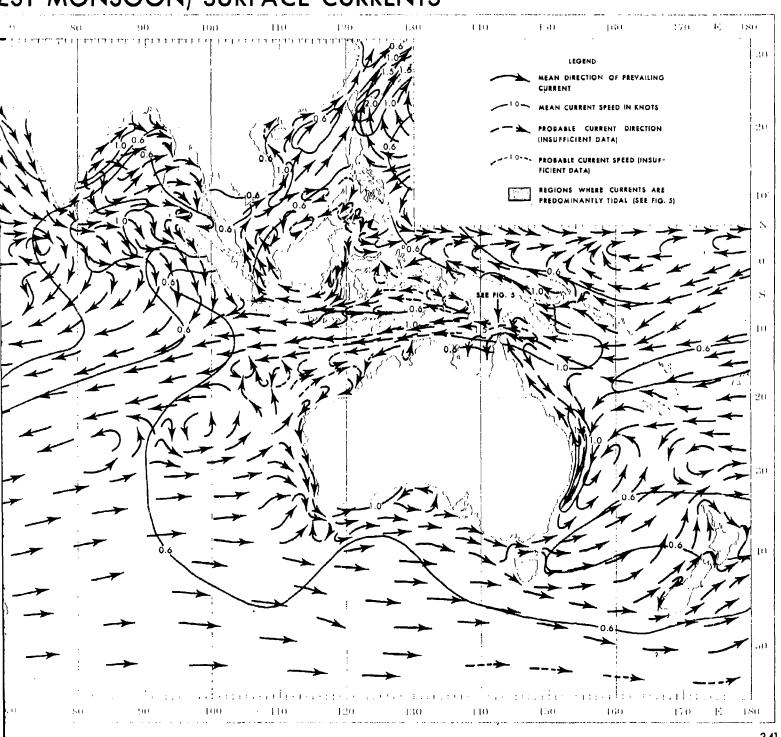
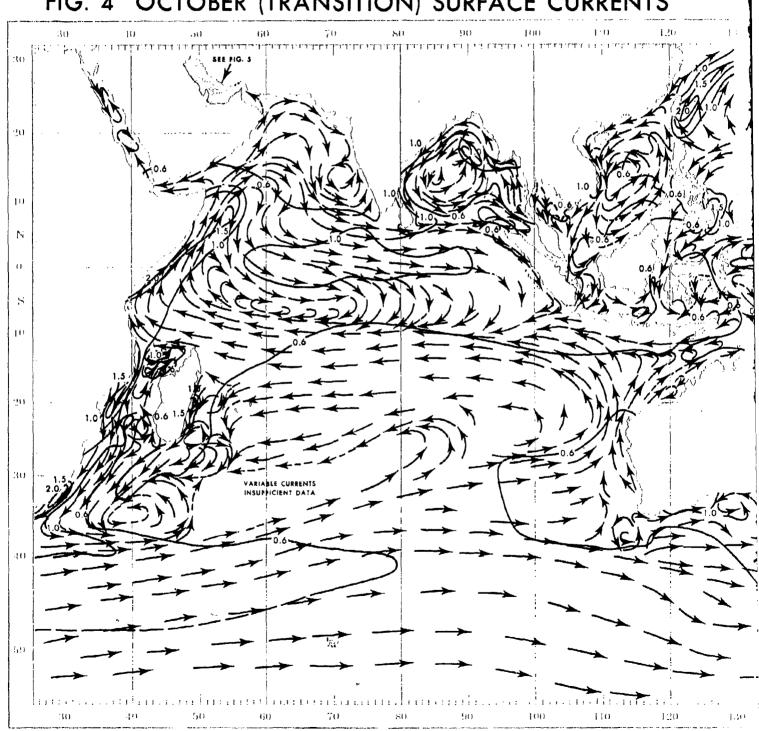


FIG. 4 OCTOBER (TRANSITION) SURFACE CURRENTS



ITION) SURFACE CURRENTS

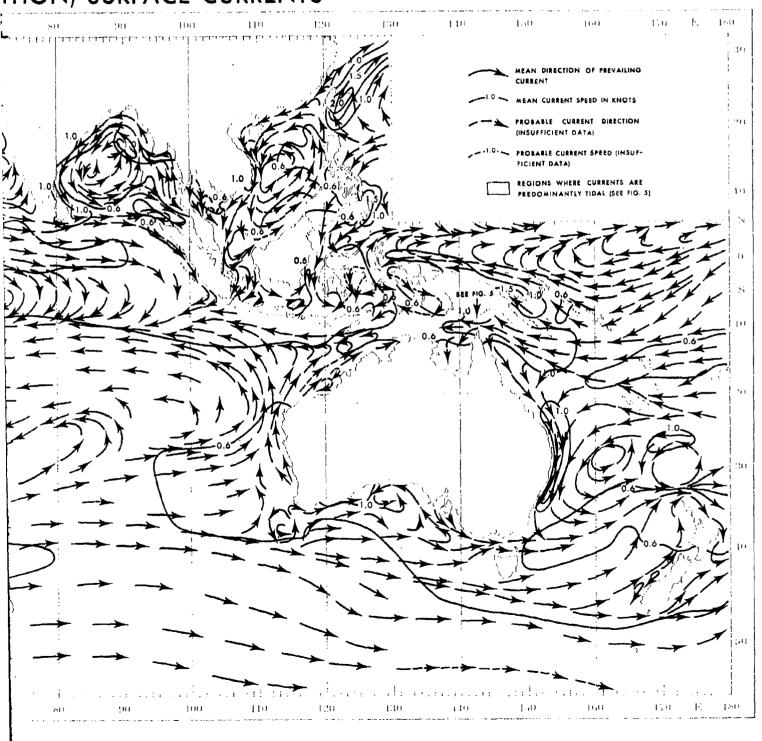
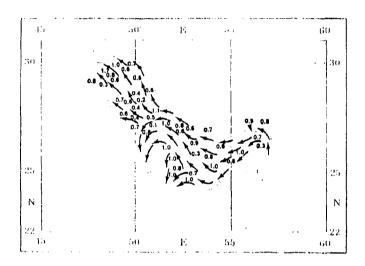


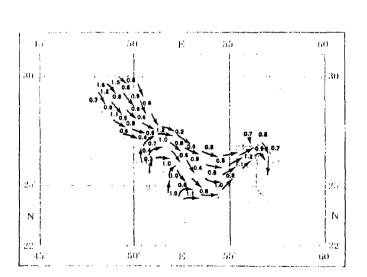
FIG. 5 TIDAL CURRENTS - PERSIAN GULF AND TORRES S'

FLOOD OR EBB CURRENT DIRECTION
1.2 MEAN TIDAL CURRENT SPEED IN KNOTS

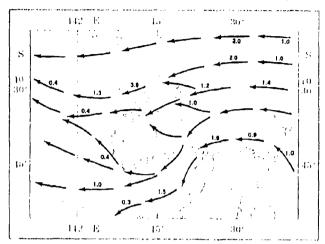
NOTE: THE APPROXIMATE MEAN STRENGTH OF FLOOD AND EBB CURRENTS AT SPRINGS OR TROPICS IS DETERMINED BY MULTIPLYING THE MEAN SPEED BY 1.4: THE APPROXIMATE MEAN SPEED OF FLOOD AND EBB AT NEAPS IS DETERMINED BY MULTIPLYING THE MEAN SPEED BY 0.6.



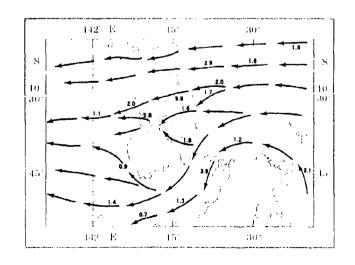
FLOOD CURRENT



EBB CURRENT



FLOOD CURRENT
DECEMBER THROUGH FEBRUARY

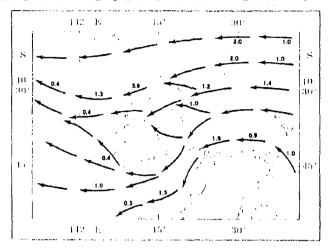


FLOOD CURRENT MARCH THROUGH NOVEMBER

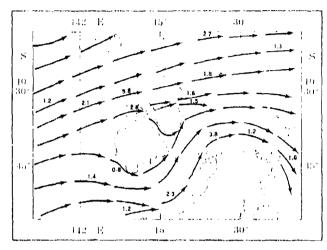
PERSIAN GULF

TORRE

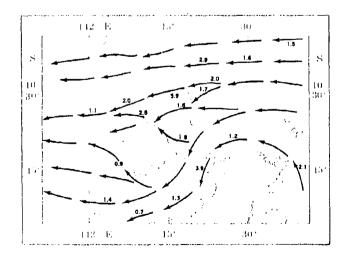
PERSIAN GULF AND TORRES STRAIT



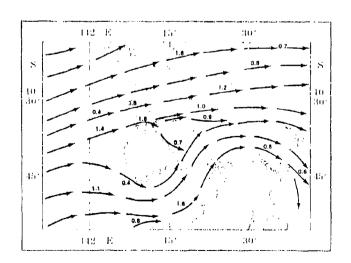
FLOOD CURRENT
DECEMBER THROUGH FEBRUARY



EBB CURRENT
DECEMBER THROUGH FEBRUARY



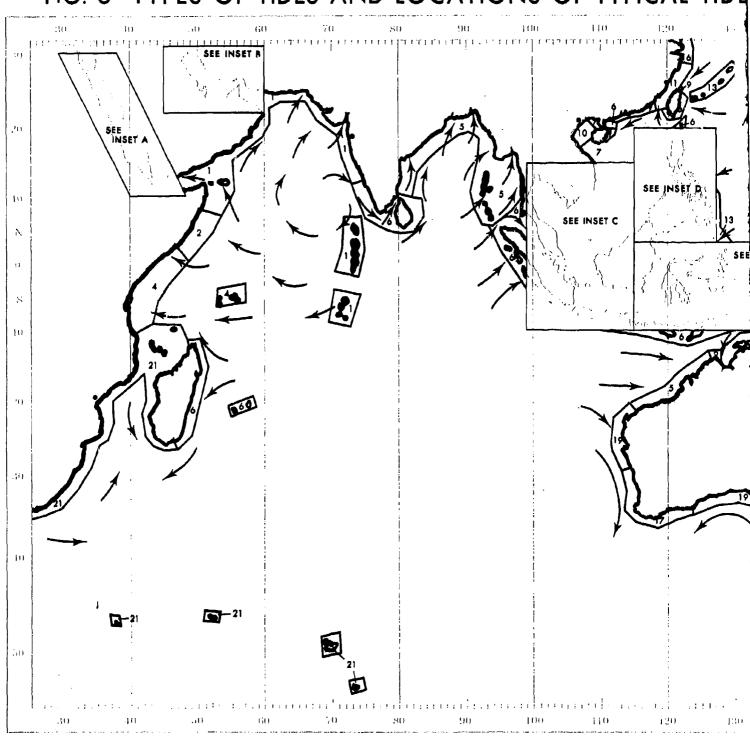
FLOOD CURRENT MARCH THROUGH NOVEMBER



EBB CURRENT
MARCH THROUGH NOVEMBER

TORRES STRAIT

FIG. 6 TYPES OF TIDES AND LOCATIONS OF TYPICAL TIDE



S AND LOCATIONS OF TYPICAL TIDE CURVES

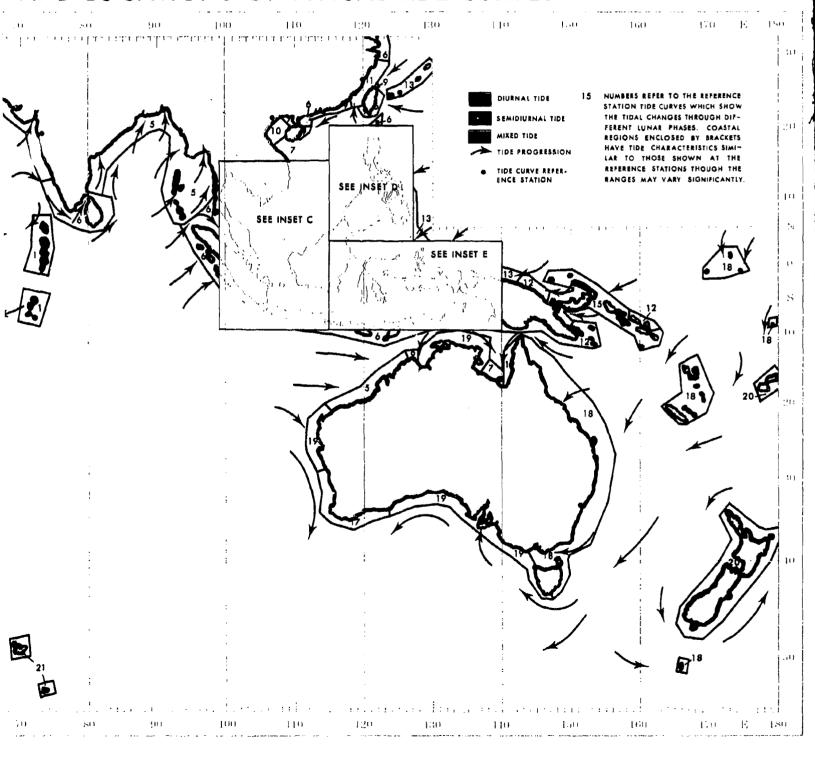
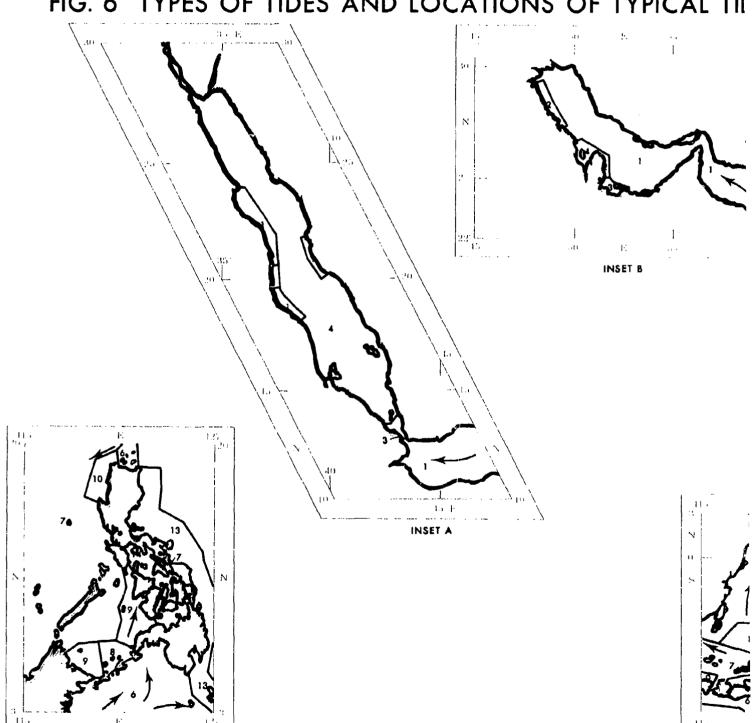
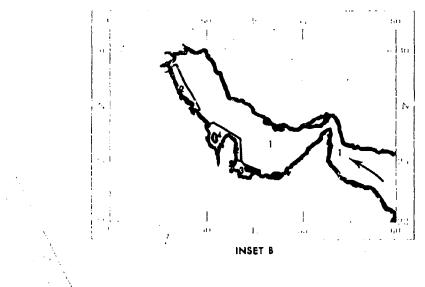


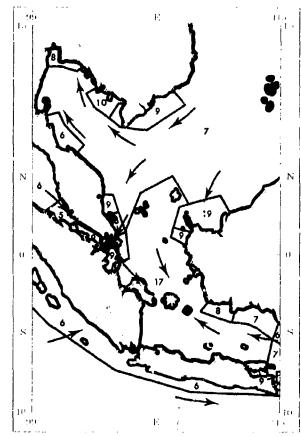
FIG. 6 TYPES OF TIDES AND LOCATIONS OF TYPICAL TIL



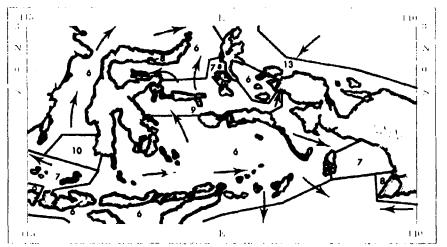
AND LOCATIONS OF TYPICAL TIDE CURVES (Cont'd.)



INSET A



INICET



INSET E

FIG. 7 TYPICAL TIDE CURVES

(SEE FIG. 6 FOR LOCATION OF TIDE CURVES)

AND MEAN 100 MAIL STAGES OF THE IDES

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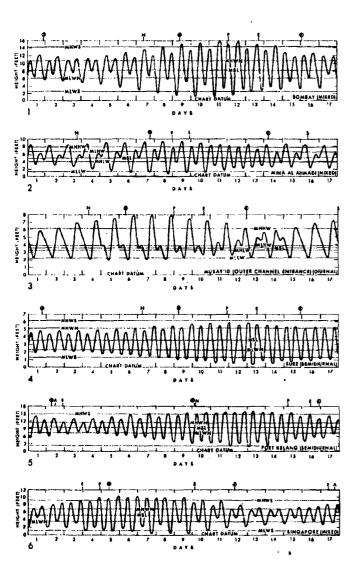
WATER OF WATER THE AVERAGE HEIGHT OF THE LOW

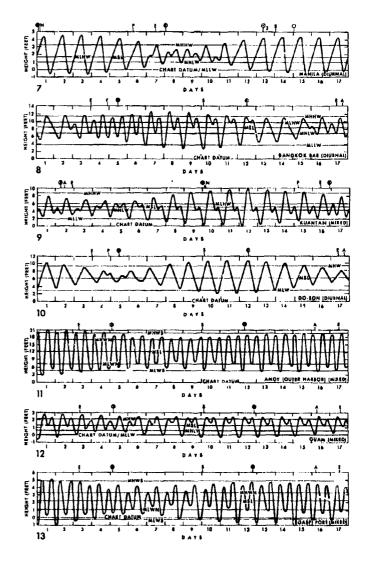
WATER OF WATER THE AVERAGE HEIGHT OF THE LOW

WATER OF WATER THE TIME OF WATER THE TIME OF WATER THE AVERAGE HEIGHT OF THE HIGHER

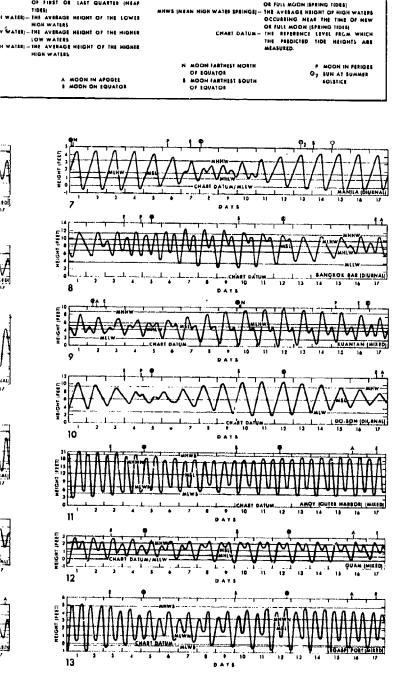
MIN MEAN HARD WATER THE TIME OF WATER THE TIME OF WATER THE TIME OF WATER THE TIME OF WATER THE TIME OF WATER THE AVERAGE HEIGHT OF THE HIGHER

MIN MEAN HARD WATER THE TIME OF WATER THE TIME





R LOCATION OF TIDE CURVES)
(R MEATS)—THE AVERAGE HEIGHT OF THE HIGH
WATERS OCCURRING MEAR THE TIME
OF FIRST OR LAST QUARTER (NEAF



THE AVERAGE HEIGHT OF LOW WATERS OCCURRING NEAR THE TIME OF NEW OR FULL MOIGH (SPRING TIDES)

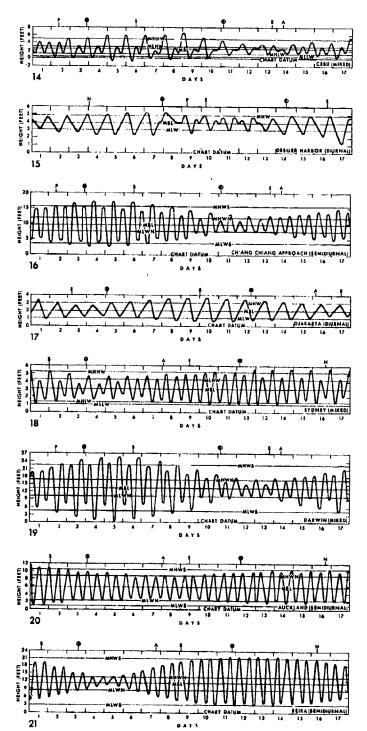
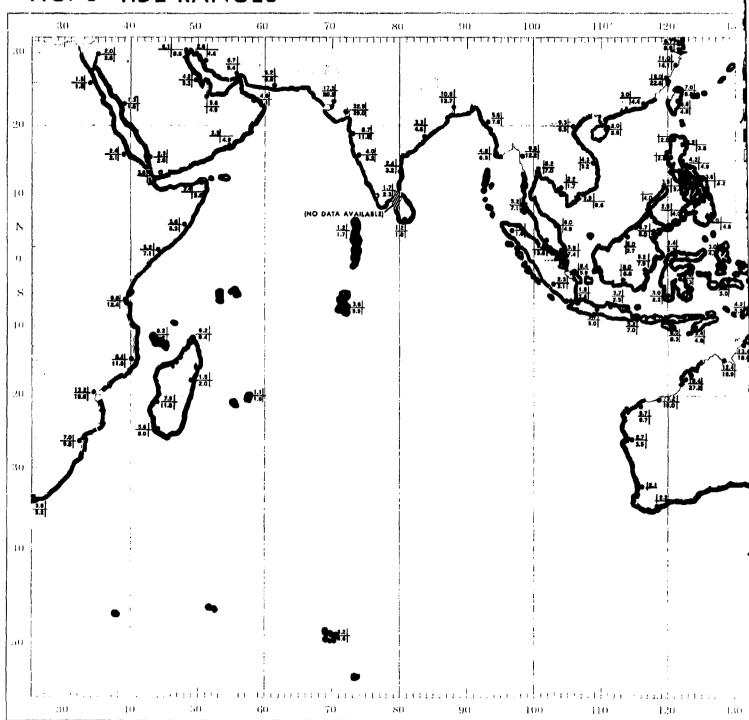


FIG. 8 TIDE RANGES



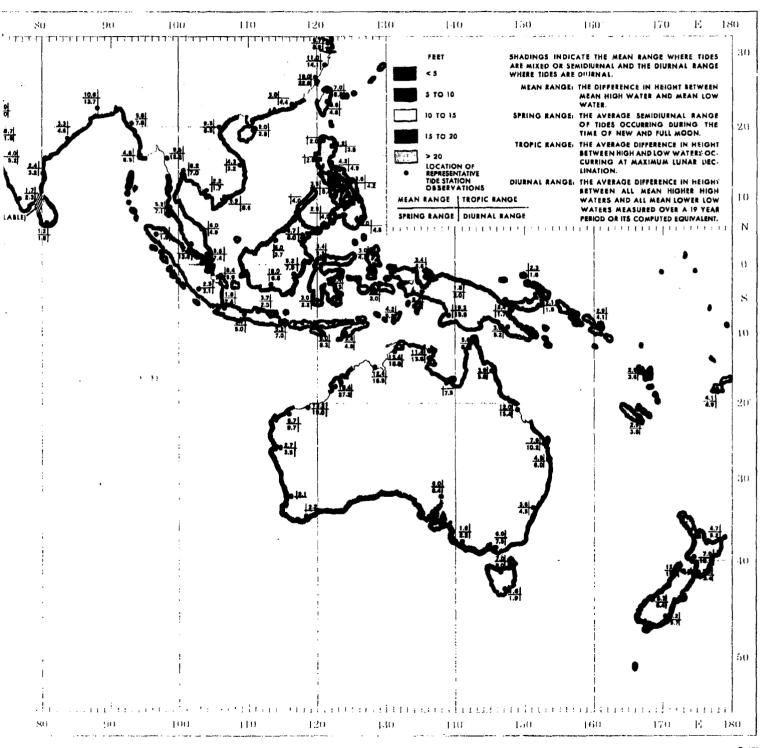


FIG. 9 ICE CONDITIONS

